CALCULATION OF THE UNPERTURBED DIMENSIONS FOR LINEAR ATACTIC POLYMERS ON A SQUARE LATTICE

Thesis for the Degree of M. S.
MICHIGAN STATE UNIVERSITY
Robert C. Thomas
1963

Thesia

LIBRARY
Michigan State
University

MICHIGAN STATE UNIVERSITY DEPARTMENT OF CHEMISTRY EAST LANSING, MICHIGAN

ABSTRACT

CALCULATION OF THE UNPERTURBED
DIMENSIONS FOR LINEAR ATACTIC
POLYMERS ON A SQUARE LATTICE

by Robert C. Thomas

Body of Abstract

A two-dimensional square lattice model for linear atactic polymers of type CH₂-CHR has been formalized. The three-dimensional equations developed by Yoo and Kinsinger were reduced to a regular planar square lattice and several computer programs were written to calculate the mean-square end-to-end-dimensions for several polymeric models.

The model allows the carbon atoms of the polymer chain to occupy adjacent corners of the square lattice. Each step in the polymer chain has a fixed length 1 and is not allowed to reverse its previous direction. Thus, the bonds are permitted to go forward 0°, left turn -90°, or right turn +90°. This model accounts for both first and second neighbor interactions and the chain configuration can be either atactic, isotactic, or syndiotactic.

The values of $\langle h^2 \rangle / nl^2$ for the seven polymer cases ranged from 1.14 to 2.01 while a value of 1.67 was obtained for a polymer with randon configuration and randon conformation. Some comparisons are made between the results obtained on the two dimensional lattice and what would be expected for the three dimensional case.

CALCULATION OF THE UNPERTURBED DIMENSIONS FOR LINEAR ATACTIC POLYMERS ON A SQUARE LATTICE

bу

ROBERT C. THOMAS

A THESIS

Submitted to
Michigan State University
in partial fulfillment of the requirements
for the degree of

MASTER OF SCIENCE

Department of Chemistry

1963

7 9-05

ACKNOWLEDGEMENTS

The author gratefully acknowledges the invaluable guidance and assistance given to him by his research director, Dr. J. B. Kinsinger. He also wishes to thank Mrs. S. J. Yoo for her assistance in defining this problem. The author is indebted to many persons at the Computer Laboratory at MSU and the Computations Research Laboratory at Dow Chemical Company. Midland. Michigan. Appreciation is extended to the Nuclear and Basic Research Laboratories and the Computations Research Laboratory at Dow Chemical Company, Midland. for covering the cost of computer time on the Burroughs 220.

TABLE OF CONTENTS

			Page
I.	INT	RODUCTION	1
	A .	General	1
	В.	Experimental Model	4
II.	CAS	ES STUDIED AND COMPUTATIONAL PROCEDURE	23
	Α.	Cases Studied	23
	В.	Computational Procedure	27
III.	CO	NCLUSIONS	33
	Α.	Results	33
	В.	Discussion of Results	39
IV.	BIB	LIOGRAPHY	43
v.	APP	ENDIX	44
	A .	Derivation of the Transformation Matrices	
		D _{2V} and D _{2V1}	44
	В.	Block Method for Determining the	
		Eigenvalues of a Matrix	48
	С.	Algol 58 Computer Procedures	50

LIST OF FIGURES

Figure)	Page
1	Polymer chain on the square lattice	4
2	Numbering system used for the chain	
	atoms and bonds	6
3	Schematic diagram showing the first	
	and second neighbor interactions for	
	a (2 \mathbf{V} 1) and a (2 \mathbf{V}) bond	8
4 ·	Schematic diagram depicting the polymer	
	chain in case 6	41
5	Diagram used to determine the sin-cosine	
	transformation matrices when the same	4.1
	coordinate system is used for both bonds	
6	Diagram used to determine the sin-cosine	
	transformation matrices when different	
	coordinate systems are used for the	
	two bonds	45

LIST OF TABLES

Table		Page
1.	Conformational states for the square	5
	lattice model	
2.	Configurational states for the square	
	lattice model	. 5
3.	Bonds of matrix $\left[\begin{array}{cccccccccccccccccccccccccccccccccccc$. 14
4.	Bonds of matrix	. 15
5.	Matrix [Dav]	
6.	Matrix [D2v+]	. 17
7.	Matrix []	. 18
8.	Matrix Davida	
9.	Matrix [[ave] va	
10.	Equalities of the U_{ij} elements	. 21
11.	Equalities in the first and second neighbor	
	parts of the $\mathtt{U}_{i,j}$ elements	. 22
12.		
13.	Matrix [av] [avi] [avi] cases 1-4 Matrix [av] [avi] [avi] cases 5-7	. 29
14.	Key to the symbols in Tables 13 and 14	
15.	Non-normalized eigenvectors	. 34
16.	Non-normalized eigenrows	. 35
17.	Normalized eigenvectors	. 36
18.	Normalized eigenrows	. 37
19.	Final results	. 38

I. INTRODUCTION

A. General

In 1958, interest in the theory of dilute polymer solutions was rekindled when Volkenstein's calculations 1 of the relationship of discrete rotational states to the average unperturbed end-to-end dimensions of polymer chains became known to western scientists. By this time, Volkenstein and coworkers had developed their theories to include polymer chains with both symmetric and asymmetric structures with statistically independent rotational states. In addition, they had closed form solutions for the newly discovered isotactic and syndiotactic stereoisomeric polymers which related the average end-to-end dimensions to chain geometry. Moreover, they developed equivalent equations for atactic polymers, the configurational (d,1) placements mathematically described by a single distribution parameter, and the chain with statistically independent rotations.

Shortly, however, it was evident that a statistically independent model could not adequately describe the unperturbed dimensions, and Lifson² and Nagai³ introduced the statistically dependent rotational model which was treated through the formalism of the linear Ising problem and took into account cooperative effects between first and second neighbors in the chain.

This successful treatment, however, made the mathematical process somewhat more complex, and in the past several years.

many papers have appeared 4,5,6,7 for chains with symmetric structure and for the asymmetric stereoregular isotactic and syndiotactic forms. You and Kinsinger developed a comprehensive formalism which included a two parameter distribution for the stereosequences in the chain plus a second · neighbor interaction distribution for chain conformations. all based on a statistically dependent model. This master equation for atactic chains can, with appropriate change, be converted to handle either the asymmetric syndiotactic or isotactic chains and symmetric chains as well. The states of the chain, however, are numerous since two parameters are needed to describe the d,l sequences which arise from the polymerization conditions and these, in turn, have several conformational states for each different triplet d,1 sequence in the backbone. This results in a large number of joint configurational-conformational states for the system, and the formalism requires a generator matrix of rather large size with an excessive number of parameters. Since, at best, two parameters can be obtained from current experimental data. the formalism cannot be evaluated properly. Future work on configurational and conformational distributions by various spectroscopic techniques may yield sufficient evidence to utilize and verify the theory.

However, it is instructive to reduce the formalism to computations based upon our best current knowledge of the distribution of configurational and conformational states of polymer chains. In this way, the formalism can be checked

independently for completeness and the effect of the joint distribution can be revealed. Even a cursory glance at the computational problem will show that a three dimensional representation of the chain has prohibitive complexity and detail. Hence, it was decided to reduce the chain problem to a regular two dimensional square lattice. While this seemingly may restrict the computations to a very special case, the principles contained therein in the formalism and the inter-relationship of the joint states should be revealed by such a calculation.

In this model, therefore, the two dimensional square lattice will have two types of lattice sites, corresponding to the d or 1 configuration in the chain. While the model is not truly asymmetric, the different sites will reflect the influence of the corresponding d,1 states in the three dimensional chain. Each step will have a fixed length 1 as in a real polymer chain, but the bond angles will vary depending upon the steps taken along the lattice, and they will be permitted to go forward 0°, left turn -90°, right turn +90°. In this sense, the variable bond angles will correspond to the rotational states in the three dimensional chain. While this may seem superficial, the fixed bond angles in the three dimensional chain contributes only a multiplicative term to the mean square end-to-end dimension and, hence, enters as a constant.

B. Experimental Model

The square lattice model used for this study of polymer type chains $(-CH_2-CHR-)_n^*$ is described as follows:

1. Let it be possible for an A or B to be present at every other corner of the square lattice. (see Figure 1) A and B are equivalent to the asymmetric carbon atoms of the vinylic chain.

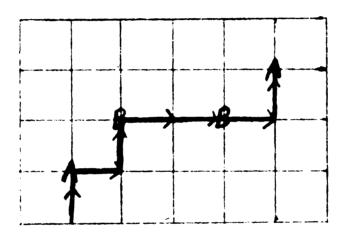


Figure 1. Polymer Chain on the Square Lattice.

- 2. Place the initial bond along the positive direction of the Y axis.
- 3. The conformational states are then defined as shown in Table 1.

^{*} chains of this type have a periodicity of two

TABLE 1.

Conformational States for the Square Lattice Model

State	${f \gamma}^{ m th}$ Bond Vector	$(v-1) + v)^{th}$ Bonds	Bond Angle
1	\uparrow	*	0
2	>	→	$3\pi/2$
3*	↓ .	11	π
4		(7	$\pi \mathbb{Z}_2$

is measured in a counter-clockwise direction from the projection of the Y axis (V-1)th bond vector.

4. The configurational states are defined as shown in Table 2.

TABLE 2.

Configurational States for the Square Lattice Model

Configuration	Growing Chain Ends	Reaction Products	Free Energy of Activa- tion
$A A A \longrightarrow 1$	d d	d d d I	${\cal E}_1$
A A B → 2	d d	d d l H	\mathfrak{t}_{2}
В В В→3	1 1	1 1 1 I	$\epsilon_{\scriptscriptstyle 3}$
В В А.——————————————————————————————————	1 1	1 1 d H	£ 4
B A B → 5	l d	1 d 1 S	□ ₅
B A A-→6	1 d	ldd H	ε_6
A B B-→7	d 1	d 1 1 H	É7
A B A→8	d 1	d 1 d S	<u> 6</u> 8

5. The numbering system used for the chain atoms and bonds is shown in Figure 2.

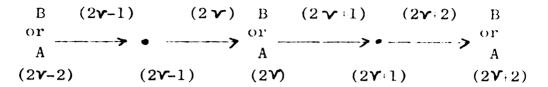


Figure 2. Numbering System Used for the Chain Atoms and Bonds.*

- 6. The coordinate system used is the same as that described by Yoo and Kinsinger. For a bond vector terminating at an asymmetric chain atom, a right-handed system is used for a bond terminating at a d configuration (A site) and a left-handed system is used for a bond terminating at an 1 configuration (B site). For a bond vector terminating at a methylenic type chain atom, a right-handed system is used if the CHR-CH₂ bond originates from a d configuration (A site) and a left-handed system is used if the CHR-CH₂ bond originates from a d configuration (A site) and a left-handed system is used if the CHR-CH₂ bond originates from an 1 configuration (B site).
- 7. The equations used are those described by Yoo and Kinsinger. We consider here only first and second neighbor interactions. The generator (or state) matrices are defined on the following pages.

^{*}The numbers for the bonds appear at the top of the figure directly above the bond which is shown as an arrow. The numbers for the chain atoms appear at the bottom of the figure directly under the chain atom.

$$\begin{bmatrix} U_{11}^{0 \, (W)} & U_{12}^{0 \, (W)} & U_{13}^{0 \, (W)} & U_{14}^{0 \, (W)} \\ U_{21}^{0 \, (W)} & U_{22}^{0 \, (W)} & U_{23}^{0 \, (W)} & U_{24}^{0 \, (W)} \\ U_{31}^{0 \, (W)} & U_{32}^{0 \, (W)} & U_{33}^{0 \, (W)} & U_{34}^{0 \, (W)} \\ U_{41}^{0 \, (W)} & U_{42}^{0 \, (W)} & U_{43}^{0 \, (W)} & U_{44}^{0 \, (W)} \end{bmatrix}$$

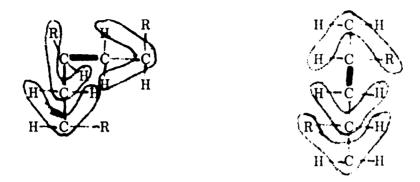
$$(1)$$

Matrix (1) is a generator matrix for one of the conformational matrices. The elements of matrix (1) are defined in equation (2).

$$U_{rt}^{0 (W)} = \exp \left[-\left\{ \mathcal{E}^{(W)} \left(\frac{\mathbf{e}_{2\mathbf{Y}+1}^{(r)}}{\mathbf{e}_{2\mathbf{Y}+1}^{(w)}} \right) + \mathcal{E}^{(W)} \left(\frac{\mathbf{e}_{2\mathbf{Y}}^{(r)}}{\mathbf{e}_{2\mathbf{Y}+1}^{(w)}} \right) \right] \right]_{RT}$$
(2)

first neighbor interaction term

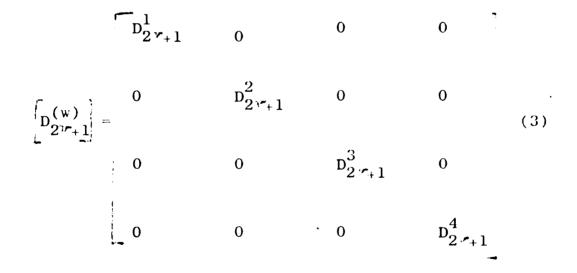
In U_{2Y+1} the $_{2Y+1}$ signifies the rotation of the $_{2Y+2}$ bond about $_{2Y+1}$. $U_{rt}^{(W)}$ is a term proportional to the probability that the last bond will be in state r when the previous bond is in state t and the configuration state is (W). The first and second neighbor interactions are depicted schematically in Figure 3.



a $(2^{n}+1)$ bond

a (2.7) bond

Figure 3. Schematic diagram showing the first and second neighbor interactions for a (2%1) and a (2%) bond.



Matrix (3) is a transformation matrix which is part of the transformation matrix $\begin{bmatrix} D_2 & \cdots & D_2 \end{bmatrix}$.

$$\begin{bmatrix} \Phi_{2\mathbf{Y}+1} \end{bmatrix} = \begin{bmatrix} \mathbf{U}_{2\mathbf{Y}+1}^{(1)} & 0 & 0 & 0 \\ 0 & \mathbf{U}_{2\mathbf{Y}+1}^{(2)} & 0 & 0 \\ 0 & 0 & \mathbf{U}_{2\mathbf{Y}+1}^{(3)} & 0 \\ 0 & 0 & 0 & \mathbf{U}_{2\mathbf{Y}+1}^{(4)} \end{bmatrix}$$
(4)

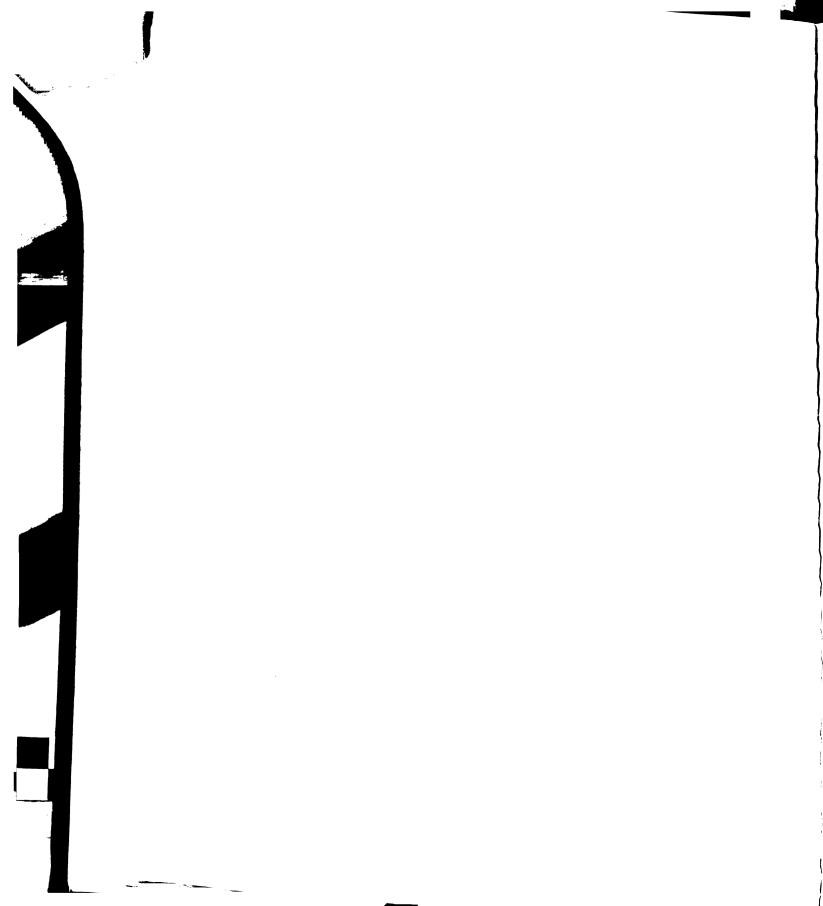
Matrix (4) is the conformational matrix for 2V:2 bonds about 2V:1 bonds.

$$\begin{bmatrix} 2 & 2 & 1 \\ 2 & 2 & 1 \end{bmatrix} = \begin{bmatrix} c_1 & 0 & c_6 & c_6 & 0 \\ 0 & c_3 & 0 & c_7 \\ 0 & c_4 & 0 & c_8 \\ c_2 & 0 & c_5 & 0 \end{bmatrix}$$
 (5)

Matrix (5) is the configuration generator matrix.

$$C_i = \exp - \xi_i / RT$$
 (6)

where $\mathbf{f}_{\mathbf{i}}$ is the free energy of activation for a given configuration as defined in Table 2.



$$\begin{bmatrix} D_{2Y+1} & 0 & 0 & 0 \\ 0 & D_{2Y+1}^{(2)} & 0 & 0 \\ 0 & 0 & D_{2Y+1}^{(3)} & 0 \\ 0 & 0 & 0 & D_{2Y+1}^{(4)} \end{bmatrix}$$
(7)

Matrix (7) is the transformation matrix for transforming the coordinates of a 2Y+2 bond into the coordinate system for a 2Y+1 bond and each element on the diagonal is a transformation matrix as given in (3).

Up to this point we have been considering the bond type

Now in a similar fashion we will consider the bond type

Then: $\begin{bmatrix} U_{11}^{E(w)} & U_{12}^{E(w)} & U_{13}^{E(w)} & U_{14}^{E(w)} \\ U_{21}^{E(w)} & U_{22}^{E(w)} & U_{23}^{E(w)} & U_{24}^{E(w)} \\ U_{31}^{E(w)} & U_{32}^{E(w)} & U_{33}^{E(w)} & U_{34}^{E(w)} \\ U_{41}^{E(w)} & U_{42}^{E(w)} & U_{43}^{E(w)} & U_{44}^{E(w)} \end{bmatrix}$ (8)

Matrix (8) is a generator matrix for one of the conformational matrices.

where w 1 when • ---- A ---- A when • ---- B ----

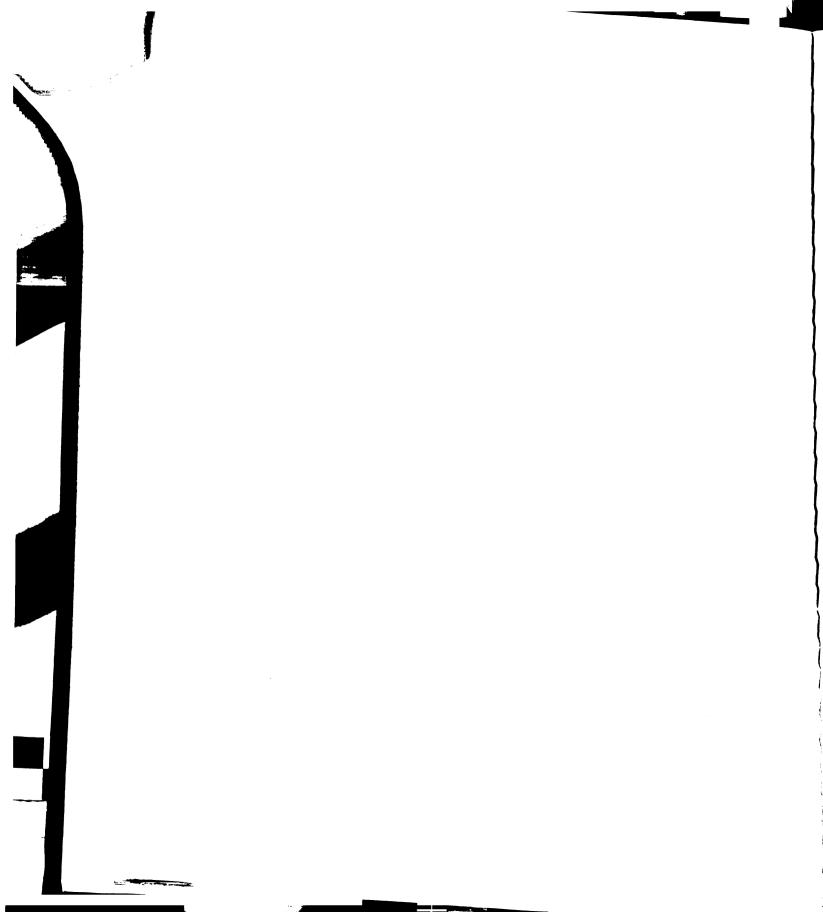
$$U_{rt}^{E(w)} = \exp \left[-\left\{ \left(\begin{array}{c} (w) & (\theta_{2\mathbf{v}}^{(r)}) + \left(\begin{array}{c} (w) & (\theta_{2\mathbf{v}-1}^{t}) \\ \end{array} \right) \\ \text{first neighbor interaction term} \right]$$
second neighbor interaction term

$$\begin{bmatrix} D_{2\Upsilon}^{1} & 0 & 0 & 0 \\ 0 & D_{2\Upsilon}^{2} & 0 & 0 \\ 0 & 0 & D_{2\Upsilon}^{3} & 0 \\ 0 & 0 & 0 & D_{2\Upsilon}^{4} \end{bmatrix}$$
(10)

Matrix (10) is a transformation matrix which is part of the transformation $\left[\mathbf{D}_{2\mathbf{V}}\right]$

$$\begin{bmatrix} \Phi_{2\mathbf{Y}} & 0 & 0 & 0 \\ 0 & U_{2\mathbf{Y}}^{(2)} & 0 & 0 \\ 0 & 0 & U_{2\mathbf{Y}}^{(1)} & 0 \\ 0 & 0 & 0 & U_{2\mathbf{Y}}^{(1)} & 0 \\ 0 & 0 & 0 & U_{2\mathbf{Y}}^{(2)} \end{bmatrix}$$
(11)

Matrix (11) is the conformational matrix for $2V \cdot 1$ bonds about 2V bonds.



$$\begin{bmatrix}
D_{2} \\
D_{2}
\end{bmatrix} = \begin{bmatrix}
D_{2} \\
0 & D_{2} \\
0 & D_{2}
\end{bmatrix}$$
(12)

Matrix (12) is the transformation matrix for transforming the coordinates of a 211 bond into the coordinate system for a 27bond and each element on the diagonal is a transformation matrix as given in (10).

The final equation used to calculate the unperturbed dimensions of the various cases is shown in equation (13) as adopted from the three dimensional formalism of Yoo and Kinsinger.

$$\langle n^2 \rangle n n^2 = \{0 \ 1\} \left[E_2 + \Delta^* N \Delta \cdot \Delta^* (E_{32} + N) (E_{32} - M)^{-1} (M + D_{27}) \Delta \right]_1^0 \right]$$
where $M = \left[D_{27} \right] \left[D$

$$\Delta = \begin{bmatrix} J \\ J \end{bmatrix}_{2}$$

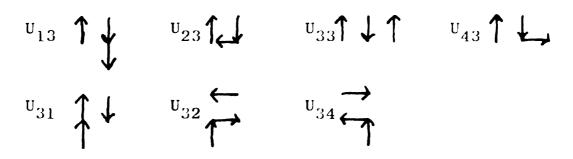
$$J = \text{the largest positive eigenvalue of } \begin{bmatrix} 2 & J \end{bmatrix}_{2} \begin{bmatrix} J \\ J \end{bmatrix}_{2}$$

f = the eigenvector corresponding to the above
eigenvalue = the eigenrow corresponding to the above

 E_2 = a 2 x 2 identity matrix E_{32} = a 32 x 32 identity matrix

The bonds considered in matrices $\left[\begin{array}{c} \Phi_{2} \mathbf{v} \end{array} \right]$ and $\left[\begin{array}{c} \Phi_{2} \mathbf{v} \end{array} \right]$ are shown in Tables 3 and 4. The matrices $\left[\begin{array}{c} D_{2} \mathbf{v} \end{array} \right]$. $\left[\begin{array}{c} D_{2} \mathbf{v} \end{array} \right]$, $\left[\begin{array}{c} \Phi_{2} \mathbf{v} \end{array} \right]$, and $\left[\begin{array}{c} D_{2} \mathbf{v} \end{array} \right]$, and $\left[\begin{array}{c} D_{2} \mathbf{v} \end{array} \right]$, are shown in Tables 5, 6, 7, 8, and 9. The derivations of the two transformation matrices are given in Appendix A.

8. In this square lattice we only allow the growing chain end to go in three directions. We disallow it to reverse its previous direction. This causes the following elements of the U matrices to be zero.



Due to symmetry many of the elements within U are identical to other U elements. These identities are shown in Tables 10 and 11.

Bonds of
Matrix Fay

TABLE 5.

TRANSFORMATION MATRIX Dor

	1	2	3	4	5	6		7 8	3	9	10	11	12	1:	3 1	4	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	1	0							Det 1																									
2	0	1							S. Carrie																									
3			0 -	1					Contract of the Contract of th																									
4			1	0																														
5					-1	0				i																								
6					0	-1																					-							
7								0	1																		4 9 5							
8	Sin i manusina	Birmer or s				-		1 (0				********	nh none	-					-								-			D. Martin James and		T-Annah (12.2)	and the contract of the contra
9									- Control	1	0																1							
10				1						0	1				1																			
11				-					- Common		-	0	1		1				- Andrews								-							
12		-										-1	0						1								Canal Canal							
13									Total Control					-		0			-															
14		-							1					() -	-1			and the second															
15			1				+		1								0	-1	in a second								State of the state							
16	Barren for	naucuveja	EDITOR AND			************	week the same	- Constitute		pr snowing w	The same state of	ALCONOMICS SCHOOL	18 00-7-1002	SER MORPHONICAL	aun den stee	man-cin	1	0	· ·	-	Dr on ROAD	-	******	due 101 1	Advantage .	-		-	Gara rational show	-				Livery powers
17									-				1						1	0							-							
18								-	1	-									0	1							The same							
19									41.17										and the same of th		0	-1					4							
20		-					1		-										-		1	0					-							
21	-								*										Constitution of the				-1	0										
22			1					-	- Kerney										-				. 0	-1									1	
23	+ -+	1							Mary Mary										-						0	1	and Store &							
24		*******	Cara British		A a bottomacon	Name of			-				Special services			ب نیاداد او در	400000000000000000000000000000000000000		-		4	A			-1	0	-	-				(Allentering)	Section 1981 and	
25	-						+		-															. 2			11	0						
26								4	The same				-						-								0	, 1						
27	-								2000				1						-										0	1				
28									The same										-										-1	0				
29																															-1	0		
30			+						and the second										-								100					-1		
31									The same of										-								- April -						0	-1
32					1	1	1		Charles Company					1													THE PERSON NAMED IN COLUMN TO PERSON NAMED I							0

TABLE 6.

TRANSFORMATION MATRIX Deril

	1	2 :	3 4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	1	0						-																							
2	0	1			-			Salar Salar																-							
3			0 -1					Separate Sep								1															
4	1		1 0					Alexander .								- Company								Sales Comment							
5				-1	0			Sheekly.																town							
6				0	-1			A Company																1							
7						0	1	Secretary.																-							-
8				1		-1	0	Sale Comment																-							
9	rann-aga	a) entrage	DET SWINGLES	internal	TAN TOTAL CAN	-	1600	1	0	facility report	Aces - re art	acrometer.	Ballingal	Lake and the second	de rocción d		inevanie e	parea and	\$1.00 to to to to	iv = 10 miles	homes			1		4 manda	President	Anto name	D.S.C.L./CHICA	(Katalan Internal	orkfore/fit: 74
10								0	1																						
11	+ -+							- Charles		0	1					1								-							
12								- Constitution		-1	0				1									**							
13								demonstra				-1	0						1					And the second							-
14	11			+	1	1		-	-			0	-1	1		Control in such								Andrew St.							1
15								Supplied to			1			0	-1	- Company								A Commercial Accounts of the Commercial Accounts							
16						1		- Contraction	-			-		1	0	-										+					
17	- HISPERS	and a supplied	Marie Agrica Co.	- SEMILEUM	2.1 \$1.2 miles 2.2	-	NO. OF THE REAL PROPERTY.	The state of the s		ALTON CONTRACTOR	Acres de Rich a 19	AZIALEDOLE:	ALTON ATOM	45.		0	1		1	1002000		destains.		and the second	400000000000000000000000000000000000000	Marin Charles and Share of	Mil - Mil Mil Zo		to black or a		
18								*	1		1		-		1	1	0							Acres de la constante de la co						-	
19			-	1				A STORY	1	-								-1	0					Sales de la constitución de la c							
20				- The state of	-			1			the manufacture		1	1 1 02 0		1		0	1					- Control							
21	1		TOTAL PLANE	-		1				-	1	-			+			1		0	-1	-		-						1	
22					-	1		- Constant				-	1							-1	0			A. Land							-
23								The same of				1				-						1	0	D. Salar			-				
24																						0	-1	*						-	+
25			COMPANY AND A		million man	Design also make		- Action		Think it have	-		- Comment		-		A LOP OF THE	abora na aktoria	and a production of the		e Byron e barne e the e	Act of the same of	- Control of the state	0	1	Philadelphia in	- breeze had	Salphane S.	+ + + + + + + + + + + + + + + + + + + +	Alexandria de deservi	Acces Cartina
26								- Charles		-						Andrew Control								1	0						-
27								School								and the same								Same and a second		1	0	1	***********		
27 28 29								School of the last								The second second				1				Residencia		0	-1				
29				-				1			1	1				Contract of the Contract of th		1	1					NAME OF TAXABLE PARTY.				0	-1		4-1-11-11-11
30		-						The same				1		1		produce and							1	the state of the s				-1	0		
31					1				A CONTRACTOR LABORATOR	- Partition	1				-	* · · · ·		1.00	1	, ,		*		451770ca		1	1		-	-1	0
32			1			1		1	-		1	1			1	Total Section of		1	1	1	-	-		Carterin	1	1	1		1	0	1

18	TABLE 7.	Matrix [] avla	
	9 10 11 12 13 14 15	16 17. 18 19 20 21 22 23 24	25 26 27 28 29 30 31 32
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			
5 and 6			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			
8 U_{41}^{E1} U_{42}^{E1} U_{44}^{E1}			
9	${\tt U}_{11}^{{\tt E}2} \hspace{0.5cm} {\tt U}_{12}^{{\tt E}2} \hspace{0.5cm} {\tt U}_{14}^{{\tt E}2}$		
10	$\mathbf{U}_{11}^{\mathrm{E2}} \mathbf{U}_{12}^{\mathrm{E2}} \mathbf{U}_{12}^{\mathrm{E3}}$	U ₁₄ ^{E2}	
11	${\tt U}_{21}^{{\tt E}2} \qquad {\tt U}_{22}^{{\tt E}2} \qquad {\tt U}_{24}^{{\tt E}2}$		
12	${\rm U}_{21}^{{\rm E}2} {\rm U}_{22}^{{\rm E}2} {\rm U}_{22}^{{\rm E}3}$	E2 24	
13 and 14			
15	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
16		UE2 44	
17		${\tt U}_{11}^{{\tt E}3} {\tt U}_{12}^{{\tt E}3} {\tt U}_{14}^{{\tt E}3}$	
18		${\tt U}_{11}^{{\tt E}3} \qquad {\tt U}_{12}^{{\tt E}3} \qquad {\tt U}_{14}^{{\tt E}3}$	
19		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
20		$u_{21}^{\mathrm{E3}} u_{22}^{\mathrm{E3}} u_{24}^{\mathrm{E3}}$	
21 and 22			
23		${\tt U}_{41}^{{\tt E}3} {\tt U}_{42}^{{\tt E}3} {\tt U}_{44}^{{\tt E}3}$	
24		${\rm U}_{41}^{{\rm E}3} {\rm U}_{42}^{{\rm E}3} {\rm U}_{44}^{{\rm E}3}$	
25			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
26			${\tt U}_{11}^{{\rm E}4} \qquad {\tt U}_{12}^{{\rm E}4} \qquad {\tt U}_{14}^{{\rm E}4}$
27			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
28			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
29 and 30			DA DA
31			$U_{41}^{E4} \qquad U_{42}^{E4} \qquad \qquad U_{44}^{E4}$
32			$\begin{array}{cccccccccccccccccccccccccccccccccccc$

19	TABLE 8. Matri	[Farti]	
	9 10 11 12 13 14 15 16	17 18 19 20 21 22 23 24	25 26 27 28 29 30 31 32
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			
5 and 6			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			
$v_{41}^{01} v_{42}^{01} v_{44}^{01}$			
9	$U_{11}^{O2} \qquad U_{12}^{O2} \qquad U_{14}^{O2}$		
10	$U_{11}^{02} \qquad U_{12}^{02} \qquad U_{14}^{02}$		
11	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
12	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
13 and 14			
15	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
16	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
17		$v_{11}^{O3} v_{12}^{O3} v_{14}^{O3}$	
18	1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
19		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
20		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
21 and 22			
23		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
24		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
25			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
26			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
27			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
28			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
29 and 30	,		
31			$\begin{array}{cccccccccccccccccccccccccccccccccccc$
32			$\begin{array}{cccccccccccccccccccccccccccccccccccc$

												TAL	BLE	9.		\sum_{2}	W1	2x	1													
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	C_1																C ₆															
2	1	Ci				-												C ₆														
3		-	C_1		-											-			C ₆													
4				C_1																C ₆												
5					C_1																C6											
6	-					C_1																C ₆										
7							c_1																C ₆									
8	ACCULATION							c_1																C ₆	-					-		
9									C3																C ₇							
11										C ₃	C .															C ₇	C .					
12					-						C3	C												-			C ₇	C ₇				
13				-			-					C ₃	C ₃															7	C ₇			
14													3	C ₃															- 1	C ₇		
15					-			-			-				C ₃															-	C7	
16						-										C3		-														C ₇
17									C_4		-					-									C ₈			-				
18										C_4																C ₈						
19											C_4																C ₈					
20												C_4																C ₈				
21 22			-	-	-							-	C ₄	-															C ₈			
23		-		-	-	-					-			C ₄	C_4	-									-					C ₈	0	
24		-	-	-	-	-									4	C_4				-											C ₈	C
25	C ₂		-	-	-						-					4	C ₅												-			C8
26		C ₂		-	-	-		-				-					2	C ₅						-	-							
27		-	C2			-					-							3	C ₅													
28			-	C2															0	C ₅												
29		-			C2																C ₅			-								
30						C2																C ₅					3					
31							C2				1												C ₅									
32				1	1			C_2	1													1		C ₅								

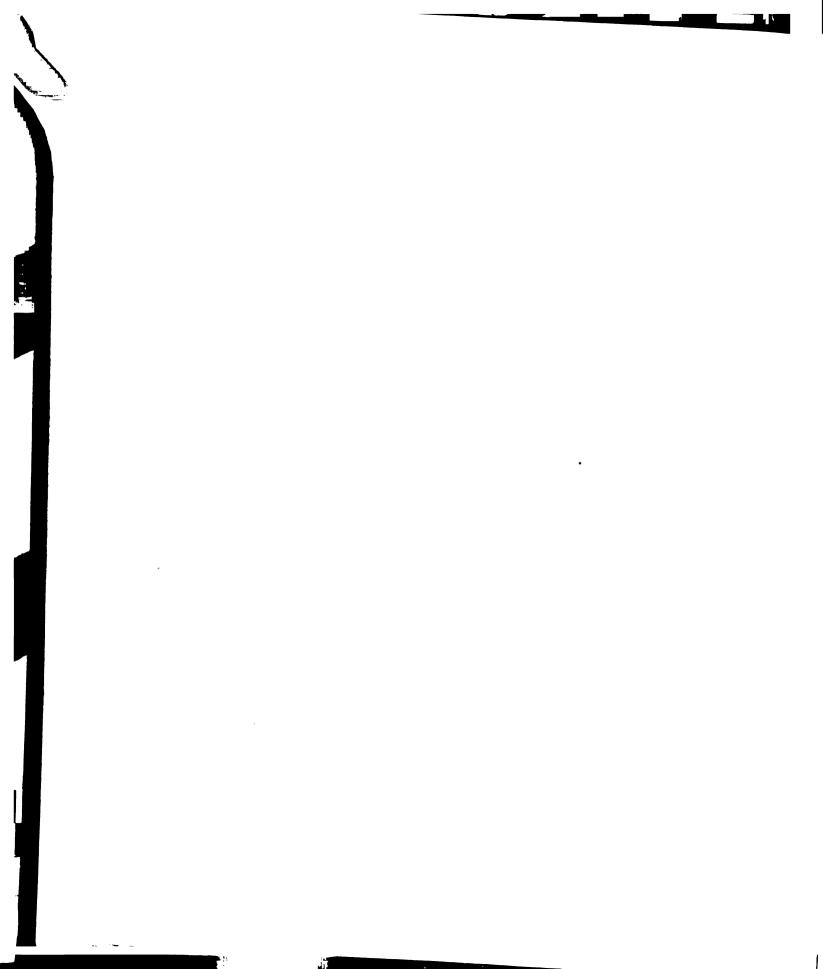
TABLE 10.

Equalities in the $\mathbf{U}_{i,j}$ elements.

$v_{11}^{01} -$	v_{11}^{02}	${\color{red} {\rm U}_{22}^{03}}$	-,-	v_{44}^{04}
003 =	0.04	\mathtt{U}_{24}^{01}	*#:	${\color{red} {\rm U}_{42}^{02}}$
$v_{12}^{01} -$	$U_{1.4}^{0.2}$	${\rm U}_{24}^{03}$	-	v_{42}^{04}
$v_{12}^{03} =$	$v_{14}^{0.4}$	$\mathbf{v_{41}^{01}}$	÷	v_{21}^{02}
$v_{14}^{01} -$	v_{12}^{02}	v_{41}^{03}	2	\mathbf{U}_{21}^{04}
$\mathtt{U}_{14}^{03} =$	$0.04 \\ 0.12$	${\tt U}_{42}^{01}$	~-	\mathtt{U}_{24}^{02}
$u_{21}^{01} =$	${\bf U_{41}^{02}}$	\mathtt{U}_{42}^{03}	==	v_{24}^{04}
\mathbf{U}_{21}^{03} =	${f U}_{41}^{04}$	U_{44}^{01}	:-	${\color{red} \mathtt{U}_{22}^{02}}$
${\tt U}_{22}^{01}$ -	0.02	v_{44}^{03}		${\rm U}_{22}^{04}$

Table 11

Equalities in the first and second neighbor parts of the $U_{i,j}$ elements.



II. CASES STUDIED AND COMPUTATIONAL PROCEDURE

A. Cases Studied

A description of the seven cases studied is shown on the following pages.

Case 1

$$c_i = e^{-\frac{\epsilon_i}{RT}} \mathcal{E}_1 = c_2 = \epsilon_3 = c_4 = c_5 = c_6 = c_7 = c_8 = 7.000 \text{ Cal mole}$$

$$v = e^{-\frac{\epsilon_i}{RT}} \quad \text{where \mathfrak{t} is the sum of the first and second}$$
 neighbor interaction energies.

In case one the polymer has a random configuration.

U Conformation Element Rotational Energy Assumed*

'**O's = "E's 1000 Cal/mole

'O's = /E's 1000 Cal/mole

where $\gg 0$ is the 2+1 first neighbor interaction energy $\approx E$ is the 2+first neighbor interaction energy γ^2 0 is the 2+1 second neighbor interaction energy γ^2 E is the 2 γ^2 second neighbor interaction energy

This specifies that the polymer in case one has a random conformation in addition to a random configuration.

* The rotational energy values correspond to the energy differences between an arbitrary energy level and the lowest point in the rotational potential well.

Case 2

$$\boldsymbol{\xi}_1 = \boldsymbol{\xi}_2 = \boldsymbol{\xi}_3 = \boldsymbol{\xi}_4 = \boldsymbol{\xi}_5 = \boldsymbol{\xi}_6 = \boldsymbol{\xi}_7 = \boldsymbol{\xi}_8 = 7,000$$
 cal/mole This polymer has a random configuration.

U Conformation Element	Rotational Energy assumed
odo's = odE's	1000 cal/mole
% E1 ₁₁	100 cal/mole
all other F E's except F El ₁₁	200 cal/mole
% 03 ₁₁	100 cal/mole
all 3 03's that have a bent conformation	750 cal/mole
all 3 01's that have a bent conformation that permits the R groups to be further apart	1250 cal/mole
all 7 01's that have a bent conformation that permits the R groups to be closer together	2000 cal/mole

The preserved consumations have the lowest rotational energies.

 \mathcal{B} El $_{11}$ is the 2 $ilde{r}$ second neighbor interaction energy of element ${\tt U}_{11}^{(1)}$ which is $ilde{r}$ - $ilde{k}$

 \mathcal{F} 03₁₁ is the 2 \mathcal{T} +1 second neighbor interaction energy of element $\mathbf{U}_{11}^{(3)}$ which is \mathcal{R} - \mathcal{T}

Case 3

 $\pmb{\xi}_1 = \pmb{\xi}_2 = \pmb{\xi}_3 = \pmb{\xi}_4 = \pmb{\xi}_5 = \pmb{\xi}_6 = \pmb{\xi}_7 = \pmb{\xi}_8 = 7,000 \text{ cal/mole}$ This polymer has a random configuration.

U Conformation Element	Rotational energy assumed
$\alpha = \alpha E'S$	500 cal/mole
p o's = p E's	500 cal/mole

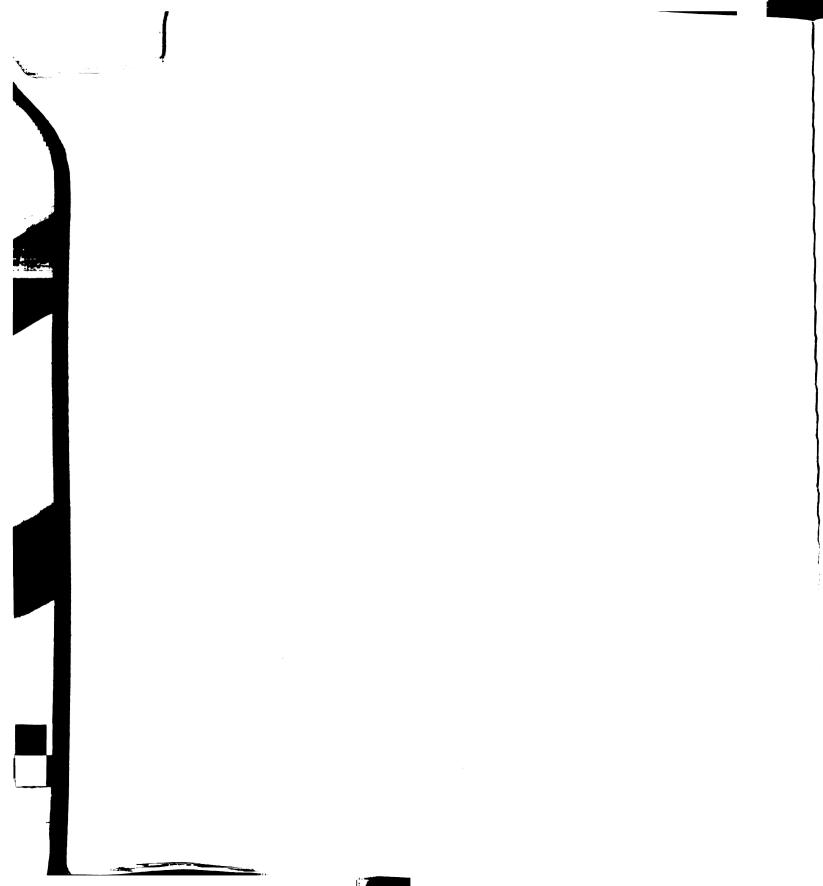
This polymer has a random conformation.

Case 4

 $\xi_1=\xi_2=\xi_3=\xi_4=\xi_5=\xi_3=\xi_7=\xi_8=7,000 \text{ cal/mole}$ This polymer has a random configuration.

U Conformation Element	Rotational Energy assumed
first neighbor H H	50 cal/mole
first neighbor H R	250-1000 cal/mole
second neighbor H H	50-600 cal/mole
second neighbor H R	200-2000 cal/mole
second neighbor R R	800-2500 cal/mole

The rotational energies assumed were assigned after comparing the first and second neighbor interactions which can be seen in Tables 3 and 4. A "most probable" energy was assigned to each conformation based on our best interpretation of a real chain.



Case 5

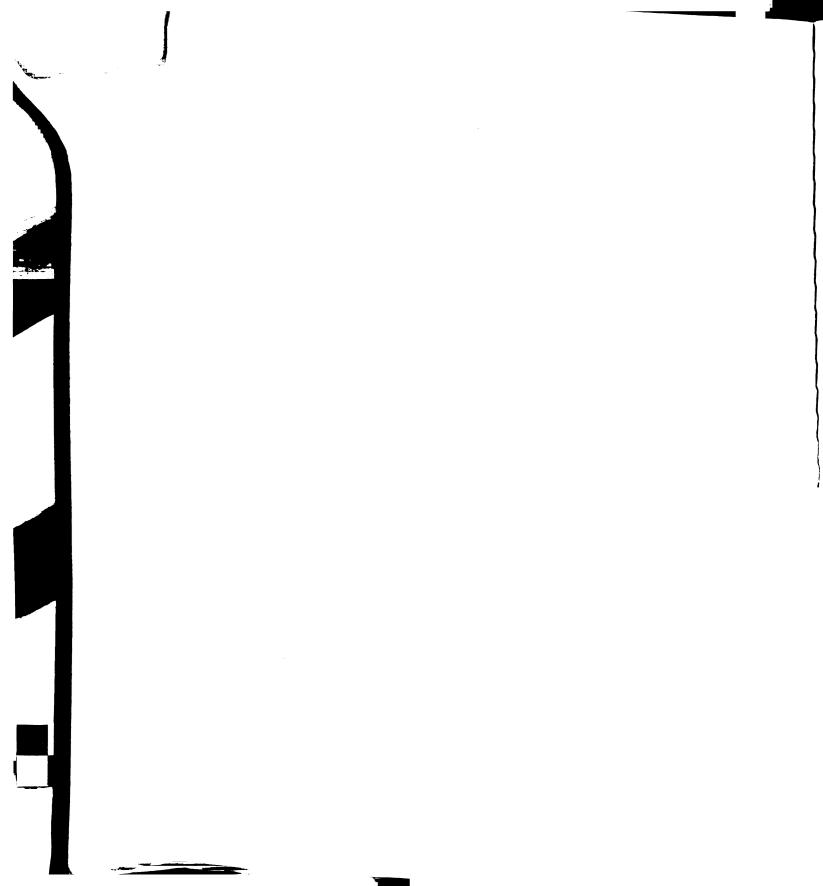
$$\boldsymbol{\xi}_1 = \boldsymbol{\xi}_2 = \boldsymbol{\xi}_3 = \boldsymbol{\xi}_4 + \boldsymbol{\xi}_5 = \boldsymbol{\xi}_6 - \boldsymbol{\xi}_7 = \boldsymbol{\xi}_8 = 7.000$$
 cal mole This polymer has a random configuration.

U Conformation Element	Rotational Energy assumed
Bosh Polask	500 cal/mole
B 03 ₁ f 4	50 cal/mole
7 0144 R	50 cal/mole
all other 3 0's	1000 cal/mole
all B E's	1000 cal/mole

$$\boldsymbol{\epsilon}_1 = \boldsymbol{\epsilon}_2 = \boldsymbol{\epsilon}_3 = \boldsymbol{\epsilon}_4 = \boldsymbol{\epsilon}_6 = \boldsymbol{\epsilon}_7 = 7,000 \text{ cal/mole}$$

 $\boldsymbol{\epsilon}_5 = \boldsymbol{\epsilon}_8 = 2,000 \text{ cal/mole}$

This polymer has a predominantly syndiotactic configuration.



U Conformation Element Rotational Energy Assumed Co's = C's Cal/mole Cal/mole

Case 7

$$\boldsymbol{\ell}_2 = \boldsymbol{\ell}_4 = \boldsymbol{\ell}_5 = \boldsymbol{\ell}_6 = \boldsymbol{\ell}_7 = \boldsymbol{\ell}_8 = 7,000 \text{ Cal/mole}$$

 $\boldsymbol{\ell}_1 = \boldsymbol{\ell}_3 = 2,000 \text{ Cal/mole}$

This polymer has a predominately isotactic configuration preferred.

U Conformation Element	Rotational Energy Assumed
~ 0's = ~ E's	500 Cal/mole
6 0's = 6 E's 7 03 ₁₁ 6 7	50 Cal/mole
8 01 44A- 57-8	50 Cal/mole
All other \$ 0's	1000 Cal/mole
All % E's	1000 Cal/mole

Tables 12, 13, and 14 show the reduced 12 x 12 matrix of $\left[\boxed{1}_{2} \mathbf{v} \right] \left[\boxed{1}_{2} \mathbf{v}_{+1} \right] \left[\boxed{1}_{2} \mathbf{v}_{+1} \right]_{4}$.

B. Computational Procedure

Case 1 will now be used as an example and the methods of computation will be described. The first step after assigning energies and calculating the various U_{j} elements was to calculate the 16 x 16 matrix 2v 2v 1 1

Table 12 Matrix Far Fare 1-4

case 1

AAA	AAA	A A A				A A A	AAA	A A A			
				AAA	A				A	A A A	A
			A	AAA	A				AAA	AAAA	AAA
AAA	AAA	AAA				AAA	A	AAA			

case 2

BDD	BDDD	CEE				B D D	BDD	CEE			
			BDDD	C E E	D				B D D	CEE	BDDD
			H	GII	I				FHH	6 I I	
H	I	I				H	GII	I	:		

case 3

J J J J J J J J J				ゴゴ ゴゴ ゴゴ	_			
000	J	丁プ	J	5 0	<u> </u>	J	JJ	
	J	J	J				JJ	4
	\mathcal{J}	J J J	J			J	コゴゴ	7
535	V	<u>U</u>	<u>U</u>	JJ	J	0	<u> </u>	
J J J J				J J J J				

case 4

MNPQRS		RLU MNP QRS	
	TUL QSR MPN		TUL Q5R MPN
	VWX YZ & BYS		V W X Y Z & B 8 8
EJ N B O) Y M E		EJN BOX YUS	

Table 12 Matrix Fari Landases 1-4

case 1

AAA							A A A	A			
			A	AAA	A				A	A	A
			A	A					A	AAAA	A
AAA	AAA	AAA		air		AAA	AAA	A			

case 2

BDD	B D D	CEE				BDD	BDD	CEE			
			BDDD	C E E	D				D	CEE	BDDD
			H	GI	I				FHH	6 I I	
1	G I I	II				H	G I I	I	i		

case 3

J J J J J J					丁 丁				
JJJ				J	J	J			
	J	J	J				J	J	\mathcal{J}
	J	J	J				J	J	\mathcal{J}
	J	J	J				J	J	J
	_	J	_				1		J
	\mathcal{J}	J	J				J	J	J
	J	J	J				J	J	乙
JJJ				J	J	J			
JJJ				J	J	J			
JJJ				J	J	J			

case 4

KLU MNP QRS		RLU MNP QRS	
	TUL QSR MPN		TUL Q5R MPN
	VWX YZ & BYS		> w x Y Z ~ B X S
EJN BOX YME		EJ N B O X Y LL E	

Table 13

Matrix [[] [] [] [] cases 5-7

				C	as	e 5					
TT	11	0				TT	T	T			
17	π	σ				IT	Π	σ			
T	IT	σ				IT	n	σ			
			11	σ	IT				1	0	IT
			Π	σ	π				IT	σ	π
			TT	σ	π				IT	0	π
			σ	IT	11				0	T	T
			σ	IT	IT				0	π	π
			σ	IT	17				5	TT	11
0	Π	T				0	17	11			
O	IT	π				σ	11	II			
10	π	π				0	17	π			

11 11 0 11 11 0 11 11 0		11 11 0 11 11 0 11 11 0	
	11 0 11 11 0 11 11 0 11		त्तरा त्रा त्रा
	σπ π σππ σππ		444 444 444
σΠΠ σΠΠ σΠΠ		P Y Y P Y Y	

case 6

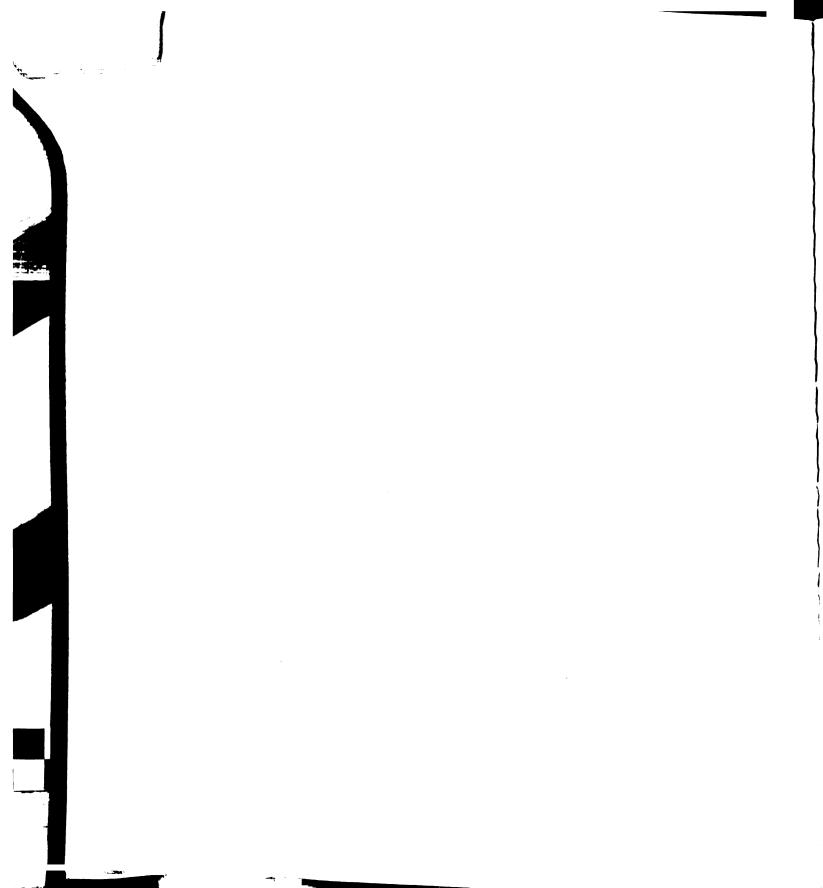
case 7

444		### ##################################	
	444 444 446		TON TON
	σΠ Π σΠ Π σΠ Π		ना । ना । ना ग
$\sigma \pi \pi$		OTT 11	
$\sigma \pi \pi$		$\sigma \pi \pi$	
OTIT		OTTT	

Table 14

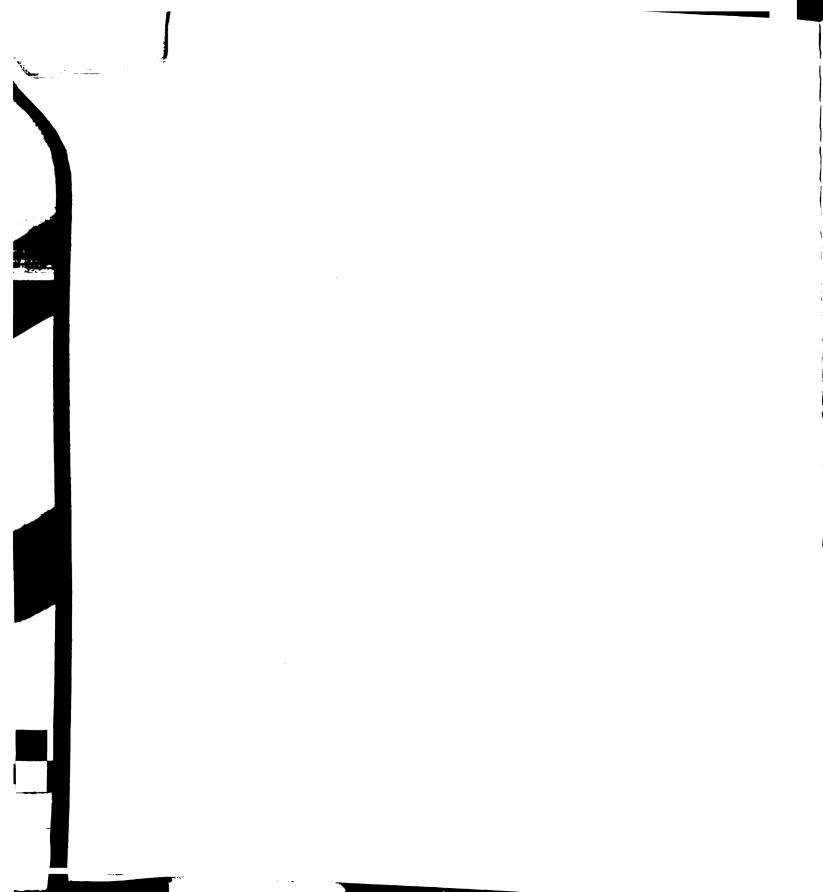
Key to the symbols in Tables 13 and 14

$A = 2.57 \text{x} 10^{-8}$	$B = 3.51 \times 10^{-8}$	$C = 5.35 \text{x} 10^{-8}$
$D = 3.39 \times 10^{-8}$	$E = 4.32 \times 10^{-8}$	$F = 2.80 \text{x} 10^{-7}$
$G = 1.61 \times 10^{-7}$	$H = 2.52 \text{x} 10^{-7}$	$\mathbf{I} = 1.51 \text{x} 10^{-7}$
$J = 7.53 \text{x} 10^{-7}$	$k = 3.96 \text{x} 10^{-6}$	$L = 3.37 \text{x} 10^{-6}$
$M = 6.19 \text{x} 10^{-7}$	$N = 5.88 \times 10^{-7}$	$P = 8.20 \times 10^{-7}$
$Q = 1.67 \times 10^{-6}$	$R = 1.24 \times 10^{-6}$	$S = 3.52 \text{x} 10^{-6}$
$T = 3.96 \times 10^{-6}$	$V = 6.66 \times 10^{-6}$	$V = 4.87 \text{x} 10^{-6}$
$W = 4.52 \text{x} 10^{-6}$	$X = 2.02 \text{x} 10^{-6}$	$y = 5.76 \times 10^{-7}$
$7 - 5.61 \times 10^{-7}$	$\sim 1.42 \times 10^{-7}$	$\beta = 2.66 \times 10^{-6}$
$3 = 2.42 \times 10^{-6}$	$\int = 1.81 \times 10^{-6}$	$\epsilon = 4.87 \text{x} 10^{-6}$
$\mathbf{J} = 2.84 \text{x} 10^{-6}$	$n = 5.85 \text{x} 10^{-6}$	$\boldsymbol{\theta} = 1.72 \text{x} 10^{-6}$
$\lambda = 2.87 \times 10^{-6}$	$\mu = 3.03 \times 10^{-7}$	$\xi = 7.78 \times 10^{-7}$
$\pi = 1.39 \times 10^{-7}$	$\sigma = 3.24 \times 10^{-7}$	$\phi = 9.24 \times 10^{-8}$
$p = 3.98 \times 10^{-8}$		



Matrix Zartly is an expanded form of matrix Zartl in which each element of the 4 x 4 matrix is multiplied by E_4 , a 4 x 4 identity matrix. Because we do not allow the bond to reverse its direction, rows 3, 7, 11, 15 and columns 3, 7, 11, 15 are all zero. This then allows the matrix to be reduced to a 12 x 12 for the purpose of calculating the largest positive eigenvalue and the corresponding eigenvector and eigenrow. A machine language program to do these calculations was written for Michigan States' digital computor which was called MISTIC. from the 28 distinct $U_{i,j}$ elements and the 8 C_{i} elements. Michigan State University computor program MA5M was then used to determine the characteristic polynomial of the 12 x 12 reduced matrix. Michigan State University computor program J2 was then used to determine the roots of this polynomial which would be the eigenvalues of the matrix. This approach gave erroneous answers because of its method of calculating the characteristic polynomial. Program MA5M uses the N + 1 points method which will give erroneous results when the eigenvalues lie close together. Case 1 has only two different rows in its reduced 12 x 12 matrix which indicates that it has not more than two non-zero eigenvalues.

Various other methods were investigated until a program was written to use the iterated vector method. 9.10 The remaining programs were run on a Burroughs 220 digital



Computer at Dow Chemical Company's Computations Research
Laboratory at Midland, Michigan. These programs were
written in Burroughs Algol 58. Some hand calculations
using the iterated vector method gave the largest positive
eigenvalue for Cases 1, 2, 3, and 5 before the computer
program was written.

A method of blocking the matrix was used to solve for all of the eigenvalues of the matrix for Cases 1 and 3. The procedure is described in Appendix B.

The eigenvector and eigenrow output from the first program in Appendix A had to be normalized so that $\sum_{i=1}^{16} \chi_{i}$

1. Then the next step was to calculate matrices [N]. $[M+D_{2}v]$ and $[E_{32}-M]^{-1}$. This data was output on cards because of a limit of 8000 words of core memory available on the computer. This data could have been put on magnetic tape and used later but since the time required to punch out the natrices was reasonably short, it was decided to take the easiest approach. The final program in Appendix A calculates $\langle h^2 \rangle$ ol². The new Burroughs B 5000 which is at the Corputations Research Laboratory now could very easily handle all of the total calculations in one step. This would require only the 28 U_{ij} variables and the 8 C_i variables to be input.

III. CONCLUSIONS

A. Results

The eigenvalues, eigenvectors, eigenrows and $\Delta^2 > 0.1^2$ are shown in Tables 15, 16, 17, 18, and 19. Table 19 also includes the values of two 2 x 2 matrices which are called MAT2 and MAT3. MAT2 is the product of multiplying Δ^* N Δ while MAT3 is the product of $\Delta^* \left[\mathbb{E}_{32} + \mathbb{N} \right] \left[\mathbb{E}_{32} - \mathbb{M} \right]^{-1}$ $\left[\mathbb{N} \cdot \mathbb{D}_2 \sqrt{\Delta} \right] \Delta$ (see equation 13). One can see upon analysis of equation (13) that $\Delta^2 > 11^2$ is equal to 1 + MAT2(2,2) + MAT3(2,2).

TABLE 15.
Non-normalized
eigenve tors.

X ₁₆	x_{15}	X 1.4	X 1 သ	X 12	X ₁₁	X 10	х ₉	×	× ,	ນ ×	. ان ا	<u>,</u>	ಬ	X 2	×	
.1000,+01	.0000.+00	.1000,+01	.1000,+01	.1000,+01	.0000,+00	.1000.+01	.1000.+01	.1000,+01	.0007.+00	.1000,+01	.1000,+03	.1000,+01	.0000.+00	.1000,+01	.1000,+01	CASE 1
.8499,+00	.0000, +00	.8499,+00	.1000.+01	.8499.+00	.0000.+00	.8499.+00	.9998,+00	.331601	.0000,+00	.3316,-01	.4093,-01	.332701	.0000.+00	.381601	.409301	CASE 2
.1000,+01	.0000.+00	.1000.+01	.1000.+01	.1000,+01	.0000,+00	.1000,+01	.1000.+01	.1000,+01	.0000,+00	.1000,+01	.1000.+01	.1000,+01	.0000.+00	.1000.+03	.1000.+01	CASE 3
.1563,-01	.0000,+00	.2892,+00	.1000,+01	.2809.+00	.0000,+00	.1270,-01	.9080.+00	.203301	.0000.+00	.2147,+00	.9941,+00	.2010.+00	.0000.+00	.189301	.9318.+00	CASE 4
.1000,+01	.0000,+00	.1000,+01	.1000,+01	.1000,+01	.0000.+00	.1000,+01	.1000,+01	.1000.+01	.0000.+00	.1000.+01	.1000.+01	.1000.+01	.0000.+00	.1000.+01	.1000.+01	CASE 5
.1254,-03	.0000,+00	.125403	.1254,-03	.157407	.0000,+00	.157407	.1574,-07	.7840,-07	.0000.+00	.784007	.784007	.1000.+01	.0000.+00	.1000.+01	.1000,+01	CASE 6
.1254,-03	.0000.+00	.125403	.125403	. 1574,-07	.0000,+00	.157407	.157407	.784007	.0000.+00	.784007	.7840,-07	.1000.+01	.0000.+00	.1000.+01	.1000.+01	CASE 7

1000, +01 1000, +01 0000, +00 1000, +01

1000,+01

.0000,+00 .8499,+00

1000.+01

.0000,+00

.0000,+00

0000,+00

1254,-03 1254,-03

> 1574.-07 0000,+00 1574,-07 1254.-03

1254. - 03

1254,-03

0000.+00 1254,-03 1000,+01

1000,+01

1563, -01

1000,+01

.8499,+00

.1000.+01

, 1000, +01

2809.+00 1000,+01

1000,+01

1574.-07 0000,+00 1574.-07

1000.+01

2892.+00

1000,+01

0000,+00

0000,+00

 $9080. \pm 00$

1000,+01

. 1574, -07

1574,-07

7840.-07

7840.-07 0000.+00

7840.-07 0000.+00 7840.-07

2033.-01

1000.+00

1270,-01

.0000.+00

8499.+00

.9998,±00 .8499.±00

.0000,+00 .1000,+01 .1000,+01 .1000,+01

1000,+00

1,000,+01

. 1**000,+01** . 0000. +00

.3316,-01

1000,+01

.2147,+00 .0000.+00

.1000.+01

.0000,+00

3316.-01

.1000,+03	.1000,+01	.0000,+00	.1000,+01	.1000,+01	CASE 1
.4093,-01	.332701	.0000.+00	.381601	.409301	CASE 2
.1000.+01	.1000,+01	.0000.+00	.1000.+03	.1000.+01	CASE 3
.9941,+00	.2010.+00	.0000.+00	.189301	.9318.+00	CASE 4
.1000.+01	.1000.+01	.0000.+00	.1000.+01	.1000,+01	CASE 5
.784007	.1000.+01	.0000.+00	.1000.+01	.1000.+01	CASE 6
.7340,-07	.1000.+01	.0000.+00	.1000.+01	.1000.+01	CASE 7

TABLE

۲. ن .

Non-normalized eigenvectors.

NON-NORMALIZED EIGENROW

Y_{16}	Y 15	Y ₁₄	Y 13	Y 12	\mathbf{Y}_{1}	V 10	$\tilde{\chi}_{0}$	$\mathbf{x}^{\mathbf{Y}}$	Y ₇	y	υ, ,	, z	ا کنا	7,	Y	
.1000,+01	.0000,+00	.1000,+01	.1000.+01	.1000.+01	.0000,+00	.1000.+01	.1000,+01	.1000.+01	.0000.+00	.1000,+01	.1000.+01	.1000.+01	.0000.+00	.1000,+01	. 1000.+01	CASE 1
.4032,+00	.0000,+00	.4615,+00	.9978.+00	.4616.+00	.0000,+00	.4034.+00	.9978.+00	.4032.+00	.0000.+00	.4615,+00	.9978,+00	.4616,+00	.0000,+00	.4034.+00	.1000.+01	CASE 2
.1000.+01	.0000,+00	.1000,+01	.1000.+01	.1000,+01	.0000,+00	.1000,+01	.1000,+01	.1000,+01	.0000.+00	.1000,+01	.1000,+01	.1000.+01	.0000,+00	.1000.+01	.1000.+01	CASE 3
.2025,+00	.0000,+00	.8071,+00	.4850,+00	.9942,+00	.0000.+00	.1898,+00	.4771,+00	.2025.+00	.0000.+00	.8071.+00	.4850,+00	.1000.+01	.0000.+00	.1900.+00	. 4771.+00	CASE 4
.3619,+00	.0000,+00	.1000,+01	.1000.+01	.1000,+01	.0000,+00	.3619,+00	.1000,+61	.3619.+00	.0000,+00	.1000.+01	.1000.+01	.1000,+01	.0000.+00	$.3619.\pm00$.1000.+01	CASE 5
.1160;-08	.0000,+00	.1176,-08	.2696,-07	.2149,-03	.0000,+00	.924305	.9243,-05	.3488,-07	.0000.+00	.7956,-07	.606807	. 1000, + 01	.0000.+00	.4301,+00	. 1001,+00	CASE 6
.1160,-08	.0000.+00	.1176,-08	.2696,-07	.2149,-03	.0000.+00	.9243,-05	.9243,-05	.348807	.0000,+00	.7956,-07	.606807	.1000.+01	.0000.+00	.4301.+00	.4301.+00	CASE 7

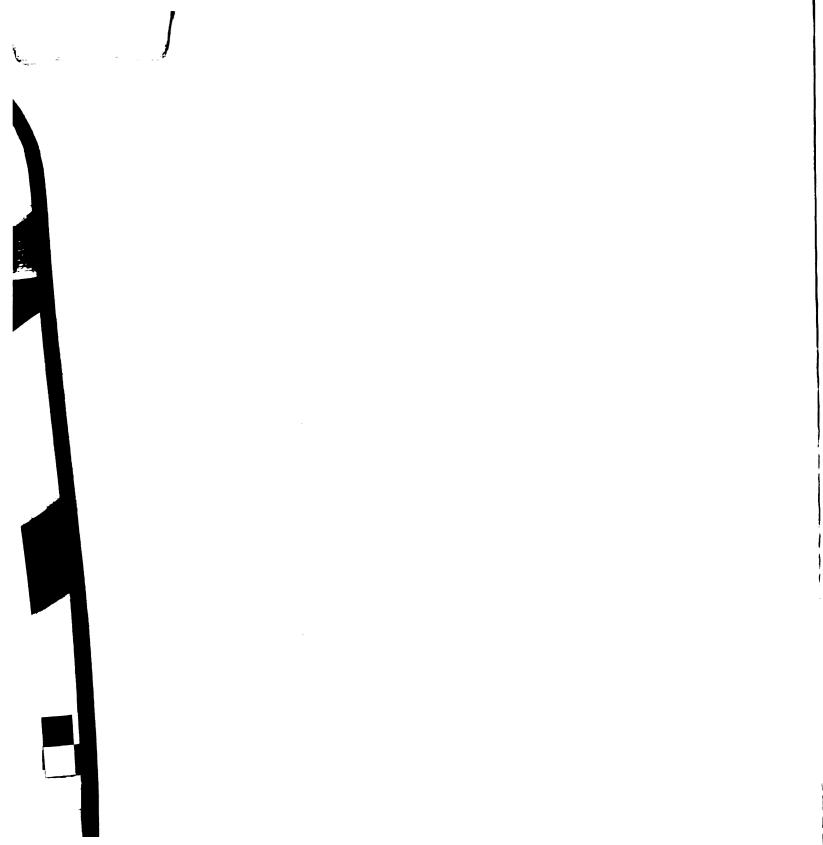
TABLE 16.

Non-normalized eigenrows.

NORMALIZED EIGENVECTOR

916	5	<u>3</u>	<u>သ</u> ယ	٠٠٠٠	٠ <u>٠</u> .	ري ري آخر		ż.	7 (5	à.,	<u>.</u>	ر دی ا	٠ ان	<u>:</u>	
.2887,+00	.0000,+00	.2887.+00	.2887,+00	.2887,+00	.0000,+00	.2887,+00	.2887.400	.2887,+00	.0000.+00	.2887.+00	.2887,+00	. 2887.+00	.0000.+00	.2887.+00	.2887.+00	CASE 1
.3891,+00	.0000,+00	.3891.+00	.4221,+00	.3891,+00	.0000,+00	.3891,+00	.4220.+00	.7686,-01	.0000.+00	.768601	. 853801	.769501	.000000	.768601	.853801	CASE 2
.2887,+00	.0000,+00	.2887,+00	.2887,+00	.2887,+00	.0000,+00	.2887,+00	.2887,+00	$.2887_{,+00}$.0000.+00	.2887.+00	.2887.+00	.2387.+00	.0000.+00	.2887,+00	. 2337, +00	CASE 3
.5654,-01	.0000.+00	.2433.+00	.4523,+00	.2397,+00	.0000,+00	.5098,-01	.4310.+00	.6450,-01	.0000.+00	.2096. + 00	.4511,+00	.2028.+00	.0000.+00	.621401	. 4366, 400	CASE 4
.2887.+00	.0000.+00	.2887.+00	.2887.+00	.2887.+00	.0000.+00	.2857,+00	.2887,+00	.2887,+00	.0000.+00	.2887.+00	.2887.+00	$.2857. \pm 00$.0000.+00	.2887.+00	.2507.400	CASE 5
.724204	.0000.+00	.7242,-04	.7242,-04	.9089,-08	.0000.+00	.9089,-08	.908908	. 4527,-07	.0000.+00	.4527,-07	.4527,-07	.577.1.+00	.0000, +00	.5774.+00	.5774.+00	CASE 6
.724204	.0000,+00	.724204	.7242,-04	.9089,-08	.0000.+00	.908908	.908908	.452707	.0000,+00	.4527,-07	.452707	.5774.+00	.0000.+00	.5774.+00	.5774.+00	CASE 7

Normalized disenvectors.



NORMALIZED EIGENROW

5 * 16	<u>~</u> , 15	c 14	े 13	£ 12	NORM			EIG *			ار 10 *	·. 4 *	<u>ئ</u> دئ *	ئ 2 *	⊢ ' }	
.2887.+00	.0000.+00	.2887,+00	.2887,+00	.2887,+00	.0000,+00	.2887,+00	.2887,+00	.2887,+00	.0000.+00	.2887,+00	.2887.+00	.2887,+00	.0000.+00	.2887,+00	.2887.+00	CASE 1
.2326.+00	.0000,+00	.2488.+00	.3659,+00	.2489,+00	.0000.+00	.2326,+00	.3659,+00	.2326,+00	.0000,+00	.2488.+00	.3659.+00	.2489.+00	.0000,.00	.2326,+00	.366300	CASE 2
.2887.+00	.0000,+00	.2887,+00	.2887,+00	.2887,+00	.0000,+00	.2887.+00	.2887,+00	.2887,+00	.0000.+00	.2887,+00	.2887,+00	.2887.+00	.0000,+00	.2887.+00	.2887.+00	CASE 3
. 1790,+00	.0000,+00	.3574,+00	.2771,+00	.3967,+00	.0000,+00	.1733,+00	.2748,+00	.1790.+00	.0000,+00	.3574.+00	.2771,+00	.3979,+00	.0000.+00	.1734.+00	.2748,+00	CASE 4
.1957.+00	.0000,+00	.3254.+00	.3254,+00	.3254,+00	.0000.+00	.1957,+00	.3254,+00	.1957.+00	.0000.+00	.3254.+00	.3254,+00	.3254.+00	.0000. +00	.1957.+00	.3254.+00	CASE_5
.991309	.0000.+00	.1005,-08	.2303,-07	.1836,-03	.0000.+00	.7896,-05	.7896,-05	.298007	.0000,+00	.679707	.518407	.8543.+00	.0000.+00	.3675.+00	.3675.+00	CASE 6
.9913,-09	.0000.+00	.100508	.2303,-07	.1806,-03	.0000,+00	.789605	.7896,-05	.2980,-07	.0000,+00	.6797,-07	.518407	.8543.+00	.0000,+00	.3675.+00	.3675.+00	CASE 7

North lized eight ows.

TABLE 19. Final results.

1.14	1 21	1.62	2.01	1.67	1.68	1.67	h^2/nl^2
675,-01	+.112.+00	+.509.400	+.830,+00	+.500.+00	+.633.+00	+.260,+00	MATU(2.2)
282,+00	281,+00	+.298,+00	889,-01	+.167.+00	+.467,+00	+.167,+00	MAT: (2,1)
+.232,+00	÷.281,+00	+.668,+00	+.169.+01	+.167.+00	+.612,+00	+.167.+00	MAT3(1,2)
675,-01	+.212,400	4.847.+00	+.653,+00	+.500,+00	+.615.+00	+ 5500,400	MAT3(1,1)
+.212,+00	4.456,-04	+.113.+00	+.183,+00	+.167.+00	4.42501	+.167.+00	MAT2(2,2)
28100	605,-04	÷.11500	+.209,+00	÷.167,+00	+.272.+00	+.167.+00	MAT2(2,1)
+.281.+00	÷.60S04	+.412.+00	+.554.+00	+.167.+00	+.382.+00	+.167,+00	MAT2(1,2)
4.212.+00	+.45604	+ . 471 . + 00	300.400	+.167.+00	+.42501	+.167.+00	MAT2(1,1)
. 28002	.280,-02	.12005	.15504	.45205	.62806	. 154, -00	
CASE 7	CASE 6	CASE	CASE 1	CASE	CASE 2	CASE 1	



B. Discussion of Results

Case two has totally random configuration, totally random first neighbor interactions, all second neighbor $2\mathbf{V}$ interactions except one are random, and a distinction is made between only the second neighbor $2\mathbf{V} \cdot 1$ interactions (see part A section two). This does not noticeably change the quantity $\frac{1}{2} \frac{1}{2} \ln 1^2$ from that obtained for the totally random case. This implies that for this model the second neighbor interactions must be quite far apart to noticeably effect the end-to-end dimension of the polymer.

In case four a distinction is made in both first and second neighbor interaction energies while the configuration is still kept random (see part A section two). This has a significant effect on the result. The rotational energies assumed were "most probable" values assigned after

comparison of the first and second neighbor interactions which are depicted schematically in Tables 3 and 4. The value of $\langle h^2 \rangle / nl^2$ obtained in case four (2.01) is essentially that obtained by considering a freely rotating polymethylene chain consisting of n bonds of identical length 1 joined at fixed valence angles 0. For large n and a tetrahedrally bonded chain ($\theta = 109.5^{\circ}$) a value of $\overline{\tau}^2/nl^2 = 2$ is obtained. Hence on a two dimensional lattice a value of 2 represents a reasonably expanded chain.

Cases 5, 6, and 7 are identical with respect to conformation but case 5 has a random configuration, while case 6 has a preferred syndiotactic configuration, and case 7 has a preferred isotactic configuration. The result for case 5 is very close to the result obtained for the totally random case. One would probably predict from the inspection of the preferred configurations for cases 5, 6, and 7

that case 6 with a preferred syndiotactic configuration would have a higher value of $\langle h^2 \rangle / nl^2$ than a random case while case 7 with a preferred isotactic configuration would have a lower value than a random case.

The result for case 7 is in agreement with this reasoning while that for case 6 is not in agreement. Because of the disagreement of case 6 with this theory, case 6 was run thru the various computer programs a second time. The same result was obtained in both determinations.

Further study on the model in case 6 led to the idea that the polymer was actually running in a straight line for a while and then turning around and going back in the direction in which it previously came. A schematic diagram depicting this is shown in Figure 4.

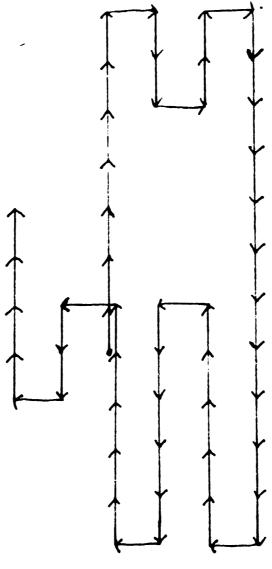


Figure 4

Schematic diagram depicting the polymer chain in case 6

A three dimensional model would allow the polymer to make many more moves than the square lattice and hence the results would be different in many cases. If the isotactic polymer in case 7 were allowed to proceed in three dimensions it would undoubtedly coil up and form a helix with a longer end-to-end dimension.

These preliminary analyses have aroused more problems and questions than they have answered. It would be extremely interesting to determine the effect of temperature on the end-to-end dimension. There are many more different cases which would provide more information about the polymer model. It would be quite beneficial to have the matrices M and N (equations 14 and 15) multiplied out in symbolic form so that one could see the positions of the favored conformations in the two matrices.

IV. BIBLIOGRAPHY

- 1. M. V. Volkenstein, J. Polymer Sci., 29, 441 (1958).
- 2. S. Lifson, J. Chem. Phys. 30, 964 (1959).
- 3. K. Nagai, J. Chem. Phys. 31, 1169 (1959).
- 4. S. Lifson, J. Chem. Phys. 29, 80 (1958).
- 5. K. Nagai, J. Chem. Phys. 30, 660 (1959).
- 6. C. A. J. Hoeve, J. Chem. Phys. 32, 883 (1960).
- 7. C. A. J. Hoeve, J. Chem. Phys. 35, 1266 (1961).
- 8. S. J. Yoo and J. B. Kinsinger, J. Chem. Phys. 36, 1371 (1962).
- 9 E. Bodewig, "Matrix Calculus", North-Holland
 Publishing Company, Amsterdam, 1959, Part IV,
 Chap. 2.
- 10. C. Lanczos, "Applied Analysis", Prentice Hall, Inc. Englewood Cliffs, N. J., 1961, Chap. II.
- 11. P. Flory, "Principles of Polymer Cheristry", Cornell University Press, Ithaca, New York, 1953, Chap. X.

APPENDIX A

FIGURE 5

Diagram used to determine the sin-cosine transformation matrices when the same coordinate system is used for

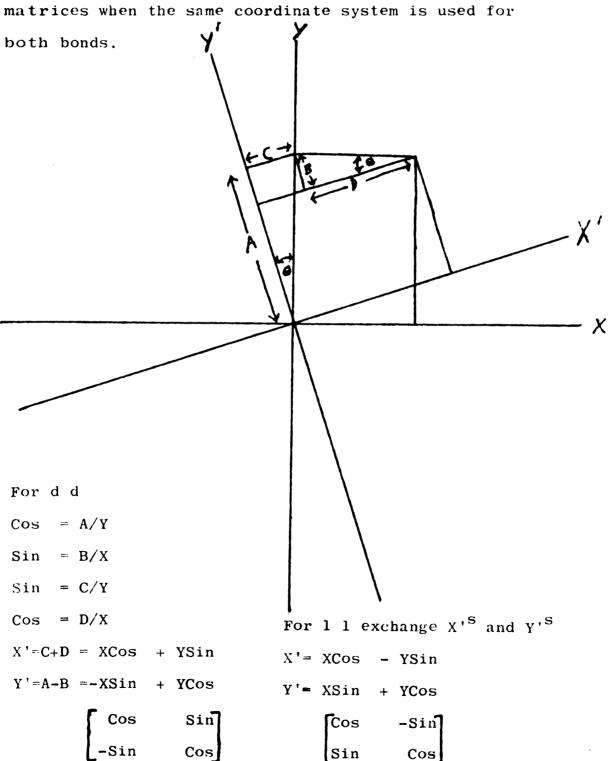
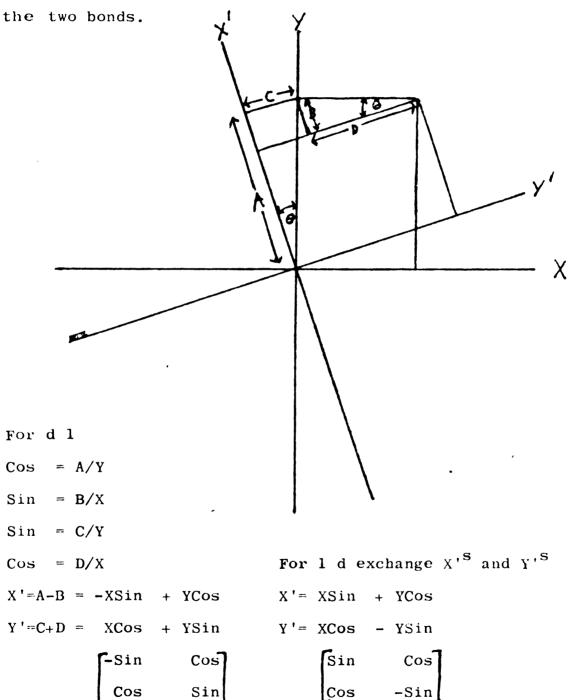


FIGURE 6

Diagram used to determine the sin-cosine transformation matrices when different coordinate systems are used for



The values of the sin and cosine of the four bond angles are shown below.

angle 0 $\pi/2$ π $3\pi/2$ sin 0 1 0 -1

cos 1 0 -1 0

Matrix $\begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$ is d d therefore the sin-cosine matrix used is $\begin{bmatrix} \cos & \sin \\ -\sin & \cos \end{bmatrix}$

state	bond angle	matrix
1	0	1 0
2	$3\pi/2$	0 1 0-1 1 0
3	π	-1 0 0 -1
4 .	$\pi/2$	0 1 -1 0

Matrix $\begin{bmatrix} a \\ b \end{pmatrix}$ is 11 therefore the sin-cosine matrix used is $\begin{bmatrix} \cos & -\sin \\ \sin & \cos \end{bmatrix}$

state	bond angle	matrix
1	0	$\begin{matrix}1&0\\0&1\end{matrix}$
2	$3\pi/2$	0 1 -1 0
3	π	$ \begin{array}{cccc} -1 & 0 \\ 0 & -1 \end{array} $
4	$\pi/2$	0 -1 1 0



```
Matrix \begin{bmatrix} \beta \\ 2v_{1} \end{bmatrix} is 1 d therefore the sin-cosine matrix used is \begin{bmatrix} \sin & \cos \\ \cos & -\sin \end{bmatrix}
```

state	bond angle	matrix
1	0	$\begin{array}{ccc} 0 & 1 \\ 1 & 0 \end{array}$
2	$3\pi/2$	$ \begin{array}{ccc} -1 & 0 \\ 0 & 1 \end{array} $
3	π	$ \begin{array}{cccc} 0 & -1 & & \\ -1 & 0 & & \\ \end{array} $
4	$\pi/2$	1 0 0 -1

Matrix [is d l therefore the sin-cosine matrix used is [-sin cos] cos sin

state	bond angle	matrix
1	0	$egin{array}{ccc} 0 & 1 \ 1 & 0 \end{array}$
2	$3\pi/2$	1 0 0 -1
3	π	$ \begin{array}{ccc} 0 & -1 \\ -1 & 0 \end{array} $
4	$\pi/2$	-1 0 -1 0

But for matrix []27

$$\left[D_{ar}^{(i)}\right] = \left[D_{arti}^{(i)}\right]$$

APPENDIX B

BLOCK METHOD FOR DETERMINING THE EIGENVALUES OF A MATRIX

Let
$$\beta = \begin{bmatrix} A & A & A \\ A & A & A \\ A & A & A \end{bmatrix}$$
 and $O = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$ as shown for

case one in Table 10. The 12x12 matrix then becomes

$$\begin{bmatrix} \beta & O & \beta & O \\ O & \beta & O & \beta \\ O & \beta & O & \beta \\ \beta & O & \beta & O \end{bmatrix}$$
 Upon solving for the eigenvalues(Y), the matrix becomes
$$\begin{bmatrix} \beta-Y & O & \beta & O \end{bmatrix}$$

$$\begin{bmatrix} \beta-Y & O & \beta & O \\ O & \beta-Y & O & \beta \\ O & \beta & -Y & \beta \\ \beta & O & \beta & -Y \end{bmatrix}$$
 Which upon multiplication yields
$$\begin{bmatrix} \beta-Y & \beta & \beta & \beta \\ \beta & -Y & \beta & \beta \\ \beta & -Y & \beta & \beta \\ O & \beta & -Y \end{bmatrix} + \beta \begin{bmatrix} O & \beta-Y & \beta \\ O & \beta & \beta \\ \beta & O & -Y \end{bmatrix} = 0$$

$$\begin{bmatrix}
\beta - Y & G & B \\
B & -Y & B \\
O & B & -Y
\end{bmatrix} + B \begin{bmatrix}
O & B - Y & B \\
O & B & B \\
B & O & -Y
\end{bmatrix} = 0$$

Upon multiplying out further

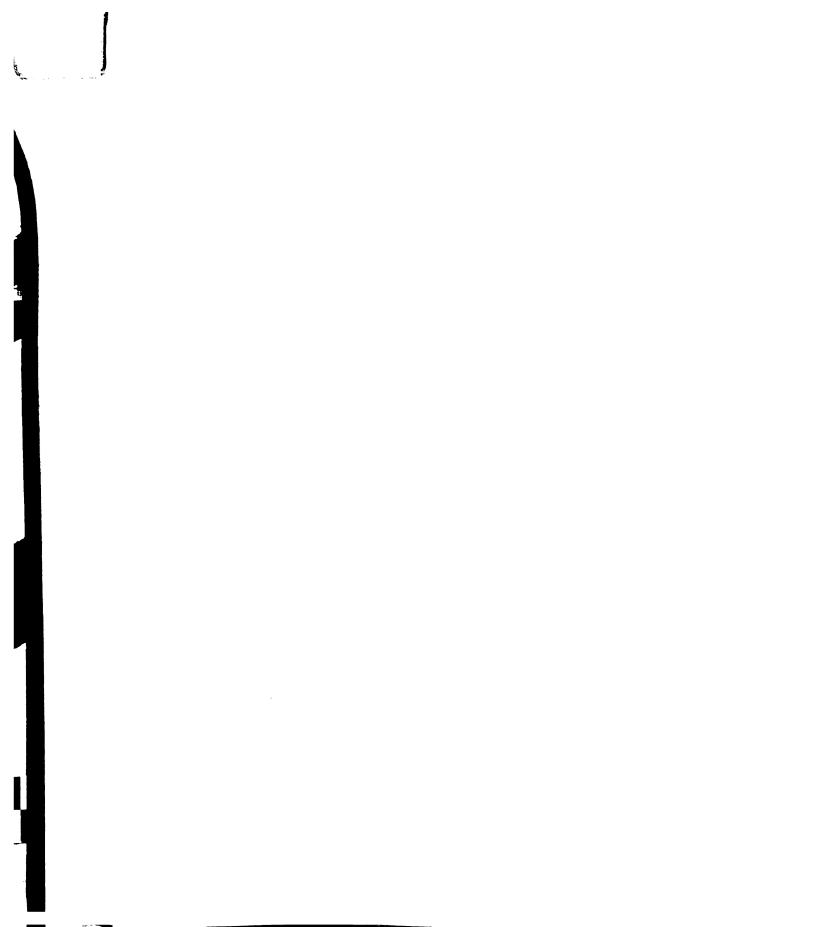
$$(\beta-Y)^{2}(Y^{2}-\beta^{2}) + (\beta-Y)\beta\beta^{2} + \beta(\beta-Y)(+\beta^{2}) + \beta^{2}(-\beta^{2}) = 0$$

$$\beta^{2}Y^{2} - 2\beta Y^{3} + Y^{4} - \beta^{4} + 2\beta^{3}Y - \beta^{2}Y^{2} + \beta^{4} - \beta^{2}Y + \beta^{4} - \beta^{3}Y - \beta^{4}=0$$

$$-2\beta Y^{3} + Y^{4} = 0 \qquad Y^{3}(Y-2\beta) = 0, Y=0,0,0,+2\beta$$

But
$$\beta = \begin{bmatrix} A & A & A \\ A & A & A \\ A & A & A \end{bmatrix}$$
, so $2\beta = 2A$ $\begin{bmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix}$

The next step is to solve for the eigenvalues(x) of the 3by3 matrix.



Upon solving for the eigenvalues(x) the matrix becomes

$$\begin{bmatrix} 1-x & 1 & 1 \\ 1 & 1-x & 1 \\ 1 & 1 & 1-x \end{bmatrix}$$
 Which upon multiplication becomes
$$(1-x)\begin{bmatrix} (1-x^2) & -1 \end{bmatrix} -1\begin{bmatrix} (1-x) & -1 \end{bmatrix} +1\begin{bmatrix} 1-(1-x) \end{bmatrix} = 0$$

$$(1-x)(1-2x+x^2-1) +x +x = 0 -2x+x^2+2x^2-x^3+2x = 0$$

$$3x^2-x^3=0 -x^2(x-3)=0 x=0,0,+3$$

Therefore the twelve eigenvalues of the original 12 by 12 matrix are eleven zeros and 6A. Thus the largest positive eigenvalue of (2.57×10^{-8}) which is 1.54×10^{-7} .

APPENDIX C

ALGOL 58 COMPUTER PROCEDURES

COMMENT ITERATED VECTOR METHOD FOR CALCULATING THE LARGEST POSITIVE LIGENVALUE OF A TWELVE BY TWELVE MATRIX. THIS PROGRAM ALSO PRINTS OUT THE CORRESPONDING EIGENVECTOR AND LIGENROW.

R. C. THOMAS:

INTEGER I, J, K, L;

ARRAY TMATRIX(12,12).MATRIX(12,12),PRESVECTOR(12), PREVVECTOR(12),Y(12);

LO. K L=0;

FOR I (1,1,12) PREVVECTOR(I)=0.0;

PRESVECTOR(1)-1.0;

FOR J=(2,1,12); PRESVECTOR(J)=0.0;

INPUT MAT (FOR I=(1,1,12); FOR J=(1,1,12);

MATRIX(I,J):

READ (;; MAT);

L1.. K=K+1; IF K EQL 100; GO TO L0;

FOR I = (1, 1, 12):

BEGIN Y(I) = 0.0;

FOR J = (1, 1, 12):

Y(I) = Y(I) + MATRIX (I,J).PRESVECTOR(J) END;

L2.. LRG-0.0;

FOR I = (1, 1, 12); BEGIN

IF Y(I) GTR LRG; BEGIN

LRG = Y(I) END END;

```
L3.. WRITE(;;LARGE,FORM1);
      OUTPUT LARGE (LRG);
      FORMAT FORM1 (B7, F11.5, W);
L4.. FOR I = (1,1,12); PREVVECTOR(I) = PRESVECTOR(I):
      FOR I=(1,1,12); PRESVECTOR(I) = Y(I) 'LRG:
L5.. FOR I=(1,1,12); BEGIN
      IF (ABS(PRESVECTOR(I) - PREVVECTOR(I))GTR 0.00001);
      GO L1 END;
L6.. FOR I = (1, 1, 12): BEGIN
      WRITE(:;VECROW,FORM1);
      OUTPUT VECROW (1 RESVECTOR(I)) END;
      L=L+1; IF (L EQL 2); GO TO LO:
L7.. FOR I=(1,1,12). FOR J^{-}(1,1,12);
      TMATRIX(J,I) = MATRIX(I,J);
      FOR I = (1, 1, 12); FOR J = (1, 1, 12):
      MATRIX(I,J) = TMATRIX(I,J):
Lo.. GO TO L1;
      FINISH;
```

COMMENT THIS PROGRAM CALCULATES MATRICES M AND N. IT

ALSO PUNCHES OUT ON CARDS IN THE FOLLOWING ORDER MATRICES

N, (M+D2V), AND (E32-M)-1. (PH12V)2.(D2V+1) AND

(PH12V+1)2.(SIGMA2V+1)2x4 AND LEIG ARE READ IN ON CARDS

IN THAT ORDER, R. C. THOMAS;

ARRAY MATA(32,32), MATB(32,32), MATC(32,32), MATD(32,32), MATE(32,32);

INTEGER I, J, K, N;

PROCEDURE INVERT1 (N,A(,);:ERR1); BEGIN

COMMENT INVERT A SQUARE MATRIX, IN PLACE, BY THE NBS

PIVOTAL ROW METHOD. INPUT CONSISTS OF THE ORDER

AND NAME OF THE MATRIX. OUTPUT IS THE INVERSE,

WITH THE SAME NAME. REFERENCE MUST INCLUDE A

STATEMENT LABEL TO WHICH A TRANSFER MAY BE MADE IF

THE MATRIX IS SINGULAR, A PRINT OUT STATING INVERSION

FAILURE WILL BE MADE.

NOTE THAT ARRAY DECLARATION ALLOWS FOR A MAXIMUM MATRIX OF ORDER 30. IF LARGER ORDER IS NEEDED, CHANGE ARRAY DECLARATIONS ACCORDINGLY.

AUTHOR - C.D. ALSTAD;

INTEGER I, J, K, L, SJ, N;

ARRAY ORDER (32), SAVE (32), SHIFT (32);

FORMAT FINV1(B10, *MATRIX SINGULAR, INVERSION FAILED*, WO):

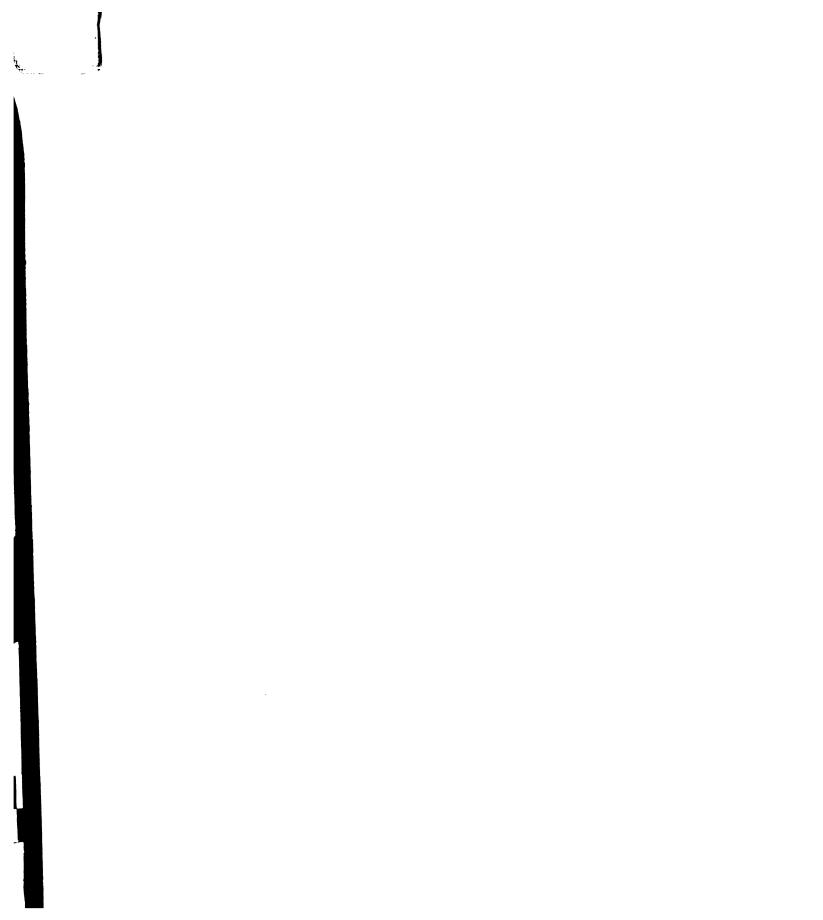
FOR I=(1,1,N); BEGIN ORDER(I) = 0; SHIFT(I) = 0 END;

```
M1. FOR L = (1,1,N); BEGIN CHAMP = 0;
M2.. FOR I = (1,1,N): BEGIN Z = A(I,1):
M3.. IF ABS(Z) GEQ ABS(CHAMP); BEGIN K = I;
     FOR J = (1,1,L); IF ORDER(J) EQL K; GO ONSEEK:
     CHAMP = Z; ORDER(L) = K;
ONSEEK.. END M3 END M2; Z = CHAMP; K = ORDER(L):
     IF CHAMP EQL 0; BEGIN WRITE (;;FINV1); GO ERR1 FND:
     FOR J = (1, 1, N-1) : A(K, J_1) = A(K, J+1) / Z : A(K, Y_1) / Z :
M4.. FOR I = (1,1,N); BEGIN IF I EQL K: GO M5: MULT A(1,1):
     FOR J = (1, 1, N-1); A(I,J) = A(I,J+1) - MULT.A(K,J);
     A(I,N) = -MULT.A(K,N);
M5.. END M4 END M1;
COMMENT MATRIX NOW INVERTED BUT SCRAMBLED, SO UNSCRAMBLE:
COMMENT UNSCRAMBLE ROWS: K=0;
MR1.. FOR L = (1,1,N); IF SHIFT(L) EQL 0; GO MR2;
MR2.. IF ORDER(L) EQL L; BEGIN SHIFT(L) = L:K == K+1:
      IF K EQL N; GO MC4: GO MR1 END;
     FOR J^{\infty}(1,1,N); SAVE(J) = A(L,J); SJ = L;
MR3.. I = ORDER(L); FOR J=(1,1,N); A(L,J) = A(I,J);
     SHIFT(L) = I; L=I; K=K+1; IF K EQL N; GO MC4;
      IF ORDER(L) NEQ SJ; GO MR3;
     FOR J = (1,1,N); A(L,J) = SAVE(J):
     SHIFT(L) = SJ; K = K+1;
     IF K NEQ N; GO MR1:
```

```
COMMENT NOW UNSCRAMBLE COLUMNS;
MC4...FOR I = (1,1,N); SHIFT(I) = 0; K = 0;
MC5.. FOR L= (1,1,N); IF SHIFT(L) EQL 0; GO MC6;
MC6.. IF ORDER(L) EQL L; BEGIN SHIFT(L) = L; K : K + 1.
     IF K EQL N; GO MC9; GO MC5 END MC6;
     FOR J=(1,1,N); SAV\Gamma(J) = A(J,L); SJ = L;
     FOR I=(1,1,N); IF ORDER(K) EQL L; GO MC7;
MC7.. FOR J=(1,1,N); A(J,L) = A(J,I):
     SHIFT(L) = I; L = I; K = K+1; IF K EQL N; GO MC9;
     FOR I = (1,1,N); IF ORDER(I) EQL L; GO MC8;
MC8.. IF I NEQ SJ; GO MC7;
     FOR J=(1,1,N); A(J,L) = SAVE(J);
     SHIFT(L) = SJ; K = K+1; IF K NEQ N; GO MC5;
MC9.. RETURN END INVERTI();
LO1.. FOR I=(1,1,32); FOR J=(1,1,32); BEGIN MATA(I,J)=0.0;
     MATB(I,J) = 0.0; MATC(I,J) = 0.0; MATD(I,J) 0.0;
     MATE(I,J)=0.0 END LO1;
LO2.. FOR I=(1,8,25); MATA(I,I)-1.0; FOR I=(2.8,26)
     MATA(I,I)=1.0; FOR I=(5,8,29); MATA(I,I)=-1.6;
     FOR I=(6,8,30); MATA(I,I)=-1.0;
     MATA(4,3)=1.0; MATA(3,4)=-1.0; MATA(7,8)=1.0;
     MATA(8,7) = -1.0; MATA(11,12) = 1.0; MATA(12,11) -1.0;
     MATA(16,15)=1.0; MATA(15,16)=-1.0;
     FOR I = (1,1,32): MATB(I,I)-1.0:
LO3.. INPUT MATI(FOR I=(1,1,8); FOR J=(1,1,8); MATC(I,J));
     READ(; : MAT1);
```

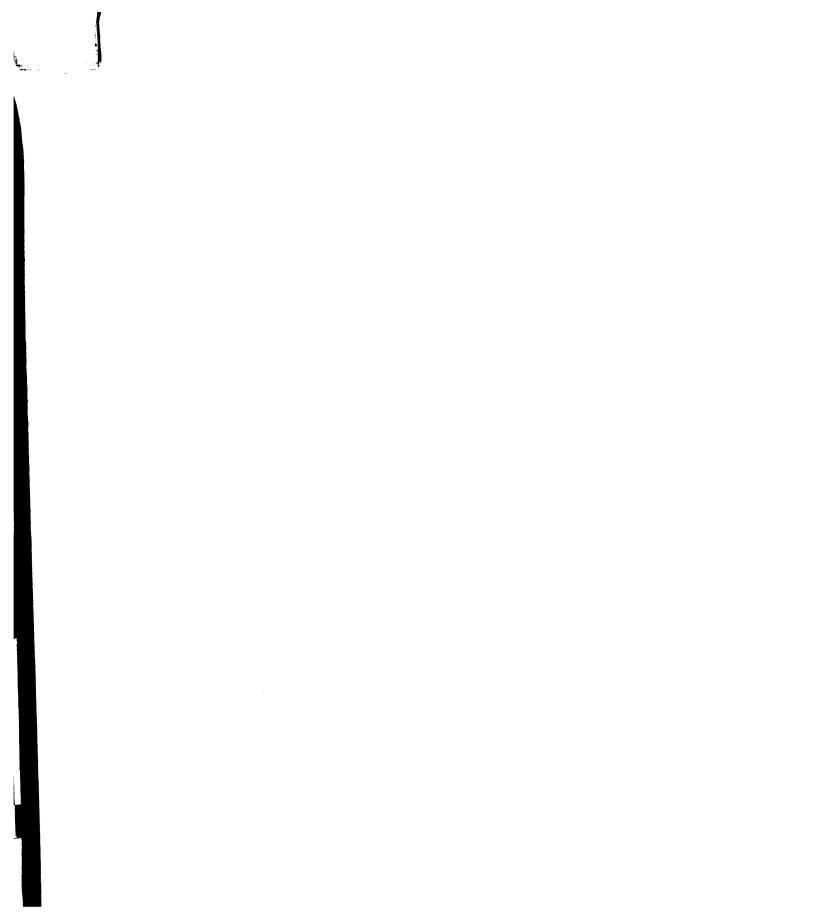
```
INPUT MAT2(FOR I=(9,1,16); FOR J=(9,1,16);
     MATC(I,J); READ(;;MAT2);
     INPUT MAT3 (FOR I=(17,1,24); FOR J=(17,1,24);
     MATC(I,J)); READ(;;MAT3);
     INPUT MAT4(FOR I=(25,1,32); FOR J=(25,1,32);
     MATC(I,J)); READ(;;MAT4);
L04.. INPUT MAT5(FOR I=(1,1,8); FOR J=(1,1,8):
     MATD(I,J); READ(;; MAT5):
     INPUT MAT6 (FOR I = (1, 1, 8); FOR J = (17, 1, 24);
     MATD(I,J)); READ(;; MAT6);
     INPUT MAT7(FOR I=(9,1,16); FOR J=(9,1,16);
     MATD(I,J); READ(;; MAT7);
     INPUT MATS(FOR I=(9,1,16); FOR J=(25,1,32);
     MATD(I,J)); READ(;:MATS);
     INPUT MAT9 (FOR I = (17, 1, 24); FOR J = (9, 1, 16);
     MATD(I,J); READ(::MAT9);
     INPUT MAT10(FOR I=(17,1,24): FOR J=(25,1,32):
     MATD(I,J); READ(::MAT10);
     INPUT MAT11(FOR I=(25,1,32); FOR J=(1,1,8);
     MATD(I,J); READ(;; MAT11);
     INPUT MAT12 (FOR I = (25, 1, 32); FOR J = (17, 1, 24);
     MATD(I,J); READ(;;MAT12);
LO5.. INPUT LEIGV(LDIG); READ(;;LEIGV);
     FORMAT FORM6 (W5);
```

```
COMMENT INITIALLY AFTER INPUT MATA=D2V, MATB=E32,
     MATC = (PHI2V)2(D2V+1), MATD = (PHI2V+1)2(SIGMA2V+1)2x4;
L06..FOR I=(1,1,32); FOR J=(1,1,32); BEGIN S=0.0;
     FOR K=(1,1,32); S=S+MATC(I,k).MATD(K,J);
     MATE(I,J)=S END:
L07.. FOR I=(1,1,32); FOR J=(1,1,32); BEGIN S=0.0;
     FOR K = (1, 1, 32); S = S + MATA(I, K) \cdot MATE(K, J);
     MATC(I,J)=S/LEIG END;
COMMENT MATC NOW IS MATRIX(M):
     FOR I = (1, 1, 32): FOR J = (1, 1, 32); MATD(I, J) = MATL(I, J)
     /LEIG:
     COMMENT MATD NOW IS MATRIX(N);
     WRITE(;;FORM6);
     WRITE(;; N, FORM2); OUTPUT N(FOR I=(1,1,32);
     FOR J = (1, 1, 32); MATD(I,J));
     FORMAT FORM2 (*5*,6F12.5,W5);
     FOR I = (1, 1, 32); FOR J = (1, 1, 32);
     MATD(I,J) = MATA(I,J) + MATC(I,J):
COMMENT MATD NOW IS D2V+M;
     WRITE(::FORM6);
     WRITE(;; D2VPM, FORM2);
     OUTPUT D2VPM (FOR I=(1,1,32); FOR J=(1,1,32);
     MATD(I,J));
LOS., FOR I=(1,1,32); FOR J=(1,1,32);
     MATD(I,J) = MATB(I,J) - MATC(I,J):
```



```
FOR I=(1,1,32); FOR J=(1,1,32); MATB(I,J)=MATD(I,J);
INVERT1 (32,MATD (,);; L01);
FOR I=(1,1,32); FOR J=(1,1,32); BEGIN S=0.0;
FOR K=(1,1,32); S=S+MATB(I,K).MATD(K,J);
MATC(I,J)=S END;
WRITE(;;FORM6);
WRITE(;;E32MMM1,FORM2);
OUTPUT E32MMM1 (FOR I=(1,1,32); FOR J=(1,1,32);
MATD(I,J)); WRITE(;;UNITIFINV,FORM3);
OUTPUT UNITIFINV (FOR I=(1,1,32); FOR J=(1,1,32);
MATC(I,J)); FORMAT FORM3 (8(X9.5),W);
L09.. GO TO L01;
```

.



COMMENT THIS PROGRAM CALCULATES H2/NL2. MATRICES M+D2V, (E32-M)-1,N, DELV, AND DELR ARE INPUT IN THAT ORDER.

R. C. THOMAS;

ARRAY MATA(32,32), MATB(32,32), MATC(32,32), MATD(32,32), DELV(32,2), DELR(2,32), SUM1(2,32), MAT1(2,2), MAT2(2,2), MAT3(2,2), MAT4(2,2), MT1(1,2), MT2(2,1), MT3(1,2):

INTEGER I,J,K,L:

- LO1.. FOR I=(1,1,32); FOR J=(1,1,32); BEGIN MATA(I,J)=0.0;

 MATB(I,J)=0.0; MATC(I,J)=0.0; MATD(I,J)=0.0 END:

 FOR I=(1,1,32); FOR J=(1,1,2); DELV(I,J)=0.0;

 FOR J=(1,1,32): FOR I=(1,1,2): BEGIN DELR(I,J)=0.0;

 SUM1(I,J)=0.0 END;
- LO2.. FOR I=(1,1,2); FOR J=(1,1,2); BEGIN MAT1(I,J)=0.0;

 MAT2(I,J)=0.0; MAT3(I,J)=0.0; MAT4(I,J)=0.0 END'

 MT1(1,1)=0.0; MT1(1,2)=1.0; MT2(1,1)=0.0;

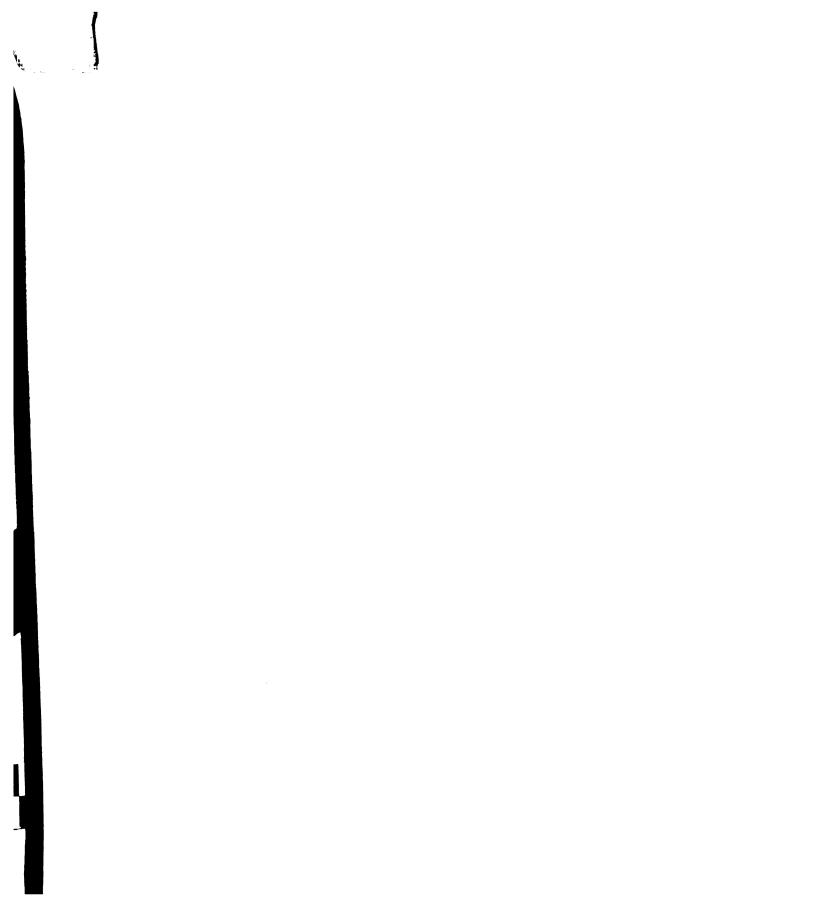
 MT2(2,1)=1.0; MT3(1,1)=0.0; MT3(1,2)=0.0;

 MAT1(1,1)=1.0; MAT1(1,2)=0.0; T1(2,1)=0.0;

 MAT1(2,2)=1.0;
- LO3.. INPUT MPD2V (FOR I=(1,1,32): FOR J=(1,1,32); MATA(I,J)); READ(''MPD2V);
- L04.. INPUT E32MMM1 (FOR I=(1,1,32); FOR J=(1,1,32):

 MATB(I,J)); READ(;;E32MMM1);
- LO5.. INPUT N (FOR I=(1,1,32); FOR J-(1,1,32);

 MATC(I,J)); READ(;;N);
- L06.. INPUT VECTOR (FOR I=(1,1,32); FOR J=(1,1,2);



```
DELV(I,J); READ(::VECTOR);
LO7.. INPUT ROW (FOR I=(1,1,2); FOR J=(1,1,32);
     DELR(I,J); READ(;;ROW):
LOS.. FOR I=(1,1,32); FOR J=(1,1,32); BEGIN S=0.0;
     FOR K = (1, 1, 32); S = S + MATB(I, K) \cdot MATA(K, J);
     MATD(I,J) = S END;
L09. FOR I=(1,1,32): FOR J=(1,1,32); MATA(I,J)=0.0;
     FOR I (1,1,32); MATA(I,J)=1.0; FOR I-(1,1,32);
     FOR J = (1, 1, 32); MATB(I, J) = MATA(I, J) + MATC(I, J);
L10.. FOR I = (1,1,32); FOR J = (1,1,32); BEGIN S=0.0;
     FOR K=(1,1,32); S=S+MATB(I,K).MATD(K,J);
     MATA(I,J)=S END;
COMMENT MATA NOW IS (E32+N), (E32-M)-1, (M+D2V);
L11.. FOR I=(1,1,2); FOR J(1,1,32); BEGIN S+0.0;
     FOR K^{\perp}(1,1,32); S=S+DELR(I,K).MATA(K,J);
    SUM1(I,J) = S END:
1.12.. FOR I = (1,1,2); FOR J = (1,1,2); BEGIN S=0.0;
     FOR K^{-}(1,1,32): S^{-}S+SUM1(1,K).DELV(K,J);
     MAT3(I,J)=S END;
1.13.. FOR I=(1,1,2); FOR J=(1,1,32); BEGIN S=0.0;
     FOR K = (1,1,32); S = S + DELR(I,K) \cdot MATC(K,J);
     SUM1(I,J)=S END;
L14.. FOR I=(1,1,2); FOR J=(1,1,2); BEGIN S=0.0;
     FOR K=(1,1,32); S=S+SUM1(I,K).DELV(K,J);
```

MAT2(I,J)=S END;

```
WRITE(;;SUM2,FORM5); OUTPUT SUM2 (FOR I=(1,1,2);
FOR J=(1,1,2); MAT2(I,J));
FORMAT FORM5(4(F13.6,B2,W0));
WRITE(;;SUM3, FORM5); OUTPUT SUM3 (FOR I=(1,1,2);
FOR J=(1,1,2); MAT3(I,J));
L15.. FOR I=(1,1,2): FOR J=(1,1,2); MAT4(I,J)=MAT1(I,J)+
MAT2(I,J)+MAT3(I,J);
L16.. I=1; FOR J=(1,1,2); BEGIN S=0.0; FOR K=(1,1,2);
S=S+MT1(I,K).MAT4(K,J); MT3(I,J)=S END;
L17.. S=0.0; S=MT3(1,1).MT2(1,1) + MT3(1,2).MT2(2,1);
L18.. WRITE(;;FINAL, FORM 4); OUTPUT FINAL (S);
FORMAT FORM4(B7,F10.4,W);
L19.. GO TO L01;
```

CHEMISTRY LIBRARY

MICHIGAN STATE UNIVERSITY LIBRARIES
3 1293 03177 3595