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AN EXPERIMENTAL STUDY OF
ANALYSIS OF TRANSMISSION TOWERS
THESIS FOR DEGREE OF B. S.
E. A. PIERSON

1926

THESIS

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OF AGR. AND APP. SCIENCE

Civil engineering

Structural engineering

PREFACE

The writer of this thessis in this note wishes to thank the members of the faculty of the Michigan State College for the help he has received during the past years and in due concideration has written this thessis to show his appreciation.

AN EXPERIMENTAL STUDY OF
ANALYSIS OF TRANSMISSION TOWERS

Thesis submitted to the Faculty of

THE MICHIGAN STATE COLLEGE

by
E.A. Pierson

Candidate for the Degree of Bachelor of Science

June 1926

THESIS

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Analysis of Two general types

Flex Towers,

Flexible frames are heavier than poles and are intended to take care of longer spans. Their chief function is to take care primarily of transverse loads with a small margin of safety so that under unusual conditions of service they could provide a little resistance in the direction of the line and distribute a load coming in this direction over a number of supporting structures and transfer such a load to the still heavier structures placed at regular intervals in the line or they may transfer all loads coming on them in the direction of the line to a point where they will be resisted.

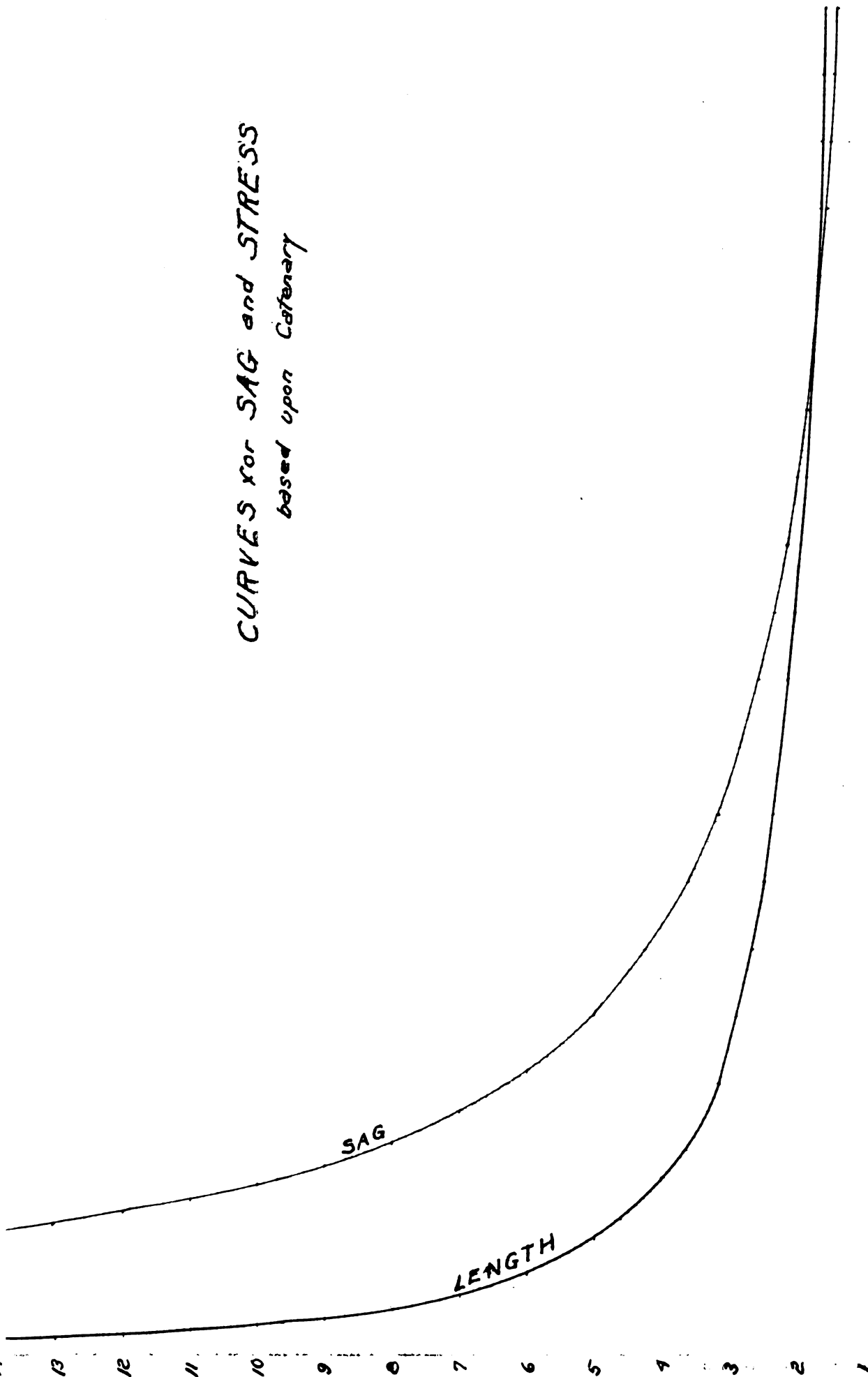
Rigid Towers

Rigid towers are the largest and heaviest structures made for transmission line supports. They are intended to have strength to carry loads coming upon them either in the directions of the line or at right angles to this direction. They are usually designed for a combination of both loads. These towers are built in triangular rectangular or square depending upon conditions. The width at ground line varies from one seventh to one third the total height.

loadings,

- 1 Dead load of the wires together with any coating on them also dead weight of structure itself.
- 2 Wind loads on the wires and the structure transverse to the direction of the line.
- 3 Pulls in the direction of the line caused by dead load and the wind load on the wires.

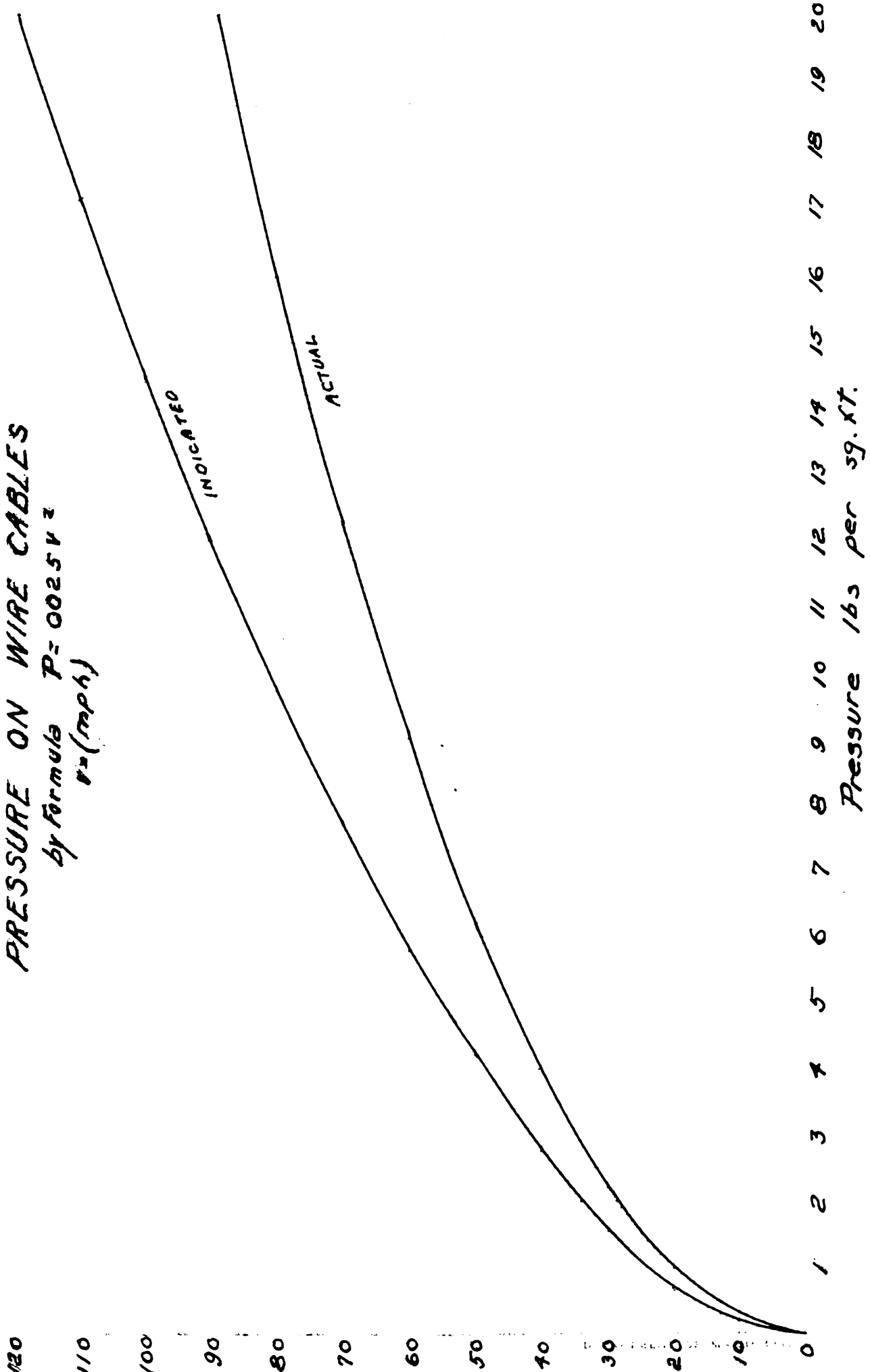
CURVES for SAG and STRESS based upon Catenary



0	1	2	3	4	5	6	7	8	9	10	11	12	13
0	1.000	1.001	1.002	1.003	1.004	1.005	1.006	1.007	1.008	1.009	1.010	1.011	1.012
0	1.000	1.001	1.002	1.003	1.004	1.005	1.006	1.007	1.008	1.009	1.010	1.011	1.012

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INDICATED and ACTUAL WIND VELOCITY AND PRESSURE ON WIRE CABLES by Formula $P = 0.025 V^2$ $V = (\text{mph})$



Reference for use of Thomas's Curve

Formula stress factor = $\frac{\text{Stress in line}}{\text{length of Conductor x } t. \text{ per ft.}}$

Stress factor is ordinate for both Sag and Stress

Sag = Span x abscissa of sag curve

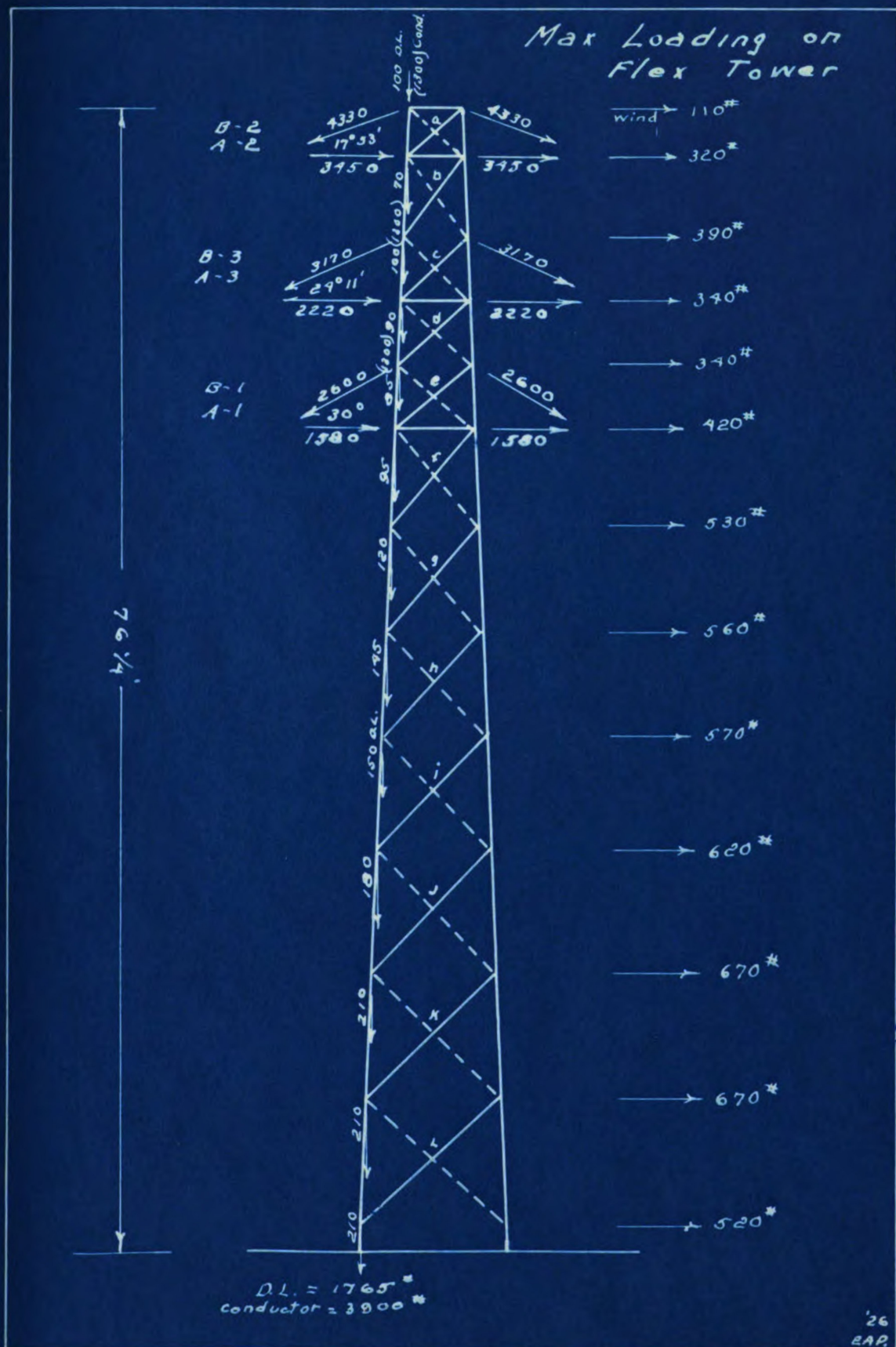
Length = Span x abscissa of length curve

Wind pressure on conductor

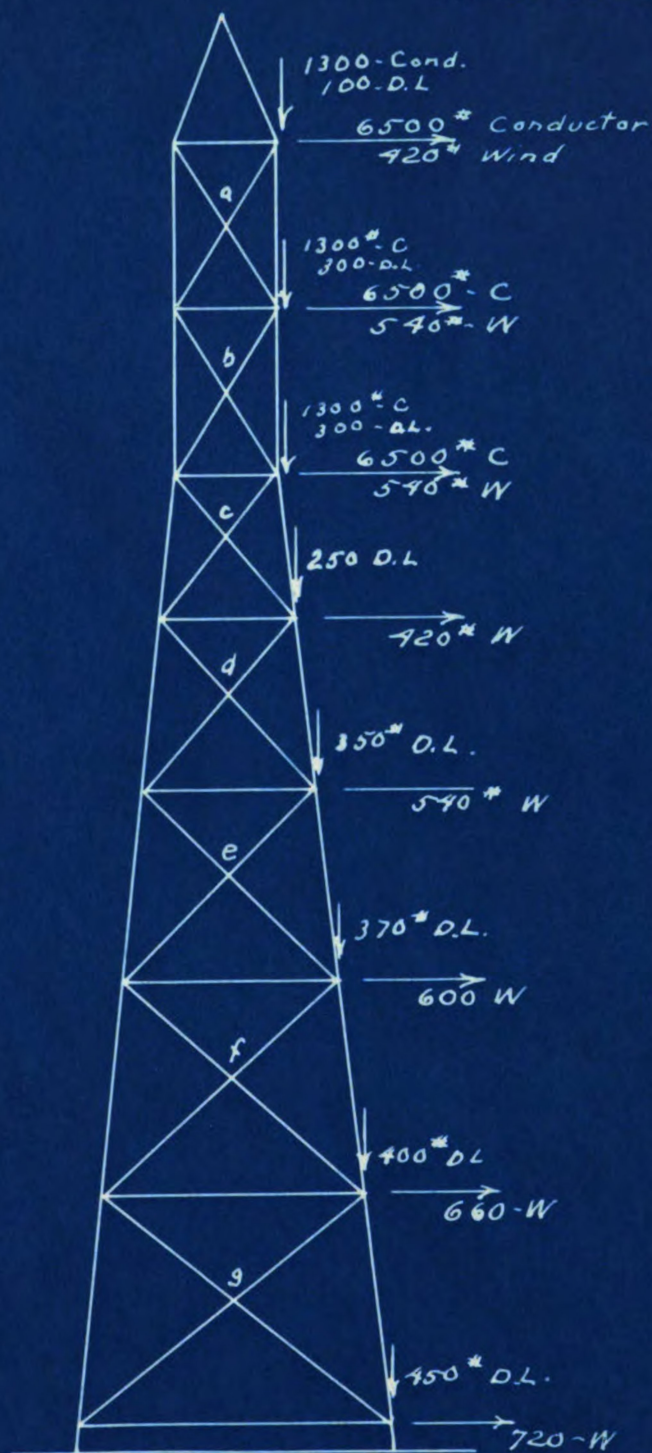
It has been determined by many experiments that the
wind pressure on circular objects = $.0025V^2$

In which V = velocity in m.p.h.

The two curves indicated and actual velocities are based
upon experiments. The indicated is the velocity used by
the U.S.W.S. As a result of considerable investigation
the corrected velocity times a logarithmic factor equals
the true velocity.



Max Loading on Anchor Tower



CONDUCTOR LOADINGS

Class "B"

Gauge # & S	Diameter	Area	Ultimate Tension
500,000	.819	.3924	23,540

Load per

Lin. ft. vert.	Lin. ft. horiz.	Max. load Plane resultant
Dead 1/2" ice	1/2" ice	
1.525 2.345	1.213	2.64

Length of conductor and sag

Tower span 550 ft.

Stress equals 3,500

From Curves

$$\text{Stress Factor} = \frac{3,500}{550 \times 1.525} = 4.17$$

$$\text{Sag} = 550 \times .031 = 17.1 \text{ ft.}$$

$$\text{Length} = 550 \times 1.0024 = 551.32 \text{ ft.}$$

Max. vertical stress 1,300

Max. horizontal stress 670

Tower Loadings

Wind Flex tower 20# per sq. ft.

Anchor tower 30# " " "

Flex towers are designed to stand max. stress perpendicular to line

Anchor towers are designed to stand max stress from all directions

BAR	STRESS	ALLOWABLE	STRESS	ALLOWABLE
(a) $\frac{4120 \times 42.5 + 110 \times 42.5}{2 \times 45.95}$	= 2,450	$\frac{4.3}{3.3}$	3200	13,000
(b) $\frac{180000 + 3610 \times 41.5}{2 \times 46.2}$	3,595	$\frac{6.5}{3.5}$	6400	"
(c) $\frac{344,500 + 3085 \times 51}{2 \times 53.1}$	4740	$\frac{6.0}{4.5}$	7070	"
(d) $\frac{502,000 + 2390 \times 55.25}{2 \times 57.5}$	5540	$\frac{6.5}{3.9}$	7730	"
(e) $\frac{631,200 + 2405 \times 59.50}{2 \times 61.6}$	6410	$\frac{6.3}{4.5}$	8640	"
(f) $\frac{777,700 + 1792 \times 61.25}{2 \times 66.35}$	6670	$\frac{7.2}{5.5}$	9550	"
(g) $\frac{891200 + 265 \times 70.55}{2 \times 73.88}$	6130	$\frac{8.1}{5.5}$	9910	"
(h) $\frac{893,060 + 280 \times 77.65}{2 \times 81.15}$	5525	$\frac{9.3}{6.5}$	8570	"
(i) $\frac{895,232 + 285 \times 77.65}{2 \times 87.23}$	5160	$\frac{10.1}{6.6}$	7900	"
(j) $\frac{897,647 + 310 \times 92.35}{2 \times 95.05}$	4730	$\frac{11.2}{7.3}$	7240	"
(k) $\frac{900,507 + 325 \times 100.55}{2 \times 104.45}$	4560	$\frac{11.55}{8.5}$	6600	"
(l) $\frac{903,777 + 325 \times 108.89}{2 \times 111.79}$	4070	$\frac{12.1}{8.6}$	5720	"

A-I	Stress 3,450	Allowable	7,500
B-I	4,330	"	"
A-2	2,600	"	"
B-2	1,582	"	"
A-3	2,220	"	"
B-3	3,170	"	"

ANNEX 21 (PARTIALS)

BAR MOMENT ABOUT TIME AND DIVISIONS

I-a	110 x 1.45	160
I-b	160 + 110 x 4.25 + 7820 x 2.7	20,108
I-c	20,108 + 7500 x 4.9 + 390 x 2.1	56,878
I-d	56,878 + 7720 x 4.25 + 4780 x 2.1	99,778
I-e	99,778 + 12,500 x 4.25 + 540 x 2.1	153,693
I-f	153,693 + 1284 x 5.45 + 5084 x 3.0	235,513
I-g	235,513 + 16424 x 6.83 + 550 x 3.5	349,463
I-h	349,463 + 16954 x 7 + 550 x 3.5	460,023
I-i	460,023 + 17514 x 7.18 + 570 x 3.6	587,873
I-j	587,873 + 16084 x 7.8 + 620 x 2.9	730,793
I-k	730,793 + 18704 x 8.23 + 670 x 3.9	889,203
I-l	889,203 + 19374 x 8.33 + 670 x 3.7	1,052,683

	MOMENT	DIVISION	BAR AREA	ALLOY
I-a	160	3.5 + 1.45/3	40	40,000
I-b	20,108	3.8 + 2.7/3	4,270	"
I-c	56,878	4.4 + 2.1/3	11,150	"
I-d	99,778	4.6 + 2.1/3	18,800	"
I-e	153,693	5.1 + 2.1/3	26,500	"
I-f	235,513	5.5 + 3.5/3	35,600	"
I-g	349,463	6.2 + 3.5/3	47,600	71,000
I-h	460,023	6.8 + 3.5/3	57,800	"
I-i	587,873	7.5 + 3.6/3	66,800	"
I-j	730,793	8.2 + 3.9/3	76,800	96,500
I-k	889,203	8.9 + 3.9/3	87,800	"
I-l	1,052,683	9.7 + 3.9/3	90,500	"

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2.

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TABLE 10-21

BAR MOMENT ABOUT INITIAL PLASTIC NEUTRAL AXIS

L-a	$500 \times 11.12 + 6920 \times 4.375$	35,780
L-b	$35,780 + 7420 \times 8.75 + 7040 \times 4.375$	131,700
L-c	$131,700 + 14,460 \times 7.625 + 7040 \times 4.375$	265,000
L-d	$265,000 + 22,500 \times 8.1 + 420 \times 3.85$	440,620
L-e	$440,620 + 22,520 \times 9.5 + 540 \times 4.5$	597,050
L-f	$667,050 + 23,460 \times 10.5 + 500 \times 5.0$	780,500
L-g	$780,500 + 24,060 \times 11.5 + 660 \times 5.5$	1,060,000

BAR	MOMENT	DIVISOR	ACTUAL STRESS	ADJUSTED STRESS
L-a	35,780	$5.12 + 8.75/7$	5,600	30,900
L-b	131,700	$5.12 + 8.75/7$	16,500	"
L-c	265,000	$6.75 + 7.5/7$	29,000	"
L-d	440,620	$8.85 + 9.0/7$	37,700	52,700
L-e	597,050	$11.12 + 10/7$	42,500	"
L-f	780,500	$13.66 + 11.1/7$	45,000	"
L-g	1,060,000	$17.21 + 12.1/7$	51,700	"

UNIT 1: THE FUTURE OF THE FUTURE

DATE	MONTH	RENTAL	STREETS
(a)	$\frac{69200}{5.1}$		13,580
(b)	$\frac{69200}{5.1}$		13,580

DATE	MONTH	RENTAL	STREETS
(c)	$\frac{6920 \times 6.75 + 7040 \times 15.5 + 7040 \times 24.25}{2 \times 27.5}$		
		$6125 \times \frac{11}{5.5}$	10,360
(d)	$\frac{136,900 + 420 \times 31.75}{2 \times 35.6}$	$4920 \times \frac{14}{8.8}$	7,840
(e)	$\frac{350,200 + 540 \times 40.6}{2 \times 45.1}$	$4130 \times \frac{16.7}{11.6}$	5,760
(f)	$\frac{371,850 + 600 \times 50.6}{2 \times 55.6}$	$3850 \times \frac{19.5}{14.5}$	4,920
(g)	$\frac{401,850 + 660 \times 61.6}{2 \times 67.1}$	$3300 \times \frac{22.5}{17.5}$	4,240

RIVETS

All rivets in towers are in single shear allowable 10,000

Flex tower

Max. stress in cross arms

$$\frac{9,910}{10,000} \quad 2 \text{ rivets}$$

Max. stress in channel

$$\frac{96,500}{10,000} \quad 10 \text{ rivets}$$

Anchor tower

Max stress in cross arms

$$\frac{13,000}{10,000} \quad 2 \text{ rivets}$$

Max. stress angles

$$\frac{52,700}{10,000} \quad 6 \text{ rivets}$$

Pocket
has:
2 Plans



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