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**A COMPARATIVE STUDY OF
BOUNDARY ELEMENT SHAPE FUNCTIONS
FOR LINEAR ELASTOSTATICS**

By

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A THESIS

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Michigan State University
in partial fulfillment of the requirements
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ABSTRACT

A COMPARATIVE STUDY OF BOUNDARY ELEMENT SHAPE FUNCTIONS FOR LINEAR ELASTOSTATICS

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Many types of boundary elements are available in the boundary element method. With so many available, however, one needs to know what elements are best suited for different problem types.

This thesis begins to explore this issue. Three simple elements are applied to a select group of problems and compared to exact results. The first element utilizes constant displacement and constant traction approximations, the second employs linear displacements and constant tractions, and the third employs linear approximations for both displacements and tractions. It is found that an element which uses linear displacements and constant tractions yields the most consistent and accurate results.

To the loving memory of my mother, Evelyn

ACKNOWLEDGEMENTS

I wish to thank my academic advisor, Dr. Nicholas Altiero, for his inspiration and invaluable research notes. I also thank my typist, Carrie Coker, for her patience and hard work. Finally, a special thank you to my father, Richard Zwier, for his support and thoughtful guidance.

TABLE OF CONTENTS

LIST OF TABLES	iv
LIST OF FIGURES	vi
CHAPTER 1 INTRODUCTION	1
CHAPTER 2 THE BOUNDARY ELEMENT METHOD	5
CHAPTER 3 NUMERICAL TREATMENT	12
3.1 BOUNDARY APPROXIMATION	12
3.2 NUMERICAL MODELS	13
3.3 MATRIX EVALUATION	16
3.4 INTERIOR FIELD POINTS	24
CHAPTER 4 EXAMPLES AND RESULTS	27
4.1 PROBLEM DESCRIPTIONS	27
4.2 TABLES	31
4.3 DISCUSSION	31
CHAPTER 5 CONCLUSIONS	75
APPENDIX COMPUTER CODE	76
LIST OF REFERENCES	117

LIST OF TABLES

Table 1 Pure Extension - 21 Nodes X-Displacements	33
Table 2 Pure Extension - 21 Nodes Y-Displacements	33
Table 3 Pure Extension - 21 Nodes X-Tractions	34
Table 4 Pure Extension - 21 Nodes Y-Tractions	34
Table 5 Pure Extension - 21 Nodes Interior Values	35
Table 6 Pure Extension - 21 Nodes Percent Differences	36
Table 7 Pure Extension - 63 Nodes X-Displacements	38
Table 8 Pure Extension - 63 Nodes Y-Displacements	39
Table 9 Pure Extension - 63 Nodes X-Tractions	40
Table 10 Pure Extension - 63 Nodes Y-Tractions	42
Table 11 Pure Extension - 63 Nodes Interior Values	43
Table 12 Pure Extension - 63 Nodes Percent Differences	44
Table 13 Square - 21 Nodes X-Displacements	47
Table 14 Square - 21 Nodes Y-Displacements	48
Table 15 Square - 21 Nodes X-Tractions	48
Table 16 Square - 21 Nodes Y-Tractions	49
Table 17 Square - 21 Nodes Interior Values	49
Table 18 Square - 21 Nodes Percent Difference	50
Table 19 Square - 63 Nodes X-Displacements	52
Table 20 Square - 63 Nodes Y-Displacements	54
Table 21 Square - 63 Nodes X-Tractions	55
Table 22 Square - 63 Nodes Y-Tractions	56

Table 23 Square - 63 Nodes Interior Values	58
Table 24 Square - 63 Nodes Percent Differences	58
Table 25 Disk - 19 Nodes X-Displacements	62
Table 26 Disk - 19 Nodes Y-Displacements	62
Table 27 Disk - 19 Nodes X-Tractions	63
Table 28 Disk - 19 Nodes Y-Tractions	63
Table 29 Disk - 19 Nodes Interior Values	64
Table 30 Disk - 19 Nodes Percent Differences	65
Table 31 Disk - 35 Nodes X-Displacements	67
Table 32 Disk - 35 Nodes Y-Displacements	68
Table 33 Disk - 35 Nodes X-Tractions	69
Table 34 Disk - 35 Nodes Y-Tractions	70
Table 35 Disk - 35 Nodes Interior Values	70
Table 36 Disk - 35 Nodes Percent Differences	72

LIST OF FIGURES

Figure 1 Planar Region	5
Figure 2 Integration Around Singular Point	10
Figure 3 Boundary Approximation	12
Figure 4 Local Coordinates	13
Figure 5 Free Term Coefficient	18
Figure 6 Local Coordinates On element $m = n$	19
Figure 7 Local Coordinates On element $m = n + 1$	20
Figure 8 Problem One - Pure Extension	28
Figure 9 Problem Two - Square With Variable Boundary Conditions	29
Figure 10 Problem Three - Circular Disk Under Uniform Pressure	30

CHAPTER 1

INTRODUCTION

Engineers and scientists routinely develop mathematical models to describe the systems they wish to study. These models, however, typically involve differential equations and boundary conditions which are not easily solved. Therefore, in order to obtain a solution, some form of approximate method is employed.

Many such methods exist today. However, the three most powerful are finite differences, finite elements and boundary elements. Although this thesis deals with boundary elements, all three will be discussed briefly because, when viewed historically, they show a trend which, in part, prompted this work.

Before examining the individual methods, it should be pointed out that they possess common characteristics. First, they each require the region of interest to be discretized using a set of points called nodes. Second, through differing mathematical approaches, each method reduces the system of differential equations to a system of algebraic equations, which, when solved, give values for the physical variables at the nodes.

Of the three subject methods, finite differences evolved first (1). It is probably the most natural way to approximate a set of differential equations because it utilizes the basic definition of the derivative. Applying this definition and a finite nodal spacing to the derivatives in the governing equations results in a system of algebraic difference equations.

In theory, finite differences may be applied to any differential equation. In practice, however, it is somewhat limited. This is due to the fact that certain boundary conditions can be cumbersome to incorporate and it is difficult to work with curved or irregular boundaries. Also, since the solution accuracy is primarily dependent on nodal spacing, many equations are necessary to achieve good results. On the other hand, the method works well on problems involving first and second derivatives such as heat transfer, fluid mechanics and two dimensional problems with straight boundaries (2,3).

The finite element method is by far the most popular method in use today. It is, in a sense, a progression from finite differences in that it approximates the physical domain itself with small regions, or elements, which simulate the behavior of the portion of the domain they represent. The differential equations are then applied to each element in turn and rewritten in terms of variational, weighted residual, or virtual work expressions (2).

Finite elements have an advantage over finite differences in that irregular regions pose no significant problems. The method allows for a great deal of flexibility in terms of element types and shapes and, therefore, may be applied to many types of problems and regions. This kind of flexibility is partly responsible for the method's popularity and has prompted the development of many types of elements (2). Another reason for its popularity lies in the fact that it has its roots in the study of differential equations which was well established in the nineteenth century (1) and, therefore, the underlying mathematics are generally understood today by practicing engineers and scientists.

The boundary element method is, in a sense, a progression from the finite element method because it attempts to integrate the differential equations before it discretizes the region. The result is a system of integral equations which involves only the boundary values of the system. Thus, only the region boundary needs to be discretized and the problem dimensionality is reduced by one.

It should be noted that the boundary element method is similar to the finite element method in that they both can be considered weighted residual methods (4,14). However, the boundary element method does have the advantage of only requiring boundary discretization and thus fewer nodes.

In addition, numerical integration is more accurate than numerical differentiation and there is little or no numerical differentiation in the boundary element method (1). Perhaps the biggest disadvantage for the method is that the study of integral equations is more recent and mathematically more difficult than the study of differential equations. This has, until recently, hampered its development.

Integral equations have been studied rigorously since the turn of the century (1,5). However, the contributions which have developed into the boundary element method have come as recently as the 1950's and 1960's (5,15). The nature of the mathematics involved in these works prevented them from being recognized by the majority of engineers and applied scientists. However, they were recognized by some, and in the late 1960's and early 1970's, papers began to be published which applied Integral equations to the solution of engineering problems (6,7,8,9,13).

Throughout the 1970's, the number of papers increased and the term "boundary elements" emerged from works by Brebbia and others within the department of civil engineering at the University of Southampton (10). By the end of the 1970's, it became evident that the boundary element method was becoming a legitimate analysis tool and international conferences on the topic were established (11). These conferences are designed to solicit work in the field and promote the method. To that end, they have been successful as evidenced by the increasing number and diversity of the papers presented at each conference (11). Now in the late 1980's, efforts such as the BETECH conferences (12) have begun which are designed to increase the popularity of the method and bridge the gap between industry and academia.

Efforts such as these are increasing the popularity of the method and already, several commercial software packages are available (13). This is not to say that boundary elements are replacing finite elements. It does appear, however, that they will reach equal levels of development and coexist as complementary methods. In fact, since most problems solved by finite elements may also be solved by boundary elements (1), such a coexistence is desirable to make use of the relative merits of both methods and advance the quality of solutions.

Similarly, within each method it is desirable to use different element types in a complementary manner depending on the problem characteristics. By knowing when to apply certain element types, more efficient and accurate solutions may be obtained. This does not mean that each problem should have its own type of element. It does, however, suggest that efforts

should be made to study the applicability of basic element types and indeed such works have begun to appear in the literature (17).

The purpose of this thesis then is to examine three types of boundary elements in the direct boundary element method for linear isotropic elasticity. Each element type will be applied to a range of problem types and assessed in terms of accuracy and quality of solution. It is hoped that this work will help establish guidelines for element applicability and show the usefulness of simpler, extrapolated models.

CHAPTER 2

THE BOUNDARY ELEMENT METHOD

There are three natural formulations for the boundary element method. The indirect formulation expresses the integral equations in terms of a unit singular solution of the original differential equations. This solution is distributed over the boundary by way of density functions. The density functions have no physical significance and once they are obtained from the numerical solution of the integral equations, the values of the physical variables may be found by simple integration at any point within the region.

The semi-direct formulation utilizes unknown functions, analogues to airy stress functions, as unknowns in the integral equations. Once these functions are found, the physical variables may be obtained by differentiation at any point within the region. This is the only numerical differentiation required in the boundary element method. As pointed out in Chapter 1, numerical differentiation is less accurate than numerical integration and, therefore, the semi-direct formulation is less useful than the other two formulations.

The direct formulation expresses the integral equations in terms of the actual physical variables. Numerical solution of the integral equations gives the boundary values of the physical variables. Interior values are subsequently found by simple numerical integration. This thesis deals specifically with the direct formulation because it is well suited to problems of plane isotropic elasticity. We will now proceed to develop the basic integral equations and in Chapter 3, we will develop the numerical solution schemes for these equations.

Consider the following planar region:

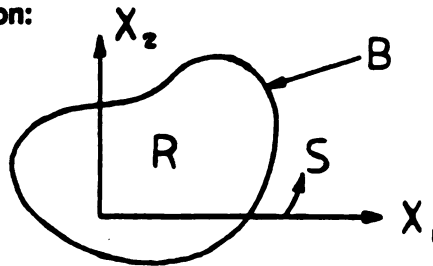


Figure 1. Planar Region

At any point $\underline{x}$ in R , we can write the equilibrium equations as

$$\begin{aligned}\sigma_{11,1} + \sigma_{12,2} + X_1 &= 0 \\ \sigma_{12,1} + \sigma_{22,2} + X_2 &= 0\end{aligned}\quad [1]$$

where $\underline{\sigma}$ is the stress tensor and $\underline{X}$ is the body force vector. Also, the notation $\sigma_{ij,j}$ indicates differentiation of σ_{ij} with respect to coordinate direction j .

Hooke's law for plane stress is given by:

$$\begin{aligned}\sigma_{11} &= 2G(u_{1,1} + \nu u_{2,2}) / (1 - \nu) \\ \sigma_{22} &= 2G(u_{2,2} + \nu u_{1,1}) / (1 - \nu) \\ \sigma_{12} &= G(u_{1,2} + u_{2,1})\end{aligned}\quad [2]$$

where $\underline{u}$ is the displacement vector, G is the shear modulus and ν is Poisson's ratio.

Substitution of eqs. [2] into eqs. [1] results in Navier's equations.

$$\begin{aligned}(u_{1,11} + u_{2,21})(1 + \nu) / (1 - \nu) + \nabla^2 u_1 + X_1 / G &= 0 \\ (u_{1,12} + u_{2,22})(1 + \nu) / (1 - \nu) + \nabla^2 u_2 + X_2 / G &= 0\end{aligned}\quad [3]$$

Shifting attention now from the region to the boundary B , we have the traction vector $\underline{t}$ given by:

$$\begin{aligned}t_1 &= \sigma_{11}n_1 + \sigma_{12}n_2 \\ t_2 &= \sigma_{12}n_1 + \sigma_{22}n_2\end{aligned}\quad [4]$$

for any surface defined by unit normal $\underline{n}$. Inserting eq. [2] into eq. [4] gives:

$$\begin{aligned}t_1 &= G[u_{1,n} + u_{1,1}n_1 + u_{2,1}n_2 + 2\nu(u_{1,1} + u_{2,2})n_1 / (1 - \nu)] \\ t_2 &= G[u_{2,n} + u_{1,2}n_1 + u_{2,2}n_2 + 2\nu(u_{1,1} + u_{2,2})n_2 / (1 - \nu)]\end{aligned}\quad [5]$$

Making use of the coordinate s , measured along B , we specify the boundary conditions as

$$u_i = g_i(s) \text{ or } t_i / G = h_i(s) \quad [6]$$

for $i = 1, 2$.

We now have the basic formulation of the elasticity problem with field equations, eq. [3], and boundary conditions, eq. [6]. However, we desire eq. [3] in a more convenient form. To accomplish this, we define a vector function $\underline{\phi}$, such that:

$$\begin{aligned} u_1 &= \nabla^2 \phi_1 - (1 + \nu) (\phi_{1,11} + \phi_{2,12}) / 2 \\ u_2 &= \nabla^2 \phi_2 - (1 + \nu) (\phi_{1,21} + \phi_{2,22}) / 2 \end{aligned} \quad [7]$$

and substitute into eq. [3] to yield the inhomogeneous biharmonic equation

$$\nabla^2 (\nabla^2 \phi_i) = X_i / G \quad [8]$$

for $i = 1, 2$.

The biharmonic operator is well understood and is known to possess a principal solution which satisfies

$$\nabla^2 (\nabla^2 \phi_i) = - \delta(\mathbf{x} - \xi) \mathbf{e}_i / G \quad [9]$$

for $i = 1, 2$. Here $\mathbf{e}_i$ is a unit vector and $\delta(\mathbf{x} - \xi)$ is a Dirac delta function which represents a point singularity at the source point ξ . For equations such as eq. [9], the solution is a function only of the distance between the source point ξ and the field point $\mathbf{x}$. This distance is given by:

$$\rho = [(x_1 - \xi_1)^2 + (x_2 - \xi_2)^2]^{0.5}.$$

The solution to eq. [9] is then:

$$\phi_i = - \rho^2 \ln(\rho) \mathbf{e}_i / 8\pi G. \quad [10]$$

Substitution of eq. [10] for ϕ_i in eq. [7] gives the displacement field for the principal solution as:

$$\begin{aligned} U_1 &= \{[-(3 - \nu) \ln \rho + (1 + \nu) q_1^2] \mathbf{e}_1 + (1 + \nu) q_1 q_2 \mathbf{e}_2\} / 8\pi G \\ U_2 &= \{[-(3 - \nu) \ln \rho + (1 + \nu) q_2^2] \mathbf{e}_2 + (1 + \nu) q_1 q_2 \mathbf{e}_1\} / 8\pi G \end{aligned} \quad [11]$$

Here we have defined q_1 and q_2 as:

$$q_1 = (x_1 - \xi_1) / \rho \quad \text{and} \quad q_2 = (x_2 - \xi_2) / \rho$$

Similarly, substitution of eq. [11] for u_i into eq. [5] gives the traction field for the principal solution

$$\begin{aligned} T_1 &= \{[2(1 + \nu)(-n_1 q_1^3 + n_2 q_2^3) - (1 - \nu)n_1 q_1 - (3 - \nu)n_2 q_2] \mathbf{e}_1 \\ &\quad + [2(1 + \nu)(n_2 q_1^3 + n_1 q_2^3) - (3 + \nu)n_2 q_1 - (1 + 3\nu)n_1 q_2] \mathbf{e}_2\} / 4\pi\rho \\ T_2 &= \{[2(1 + \nu)(n_2 q_1^3 + n_1 q_2^3) - (1 + 3\nu)n_2 q_1 - (3 + \nu)n_1 q_2] \mathbf{e}_1 \\ &\quad + [2(1 + \nu)(n_1 q_1^3 - n_2 q_2^3) - 3 + \nu)n_1 q_1 - (1 - \nu)n_2 q_2] \mathbf{e}_2\} / 4\pi\rho. \end{aligned} \quad [12]$$

If we now define the displacement and traction vectors for the principal solution to be:

$$\begin{aligned} U_i(\mathbf{x}) &= U_{i1}(\mathbf{x}, \xi) \mathbf{e}_1(\xi) + U_{i2}(\mathbf{x}, \xi) \mathbf{e}_2(\xi) \\ T_i(\mathbf{x}) &= T_{i1}(\mathbf{x}, \xi) \mathbf{e}_1(\xi) + T_{i2}(\mathbf{x}, \xi) \mathbf{e}_2(\xi), \end{aligned} \quad [13]$$

then we can write

$$\begin{aligned} U_{11} &= [- (3 - \nu) \ln \rho + (1 + \nu) q_1^2] / 8\pi G \\ U_{12} &= (1 + \nu) q_1 q_2 / 8\pi G \\ U_{21} &= (1 + \nu) q_1 q_2 / 8\pi G \\ U_{22} &= [- (3 - \nu) \ln \rho + (1 + \nu) q_2^2] / 8\pi G \end{aligned} \quad [14]$$

and

$$\begin{aligned} T_{11} &= [2(1 + \nu) (-n_1 q_1^3 + n_2 q_2^3) - (1 - \nu) n_1 q_1 - (3 + \nu) n_2 q_2] / 4\pi\rho \\ T_{12} &= [2(1 + \nu) (n_2 q_1^3 + n_1 q_2^3) - (3 + \nu) n_2 q_1 - (1 + 3\nu) n_1 q_2] / 4\pi\rho \\ T_{21} &= [2(1 + \nu) (n_2 q_1^3 + n_1 q_2^3) - (1 + 3\nu) n_2 q_1 - (3 + \nu) n_1 q_2] / 4\pi\rho \\ T_{22} &= [2(1 + \nu) (n_1 q_1^3 - n_2 q_2^3) - (3 + \nu) n_1 q_1 - (1 - \nu) n_2 q_2] / 4\pi\rho. \end{aligned} \quad [15]$$

The quantities given by eq. [14] and eq. [15] represent the effects caused at the field point $\mathbf{x}$ by a unit force at the point ξ in the infinite plane. Thus U_{i1} , $i = 1, 2$, are the displacements and tractions respectively at a point $\mathbf{x}$ due to a unit force in the x_1 - direction applied at ξ . Similarly, U_{i2} and T_{i2} are generated at $\mathbf{x}$ by a unit force in the x_2 - direction at ξ .

We now recall Betti's reciprocal work theorem which states that, if two elastic equilibrium states (X_i, t_i, u_i) and (X_i^*, t_i^*, u_i^*) exist in a region R bounded by B , then the work done by the forces of the first system on the displacements of the second is equal to the work done by the forces of the second on the displacements of the first. Thus, we write:

$$\begin{aligned} &\int_B t_i^*(\mathbf{x}) u_i(\mathbf{x}) ds(\mathbf{x}) + \int_R X_i^*(\mathbf{x}) u_i(\mathbf{x}) da(\mathbf{x}) \\ &= \int_B t_i(\mathbf{x}) u_i^*(\mathbf{x}) ds(\mathbf{x}) + \int_R X_i(\mathbf{x}) u_i^*(\mathbf{x}) da(\mathbf{x}) \end{aligned} \quad [16]$$

for $i = 1, 2$ and where we have employed Einstein's summation convention, i.e. we infer summation over repeated indices.

Now, if we choose the principal solution to be one of the two elastic states, then

$$u_i^* = U_i = U_{ij}(\mathbf{x}, \xi) e_j(\xi)$$

$$t_i^* = T_i = T_{ij}(\mathbf{x}, \xi) e_j(\xi)$$

$$X_i^* = \delta(\mathbf{x} - \xi) e_i(\xi).$$

Substituting these into eq. [16] gives

$$\begin{aligned} & e_j(\xi) \int_B T_{ij}(\mathbf{x}, \xi) u_i(\mathbf{x}) ds(\mathbf{x}) + e_i(\xi) \int_R \delta(\mathbf{x} - \xi) u_i(\mathbf{x}) da(\mathbf{x}) \\ &= e_j(\xi) \left[\int_B U_{ij}(\mathbf{x}, \xi) t_i(\mathbf{x}) ds(\mathbf{x}) + \int_R U_{ij}(\mathbf{x}, \xi) X_i(\mathbf{x}) da(\mathbf{x}) \right]. \end{aligned} \quad [17]$$

We can write

$$e_i(\xi) \int_R \delta(\mathbf{x} - \xi) u_i(\mathbf{x}) da(\mathbf{x}) = e_i(\xi) u_i(\xi) = e_j(\xi) u_j(\xi)$$

provided ξ is in R . Then, equating coefficients of e_j , we obtain

$$\begin{aligned} u_j(\xi) &= - \int_B u_i(\mathbf{x}) T_{ij}(\mathbf{x}, \xi) ds(\mathbf{x}) + \int_B t_i(\mathbf{x}) U_{ij}(\mathbf{x}, \xi) ds(\mathbf{x}) \\ &+ \int_R X_i(\mathbf{x}) U_{ij}(\mathbf{x}, \xi) da(\mathbf{x}). \end{aligned} \quad [18]$$

For convenience, at this point, we recognize that

$$U_{ij}(\xi, \mathbf{x}) = U_{ij}(\mathbf{x}, \xi) = U_{ji}(\mathbf{x}, \xi)$$

$$T_{ij}(\xi, \mathbf{x}) = -T_{ij}(\mathbf{x}, \xi)$$

in eq. [14] and eq. [15] provided that we let $\underline{n} = \underline{n}(\xi)$ in eq. [15]. This allows us to interchange $\mathbf{x}$ and ξ and rewrite eq. [18] as

$$\begin{aligned} u_i(\mathbf{x}) &= \int_B u_j(\xi) T_{ji}(\mathbf{x}, \xi) ds(\xi) + \int_B t_j(\xi) U_{ij}(\mathbf{x}, \xi) ds(\xi) \\ &+ \int_R X_j(\xi) U_{ij}(\mathbf{x}, \xi) da(\xi) \end{aligned} \quad [19]$$

for $\mathbf{x}$ in R and $i = 1, 2$.

Equation [19] also applies for $\mathbf{x}$ on B . However, when $\mathbf{x}$ is on B and ξ approaches $\mathbf{x}$, the integrands in the boundary integrals become singular. Specifically, $T_{ji}(\mathbf{x}, \xi)$ varies as $1/\rho$ and $U_{ij}(\mathbf{x}, \xi)$ varies as $\ln \rho$. Since $1/\rho$ is not integrable, we need to integrate around $\mathbf{x}$ as follows:

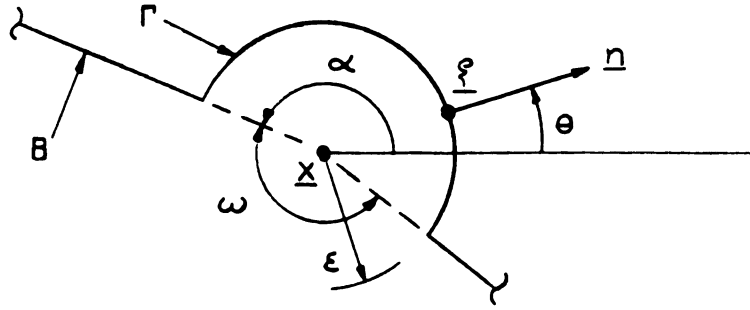


Figure 2. Integration Around Singular Point

and take the limit as ϵ goes to 0. Notice that if the boundary has no corner, $\omega = \pi$

Now on Γ we have

$$\begin{aligned} q_1 &= -\cos\theta & q_2 &= -\sin\theta \\ n_1 &= \cos\theta & n_2 &= \sin\theta \\ \rho &= \epsilon & ds &= \epsilon d\theta. \end{aligned}$$

If we think of the boundary as being in two parts, i.e., B and $B-\Gamma$, then the $1/\rho$ type integral becomes

$$\int_B u_j T_{ji} ds = \lim_{\epsilon \rightarrow 0} \left[\int_{B-\Gamma} u_j T_{ji} ds + \int_{\Gamma} u_j T_{ji} ds \right].$$

In the limit as ϵ goes to 0, the $B-\Gamma$ integral becomes a cauchy principal value integral, and we

$$\text{have} \quad \int_B u_j T_{ji} ds = \text{p.v.} \int_B u_j T_{ji} ds + \lim_{\epsilon \rightarrow 0} \int_{\Gamma} u_j T_{ji} ds.$$

If we define the coefficient β_{ji} such that

$$\lim_{\epsilon \rightarrow 0} \int_{\Gamma} u_j T_{ji} ds = \beta_{ji} u_j$$

and let $\alpha_{ji} = \delta_{ji} - \beta_{ji}$ at x on B , we obtain

$$\alpha_{ji} u_j - \text{p.v.} \int_B u_j T_{ji} ds = \int_B t_j U_{ij} ds + \int_R X_i U_{ij} da. \quad [20]$$

Taking $X = 0$ for convenience, we have

$$\alpha_{ji} u_j - \text{p.v.} \int_B u_j T_{ji} ds = \int_B t_j U_{ij} ds \quad [21]$$

where U_{ij} and T_{ji} are given by eq. [14] and eq. [15], respectively.

Equation [21] is the desired boundary integral equation. After solving it numerically, we will have the displacement and traction values everywhere on B. Then, to find the displacements at any point within R, we simply integrate, i.e.

$$u_i = \int_B u_j T_{ji} ds + \int_B t_j U_{ij} ds \quad [22]$$

Next, employing eq. [2], we have the stresses at any point within R given by

$$\sigma_{ik} = \int_B u_j S_{jki} ds + \int_B t_j D_{ikj} ds \quad [23]$$

where S_{jki} and D_{ikj} are given by

$$\begin{aligned} S_{111} &= G(1 + \nu)[(8q_1^4 - 4q_1^2 - 1) n_1 + 2q_1q_2 (4q_1^2 - 1) n_2] / 2\pi\rho^2 \\ S_{211} &= G(1 + \nu)[2q_1q_2(4q_1^2 - 1) n_1 + (8q_1^2q_2^2 - 1) n_2] / 2\pi\rho^2 \\ S_{122} &= G(1 + \nu)[(8q_1^2q_2^2 - 1) n_1 + 2q_1q_2 (4q_2^2 - 1) n_2] / 2\pi\rho^2 \\ S_{222} &= G(1 + \nu)[2q_1q_2 (4q_2^2 - 1) n_1 + (8q_2^4 - 4q_2^2 - 1) n_2] / 2\pi\rho^2 \\ S_{121} &= G(1 + \nu)[2q_1q_2 (4q_1^2 - 1) n_1 + (8q_1^2q_2^2 - 1) n_2] / 2\pi\rho^2 \\ S_{221} &= G(1 + \nu)[(8q_1^2q_2^2 - 1) n_1 + 2q_1q_2 (4q_2^2 - 1) n_2] / 2\pi\rho^2 \\ D_{111} &= [-2(1 + \nu) q_1^3 - (1 - \nu) q_1] / 4\pi\rho \\ D_{121} &= [2(1 + \nu) q_2^3 - (3 + \nu) q_2] / 4\pi\rho \\ D_{221} &= [2(1 + \nu) q_1^3 - (1 + 3\nu) q_1] / 4\pi\rho \\ D_{112} &= [2(1 + \nu) q_2^3 - (1 + 3\nu) q_2] / 4\pi\rho \\ D_{122} &= [2(1 + \nu) q_1^3 - (3 + \nu) q_1] / 4\pi\rho \\ D_{222} &= [-2(1 + \nu) q_2^3 - (1 - \nu) q_2] / 4\pi\rho \end{aligned} \quad [24]$$

[25]

CHAPTER 3

NUMERICAL TREATMENT

3.1 BOUNDARY APPROXIMATION

To numerically solve the boundary integral equation, eq [21], we will first approximate the boundary B with N straight line segments as shown below.

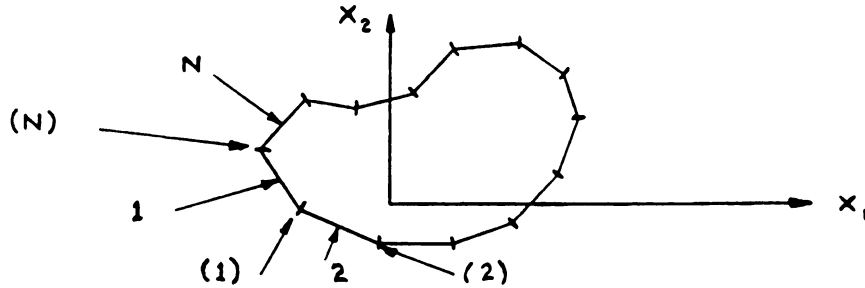


Figure 3. Boundary Approximation

Now for any boundary source point, m , and boundary field point , n , we define the following

$\underline{x}^n$ = Element Field Point

$\underline{x}^{(n)}$ = Nodal Field Point

$\underline{x}^m$ = Element Source Point

$\underline{x}^{(m)}$ = Nodal Source Point

Δs^m = Length of Element m

$$= [(x_1^{(m)} - x_1^{(m-1)})^2 + (x_2^{(m)} - x_2^{(m-1)})^2]^{0.5}$$

$\underline{n}^m$ = Unit Normal to Element m

$$n_1 = (x_2^{(m)} - x_2^{(m-1)}) / \Delta s^m$$

$$n_2 = (x_1^{(m-1)} - x_1^{(m)}) / \Delta s^m$$

ρ = Distance Between Source Point and Field Point

$$q_1 = (x_1^{(n)} - x_1^{(m)}) / \rho \quad \text{or} \quad (x_1^n - x_1^m) / \rho$$

$$q_2 = (x_2^{(n)} - x_2^{(m)}) / \rho \quad \text{or} \quad (x_2^n - x_2^m) / \rho$$

Here the "element points" are at the midpoints of boundary segments and element quantities take their midpoint values.

Now consider a typical straight segment; m ,

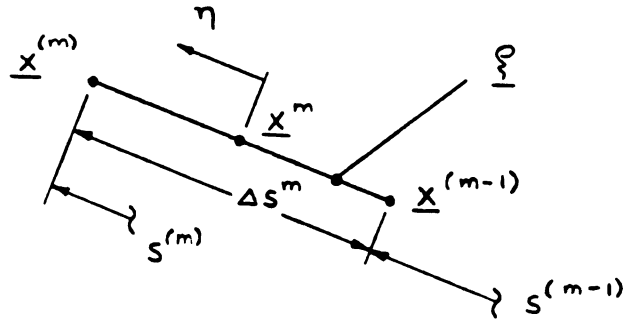


Figure 4. Local Coordinate

with local coordinate, η , where

$$-1 \leq \eta \leq 1$$

$$ds = 0.5 \Delta s^m d\eta \quad [26]$$

$$\xi = 0.5 x^{(m-1)} (1 - \eta) + 0.5 x^{(m)} (1 + \eta).$$

We can now rewrite the boundary integral equation

$$\alpha_{ji} u_j - \oint_B u_j T_{ji} ds = \oint_B t_j u_{ij} ds. \quad [21]$$

at a given boundary point, x , as

$$\begin{aligned} \alpha_{ji}(x) u_j(x) - 0.5 \sum_{m=1}^N [\Delta s^m \int_{-1}^1 u_j(\eta) T_{ji}(x, \eta) d\eta] \\ = 0.5 \sum_{m=1}^N [\Delta s^m \int_{-1}^1 t_j(\eta) U_{ij}(x, \eta) d\eta] \end{aligned} \quad [27]$$

3.2 NUMERICAL MODELS

Next, consider three cases on segment m

$$(a) u_j = u_j^m$$

$$t_j = t_j^m$$

$$(b) \quad u_j = 0.5 u_j^{(m-1)} (1 - \eta) + 0.5 u_j^{(m)} (1 + \eta)$$

$$t_j = t_j^m$$

$$(c) \quad u_j = 0.5 u_j^{(m-1)} (1 - \eta) + 0.5 u_j^{(m)} (1 + \eta)$$

$$t_j = 0.5 t_j^{(m-1)} (1 - \eta) + 0.5 t_j^{(m)} (1 + \eta)$$

Notice the differences among the cases. Case (a) is the simplest because it assumes both the displacements and tractions to be constant over segment m . Case (b) is slightly more complex in that the displacements are allowed to vary linearly. Case (c) takes the next logical progression and allows the tractions to vary linearly also. Clearly, further progressions are possible such as quadratic and cubic variations, however, for our purposes, these three are sufficient. Also, keep in mind that the constant quantities refer to values at the midpoint of segment m .

We now rewrite eq. [27] for the field point in each of the three cases.

(a) Let $\mathbf{x} = \mathbf{x}^n$

$$\begin{aligned} & \sum_{\substack{m=1 \\ m \neq n}}^N \Delta s^m \int T_{ji}(\mathbf{x}^n, \eta) d\eta \, u_j^m \\ &= 0.5 \sum_{m=1}^n \left[\Delta s^m \int U_{ij}(\mathbf{x}^n, \eta) d\eta \right] t_j^m \end{aligned} \quad [28]$$

(b) Let $\mathbf{x} = \mathbf{x}^{(n)}$

$$\begin{aligned} & \sum_{\substack{m=1 \\ m \neq n+1}}^N \Delta s^m \int (1 - \eta) T_{ji}(\mathbf{x}^{(n)}, \eta) d\eta \, u_j^{(m-1)} \\ & - 0.25 \sum_{\substack{m=1 \\ m \neq n}}^N \left[\Delta s^m \int (1 + \eta) T_{ji}(\mathbf{x}^{(n)}, \eta) d\eta \right] u_j^{(m)} \\ &= 0.5 \sum_{m=1}^N \left[\Delta s^m \int U_{ij}(\mathbf{x}^{(n)}, \eta) d\eta \right] t_j^m \end{aligned} \quad [29]$$

(c) Let $x = x^{(n)}$

$$\begin{aligned}
 \hat{\alpha}_{ji}^{(n)} u_j^{(n)} - 0.25 \sum_{\substack{m=1 \\ m \neq n+1}}^N [\Delta s^m \int_m (1 - \eta) T_{ji}(x^{(n)}, \eta) d\eta] u_j^{(m-1)} \\
 - 0.25 \sum_{\substack{m=1 \\ m \neq n}}^N [\Delta s^m \int_m (1 + \eta) T_{ji}(x^{(n)}, \eta) d\eta] u_j^{(m)} \quad [30] \\
 = 0.25 \sum_{m=1}^N [\Delta s^m \int_m (1 - \eta) U_{ij}(x^{(n)}, \eta) d\eta] t_j^{(m-1)} \\
 + 0.25 \sum_{m=1}^N [\Delta s^m \int_m (1 + \eta) U_{ij}(x^{(n)}, \eta) d\eta] t_j^{(m)}
 \end{aligned}$$

Notice that any integrals multiplying u_j^n or $u_j^{(n)}$ were incorporated into the coefficients α_{ji}^n or $\alpha_{ji}^{(n)}$ in eqs. [28], [29] and [30]. Also notice that the displacements and tractions are now either nodal or midpoint values and are, therefore, taken outside the integrals. This allows us to express the equations in matrix form as

$$\begin{aligned}
 \text{Case (a): } [A_a] \{u\}_e &= [B_a] \{t\}_e \\
 \text{Case (b): } [A_b] \{u\}_n &= [B_b] \{t\}_e \quad [31] \\
 \text{Case (c): } [A_c] \{u\}_n &= [B_c] \{t\}_n
 \end{aligned}$$

Essentially, we now have our numerical models. A more convenient form, however, would be to have

$$[F] \{x\} = \{b\}$$

for each case where $[F]$ and $\{b\}$ are known. We can obtain this desired form by recognizing that $\{u\}$ and $\{t\}$ are not known everywhere on the boundary and simply rearrange the equations to have all unknown quantities on the left and known quantities on the right.

For convenience, we will make one further adjustment to the models. Since we will be comparing results for each case on a number of example problems, we desire the input data to be consistent. As it stands, our models use both element and nodal quantities. We may change this if we let

$$\{u\}_e = [\Gamma]^T \{u\}_n$$

$$\{t\}_e = [\Gamma]^T \{t\}_n$$

so that

$$[A_a] \{u\}_e = [B_a] \{t\}_e$$

$$[A_b] [\Gamma]^T \{u\}_e = [B_b] \{t\}_e \quad [32]$$

$$[A_c] [\Gamma]^T \{u\}_e = [B_c] [\Gamma]^T \{t\}_e$$

where the number of nodes is odd and

$$[\Gamma]^T = \begin{bmatrix} I & I & -I & I & \cdot & \cdot & \cdot & -I \\ -I & I & I & -I & \cdot & \cdot & \cdot & I \\ I & -I & I & I & \cdot & \cdot & \cdot & -I \\ -I & I & I & I & \cdot & \cdot & \cdot & I \\ \cdot & \cdot & \cdot & \cdot & & & & \cdot \\ \cdot & \cdot & \cdot & \cdot & & & & \cdot \\ \cdot & \cdot & \cdot & \cdot & & & & \cdot \\ I & -I & I & -I & \cdot & \cdot & \cdot & I \end{bmatrix} \quad [\Gamma]^T = \begin{bmatrix} I & 0 & 0 & 0 & \cdot & I \\ I & I & 0 & 0 & \cdot & 0 \\ 0 & I & I & 0 & \cdot & 0 \\ 0 & 0 & I & I & \cdot & 0 \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ 0 & 0 & 0 & 0 & \cdot & I \end{bmatrix} \quad [33]$$

3.3 MATRIX EVALUATION

The coefficients in matrices [A] and [B] for each case may be calculated using simple Gauss quadrature. This is a well-known technique and will not be discussed here, however, details of the procedure may be found in (1).

To apply Gauss quadrature, we must have T_{ji} and U_{ij} in proper form. This requires ρ , q_1 , q_2 , n_1 and n_2 in terms of η . Employing eq. [26], we have

$$\begin{aligned} x^{(n)} - \xi &= [x^{(n)} - x^m] - [x^{(m)} - x^m] \eta \\ &= \delta^{(nm)} - \delta^{mm} \eta \end{aligned}$$

and

$$\begin{aligned} x^n - \delta &= [x^n - x^m] - [x^{(m)} - x^m] \eta \\ &= \delta^{nm} - \delta^{mm} \eta \end{aligned}$$

where we have defined

$$\begin{aligned} \delta^{(nm)} &= x^{(n)} - x^m \\ \delta^{nm} &= x^n - x^m \end{aligned} \quad [34]$$

Then for case (a)

$$\begin{aligned}
 \rho^2 &= [\delta^{nm} \cdot \delta^{nm}] - 2 [\delta^{nm} \cdot \delta^{mm}] \eta + [\delta^{mm} \cdot \delta^{mm}] \eta^2 \\
 q_1 &= (\delta_1^{nm} - \delta_1^{mm} \eta) / \rho \\
 q_2 &= (\delta_2^{nm} - \delta_2^{mm} \eta) / \rho \\
 n_1 &= 2 \delta_2^{mm} / \Delta s^m \\
 n_2 &= -2 \delta_1^{mm} / \Delta s^m
 \end{aligned} \tag{35}$$

and for cases (b) and (c)

$$\begin{aligned}
 \rho^2 &= [\delta^{(nm)} \cdot \delta^{(nm)}] - 2 [\delta^{(nm)} \cdot \delta^{mm}] \eta + [\delta^{mm} \cdot \delta^{mm}] \eta^2 \\
 q_1 &= (\delta_1^{(nm)} - \delta_1^{mm} \eta) / \rho \\
 q_2 &= (\delta_2^{(nm)} - \delta_2^{mm} \eta) / \rho \\
 n_1 &= 2 \delta_2^{mm} / \Delta s^m \\
 n_2 &= -2 \delta_1^{mm} / \Delta s^m
 \end{aligned} \tag{36}$$

Equations [28], [29], [30], [35] and [36], together with the matrix forms given in [31] and [32], provide the basic numerical models for each of the three cases. However, further discussion is required because the integrals become singular when the source point and field point coincide. The coefficients given by the singular integrals will be referred to as "special" coefficients and are:

$$\begin{aligned}
 \text{case (a): } \Delta s^m \left(\int_m T_{ji} d\eta \right) / 2 & \quad m = n \\
 \Delta s^m \left(\int_m U_{ij} d\eta \right) / 2 & \quad m = n \\
 \text{case (b): } \Delta s^m \left[\int_m (1 - \eta) T_{ji} d\eta \right] / 4 & \quad m = n, n + 1 \\
 \Delta s^m \left[\int_m (1 + \eta) T_{ji} d\eta \right] / 4 & \quad m = n, n + 1 \\
 \Delta s^m \left(\int_m U_{ij} d\eta \right) / 2 & \quad m = n, n + 1
 \end{aligned}$$

$$\text{case (c): } \Delta s_m^m \left[\int (1 - \eta) T_{ji} d\eta \right] / 4 \quad m = n, n + 1$$

$$\Delta s_m^m \left[\int (1 - \eta) T_{ji} d\eta \right] / 4 \quad m = n, n + 1$$

$$\Delta s_m^m \left[\int (1 - \eta) U_{ij} d\eta \right] / 4 \quad m = n, n + 1$$

$$\Delta s_m^m \left[\int (1 + \eta) U_{ij} d\eta \right] / 4 \quad m = n, n + 1.$$

Altogether then, sixteen special coefficients need to be dispositioned. Recall, however, that five of these are incorporated into the α_{ji} coefficients as shown in eqs. [28], [29] and [30]. Let's look at these coefficients more closely.

Suppose $\underline{x}$ is a corner point on B and define the following angles:

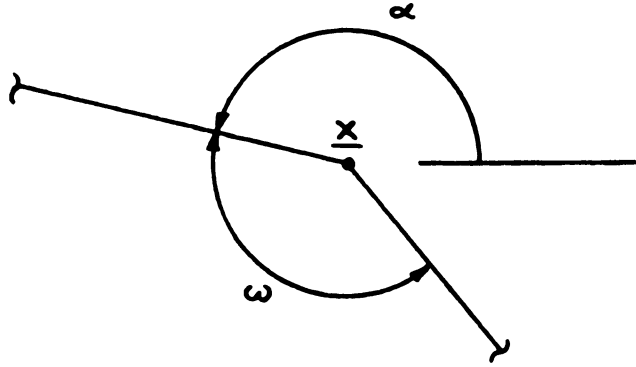


Figure 5. Free Term Coefficient

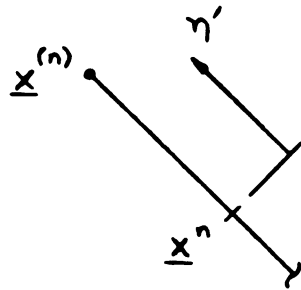
Then, proceeding as we did in Chapter 2, we get

$$\alpha_{ji} = \begin{cases} \omega/2\pi \pm (1 + \nu) [\sin 2(\alpha + \omega) - \sin 2\alpha] / 8\pi & j = i \\ (1 + \nu) [\sin^2(\alpha + \omega) - \sin^2\alpha] / 4\pi & j \neq i \end{cases}$$

so that when $\omega = \pi$, $\alpha_{ji} = \delta_{ji} / 2$. It is clear, then, that these coefficients represent only rigid-body displacements and may, therefore, be ignored.

Now we are left with eleven special coefficients. However, those involving T_{ji} in cases (b) and (c) are identical so we are actually left with nine. To evaluate these, we need the following local coordinates:

On $m = n$:



$$0 \leq \eta \leq 1$$

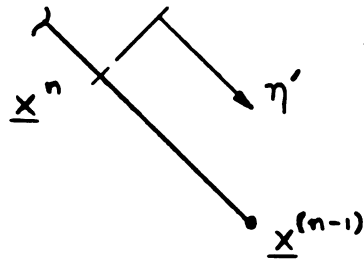
$$\eta = \eta'$$

$$d\eta = d\eta'$$

$$\rho = \Delta s^m \eta' / 2 \quad [37]$$

$$q_1 = n_2$$

$$q_2 = -n_1$$



$$-1 \leq \eta \leq 0$$

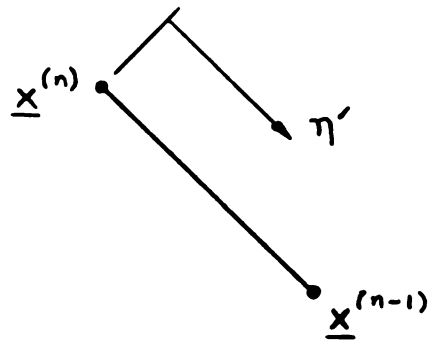
$$\eta = -\eta'$$

$$d\eta = -d\eta'$$

$$\rho = \Delta s^m \eta' / 2 \quad [38]$$

$$q_1 = -n_2$$

$$q_2 = n_1$$



$$-1 \leq \eta \leq 1$$

$$\eta = 1 - 2\eta'$$

$$d\eta = -2d\eta'$$

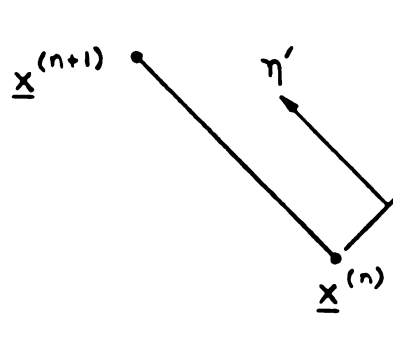
$$\rho = \eta' \Delta s^m \quad [39]$$

$$q_1 = -n_2$$

$$q_2 = n_1$$

Figure 6. Local Coordinates On $m = n$

On $m = n + 1$:



$$\begin{aligned}
 -1 &\leq \eta \leq 1 \\
 \eta &= 2\eta' - 1 \\
 d\eta &= 2d\eta' \\
 \rho &= \eta' \Delta s^m \\
 q_1 &= n_2 \\
 q_2 &= -n_1
 \end{aligned} \tag{40}$$

Figure 7. Local Coordinates On $m = n + 1$

Now consider case (a), which has the following special coefficient:

$$\Delta s^m \left(\int_m U_{ij} d\eta \right) / 2 \quad m = 1.$$

Using equations [37] and [38], this becomes

$$\int_{-1}^1 U_{ij}(x^n, \eta) d\eta = - \int_1^0 U_{ij}(\eta') d\eta' + \int_0^1 U_{ij}(\eta') d\eta'. \tag{41}$$

Equations [37] and [38] both yield identical results when substituted into equations [14] and we have

$$\begin{aligned}
 U_{11} &= [-(3 - \nu) \ln (\Delta s^m \eta' / 2) + (1 + \nu) n_2^2] / 8\pi G \\
 U_{12} &= - (1 + \nu) n_1 n_2 / 8\pi G \\
 U_{21} &= - (1 + \nu) n_1 n_2 / 8\pi G \\
 U_{22} &= [- (3 - \nu) \ln (\Delta s^m \eta' / 2) + (1 + \nu) n_1^2] / 8\pi G.
 \end{aligned} \tag{42}$$

This result allows us to write

$$- \int_1^0 U_{ij}(\eta') d\eta' + \int_0^1 U_{ij}(\eta') d\eta' = 2 \int_0^1 U_{ij}(\eta') d\eta'. \tag{43}$$

Using equations [42] and [43], we now write the special coefficients for case (a)

$$\begin{aligned}
 \Delta s^n \left(\int_n U_{11} d\eta \right) / 2 &= (\Delta s^n / 8\pi G) [(3 - \nu) - (3 - \nu) \ln (\Delta s^m / 2) + (1 + \nu) n_2^2] \\
 \Delta s^n \left(\int_n U_{12} d\eta \right) / 2 &= - (\Delta s^n / 8\pi G) (1 + \nu) n_1 n_2 \\
 \Delta s^n \left(\int_n U_{21} d\eta \right) / 2 &= - (\Delta s^n / 8\pi G) (1 + \nu) n_1 n_2 \\
 \Delta s^n \left(\int_n U_{22} d\eta \right) / 2 &= (\Delta s^n / 8\pi G) [(3 - \nu) - (3 - \nu) \ln (\Delta s^m / 2) + (1 + \nu) n_1^2]
 \end{aligned} \tag{44}$$

Both case (b) and case (c) have the following special coefficients:

$$\begin{aligned}
 \Delta s^m \left[\int_m (1 - \eta) T_{ji} d\eta \right] / 4 & \quad m = n \\
 \Delta s^m \left[\int_m (1 + \eta) T_{ji} d\eta \right] / 4 & \quad m = n + 1
 \end{aligned}$$

The singularity in T_{ji} , however, is of the form $1 / \rho$, and ρ goes to zero at the same rate as $(1 \pm \eta)$. This means that the integrals are well-behaved and may be evaluated numerically.

We now turn our attention to the U_{ij} - type coefficients of cases (b) and (c). From equations [39] and [40], we have

$m = n$:

$$\begin{aligned}
 \text{(b)} \quad \Delta s^n \left[\int_{-1}^1 U_{ij} (x^{(n)}, \eta) d\eta \right] / 2 &= \Delta s^n \int_0^1 U_{ij} (\eta') d\eta' \\
 \text{(c)} \quad \Delta s^n \left[\int_{-1}^1 (1 - \eta) U_{ij} (x^{(n)}, \eta) d\eta \right] / 4 &= \Delta s^n \int_0^1 \eta U_{ij} (\eta') d\eta' \\
 \Delta s^n \left[\int_{-1}^1 (1 + \eta) U_{ij} (x^{(n)}, \eta) d\eta \right] / 4 &= \Delta s^n \int_0^1 (1 - \eta') U_{ij} (\eta') d\eta'
 \end{aligned} \tag{45}$$

$m = n + 1$:

$$(b) \quad \Delta s^{n+1} \left[\int_{-1}^1 U_{ij}(x^{(n+1)}, \eta) d\eta \right] / 2 = \Delta s^{n+1} \int_0^1 U_{ij}(\eta') d\eta'$$

$$(c) \quad \Delta s^{n+1} \left[\int_{-1}^1 (1 - \eta) U_{ij}(x^{(n+1)}, \eta) d\eta \right] / 4 = \Delta s^{n+1} \int_0^1 (1 - \eta') U_{ij}(\eta') d\eta' \quad [46]$$

$$\Delta s^{n+1} \left[\int_{-1}^1 (1 + \eta) U_{ij}(x^{(n+1)}, \eta) d\eta \right] / 4 = \Delta s^{n+1} \int_0^1 \eta' U_{ij}(\eta') d\eta'$$

Just as equations [45] and [46] are identical in form, substitution of equations [39] and [40] into equations [15] shows that U_{ij} is identical in form on $m + n$ and $m = n + 1$.

$$\begin{aligned} U_{11} &= [-(3 - \nu) \ln(\Delta s^m \eta') + (1 + \nu) n_2^2] / 8\pi G \\ U_{12} &= -(1 + \nu) n_1 n_2 / 8\pi G \\ U_{21} &= -(1 + \nu) n_1 n_2 / 8\pi G \\ U_{22} &= [- (3 - \nu) \ln(\Delta s^m \eta') + (1 + \nu) n_1^2] / 8\pi G \end{aligned} \quad [47]$$

After making the substitutions and carrying out the integrations, we get the following results:

case (b):

$$\begin{aligned} \Delta s^m \int_0^1 U_{11} d\eta' &= \Delta s^m [- (3 - \nu) \ln \Delta s^m + (3 - \nu) + (1 + \nu) n_2^2] / 8\pi G \\ \Delta s^m \int_0^1 U_{12} d\eta' &= -\Delta s^m (1 + \nu) n_1 n_2 / 8\pi G \\ \Delta s^m \int_0^1 U_{21} d\eta' &= -\Delta s^m (1 + \nu) n_1 n_2 / 8\pi G \\ \Delta s^m \int_0^1 U_{22} d\eta' &= \Delta s^m [- (3 - \nu) \ln \Delta s^m + (3 - \nu) + (1 + \nu) n_1^2] / 8\pi G \end{aligned} \quad [48]$$

case (c):

$$\begin{aligned}
 \Delta s^m \int_0^1 \eta' U_{11} d\eta' &= \Delta s^m [-0.5 (3 - \nu) \ln \Delta s^m + 0.25 (3 - \nu) + 0.5 (1 + \nu) n_2^2] / 8\pi G \\
 \Delta s^m \int_0^1 \eta' U_{12} d\eta' &= \Delta s^m (0.5) (1 + \nu) n_1 n_2 / 8\pi G \\
 \Delta s^m \int_0^1 \eta' U_{21} d\eta' &= -\Delta s^m (0.5) (1 + \nu) n_1 n_2 / 8\pi G \\
 \Delta s^m \int_0^1 \eta' U_{22} d\eta' &= \Delta s^m [-0.5 (3 - \nu) \ln \Delta s^m + 0.25 (3 - \nu) + 0.5 (1 + \nu) n_1^2] / 8\pi G \\
 \Delta s^m \int_0^1 (1 - \eta') U_{11} d\eta' &= \Delta s^m [(3 - \nu) (0.75 - 0.5 \ln \Delta s^m) + 0.5(1 + \nu) n_2^2] / 8\pi G \\
 \Delta s^m \int_0^1 (1 - \eta') U_{12} d\eta' &= -\Delta s^m (0.5) (1 + \nu) n_1 n_2 / 8\pi G \\
 \Delta s^m \int_0^1 (1 - \eta') U_{21} d\eta' &= -\Delta s^m (0.5) (1 + \nu) n_1 n_2 / 8\pi G \\
 \Delta s^m \int_0^1 (1 - \eta') U_{22} d\eta' &= \Delta s^m [(3 - \nu) (0.75 - 0.5 \ln \Delta s^m) + 0.5 (1 + \nu) n_1^2] / 8\pi G
 \end{aligned}
 \tag{49}$$

[50]

where $m = n, n + 1$.

It is important to note that in case (c), the $(1 - \eta')$ - type integrals add together for $m = n$ and $m = n + 1$.

Recall that the coefficients in [A], which multiplied U_j^n , for all three cases, were incorporated into the α_{ji} coefficients. These were then found to represent rigid - body displacements and are therefore ignored. In doing this, however, we have created a diagonal void in the [A] matrix. We may fill this void by determining the diagonal entries in the following manner.

Consider a rigid - body displacement applied to the system. This will produce no stress and, therefore,

$$[A] \{u\} = [B] \{0\} = \{0\}.$$

In other words,

$$A_{11} u_1 + A_{12} u_2 + A_{13} u_3 + \dots + A_{12n} u_{2n} = 0.$$

So we have that the diagonal entries of [A] are the negative sums of the off-diagonal entries.

Of course, the diagonal entries referred to here are actually 2 x 2 block matrices and are given by

$$\begin{aligned} A_{(2n-1)(2n-1)} &= - \sum_{m=1}^N A_{(2n-1)(2m-1)} & m \neq n \\ A_{(2n-1)(2n)} &= - \sum_{m=1}^N A_{(2n-1)(2m)} & m \neq n \\ A_{(2n)(2n-1)} &= - \sum_{m=1}^N A_{(2n)(2m-1)} & m \neq n \\ A_{(2n)(2n)} &= - \sum_{m=1}^N A_{(2n)(2m)} & m \neq n \end{aligned} \quad [51]$$

In summary, the following equations are used to calculate the matrices:

[A] Matrix:	case (a)	[15], [35], [51]
	case (b)	[15], [36], [51]
	case (c)	[15], [36], [51]
[B] Matrix:	case (a)	[14], [35], [44]
	case (b)	[14], [36], [48]
	case (c)	[14], [36], [49], [50]

3.4 INTERIOR FIELD POINTS

Following the same reasoning used in the previous section, we may rewrite equations [22] and [23] for the three cases.

case (a):

$$\begin{aligned}
u_i &= \sum_{m=1}^N [(\Delta s^m/2) \int_m T_{ji}(\underline{x}, \eta) d\eta] u_j^m \\
&+ \sum_{m=1}^N [(\Delta s^m/2) \int_m U_{ij}(\underline{x}, \eta) d\eta] \dot{u}_j^m \\
\sigma_{ik} &= \sum_{m=1}^N [(\Delta s^m/2) \int_m S_{jki}(\underline{x}, \eta) d\eta] u_j^m \\
&+ \sum_{m=1}^N [(\Delta s^m/2) \int_m D_{ikj}(\underline{x}, \eta) d\eta] \dot{u}_j^m
\end{aligned}$$

[52]

case (b):

$$\begin{aligned}
u_i &= \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 - \eta) T_{ji}(\underline{x}, \eta) d\eta] u_j^{(m-1)} \\
&+ \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 + \eta) T_{ji}(\underline{x}, \eta) d\eta] u_j^{(m)} \\
&+ \sum_{m=1}^N [(\Delta s^m/2) \int_m U_{ij}(\underline{x}, \eta) d\eta] \dot{u}_j^m \\
\sigma_{ik} &= \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 - \eta) S_{jki}(\underline{x}, \eta) d\eta] u_j^{(m-1)} \\
&+ \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 + \eta) S_{jki}(\underline{x}, \eta) d\eta] u_j^{(m)} \\
&+ \sum_{m=1}^N [(\Delta s^m/2) \int_m D_{ikj}(\underline{x}, \eta) d\eta] \dot{u}_j^m
\end{aligned}$$

[53]

case (c):

$$\begin{aligned}
u_i &= \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 - \eta) T_{ji}(\underline{x}, \eta) d\eta] u_j^{(m-1)} \\
&+ \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 + \eta) T_{ji}(\underline{x}, \eta) d\eta] u_j^{(m)} \\
&+ \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 - \eta) U_{ij}(\underline{x}, \eta) d\eta] \dot{u}_j^{(m-1)} \\
&+ \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 + \eta) U_{ij}(\underline{x}, \eta) d\eta] \dot{u}_j^{(m)}
\end{aligned}$$

[54]

$$\begin{aligned}
\sigma_{ik} = & \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 - \eta) S_{jki} (\underline{x}, \eta) d\eta] u_j^{(m-1)} \\
& + \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 + \eta) S_{jki} (\underline{x}, \eta) d\eta] u_j^{(m)} \\
& + \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 - \eta) D_{ikj} (\underline{x}, \eta) d\eta] t_j^{(m-1)} \\
& + \sum_{m=1}^N [(\Delta s^m/4) \int_m (1 + \eta) D_{ikj} (\underline{x}, \eta) d\eta] t_j^{(m)}
\end{aligned}$$

Applying equations [24] and [25] and Gauss quadrature, these equations may be used to obtain displacements and stresses at any point in the body.

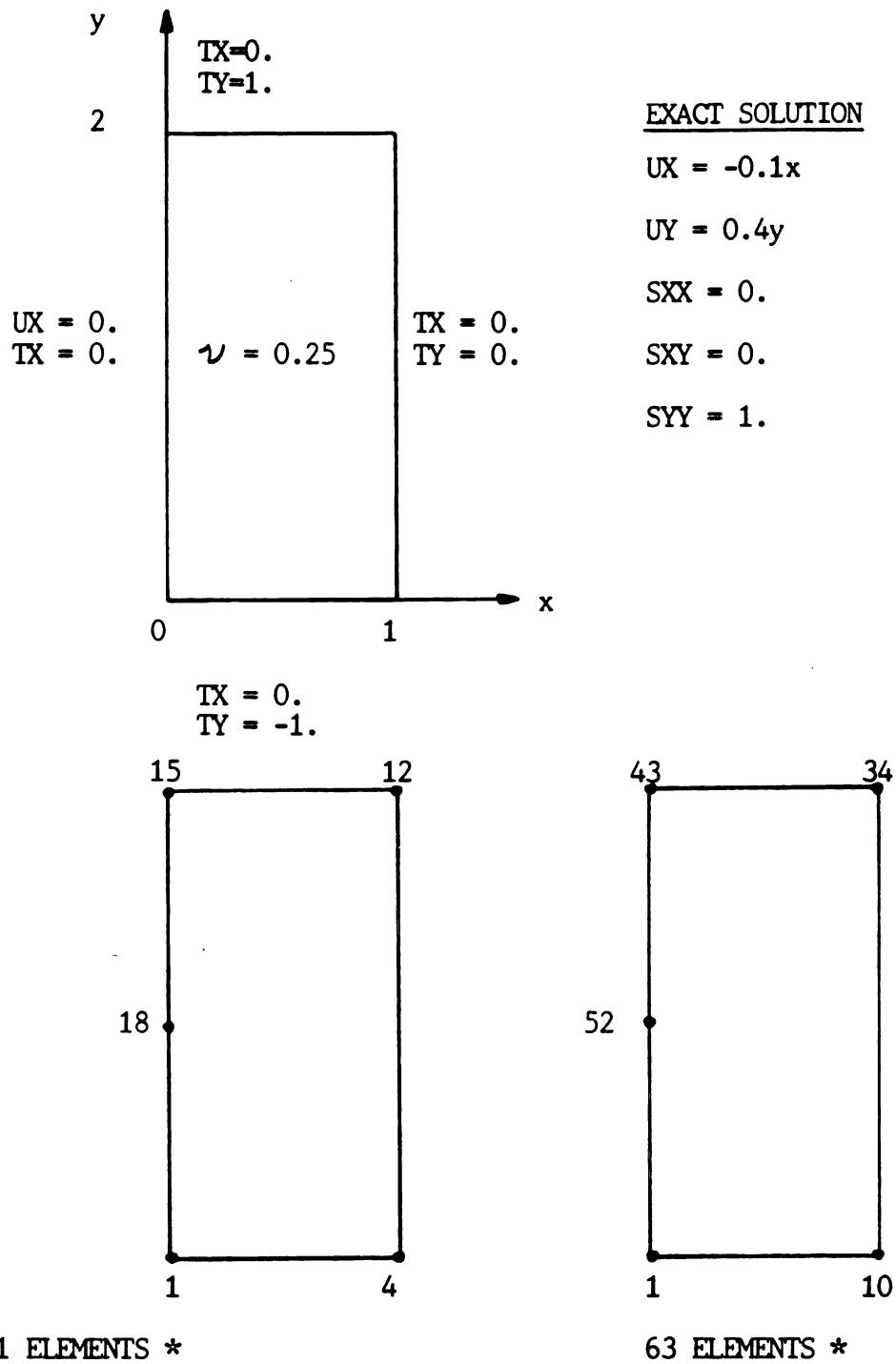
CHAPTER 4

EXAMPLES AND RESULTS

4.1 PROBLEM DESCRIPTIONS

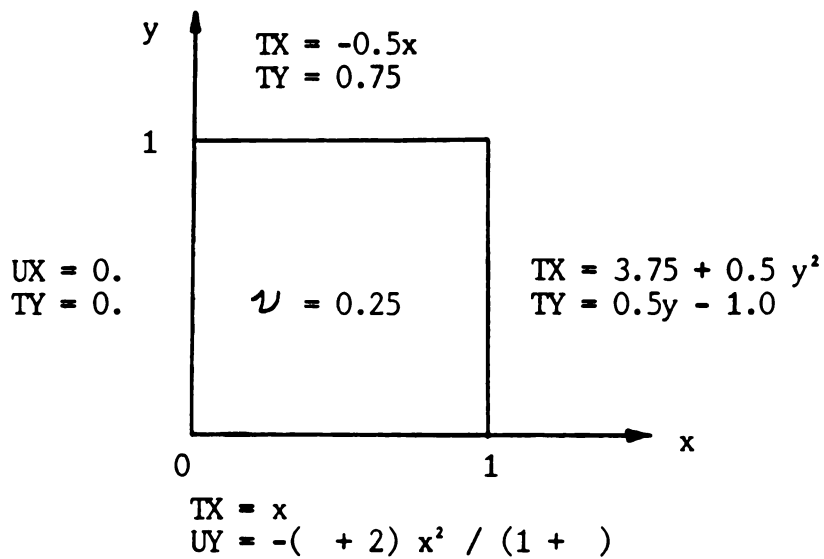
Our objective is to assess the performance of each of the three numerical models in solving linear isotropic elasticity problems. Three example problems were chosen for this purpose. They represent a range of geometries and boundary conditions intended to highlight the relative strengths and weaknesses of each model.

The example problems are described in the following figures along with boundary conditions, exact solutions and boundary meshes. These figures are followed by tables containing the output data and percent differences for all three models in each problem.



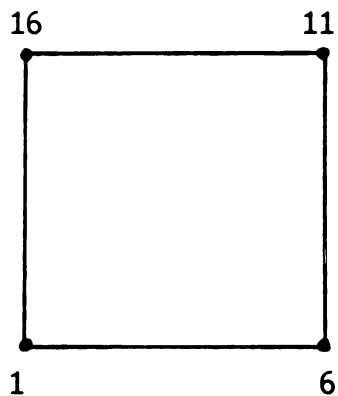
* Between each node number, elements are of equal size.

Figure 8. Problem One - Pure Extension

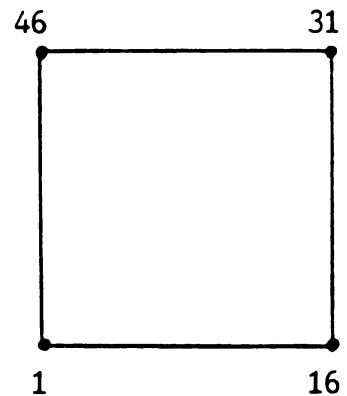


EXACT SOLUTION (18)

$$\begin{aligned}
 UX &= 0.5[4x - x^3/12 + y^2/2 - x(y - y^2/4)] / (1 + x) \\
 UY &= 0.5[y^2/2 - y^3/12 - (4y - x^2y/4 + y^3/6) - (1 + x)x^2 \\
 &\quad + x^2/2]/(1 + x) \\
 SXX &= 4 - x^2/4 + y^2/2 \\
 SXY &= xy/2 - x \\
 SYY &= y - y^2/4
 \end{aligned}$$



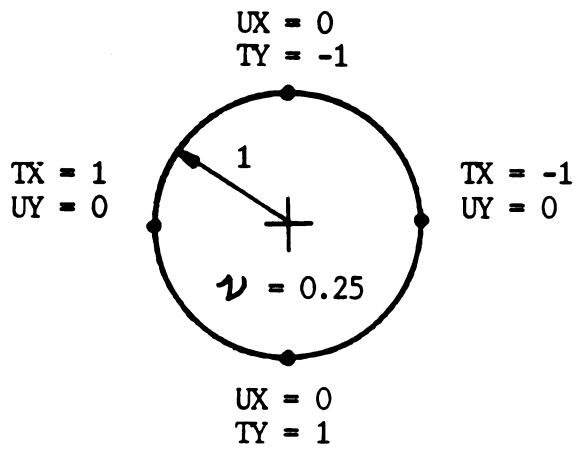
21 ELEMENTS *



63 ELEMENTS *

* Between each node number, elements are of equal size

Figure 9. Problem Two - Square With Variable Boundary Conditions



Otherwise: $TX = -nx$
 $TY = -ny$

EXACT SOLUTION

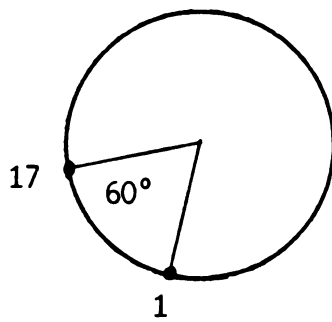
$$UX = -0.3x$$

$$UY = -0.3y$$

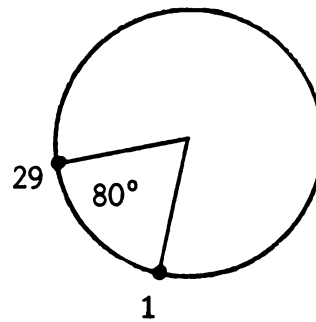
$$SXX = -1$$

$$SXY = 0$$

$$SYY = -1$$



19 ELEMENTS *



35 ELEMENTS *

* Between node numbers shown, elements are of equal size.

Figure 10. Problem Three - Circular Disk Under Uniform Pressure

4.2 TABLES OF RESULTS

The following tables summarize the numerical solutions of the three example problems. Each problem was solved twice using an increasing number of nodes.

The tables should be self-explanatory, however, two small clarifications are necessary. First, since percent difference is meaningless for elements where the quantity is either specified or equal to zero, these elements are omitted from the percent difference table. Second, all displacement values are multiplied by the shear modulus.

4.3 DISCUSSION

The problems described in the previous section represent a range of geometries and boundary conditions. These problems were chosen to include smooth boundaries and boundaries with corners as well as constant and variable boundary conditions. The performance of each model in these basic problems will then provide information on their applicability in general.

Problem one has a straight boundary with corners and linear displacements with piecewise constant tractions. The straight boundaries allow an exact boundary representation and the variable behavior is identical to that assumed in case (b). Therefore, one would expect case (b) to solve this problem exactly and, indeed, it does. The other cases differ in their assumed variable behavior and, therefore, yield approximate results. In case (a), the assumed traction behavior is consistent with the problem, however, the displacements are piecewise constant. Conversely, in case (c), the assumed displacement behavior is consistent, but the tractions are piecewise continuous. Therefore, in cases (a) and (c), we see increasing inaccuracy near corner points where there is a change in variable behavior. These inaccuracies in the boundary solution carry over into the interior solution as well. However, interior solutions are, in general, more accurate except for points near the boundary.

Problem two also has straight boundaries with corners, however, the boundary conditions are more complex. One would still expect to see inaccuracy near corners, however, it is not

clear what effect the assumed variable behavior would have. Since the piecewise constant behavior is more forgiving at corners, it would appear cases (a) and (b) might prevail.

Problem three has a circular boundary which introduces boundary approximation errors in all three cases. The variable behavior does not immediately favor any case so we expect, and find, similar results in each.

Table 1. Pure Extension - 21 Nodes: X - Displacements

X-DISPLACEMENTS

NO	X	Y	UXA	UXB	UXC	EXACT
1	0.00000	.12500	0.00000	0.00000	0.00000	0.00000
2	.16667	0.00000	-.02301	-.01667	-.02247	-.01667
3	.50000	0.00000	-.05480	-.05000	-.04920	-.05000
4	.83333	0.00000	-.08671	-.08333	.00321	-.08333
5	1.00000	.12500	-.11030	-.10000	-.03224	-.10000
6	1.00000	.37500	-.11029	-.10000	-.11801	-.10000
7	1.00000	0.62500	-.10990	-.10000	-.10915	-.10000
8	1.00000	.87500	-.10980	-.10000	-.10597	-.10000
9	1.00000	1.12500	-.11000	-.10000	-.10615	-.10000
10	1.00000	1.37500	-.11060	-.10000	-.10578	-.10000
11	1.00000	1.62500	-.11162	-.10000	-.09857	-.10000
12	1.00000	1.87500	-.11216	-.10000	-.02072	-.10000
13	.83333	2.00000	-.08878	-.08333	.01120	-.08333
14	.50000	2.00000	-.05730	-.05000	-.01054	-.05000
15	.16667	2.00000	-.02706	-.01667	.02797	-.01667
16	0.00000	1.83333	0.00000	0.00000	0.00000	0.00000
17	0.00000	1.50000	0.00000	0.00000	0.00000	0.00000
18	0.00000	1.16667	0.00000	0.00000	0.00000	0.00000
19	0.00000	.87500	0.00000	0.00000	0.00000	0.00000
20	0.00000	.62500	0.00000	0.00000	0.00000	0.00000
21	0.00000	.37500	0.00000	0.00000	0.00000	0.00000

Table 2. Pure Extension - 21 Nodes: Y - Displacements

Y-DISPLACEMENTS

NO	X	Y	UYA	UYB	UYC	EXACT
1	0.00000	.12500	.05323	.05000	.12917	.05000
2	.16667	0.00000	0.00000	0.00000	0.00000	0.00000
3	.50000	0.00000	0.00000	0.00000	0.00000	0.00000
4	.83333	0.00000	0.00000	0.00000	0.00000	0.00000
5	1.00000	.12500	.05362	.05000	.16087	.05000
6	1.00000	.37500	.15182	.15000	.14766	.15000
7	1.00000	.62500	.25156	.25000	.22970	.25000
8	1.00000	.87500	.35152	.35000	.33063	.35000
9	1.00000	1.12500	.45156	.45000	.42866	.45000
10	1.00000	1.37500	.55155	.55000	.51974	.55000
11	1.00000	1.62500	.65119	.65000	.59108	.65000
12	1.00000	1.87500	.74901	.75000	.61680	.75000
13	.83333	2.00000	.80226	.80000	.73813	.80000
14	.50000	2.00000	.80312	.80000	.76959	.80000
15	.16667	2.00000	.79939	.80000	.87782	.80000
16	0.00000	1.83333	.73029	.73333	.78077	.73333
17	0.00000	1.50000	.59941	.60000	.63285	.60000
18	0.00000	1.16667	.46688	.46667	.49113	.46667
19	0.00000	.87500	.35067	.35000	.35124	.35000
20	0.00000	.62500	.25100	.25000	.20905	.25000
21	0.00000	.37500	.15141	.15000	.15842	.15000

Table 3. Pure Extension - 21 Nodes: X - Traction

X-TRACTIONS

NO	X	Y	TXA	TXB	TXC	EXACT
1	0.00000	.12500	-.00825	.00000	-.11642	0.00000
2	.16667	0.00000	0.00000	0.00000	0.00000	0.00000
3	.50000	0.00000	0.00000	0.00000	0.00000	0.00000
4	.83333	0.00000	0.00000	0.00000	0.00000	0.00000
5	1.00000	.12500	0.00000	0.00000	0.00000	0.00000
6	1.00000	.37500	0.00000	0.00000	0.00000	0.00000
7	1.00000	.62500	0.00000	0.00000	0.00000	0.00000
8	1.00000	.87500	0.00000	0.00000	0.00000	0.00000
9	1.00000	1.12500	0.00000	0.00000	0.00000	0.00000
10	1.00000	1.37500	0.00000	0.00000	0.00000	0.00000
11	1.00000	1.62500	0.00000	0.00000	0.00000	0.00000
12	1.00000	1.87500	0.00000	0.00000	0.00000	0.00000
13	.83333	2.00000	0.00000	0.00000	0.00000	0.00000
14	.50000	2.00000	0.00000	0.00000	0.00000	0.00000
15	.16667	2.00000	0.00000	0.00000	0.00000	0.00000
16	0.00000	1.83333	-.00885	.00000	-.32744	0.00000
17	0.00000	1.50000	-.00473	.00000	-.01711	0.00000
18	0.00000	1.16667	-.02091	.00000	-.00401	0.00000
19	0.00000	.87500	.02341	.00000	.05992	0.00000
20	0.00000	.62500	.00012	.00000	.04106	0.00000
21	0.00000	.37500	-.00363	.00000	-.12700	0.00000

Table 4. Pure Extension - 21 Nodes: Y - Traction

Y-TRACTIONS

NO	X	Y	TYA	TYB	TYC	EXACT
1	0.00000	.12500	0.00000	0.00000	0.00000	0.00000
2	.16667	0.00000	-1.00351	-1.00000	-.86657	-1.00000
3	.50000	0.00000	-.99128	-1.00000	-.97328	-1.00000
4	.83333	0.00000	-1.00616	-1.00000	-1.45664	-1.00000
5	1.00000	.12500	0.00000	0.00000	0.00000	0.00000
6	1.00000	.37500	0.00000	0.00000	0.00000	0.00000
7	1.00000	.62500	0.00000	0.00000	0.00000	0.00000
8	1.00000	.87500	0.00000	0.00000	0.00000	0.00000
9	1.00000	1.12500	0.00000	0.00000	0.00000	0.00000
10	1.00000	1.37500	0.00000	0.00000	0.00000	0.00000
11	1.00000	1.62500	0.00000	0.00000	0.00000	0.00000
12	1.00000	1.87500	0.00000	0.00000	0.00000	0.00000
13	.83333	2.00000	1.00000	1.00000	1.00000	1.00000
14	.50000	2.00000	1.00000	1.00000	1.00000	1.00000
15	.16667	2.00000	1.00000	1.00000	1.00000	1.00000
16	0.00000	1.83333	0.00000	0.00000	0.00000	0.00000
17	0.00000	1.50000	0.00000	0.00000	0.00000	0.00000
18	0.00000	1.16667	0.00000	0.00000	0.00000	0.00000
19	0.00000	.87500	0.00000	0.00000	0.00000	0.00000
20	0.00000	.62500	0.00000	0.00000	0.00000	0.00000
21	0.00000	.37500	0.00000	0.00000	0.00000	0.00000

Table 5. Pure Extension - 21 Nodes: Interior Values

INTERIOR X-DISP

NO	X	Y	UXA	UXB	UXC	EXACT
1	.25000	.50000	-.02964	-.02500	-.02002	-.02500
2	.25000	1.00000	-.03032	-.02500	-.03363	-.02500
3	.25000	1.50000	-.02984	-.02500	-.00236	-.02500
4	.50000	.50000	-.05507	-.05000	-.04395	-.05000
5	.50000	1.00000	-.05523	-.05000	-.05881	-.05000
6	.50000	1.50000	-.05591	-.05000	-.04264	-.05000
7	.75000	.50000	-.08047	-.07500	-.08055	-.07500
8	.75000	1.00000	-.08036	-.07500	-.08084	-.07500
9	.75000	1.50000	-.08145	-.07500	-.07538	-.07500

INTERIOR Y-DISP

NO	X	Y	UXA	UXB	UXC	EXACT
1	.25000	.50000	.20142	.20000	.20889	.20000
2	.25000	1.00000	.40116	.40000	.40849	.40000
3	.25000	1.50000	.59992	.60000	.61530	.60000
4	.50000	.50000	.20143	.20000	.19088	.20000
5	.50000	1.00000	.40114	.40000	.39594	.40000
6	.50000	1.50000	.60077	.60000	.59726	.60000
7	.75000	.50000	.20165	.20000	.18026	.20000
8	.75000	1.00000	.40132	.40000	.38623	.40000
9	.75000	1.50000	.60101	.60000	.58238	.60000

INTERIOR SXX

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	.00035	.00000	.05022	0.00000
2	.25000	1.00000	.00967	.00000	-.00209	0.00000
3	.25000	1.50000	-.02427	.00000	1.31848	0.00000
4	.50000	.50000	-.00587	.00000	-.04520	0.00000
5	.50000	1.00000	-.00348	.00000	.02039	0.00000
6	.50000	1.50000	-.00754	.00000	-.06053	0.00000
7	.75000	.50000	.00081	.00000	-.06660	0.00000
8	.75000	1.00000	.00281	.00000	.06332	0.00000
9	.75000	1.50000	-.00018	.00000	-.02828	0.0000

INTERIOR SXY

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	-.00061	.00000	-.24064	0.00000
2	.25000	1.00000	.00162	.00000	-.23927	0.00000
3	.25000	1.50000	.00385	.00000	-.13439	0.00000
4	.50000	.50000	.00010	.00000	-.15109	0.00000
5	.50000	1.00000	.00056	.00000	-.08109	0.00000
6	.50000	1.50000	.00015	.00000	.00618	0.00000
7	.75000	.50000	.00186	.00000	.04726	0.00000
8	.75000	1.00000	.00019	.00000	-.01461	0.00000
9	.75000	1.50000	-.00320	.00000	-.03663	0.00000

Table 5 (cont'd.)

INTERIOR SKY

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	.99402	1.00000	.86865	1.00000
2	.25000	1.00000	.98745	1.00000	1.06814	1.00000
3	.25000	1.50000	1.00367	1.00000	1.03900	1.00000
4	.50000	.50000	.99949	1.00000	1.03050	1.00000
5	.50000	1.00000	.99635	1.00000	1.00854	1.00000
6	.50000	1.50000	.99900	1.00000	1.03846	1.00000
7	.75000	.50000	.99370	1.00000	1.07657	1.00000
8	.75000	1.00000	.99351	1.00000	.95636	1.00000
9	.75000	1.50000	.99346	1.00000	.98414	1.00000

Table 6. Pure Extension - 21 Nodes: Percent Differences

X-DISPLACEMENTS

NO	A	B	C
2	-38.07	.00	-34.83
3	-9.61	.00	1.60
4	-4.06	.00	103.86
5	-10.30	.00	67.76
6	-10.29	.00	-18.01
7	-9.90	.00	-9.15
8	-9.80	.00	-5.97
9	-10.00	.00	-6.15
10	-10.60	.00	-5.78
11	-11.62	.00	1.43
12	-12.16	.00	79.28
13	-6.53	.00	113.44
14	-14.61	.00	78.92
15	-62.34	.00	267.81

Y-DISPLACEMENTS

NO	A	B	C
1	-6.46	.00	-158.34
5	-7.23	.00	-221.73
6	-1.22	.00	1.56
7	-.62	.00	8.12
8	-.43	.00	5.54
9	-.35	.00	4.74
10	-.28	.00	5.50
11	-.18	.00	9.07
12	.13	.00	17.76
13	-.28	.00	7.73
14	-.39	.00	3.80
15	.08	.00	-9.73
16	.41	.00	-6.47
17	.10	.00	-5.47
18	-.05	.00	-5.24

Table 6 (cont'd.)

19	-.19	.00	-.35
20	-.40	.00	16.38
21	-.94	.00	-5.61

Y-TRACTIONS

NO	A	B	C
2	-.35	.00	13.34
3	.87	.00	2.67
4	-.62	.00	-45.66

INTERIOR X-DISP

NO	A	B	C
1	-18.57	.00	19.91
2	-21.28	.00	-34.52
3	-19.38	.00	90.57
4	-10.14	.00	12.10
5	-10.46	.00	-17.62
6	-11.83	.00	14.72
7	-7.29	.00	-7.40
8	-7.15	.00	-7.79
9	-8.60	.00	-.51

INTERIOR Y-DISP

NO	A	B	C
1	-.71	.00	-4.44
2	-.29	.00	-2.12
3	.01	.00	-2.55
4	-.72	.00	4.56
5	-.28	.00	1.02
6	-.13	.00	.46
7	-.82	.00	9.87
8	-.33	.00	3.44
9	-.17	.00	2.94

INTERIOR SYX

NO	A	B	C
1	.60	.00	13.13
2	1.25	.00	-6.81
3	-.37	.00	-3.90
4	.05	.00	-3.05
5	.37	.00	-.85
6	.10	.00	-3.85
7	.63	.00	-7.66
8	.65	.00	4.36
9	.65	.00	1.59

Table 7. Pure Extension - 63 Nodes: X - Displacements

X-DISPLACEMENTS

NO	X	Y	UXA	UXB	UXC	EXACT
1	0.00000	.04167	0.00000	0.00000	0.00000	0.00000
2	.05556	0.00000	-.00785	-.00556	-.01587	-.00556
3	.16667	0.00000	-.01849	-.01667	-.02705	-.01667
4	.27778	0.00000	-.02950	-.02778	-.03015	-.02778
5	.38889	0.00000	-.04055	-.03889	-.03953	-.03889
6	.50000	0.00000	-.05161	-.05000	-.04983	-.05000
7	.61111	0.00000	-.06268	-.06111	-.06018	-.06111
8	.72222	0.00000	-.07374	-.07222	-.06975	-.07222
9	.83333	0.00000	-.08478	-.08333	-.07539	-.08333
10	.94444	0.00000	-.09545	-.09444	-.05542	-.09444
11	1.00000	.04167	-.10337	-.10000	-.07145	-.10000
12	1.00000	.12500	-.10349	-.10000	-.10864	-.10000
13	1.00000	.20833	-.10343	-.10000	-.10299	-.10000
14	1.00000	.29167	-.10338	-.10000	-.09963	-.10000
15	1.00000	.37500	-.10335	-.10000	-.09837	-.10000
16	1.00000	.45833	-.10332	-.10000	-.09787	-.10000
17	1.00000	.54167	-.10330	-.10000	-.09769	-.10000
18	1.00000	.62500	-.10329	-.10000	-.09767	-.10000
19	1.00000	.70833	-.10329	-.10000	-.09773	-.10000
20	1.00000	.79167	-.10330	-.10000	-.09783	-.10000
21	1.00000	.87500	-.10331	-.10000	-.09796	-.10000
22	1.00000	.95833	-.10334	-.10000	-.09809	-.10000
23	1.00000	1.04167	-.10338	-.10000	-.09821	-.10000
24	1.00000	1.12500	-.10342	-.10000	-.09831	-.10000
25	1.00000	1.20833	-.10348	-.10000	-.09841	-.10000
26	1.00000	1.29167	-.10355	-.10000	-.09849	-.10000
27	1.00000	1.37500	-.10362	-.10000	-.09858	-.10000
28	1.00000	1.45833	-.10370	-.10000	-.09869	-.10000
29	1.00000	1.54167	-.10379	-.10000	-.09884	-.10000
30	1.00000	1.62500	-.10388	-.10000	-.09911	-.10000
31	1.00000	1.70833	-.10395	-.10000	-.09971	-.10000
32	1.00000	1.79167	-.10400	-.10000	-.10104	-.10000
33	1.00000	1.87500	-.10398	-.10000	-.10075	-.10000
34	1.00000	1.95833	-.10367	-.10000	-.07178	-.10000
35	.94444	2.00000	-.09569	-.09445	-.06085	-.09444
36	.83333	2.00000	-.08509	-.08333	-.07232	-.08333
37	.72222	2.00000	-.07421	-.07222	-.06603	-.07222
38	.61111	2.00000	-.06326	-.06111	-.05711	-.06111
39	.50000	2.00000	-.05230	-.05000	-.04746	-.05000
40	.38889	2.00000	-.04134	-.03889	-.03783	-.03889
41	.27778	2.00000	-.03040	-.02778	-.02868	-.02778
42	.16667	2.00000	-.01952	-.01667	-.01662	-.01667
43	.05556	2.00000	-.00927	-.00556	.00876	-.00556
44	0.00000	1.94444	0.00000	0.00000	0.00000	0.00000
45	0.00000	1.83333	0.00000	0.00000	0.00000	0.00000
46	0.00000	1.72222	0.00000	0.00000	0.00000	0.00000
47	0.00000	1.61111	0.00000	0.00000	0.00000	0.00000
48	0.00000	1.50000	0.00000	0.00000	0.00000	0.00000
49	0.00000	1.38889	0.00000	0.00000	0.00000	0.00000

Table 7 (cont'd.)

50	0.00000	1.27778	0.00000	0.00000	0.00000	0.00000
51	0.00000	1.16667	0.00000	0.00000	0.00000	0.00000
52	0.00000	1.05556	0.00000	0.00000	0.00000	0.00000
53	0.00000	.95833	0.00000	0.00000	0.00000	0.00000
54	0.00000	.87500	0.00000	0.00000	0.00000	0.00000
55	0.00000	.79167	0.00000	0.00000	0.00000	0.00000
56	0.00000	.70833	0.00000	0.00000	0.00000	0.00000
57	0.00000	.62500	0.00000	0.00000	0.00000	0.00000
58	0.00000	.54167	0.00000	0.00000	0.00000	0.00000
59	0.00000	.45833	0.00000	0.00000	0.00000	0.00000
60	0.00000	.37500	0.00000	0.00000	0.00000	0.00000
61	0.00000	.29167	0.00000	0.00000	0.00000	0.00000
62	0.00000	.20833	0.00000	0.00000	0.00000	0.00000
63	0.00000	.12500	0.00000	0.00000	0.00000	0.00000

Table 8. Pure Extension - 63 Nodes: Y - Displacements

Y-DISPLACEMENTS

NO	X	Y	UYA	UYB	UYC	EXACT
1	0.00000	.04167	.01789	.01667	.06515	.01667
2	.05556	0.00000	0.00000	0.00000	0.00000	0.00000
3	.16667	0.00000	0.00000	0.00000	0.00000	0.00000
4	.27778	0.00000	0.00000	0.00000	0.00000	0.00000
5	.38889	0.00000	0.00000	0.00000	0.00000	0.00000
6	.50000	0.00000	0.00000	0.00000	0.00000	0.00000
7	.61111	0.00000	0.00000	0.00000	0.00000	0.00000
8	.72222	0.00000	0.00000	0.00000	0.00000	0.00000
9	.83333	0.00000	0.00000	0.00000	0.00000	0.00000
10	.94444	0.00000	0.00000	0.00000	0.00000	0.00000
11	1.00000	.04167	.01797	.01667	.07223	.01667
12	1.00000	.12500	.05074	.05000	.03992	.05000
13	1.00000	.20833	.08398	.08333	.06209	.08333
14	1.00000	.29167	.11727	.11667	.09577	.11667
15	1.00000	.37500	.15058	.15000	.13026	.15000
16	1.00000	.45833	.18390	.18333	.16454	.18333
17	1.00000	.54167	.21723	.21667	.19858	.21667
18	1.00000	.62500	.25056	.25000	.23244	.25000
19	1.00000	.70833	.28389	.28333	.26615	.28333
20	1.00000	.79167	.31723	.31667	.29973	.31667
21	1.00000	.87500	.35057	.35000	.33320	.35000
22	1.00000	.95833	.38390	.38333	.36657	.38333
23	1.00000	1.04167	.41724	.41667	.39985	.41667
24	1.00000	1.12500	.45057	.45000	.43305	.45000
25	1.00000	1.20833	.48390	.48333	.46618	.48333
26	1.00000	1.29167	.51722	.51667	.49923	.51667
27	1.00000	1.37500	.55053	.55000	.53220	.55000
28	1.00000	1.45833	.58383	.58333	.56505	.58333
29	1.00000	1.54167	.61710	.61667	.59777	.61667
30	1.00000	1.62500	.65035	.65000	.63026	.65000
31	1.00000	1.70833	.68355	.68333	.66227	.68333

Table 8 (cont'd.)

32	1.00000	1.79167	.71669	.71667	.69246	.71667
33	1.00000	1.87500	.74970	.75000	.71451	.75000
34	1.00000	1.95833	.78223	.78333	.71602	.78333
35	.94444	2.00000	.80016	.80000	.76016	.80000
36	.83333	2.00000	.80096	.80000	.76540	.80000
37	.72222	2.00000	.80115	.80000	.76775	.80000
38	.61111	2.00000	.80120	.80000	.76837	.80000
39	.50000	2.00000	.80116	.80000	.76879	.80000
40	.38889	2.00000	.80106	.80000	.76899	.80000
41	.27778	2.00000	.80088	.80000	.76822	.80000
42	.16667	2.00000	.80054	.80000	.76479	.80000
43	.05556	2.00000	.79916	.80000	.81089	.80000
44	0.00000	1.94444	.77607	.77778	.77810	.77778
45	0.00000	1.83333	.73259	.73334	.72948	.73333
46	0.00000	1.72222	.68852	.68889	.67976	.68889
47	0.00000	1.61111	.64429	.64445	.63330	.64444
48	0.00000	1.50000	.59998	.60000	.58801	.60000
49	0.00000	1.38889	.55563	.55556	.54319	.55556
50	0.00000	1.27778	.51126	.51111	.49872	.51111
51	0.00000	1.16667	.46687	.46667	.45473	.46667
52	0.00000	1.05556	.42247	.42222	.41294	.42222
53	0.00000	.95833	.38362	.38333	.36846	.38333
54	0.00000	.87500	.35031	.35000	.34443	.35000
55	0.00000	.79167	.31701	.31667	.30231	.31667
56	0.00000	.70833	.28370	.28333	.26954	.28333
57	0.00000	.62500	.25040	.25000	.23668	.25000
58	0.00000	.54167	.21709	.21667	.20383	.21667
59	0.00000	.45833	.18379	.18333	.17105	.18333
60	0.00000	.37500	.15049	.15000	.13840	.15000
61	0.00000	.29167	.11719	.11667	.10594	.11667
62	0.00000	.20833	.08391	.08333	.04068	.08333
63	0.00000	.12500	.05067	.05000	.04905	.05000

Table 9. Pure Extension - 63 Nodes: X - Traction

X-TRACTIONS

NO	X	Y	TXA	TXB	TXC	EXACT
1	0.00000	.04167	-.00253	.00000	-.09736	0.00000
2	.05556	0.00000	0.00000	0.00000	0.00000	0.00000
3	.16667	0.00000	0.00000	0.00000	0.00000	0.00000
4	.27778	0.00000	0.00000	0.00000	0.00000	0.00000
5	.38889	0.00000	0.00000	0.00000	0.00000	0.00000
6	.50000	0.00000	0.00000	0.00000	0.00000	0.00000
7	.61111	0.00000	0.00000	0.00000	0.00000	0.00000
8	.72222	0.00000	0.00000	0.00000	0.00000	0.00000
9	.83333	0.00000	0.00000	0.00000	0.00000	0.00000
10	.94444	0.00000	0.00000	0.00000	0.00000	0.00000
11	1.00000	.04167	0.00000	0.00000	0.00000	0.00000
12	1.00000	.12500	0.00000	0.00000	0.00000	0.00000
13	1.00000	.20833	0.00000	0.00000	0.00000	0.00000

Table 9 (cont'd.)

14	1.00000	.29167	0.00000	0.00000	0.00000	0.00000
15	1.00000	.37500	0.00000	0.00000	0.00000	0.00000
16	1.00000	.45833	0.00000	0.00000	0.00000	0.00000
17	1.00000	.54167	0.00000	0.00000	0.00000	0.00000
18	1.00000	.62500	0.00000	0.00000	0.00000	0.00000
19	1.00000	.70833	0.00000	0.00000	0.00000	0.00000
20	1.00000	.79167	0.00000	0.00000	0.00000	0.00000
21	1.00000	.87500	0.00000	0.00000	0.00000	0.00000
22	1.00000	.95833	0.00000	0.00000	0.00000	0.00000
23	1.00000	1.04167	0.00000	0.00000	0.00000	0.00000
24	1.00000	1.12500	0.00000	0.00000	0.00000	0.00000
25	1.00000	1.20833	0.00000	0.00000	0.00000	0.00000
26	1.00000	1.29167	0.00000	0.00000	0.00000	0.00000
27	1.00000	1.37500	0.00000	0.00000	0.00000	0.00000
28	1.00000	1.45833	0.00000	0.00000	0.00000	0.00000
29	1.00000	1.54167	0.00000	0.00000	0.00000	0.00000
30	1.00000	1.62500	0.00000	0.00000	0.00000	0.00000
31	1.00000	1.70833	0.00000	0.00000	0.00000	0.00000
32	1.00000	1.79167	0.00000	0.00000	0.00000	0.00000
33	1.00000	1.87500	0.00000	0.00000	0.00000	0.00000
34	1.00000	1.95833	0.00000	0.00000	0.00000	0.00000
35	.94444	2.00000	0.00000	0.00000	0.00000	0.00000
36	.83333	2.00000	0.00000	0.00000	0.00000	0.00000
37	.72222	2.00000	0.00000	0.00000	0.00000	0.00000
38	.61111	2.00000	0.00000	0.00000	0.00000	0.00000
39	.50000	2.00000	0.00000	0.00000	0.00000	0.00000
40	.38889	2.00000	0.00000	0.00000	0.00000	0.00000
41	.27778	2.00000	0.00000	0.00000	0.00000	0.00000
42	.16667	2.00000	0.00000	0.00000	0.00000	0.00000
43	.05556	2.00000	0.00000	0.00000	0.00000	0.00000
44	0.00000	1.94444	-.00055	.00000	-.32752	0.00000
45	0.00000	1.83333	-.00387	.00000	-.00196	0.00000
46	0.00000	1.72222	-.00280	-.00001	.06990	0.00000
47	0.00000	1.61111	-.00227	.00002	.03961	0.00000
48	0.00000	1.50000	-.00194	-.00001	.00949	0.00000
49	0.00000	1.38889	-.00188	.00001	-.00142	0.00000
50	0.00000	1.27778	-.00220	.00000	-.00271	0.00000
51	0.00000	1.16667	-.00227	.00000	.00460	0.00000
52	0.00000	1.05556	-.01993	.00000	-.02681	0.00000
53	0.00000	.95833	.02456	.00000	-.04560	0.00000
54	0.00000	.87500	.00163	.00000	-.03089	0.00000
55	0.00000	.79167	.00148	.00002	.03702	0.00000
56	0.00000	.70833	.00080	-.00002	.01685	0.00000
57	0.00000	.62500	.00041	.00002	-.00200	0.00000
58	0.00000	.54167	.00009	-.00002	-.00897	0.00000
59	0.00000	.45833	-.00020	.00002	-.00738	0.00000
60	0.00000	.37500	-.00052	-.00001	-.02542	0.00000
61	0.00000	.29167	-.00091	.00001	.10233	0.00000
62	0.00000	.20833	-.00136	-.00001	.09651	0.00000
63	0.00000	.12500	-.00420	.00000	-.22024	0.00000

Table 10. Pure Extension - 63 Nodes: Y - Traction

Y-TRACTIONS

NO	X	Y	TYA	TYB	TYC	EXACT
1	0.00000	.04167	0.00000	0.00000	0.00000	0.00000
2	.05556	0.00000	-1.00852	-.99999	-.92313	-1.00000
3	.16667	0.00000	-.99576	-1.00002	-1.05889	-1.00000
4	.27778	0.00000	-.99784	-.99997	-1.05179	-1.00000
5	.38889	0.00000	-.99804	-1.00003	-1.02182	-1.00000
6	.50000	0.00000	-.99820	-.99999	-1.00505	-1.00000
7	.61111	0.00000	-.99823	-1.00000	-.99108	-1.00000
8	.72222	0.00000	-.99818	-.99999	-.98759	-1.00000
9	.83333	0.00000	-.99608	-1.00001	-.72985	-1.00000
10	.94444	0.00000	-1.01001	-1.00000	-1.51632	-1.00000
11	1.00000	.04167	0.00000	0.00000	0.00000	0.00000
12	1.00000	.12500	0.00000	0.00000	0.00000	0.00000
13	1.00000	.20833	0.00000	0.00000	0.00000	0.00000
14	1.00000	.29167	0.00000	0.00000	0.00000	0.00000
15	1.00000	.37500	0.00000	0.00000	0.00000	0.00000
16	1.00000	.45833	0.00000	0.00000	0.00000	0.00000
17	1.00000	.54167	0.00000	0.00000	0.00000	0.00000
18	1.00000	.62500	0.00000	0.00000	0.00000	0.00000
19	1.00000	.70833	0.00000	0.00000	0.00000	0.00000
20	1.00000	.79167	0.00000	0.00000	0.00000	0.00000
21	1.00000	.87500	0.00000	0.00000	0.00000	0.00000
22	1.00000	.95833	0.00000	0.00000	0.00000	0.00000
23	1.00000	1.04167	0.00000	0.00000	0.00000	0.00000
24	1.00000	1.12500	0.00000	0.00000	0.00000	0.00000
25	1.00000	1.20833	0.00000	0.00000	0.00000	0.00000
26	1.00000	1.29167	0.00000	0.00000	0.00000	0.00000
27	1.00000	1.37500	0.00000	0.00000	0.00000	0.00000
28	1.00000	1.45833	0.00000	0.00000	0.00000	0.00000
29	1.00000	1.54167	0.00000	0.00000	0.00000	0.00000
30	1.00000	1.62500	0.00000	0.00000	0.00000	0.00000
31	1.00000	1.70833	0.00000	0.00000	0.00000	0.00000
32	1.00000	1.79167	0.00000	0.00000	0.00000	0.00000
33	1.00000	1.87500	0.00000	0.00000	0.00000	0.00000
34	1.00000	1.95833	0.00000	0.00000	0.00000	0.00000
35	.94444	2.00000	1.00000	1.00000	1.00000	1.00000
36	.83333	2.00000	1.00000	1.00000	1.00000	1.00000
37	.72222	2.00000	1.00000	1.00000	1.00000	1.00000
38	.61111	2.00000	1.00000	1.00000	1.00000	1.00000
39	.50000	2.00000	1.00000	1.00000	1.00000	1.00000
40	.38889	2.00000	1.00000	1.00000	1.00000	1.00000
41	.27778	2.00000	1.00000	1.00000	1.00000	1.00000
42	.16667	2.00000	1.00000	1.00000	1.00000	1.00000
43	.05556	2.00000	1.00000	1.00000	1.00000	1.00000
44	0.00000	1.94444	0.00000	0.00000	0.00000	0.00000
45	0.00000	1.83333	0.00000	0.00000	0.00000	0.00000
46	0.00000	1.72222	0.00000	0.00000	0.00000	0.00000
47	0.00000	1.61111	0.00000	0.00000	0.00000	0.00000
48	0.00000	1.50000	0.00000	0.00000	0.00000	0.00000
49	0.00000	1.38889	0.00000	0.00000	0.00000	0.00000

Table 10 (cont'd.)

50	0.00000	1.27778	0.00000	0.00000	0.00000	0.00000
51	0.00000	1.16667	0.00000	0.00000	0.00000	0.00000
52	0.00000	1.05556	0.00000	0.00000	0.00000	0.00000
53	0.00000	.95833	0.00000	0.00000	0.00000	0.00000
54	0.00000	.87500	0.00000	0.00000	0.00000	0.00000
55	0.00000	.79167	0.00000	0.00000	0.00000	0.00000
56	0.00000	.70833	0.00000	0.00000	0.00000	0.00000
57	0.00000	.62500	0.00000	0.00000	0.00000	0.00000
58	0.00000	.54167	0.00000	0.00000	0.00000	0.00000
59	0.00000	.45833	0.00000	0.00000	0.00000	0.00000
60	0.00000	.37500	0.00000	0.00000	0.00000	0.00000
61	0.00000	.29167	0.00000	0.00000	0.00000	0.00000
62	0.00000	.20833	0.00000	0.00000	0.00000	0.00000
63	0.00000	.12500	0.00000	0.00000	0.00000	0.00000

Table 11. Pure Extension - 63 Nodes: Interior Values

INTERIOR X-DISP

NO	X	Y	UXA	UXB	UXC	EXACT
1	.25000	.50000	-.02651	-.02500	-.02447	-.02500
2	.25000	1.00000	-.02668	-.02500	-.02551	-.02500
3	.25000	1.50000	-.02686	-.02500	-.02491	-.02500
4	.50000	.50000	-.05167	-.05000	-.04911	-.05000
5	.50000	1.00000	-.05179	-.05000	-.04945	-.05000
6	.50000	1.50000	-.05204	-.05000	-.04929	-.05000
7	.75000	.50000	-.07682	-.07500	-.07360	-.07500
8	.75000	1.00000	-.07689	-.07500	-.07376	-.07500
9	.75000	1.50000	-.07726	-.07500	-.07422	-.07500

INTERIOR Y-DISP

NO	X	Y	UYA	UYB	UYC	EXACT
1	.25000	.50000	.20044	.20000	.18762	.20000
2	.25000	1.00000	.40041	.40000	.38628	.40000
3	.25000	1.50000	.60018	.60000	.58542	.60000
4	.50000	.50000	.20046	.20000	.18645	.20000
5	.50000	1.00000	.40043	.40000	.38477	.40000
6	.50000	1.50000	.60041	.60000	.58321	.60000
7	.75000	.50000	.20052	.20000	.18472	.20000
8	.75000	1.00000	.40049	.40000	.38359	.40000
9	.75000	1.50000	.60043	.60000	.58149	.60000

INTERIOR SXX

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	-.00166	.00000	.00296	0.00000
2	.25000	1.00000	-.00128	.00000	.01982	0.00000
3	.25000	1.50000	-.00140	.00000	.01597	0.00000
4	.50000	.50000	-.00161	.00000	.00258	0.00000
5	.50000	1.00000	-.00127	.00000	.00792	0.00000

Table 11 (cont'd.)

6	.50000	1.50000	-.00214	.00000	.00068	0.00000
7	.75000	.50000	-.00145	.00000	.00737	0.00000
8	.75000	1.00000	-.00107	.00000	.00631	0.00000
9	.75000	1.50000	-.00193	.00000	.00033	0.00000

INTERIOR SXY

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	-.00011	.00000	-.00569	0.00000
2	.25000	1.00000	-.00044	.00000	-.01226	0.00000
3	.25000	1.50000	.00114	.00000	-.00895	0.00000
4	.50000	.50000	.00009	.00000	-.00481	0.00000
5	.50000	1.00000	-.00025	.00000	-.00663	0.00000
6	.50000	1.50000	.00001	.00000	-.00678	0.00000
7	.75000	.50000	.00039	.00000	-.00607	0.00000
8	.75000	1.00000	-.00017	.00000	-.00480	0.00000
9	.75000	1.50000	-.00110	.00000	-.00648	0.00000

INTERIOR SYI

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	.99946	1.00000	.98993	1.00000
2	.25000	1.00000	.99902	1.00000	.99072	1.00000
3	.25000	1.50000	.99873	1.00000	.98517	1.00000
4	.50000	.50000	.99978	1.00000	.99343	1.00000
5	.50000	1.00000	.99928	1.00000	.99285	1.00000
6	.50000	1.50000	1.00025	1.00000	.99240	1.00000
7	.75000	.50000	.99960	1.00000	.99394	1.00000
8	.75000	1.00000	.99942	1.00000	.99454	1.00000
9	.75000	1.50000	.99949	1.00000	.98585	1.00000

Table 12. Pure Extension - 63 Nodes: Percent Differences

X-DISPLACEMENTS

NO	A	B	C
2	-41.21	.00	-185.61
3	-10.93	.00	-62.30
4	-6.20	.00	-8.53
5	-4.26	.00	-1.64
6	-3.22	.00	.34
7	-2.56	.00	1.53
8	-2.11	.00	3.42
9	-1.74	.00	9.54
10	-1.06	.00	41.32
11	-3.37	.00	28.55
12	-3.49	.00	-8.64
13	-3.43	.00	-2.99
14	-3.38	.00	.37
15	-3.35	.00	1.63
16	-3.32	.00	2.13

Table 12 (cont'd.)

17	-3.30	.00	2.31
18	-3.29	.00	2.33
19	-3.29	.00	2.27
20	-3.30	.00	2.17
21	-3.31	.00	2.04
22	-3.34	.00	1.91
23	-3.38	.00	1.79
24	-3.42	.00	1.69
25	-3.48	.00	1.59
26	-3.55	.00	1.51
27	-3.62	.00	1.42
28	-3.70	.00	1.31
29	-3.79	.00	1.16
30	-3.88	.00	.89
31	-3.95	.00	.29
32	-4.00	.00	-1.04
33	-3.98	.00	-.75
34	-3.67	.00	28.22
35	-1.32	.00	35.57
36	-2.11	.00	13.22
37	-2.75	.00	8.58
38	-3.52	.00	6.55
39	-4.60	.00	5.08
40	-6.30	.00	2.73
41	-9.43	.00	-3.23
42	-17.12	.00	.26
43	-66.85	.00	257.77

Y-DISPLACEMENTS

NO	A	B	C
1	-7.37	.00	-290.90
11	-7.80	.00	-333.39
12	-1.48	.00	20.16
13	-.77	.00	25.49
14	-.51	.00	17.91
15	-.38	.00	13.16
16	-.31	.00	10.25
17	-.26	.00	8.35
18	-.22	.00	7.02
19	-.20	.00	6.06
20	-.18	.00	5.35
21	-.16	.00	4.80
22	-.15	.00	4.37
23	-.14	.00	4.04
24	-.13	.00	3.77
25	-.12	.00	3.55
26	-.11	.00	3.37
27	-.10	.00	3.24
28	-.08	.00	3.13
29	-.07	.00	3.06
30	-.05	.00	3.04

Table 12 (cont'd.)

31	-.03	.00	3.08
32	.00	.00	3.38
33	.04	.00	4.73
34	.14	.00	8.59
35	-.02	.00	4.98
36	-.12	.00	4.33
37	-.14	.00	4.03
38	-.15	.00	3.95
39	-.15	.00	3.90
40	-.13	.00	3.88
41	-.11	.00	3.97
42	-.07	.00	4.40
43	.10	.00	-1.36
44	.22	.00	-.04
45	.10	.00	.53
46	.05	.00	1.32
47	.02	.00	1.73
48	.00	.00	2.00
49	-.01	.00	2.23
50	-.03	.00	2.42
51	-.04	.00	2.56
52	-.06	.00	2.20
53	-.07	.00	3.88
54	-.09	.00	1.59
55	-.11	.00	4.53
56	-.13	.00	4.87
57	-.16	.00	5.33
58	-.20	.00	5.92
59	-.25	.00	6.70
60	-.32	.00	7.73
61	-.45	.00	9.19
62	-.69	.00	51.19
63	-1.34	.00	1.90

Y-TRACTIONS

NO	A	B	C
2	-.85	.00	7.69
3	.42	.00	-5.89
4	.22	.00	-5.18
5	.20	.00	-2.18
6	.18	.00	-.51
7	.18	.00	.89
8	.18	.00	1.24
9	.39	.00	27.02
10	-1.00	.00	-51.63

INTERIOR X-DISP

NO	A	B	C
1	-6.04	.00	2.11
2	-6.74	.00	-2.02

Table 12 (cont'd.)

3	-7.46	.00	.36
4	-3.33	.00	1.78
5	-3.58	.00	1.11
6	-4.08	.00	1.42
7	-2.42	.00	1.86
8	-2.53	.00	1.66
9	-3.01	.00	1.04

INTERIOR Y-DISP

NO	A	B	C
1	-.22	.00	6.19
2	-.10	.00	3.43
3	-.03	.00	2.43
4	-.23	.00	6.78
5	-.11	.00	3.81
6	-.07	.00	2.80
7	-.26	.00	7.64
8	-.12	.00	4.10
9	-.07	.00	3.09

INTERIOR SY

NO	A	B	C
1	.05	.00	1.01
2	.10	.00	.93
3	.13	.00	1.48
4	.02	.00	.66
5	.07	.00	.72
6	-.03	.00	.76
7	.04	.00	.61
8	.06	.00	.55
9	.05	.00	1.42

Table 13. Square - 21 Nodes: X - Displacements

X-DISPLACEMENTS

NO	X	Y	UXA	UXB	UXC	EXACT
1	0.00000	.08333	0.00000	0.00000	0.00000	0.00000
2	.10000	0.00000	.16661	.15998	.12491	.15997
3	.30000	0.00000	.48854	.47872	.42453	.47910
4	.50000	0.00000	.81024	.79528	.75824	.79583
5	.70000	0.00000	1.12711	1.10769	1.10029	1.10857
6	.90000	0.00000	1.43617	1.41354	1.47046	1.41570
7	1.00000	.10000	1.57028	1.55964	1.65303	1.55892
8	1.00000	.30000	1.56760	1.55867	1.42869	1.55692
9	1.00000	.50000	1.57974	1.57500	1.44284	1.57292
10	1.00000	.70000	1.60466	1.60855	1.43724	1.60692
11	1.00000	.90000	1.62674	1.65723	1.37350	1.65892
12	.90000	1.00000	1.47094	1.52260	1.05197	1.52820

Table 13 (cont'd.)

13	.70000	1.00000	1.16171	1.19346	1.02668	1.19607
14	.50000	1.00000	.83687	.85689	.77929	.85833
15	.30000	1.00000	.50457	.51575	.49220	.51660
16	.10000	1.00000	.17078	.17233	.16281	.17247
17	0.00000	.91667	0.00000	0.00000	0.00000	0.00000
18	0.00000	.75000	0.00000	0.00000	0.00000	0.00000
19	0.00000	.58333	0.00000	0.00000	0.00000	0.00000
20	0.00000	.41667	0.00000	0.00000	0.00000	0.00000
21	0.00000	.25000	0.00000	0.00000	0.00000	0.00000

Table 14. Square - 21 Nodes: Y - Displacements

Y-DISPLACEMENTS

NO	X	Y	UYA	UYB	UYC	EXACT
1	0.00000	.08333	-.06238	-.02709	-.03212	-.03197
2	.10000	0.00000	-.00450	-.00450	-.00450	-.00450
3	.30000	0.00000	-.04050	-.04050	-.04050	-.04050
4	.50000	0.00000	-.11250	-.11250	-.11250	-.11250
5	.70000	0.00000	-.22050	-.22050	-.22050	-.22050
6	.90000	0.00000	-.36450	-.36450	-.36450	-.36450
7	1.00000	.10000	-.49160	-.48032	-.43473	-.48555
8	1.00000	.30000	-.55198	-.54201	-.46370	-.54585
9	1.00000	.50000	-.59429	-.59006	-.50192	-.59375
10	1.00000	.70000	-.62192	-.62775	-.48306	-.63165
11	1.00000	.90000	-.62797	-.65726	-.40117	-.66195
12	.90000	1.00000	-.61124	-.59490	-.40115	-.59425
13	.70000	1.00000	-.49212	-.46004	-.50421	-.45825
14	.50000	1.00000	-.39729	-.35799	-.41121	-.35625
15	.30000	1.00000	-.33432	-.29000	-.34075	-.28825
16	.10000	1.00000	-.30638	-.25592	-.36235	-.25425
17	0.00000	.91667	-.26109	-.23466	-.36142	-.23712
18	0.00000	.75000	-.23952	-.20654	-.24584	-.20859
19	0.00000	.58333	-.20439	-.17272	-.21656	-.17520
20	0.00000	.41667	-.16231	-.13256	-.16971	-.13556
21	0.00000	.25000	-.11245	-.08471	-.13878	-.08828

Table 15. Square - 21 Nodes: X - Traction

X-TRACTIONS

NO	X	Y	TXA	TXB	TXC	EXACT
1	0.00000	.08333	-4.13240	-4.01886	-3.30061	-4.00347
2	.10000	0.00000	.10000	.10000	.10000	.10000
3	.30000	0.00000	.30000	.30000	.30000	.30000
4	.50000	0.00000	.50000	.50000	.50000	.50000
5	.70000	0.00000	.70000	.70000	.70000	.70000
6	.90000	0.00000	.90000	.90000	.90000	.90000
7	1.00000	.10000	3.75500	3.75500	3.75500	3.75500
8	1.00000	.30000	3.79500	3.79500	3.79500	3.79500

Table 15 (cont'd.)

9	1.00000	.50000	3.87500	3.87500	3.87500	3.87500
10	1.00000	.70000	3.99500	3.99500	3.99500	3.99500
11	1.00000	.90000	4.15500	4.15500	4.15500	4.15500
12	.90000	1.00000	-.45000	-.45000	-.45000	-.45000
13	.70000	1.00000	-.35000	-.35000	-.35000	-.35000
14	.50000	1.00000	-.25000	-.25000	-.25000	-.25000
15	.30000	1.00000	-.15000	-.15000	-.15000	-.15000
16	.10000	1.00000	-.05000	-.05000	-.05000	-.05000
17	0.00000	.91667	-4.47629	-4.44779	-1.86205	-4.42014
18	0.00000	.75000	-4.18303	-4.24155	-5.08293	-4.28125
19	0.00000	.58333	-4.13571	-4.18825	-4.50472	-4.17014
20	0.00000	.41667	-4.07330	-4.07308	-3.96936	-4.08681
21	0.00000	.25000	-3.99275	-4.02877	-5.90831	-4.03125

Table 16. Square - 21 Nodes: Y - Traction

Y-TRACTIONS

NO	X	Y	TYA	TYB	TYC	EXACT
1	0.00000	.08333	0.00000	0.00000	0.00000	0.00000
2	.10000	0.00000	.00965	.01257	-.40149	0.00000
3	.30000	0.00000	.03890	.00244	.28765	0.00000
4	.50000	0.00000	.02188	.01382	.27392	0.00000
5	.70000	0.00000	-.00711	-.00094	.11283	0.00000
6	.90000	0.00000	-.12226	.00752	-.43576	0.00000
7	1.00000	.10000	-.95000	-.95000	-.95000	-.95000
8	1.00000	.30000	-.85000	-.85000	-.85000	-.85000
9	1.00000	.50000	-.75000	-.75000	-.75000	-.75000
10	1.00000	.70000	-.65000	-.65000	-.65000	-.65000
11	1.00000	.90000	-.55000	-.55000	-.55000	-.55000
12	.90000	1.00000	.75000	.75000	.75000	.75000
13	.70000	1.00000	.75000	.75000	.75000	.75000
14	.50000	1.00000	.75000	.75000	.75000	.75000
15	.30000	1.00000	.75000	.75000	.75000	.75000
16	.10000	1.00000	.75000	.75000	.75000	.75000
17	0.00000	.91667	0.00000	0.00000	0.00000	0.00000
18	0.00000	.75000	0.00000	0.00000	0.00000	0.00000
19	0.00000	.58333	0.00000	0.00000	0.00000	0.00000
20	0.00000	.41667	0.00000	0.00000	0.00000	0.00000
21	0.00000	.25000	0.00000	0.00000	0.00000	0.00000

Table 17. Square - 21 Nodes: Interior Values

INTERIOR X-DISP

NO	X	Y	UXA	UXB	UXC	EXACT
1	.25000	.50000	.40295	.40096	.46337	.40104
2	.50000	.50000	.80191	.79890	.74203	.79896
3	.75000	.50000	1.19548	1.19084	1.02113	1.19062

Table 17 (cont'd.)

4	.50000	.75000	.81498	.82104	.76488	.82161
5	.50000	.25000	.79826	.79032	.72923	.79036

INTERIOR Y-DISP

NO	X	Y	UYA	UYB	UYC	EXACT
1	.25000	.50000	-.21033	-.18155	-.23262	-.18359
2	.50000	.50000	-.28775	-.26358	-.30050	-.26563
3	.75000	.50000	-.41491	-.39997	-.39314	-.40234
4	.50000	.75000	-.34319	-.31498	-.35766	-.31641
5	.50000	.25000	-.21685	-.19660	-.22326	-.19922

INTERIOR SXX

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	4.10227	4.10770	3.91982	4.10938
2	.50000	.50000	4.06440	4.06207	4.04759	4.06250
3	.75000	.50000	4.00304	3.98706	4.05478	3.98438
4	.50000	.75000	4.17205	4.21496	3.72216	4.21875
5	.50000	.25000	3.98660	3.96764	4.00292	3.96875

INTERIOR SXY

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	-.19181	-.18875	-.15594	-.18750
2	.50000	.50000	-.37550	-.37543	-.34196	-.37500
3	.75000	.50000	-.54214	-.56115	-.44944	-.56250
4	.50000	.75000	-.33247	-.31565	-.28413	-.31250
5	.50000	.25000	-.43381	-.43622	-.59197	-.43750

INTERIOR SYX

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	.37973	.43102	.41555	.43750
2	.50000	.50000	.38910	.43100	.26430	.43750
3	.75000	.50000	.42416	.43216	.34010	.43750
4	.50000	.75000	.55615	.60311	.68714	.60938
5	.50000	.25000	.19261	.22925	.31365	.23438

Table 18. Square - 21 Nodes: Percent Differences

X-DISPLACEMENTS

NO	A	B	C
2	-4.15	-.01	21.92
3	-1.99	.08	11.39
4	-1.81	.07	4.72
5	-1.67	.08	.75
6	-1.45	.15	-3.87
7	-.73	-.05	-6.04
8	-.69	-.11	8.24

Table 18 (cont'd.)

9	-.43	-.13	8.27
10	.14	-.10	10.56
11	1.94	.10	17.21
12	3.75	.37	31.16
13	2.87	.22	14.16
14	2.50	.17	9.21
15	2.33	.16	4.72
16	.98	.08	5.60

Y-DISPLACEMENTS

NO	A	B	C
1	-95.10	15.27	-.45
7	-1.25	1.08	10.47
8	-1.12	.70	15.05
9	-.09	.62	15.47
10	1.54	.62	23.52
11	5.13	.71	39.40
12	-2.86	-.11	32.50
13	-7.39	-.39	-10.03
14	-11.52	-.49	-15.43
15	-15.98	-.61	-18.21
16	-20.50	-.66	-42.52
17	-10.11	1.04	-52.42
18	-14.83	.98	-17.85
19	-16.66	1.42	-23.61
20	-19.73	2.21	-25.19
21	-27.38	4.04	-57.20

X-TRACTIONS

NO	A	B	C
1	-3.22	-.38	17.56
17	-1.27	-.63	57.87
18	2.29	.93	-18.73
19	.83	-.43	-8.02
20	.33	.34	2.87
21	.95	.06	-46.56

INTERIOR X-DISP

NO	A	B	C
1	-.48	.02	-15.54
2	-.37	.01	7.13
3	-.41	-.02	14.24
4	.81	.07	6.90
5	-1.00	.01	7.73

INTERIOR Y-DISP

NO	A	B	C
1	-14.56	1.11	-26.70

Table 18 (cont'd.)

2	-8.33	.77	-13.13
3	-3.12	.59	2.29
4	-8.47	.45	-13.04
5	-8.85	1.31	-12.07

INTERIOR SXX

NO	A	B	C
1	.17	.04	4.61
2	-.05	.01	.37
3	-.47	-.07	-1.77
4	1.11	.09	11.77
5	-.45	.03	-.86

INTERIOR SXY

NO	A	B	C
1	-2.30	-.67	16.83
2	-.13	-.11	8.81
3	3.62	.24	20.10
4	-6.39	-1.01	9.08
5	.84	.29	-35.31

INTERIOR SYX

NO	A	B	C
1	13.21	1.48	5.02
2	11.06	1.49	39.59
3	3.05	1.22	22.26
4	8.73	1.03	-12.76
5	17.82	2.19	-33.82

Table 19. Square - 63 Nodes: X - Displacements

X-DISPLACEMENTS

NO	X	Y	UXA	UXB	UXC	EXACT
1	0.00000	.02778	0.00000	0.00000	0.00000	0.00000
2	.03333	0.00000	.05511	.05332	.00493	.05333
3	.10000	0.00000	.16156	.15993	.10622	.15997
4	.16667	0.00000	.26859	.26648	.21864	.26651
5	.23333	0.00000	.37552	.37287	.32572	.37291
6	.30000	0.00000	.48225	.47906	.43269	.47910
7	.36667	0.00000	.58869	.58497	.53930	.58502
8	.43333	0.00000	.69480	.69056	.64551	.69062
9	.50000	0.00000	.80049	.79577	.75136	.79583
10	.56667	0.00000	.90570	.90052	.85691	.90060
11	.63333	0.00000	1.01036	1.00477	.96229	1.00487
12	.70000	0.00000	1.11439	1.10846	1.06778	1.10857
13	.76667	0.00000	1.21772	1.21151	1.17407	1.21165
14	.83333	0.00000	1.32029	1.31387	1.28300	1.31404

Table 19 (cont'd.)

15	.90000	0.00000	1.42203	1.41548	1.40058	1.41570
16	.96667	0.00000	1.52258	1.51619	1.53791	1.51656
17	1.00000	.03333	1.56699	1.56354	1.59452	1.56358
18	1.00000	.10000	1.56300	1.55899	1.47722	1.55892
19	1.00000	.16667	1.56058	1.55640	1.47243	1.55625
20	1.00000	.23333	1.55991	1.55577	1.47058	1.55558
21	1.00000	.30000	1.56106	1.55713	1.47129	1.55692
22	1.00000	.36667	1.56409	1.56048	1.47415	1.56025
23	1.00000	.43333	1.56901	1.56582	1.47882	1.56558
24	1.00000	.50000	1.57580	1.57316	1.48506	1.57292
25	1.00000	.56667	1.58445	1.58248	1.49268	1.58225
26	1.00000	.63333	1.59491	1.59381	1.50141	1.59358
27	1.00000	.70000	1.60711	1.60712	1.51085	1.60692
28	1.00000	.76667	1.62093	1.62243	1.52022	1.62225
29	1.00000	.83333	1.63609	1.63971	1.52695	1.63958
30	1.00000	.90000	1.65191	1.65893	1.51862	1.65892
31	1.00000	.96667	1.66326	1.67983	1.45536	1.68025
32	.96667	1.00000	1.61185	1.63651	1.32756	1.63739
33	.90000	1.00000	1.50966	1.52768	1.38275	1.52820
34	.83333	1.00000	1.40348	1.41785	1.31287	1.41821
35	.76667	1.00000	1.29534	1.30720	1.21982	1.30748
36	.70000	1.00000	1.18590	1.19585	1.12010	1.19607
37	.63333	1.00000	1.07546	1.08386	1.01687	1.08403
38	.56667	1.00000	.96419	.97129	.91144	.97143
39	.50000	1.00000	.85224	.85821	.80462	.85833
40	.43333	1.00000	.73971	.74469	.69699	.74479
41	.36667	1.00000	.62670	.63078	.58906	.63086
42	.30000	1.00000	.51328	.51653	.48153	.51660
43	.23333	1.00000	.39953	.40202	.37541	.40208
44	.16667	1.00000	.28553	.28730	.27219	.28735
45	.10000	1.00000	.17138	.17243	.16830	.17247
46	.03333	1.00000	.05782	.05749	.03847	.05750
47	0.00000	.97222	0.00000	0.00000	0.00000	0.00000
48	0.00000	.91667	0.00000	0.00000	0.00000	0.00000
49	0.00000	.86111	0.00000	0.00000	0.00000	0.00000
50	0.00000	.80556	0.00000	0.00000	0.00000	0.00000
51	0.00000	.75000	0.00000	0.00000	0.00000	0.00000
52	0.00000	.69444	0.00000	0.00000	0.00000	0.00000
53	0.00000	.63889	0.00000	0.00000	0.00000	0.00000
54	0.00000	.58333	0.00000	0.00000	0.00000	0.00000
55	0.00000	.52778	0.00000	0.00000	0.00000	0.00000
56	0.00000	.47222	0.00000	0.00000	0.00000	0.00000
57	0.00000	.41667	0.00000	0.00000	0.00000	0.00000
58	0.00000	.36111	0.00000	0.00000	0.00000	0.00000
59	0.00000	.30556	0.00000	0.00000	0.00000	0.00000
60	0.00000	.25000	0.00000	0.00000	0.00000	0.00000
61	0.00000	.19444	0.00000	0.00000	0.00000	0.00000
62	0.00000	.13889	0.00000	0.00000	0.00000	0.00000
63	0.00000	.08333	0.00000	0.00000	0.00000	0.00000

Table 20. Square - 63 Nodes: Y - Displacements

Y-DISPLACEMENTS

NO	X	Y	UYA	UYB	UYC	EXACT
1	0.00000	.02778	-.02059	-.01039	.00194	-.01096
2	.03333	0.00000	-.00050	-.00050	-.00050	-.00050
3	.10000	0.00000	-.00450	-.00450	-.00450	-.00450
4	.16667	0.00000	-.01250	-.01250	-.01250	-.01250
5	.23333	0.00000	-.02450	-.02450	-.02450	-.02450
6	.30000	0.00000	-.04050	-.04050	-.04050	-.04050
7	.36667	0.00000	-.06050	-.06050	-.06050	-.06050
8	.43333	0.00000	-.08450	-.08450	-.08450	-.08450
9	.50000	0.00000	-.11250	-.11250	-.11250	-.11250
10	.56667	0.00000	-.14450	-.14450	-.14450	-.14450
11	.63333	0.00000	-.18050	-.18050	-.18050	-.18050
12	.70000	0.00000	-.22050	-.22050	-.22050	-.22050
13	.76667	0.00000	-.26450	-.26450	-.26450	-.26450
14	.83333	0.00000	-.31250	-.31250	-.31250	-.31250
15	.90000	0.00000	-.36450	-.36450	-.36450	-.36450
16	.96667	0.00000	-.42050	-.42050	-.42050	-.42050
17	1.00000	.03333	-.46505	-.46169	-.43345	-.46228
18	1.00000	.10000	-.48979	-.48510	-.44758	-.48555
19	1.00000	.16667	-.51138	-.50674	-.47872	-.50718
20	1.00000	.23333	-.53101	-.52683	-.50141	-.52725
21	1.00000	.30000	-.54904	-.54544	-.52122	-.54585
22	1.00000	.36667	-.56563	-.56268	-.53864	-.56308
23	1.00000	.43333	-.58085	-.57863	-.55390	-.57901
24	1.00000	.50000	-.59479	-.59337	-.56710	-.59375
25	1.00000	.56667	-.60751	-.60700	-.57820	-.60738
26	1.00000	.63333	-.61906	-.61961	-.58699	-.61998
27	1.00000	.70000	-.62947	-.63128	-.59291	-.63165
28	1.00000	.76667	-.63871	-.64210	-.59453	-.64248
29	1.00000	.83333	-.64665	-.65214	-.58783	-.65255
30	1.00000	.90000	-.65275	-.66148	-.56221	-.66195
31	1.00000	.96667	-.65355	-.67016	-.50541	-.67078
32	.96667	1.00000	-.64727	-.64714	-.52250	-.64714
33	.90000	1.00000	-.60051	-.59444	-.59797	-.59425
34	.83333	1.00000	-.55417	-.54536	-.55297	-.54514
35	.76667	1.00000	-.51049	-.50003	-.51040	-.49981
36	.70000	1.00000	-.47006	-.45847	-.47120	-.45825
37	.63333	1.00000	-.43311	-.42068	-.43535	-.42047
38	.56667	1.00000	-.39975	-.38668	-.40309	-.38647
39	.50000	1.00000	-.37006	-.35645	-.37460	-.35625
40	.43333	1.00000	-.34407	-.33000	-.34998	-.32981
41	.36667	1.00000	-.32181	-.30733	-.32931	-.30714
42	.30000	1.00000	-.30332	-.28844	-.31259	-.28825
43	.23333	1.00000	-.28861	-.27333	-.29958	-.27314
44	.16667	1.00000	-.27774	-.26200	-.28882	-.26181
45	.10000	1.00000	-.27085	-.25446	-.27733	-.25425
46	.03333	1.00000	-.26840	-.25068	-.31549	-.25047
47	0.00000	.97222	-.25372	-.24555	-.32345	-.24579
48	0.00000	.91667	-.24767	-.23695	-.25774	-.23712
49	0.00000	.86111	-.23845	-.22788	-.24586	-.22807

Table 20 (cont'd.)

50	0.00000	.80556	-.22876	-.21837	-.23541	-.21858
51	0.00000	.75000	-.21858	-.20837	-.22473	-.20859
52	0.00000	.69444	-.20785	-.19783	-.21357	-.19807
53	0.00000	.63889	-.19650	-.18670	-.20180	-.18696
54	0.00000	.58333	-.18450	-.17492	-.18935	-.17520
55	0.00000	.52778	-.17178	-.16245	-.17617	-.16275
56	0.00000	.47222	-.15820	-.14924	-.16222	-.14956
57	0.00000	.41667	-.14401	-.13522	-.14747	-.13556
58	0.00000	.36111	-.12887	-.12036	-.13192	-.12072
59	0.00000	.30556	-.11282	-.10460	-.11562	-.10498
60	0.00000	.25000	-.09583	-.08788	-.09867	-.08828
61	0.00000	.19444	-.07785	-.07017	-.08134	-.07058
62	0.00000	.13889	-.05885	-.05139	-.06268	-.05183
63	0.00000	.08333	-.03886	-.03151	-.04767	-.03197

Table 21. Square - 63 Nodes: X - Traction

X-TRACTIONS

NO	X	Y	TXA	TXB	TXC	EXACT
1	0.00000	.02778	-4.11647	-4.00678	-3.24222	-4.00039
2	.03333	0.00000	.03333	.03333	.03333	.03333
3	.10000	0.00000	.10000	.10000	.10000	.10000
4	.16667	0.00000	.16667	.16667	.16667	.16667
5	.23333	0.00000	.23333	.23333	.23333	.23333
6	.30000	0.00000	.30000	.30000	.30000	.30000
7	.36667	0.00000	.36667	.36667	.36667	.36667
8	.43333	0.00000	.43333	.43333	.43333	.43333
9	.50000	0.00000	.50000	.50000	.50000	.50000
10	.56667	0.00000	.56667	.56667	.56667	.56667
11	.63333	0.00000	.63333	.63333	.63333	.63333
12	.70000	0.00000	.70000	.70000	.70000	.70000
13	.76667	0.00000	.76667	.76667	.76667	.76667
14	.83333	0.00000	.83333	.83333	.83333	.83333
15	.90000	0.00000	.90000	.90000	.90000	.90000
16	.96667	0.00000	.96667	.96667	.96667	.96667
17	1.00000	.03333	3.75056	3.75056	3.75056	3.75056
18	1.00000	.10000	3.75500	3.75500	3.75500	3.75500
19	1.00000	.16667	3.76389	3.76389	3.76389	3.76389
20	1.00000	.23333	3.77722	3.77722	3.77722	3.77722
21	1.00000	.30000	3.79500	3.79500	3.79500	3.79500
22	1.00000	.36667	3.81722	3.81722	3.81722	3.81722
23	1.00000	.43333	3.84389	3.84389	3.84389	3.84389
24	1.00000	.50000	3.87500	3.87500	3.87500	3.87500
25	1.00000	.56667	3.91056	3.91056	3.91056	3.91056
26	1.00000	.63333	3.95056	3.95056	3.95056	3.95056
27	1.00000	.70000	3.99500	3.99500	3.99500	3.99500
28	1.00000	.76667	4.04389	4.04389	4.04389	4.04389
29	1.00000	.83333	4.09722	4.09722	4.09722	4.09722
30	1.00000	.90000	4.15500	4.15500	4.15500	4.15500
31	1.00000	.96667	4.21722	4.21722	4.21722	4.21722

Table 21 (cont'd.)

32	.96667	1.00000	-.48333	-.48333	-.48333	-.48333
33	.90000	1.00000	-.45000	-.45000	-.45000	-.45000
34	.83333	1.00000	-.41667	-.41667	-.41667	-.41667
35	.76667	1.00000	-.38333	-.38333	-.38333	-.38333
36	.70000	1.00000	-.35000	-.35000	-.35000	-.35000
37	.63333	1.00000	-.31667	-.31667	-.31667	-.31667
38	.56667	1.00000	-.28333	-.28333	-.28333	-.28333
39	.50000	1.00000	-.25000	-.25000	-.25000	-.25000
40	.43333	1.00000	-.21667	-.21667	-.21667	-.21667
41	.36667	1.00000	-.18333	-.18333	-.18333	-.18333
42	.30000	1.00000	-.15000	-.15000	-.15000	-.15000
43	.23333	1.00000	-.11667	-.11667	-.11667	-.11667
44	.16667	1.00000	-.08333	-.08333	-.08333	-.08333
45	.10000	1.00000	-.05000	-.05000	-.05000	-.05000
46	.03333	1.00000	-.01667	-.01667	-.01667	-.01667
47	0.00000	.97222	-4.58134	-4.48431	-.98029	-4.47261
48	0.00000	.91667	-4.35249	-4.40426	-5.11678	-4.42014
49	0.00000	.86111	-4.34655	-4.38360	-5.53915	-4.37076
50	0.00000	.80556	-4.30382	-4.31159	-4.94881	-4.32446
51	0.00000	.75000	-4.26452	-4.29182	-4.42764	-4.28125
52	0.00000	.69444	-4.22762	-4.23081	-4.18993	-4.24113
53	0.00000	.63889	-4.19348	-4.21241	-4.12636	-4.20409
54	0.00000	.58333	-4.16213	-4.16225	-4.11612	-4.17014
55	0.00000	.52778	-4.13353	-4.14524	-4.10435	-4.13927
56	0.00000	.47222	-4.10769	-4.10613	-4.08172	-4.11150
57	0.00000	.41667	-4.08454	-4.09044	-4.05309	-4.08681
58	0.00000	.36111	-4.06408	-4.06224	-4.02181	-4.06520
59	0.00000	.30556	-4.04622	-4.04791	-3.98148	-4.04668
60	0.00000	.25000	-4.03071	-4.03077	-3.93725	-4.03125
61	0.00000	.19444	-4.01726	-4.01768	-3.62106	-4.01890
62	0.00000	.13889	-4.00656	-4.01160	-3.54151	-4.00964
63	0.00000	.08333	-3.96093	-3.99992	-6.35215	-4.00347

Table 22. Square - 63 Nodes: Y - Traction

Y-TRACTIONS

NO	X	Y	TYA	TYB	TYC	EXACT
1	0.00000	.02778	0.00000	0.00000	0.00000	0.00000
2	.03333	0.00000	-.01197	.00116	-.87809	0.00000
3	.10000	0.00000	.01260	.00062	.02971	0.00000
4	.16667	0.00000	.01300	.00181	.30095	0.00000
5	.23333	0.00000	.01249	.00016	.24658	0.00000
6	.30000	0.00000	.01155	.00194	.15212	0.00000
7	.36667	0.00000	.01020	-.00017	.09823	0.00000
8	.43333	0.00000	.00839	.00206	.07835	0.00000
9	.50000	0.00000	.00611	-.00044	.07126	0.00000
10	.56667	0.00000	.00339	.00214	.06529	0.00000
11	.63333	0.00000	.00029	-.00072	.05820	0.00000
12	.70000	0.00000	-.00308	.00226	.05251	0.00000
13	.76667	0.00000	-.000650	-.00107	.05223	0.00000

Table 22 (cont'd.)

14	.83333	0.00000	-.00967	.00247	.08417	0.00000
15	.90000	0.00000	-.00986	-.00127	.06669	0.00000
16	.96667	0.00000	-.07304	.00171	-.57466	0.00000
17	1.00000	.03333	-.98333	-.98333	-.98333	-.98333
18	1.00000	.10000	-.95000	-.95000	-.95000	-.95000
19	1.00000	.16667	-.91667	-.91667	-.91667	-.91667
20	1.00000	.23333	-.88333	-.88333	-.88333	-.88333
21	1.00000	.30000	-.85000	-.85000	-.85000	-.85000
22	1.00000	.36667	-.81667	-.81667	-.81667	-.81667
23	1.00000	.43333	-.78333	-.78333	-.78333	-.78333
24	1.00000	.50000	-.75000	-.75000	-.75000	-.75000
25	1.00000	.56667	-.71667	-.71667	-.71667	-.71667
26	1.00000	.63333	-.68333	-.68333	-.68333	-.68333
27	1.00000	.70000	-.65000	-.65000	-.65000	-.65000
28	1.00000	.76667	-.61667	-.61667	-.61667	-.61667
29	1.00000	.83333	-.58333	-.58333	-.58333	-.58333
30	1.00000	.90000	-.55000	-.55000	-.55000	-.55000
31	1.00000	.96667	-.51667	-.51667	-.51667	-.51667
32	.96667	1.00000	.75000	.75000	.75000	.75000
33	.90000	1.00000	.75000	.75000	.75000	.75000
34	.83333	1.00000	.75000	.75000	.75000	.75000
35	.76667	1.00000	.75000	.75000	.75000	.75000
36	.70000	1.00000	.75000	.75000	.75000	.75000
37	.63333	1.00000	.75000	.75000	.75000	.75000
38	.56667	1.00000	.75000	.75000	.75000	.75000
39	.50000	1.00000	.75000	.75000	.75000	.75000
40	.43333	1.00000	.75000	.75000	.75000	.75000
41	.36667	1.00000	.75000	.75000	.75000	.75000
42	.30000	1.00000	.75000	.75000	.75000	.75000
43	.23333	1.00000	.75000	.75000	.75000	.75000
44	.16667	1.00000	.75000	.75000	.75000	.75000
45	.10000	1.00000	.75000	.75000	.75000	.75000
46	.03333	1.00000	.75000	.75000	.75000	.75000
47	0.00000	.97222	0.00000	0.00000	0.00000	0.00000
48	0.00000	.91667	0.00000	0.00000	0.00000	0.00000
49	0.00000	.86111	0.00000	0.00000	0.00000	0.00000
50	0.00000	.80556	0.00000	0.00000	0.00000	0.00000
51	0.00000	.75000	0.00000	0.00000	0.00000	0.00000
52	0.00000	.69444	0.00000	0.00000	0.00000	0.00000
53	0.00000	.63889	0.00000	0.00000	0.00000	0.00000
54	0.00000	.58333	0.00000	0.00000	0.00000	0.00000
55	0.00000	.52778	0.00000	0.00000	0.00000	0.00000
56	0.00000	.47222	0.00000	0.00000	0.00000	0.00000
57	0.00000	.41667	0.00000	0.00000	0.00000	0.00000
58	0.00000	.36111	0.00000	0.00000	0.00000	0.00000
59	0.00000	.30556	0.00000	0.00000	0.00000	0.00000
60	0.00000	.25000	0.00000	0.00000	0.00000	0.00000
61	0.00000	.19444	0.00000	0.00000	0.00000	0.00000
62	0.00000	.13889	0.00000	0.00000	0.00000	0.00000
63	0.00000	.08333	0.00000	0.00000	0.00000	0.00000

Table 23. Square - 63 Nodes: Interior Values

INTERIOR X-DISP

NO	X	Y	UXA	UXB	UXC	EXACT
1	.25000	.50000	.40186	.40104	.65922	.40104
2	.50000	.50000	.80031	.79896	.76110	.79896
3	.75000	.50000	1.19277	1.19065	.86015	1.19062
4	.50000	.75000	.82009	.82157	.82222	.82161
5	.50000	.25000	.79309	.79036	.70008	.79036

INTERIOR Y-DISP

NO	X	Y	UYA	UYB	UYC	EXACT
1	.25000	.50000	-.19207	-.18337	-.19715	-.18359
2	.50000	.50000	-.27281	-.26540	-.27561	-.26563
3	.75000	.50000	-.40690	-.40210	-.40024	-.40234
4	.50000	.75000	-.32509	-.31625	-.33046	-.31641
5	.50000	.25000	-.20494	-.19893	-.20476	-.19922

INTERIOR SXX

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	4.10915	4.10917	4.04201	4.10938
2	.50000	.50000	4.06554	4.06247	4.00402	4.06250
3	.75000	.50000	3.99143	3.98465	3.93337	3.98438
4	.50000	.75000	4.20651	4.21840	4.07419	4.21875
5	.50000	.25000	3.97444	3.96861	3.95307	3.96875

INTERIOR SXY

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	-.18875	-.18758	-.19350	-.18750
2	.50000	.50000	-.37560	-.37504	-.37101	-.37500
3	.75000	.50000	-.55765	-.56239	-.51642	-.56250
4	.50000	.75000	-.31989	-.31281	-.32148	-.31250
5	.50000	.25000	-.4654	-.4735	-.43464	-.43750

INTERIOR SYX

NO	X	Y	A	B	C	EXACT
1	.25000	.50000	.41995	.43683	.37092	.43750
2	.50000	.50000	.42242	.43678	.37659	.43750
3	.75000	.50000	.43477	.43686	.41777	.43750
4	.50000	.75000	.59417	.60871	.55431	.60938
5	.50000	.25000	.22260	.23379	.18115	.23438

Table 24. Square - 63 Nodes: Percent Differences

X-DISPLACEMENTS

NO	A	B	C
2	-3.34	.02	90.75

Table 24 (cont'd.)

3	-1.00	.02	33.60
4	-.78	.01	17.96
5	-.70	.01	12.65
6	-.66	.01	9.69
7	-.63	.01	7.82
8	-.60	.01	6.53
9	-.59	.01	5.59
10	-.57	.01	4.85
11	-.55	.01	4.24
12	-.53	.01	3.68
13	-.50	.01	3.10
14	-.48	.01	2.36
15	-.45	.02	1.07
16	-.40	.02	-1.41
17	-.22	.00	-1.98
18	-.26	.00	5.24
19	-.28	-.01	5.39
20	-.28	-.01	5.46
21	-.27	-.01	5.50
22	-.25	-.01	5.52
23	-.22	-.02	5.54
24	-.18	-.02	5.59
25	-.14	-.01	5.66
26	-.08	-.01	5.78
27	-.01	-.01	5.98
28	.08	-.01	6.29
29	.21	-.01	6.87
30	.42	.00	8.46
31	1.01	.02	13.38
32	1.56	.05	18.92
33	1.21	.03	9.52
34	1.04	.03	7.43
35	.93	.02	6.70
36	.85	.02	6.35
37	.79	.02	6.20
38	.75	.01	6.18
39	.71	.01	6.26
40	.68	.01	6.42
41	.66	.01	6.62
42	.64	.01	6.79
43	.63	.01	6.63
44	.63	.02	5.27
45	.63	.02	2.41
46	-.55	.02	33.10

Y-DISPLACEMENTS

NO	A	B	C
1	-87.88	5.15	117.67
17	-.60	.13	6.24
18	-.87	.09	7.82
19	-.83	.09	5.61

Table 24 (cont'd.)

20	-.71	.08	4.90
21	-.59	.07	4.51
22	-.45	.07	4.34
23	-.32	.07	4.34
24	-.18	.06	4.49
25	-.02	.06	4.80
26	.15	.06	5.32
27	.35	.06	6.13
28	.59	.06	7.46
29	.90	.06	9.92
30	1.39	.07	15.07
31	2.57	.09	24.65
32	-.02	.00	19.26
33	-1.05	-.03	-.63
34	-1.66	-.04	-1.44
35	-2.14	-.04	-2.12
36	-2.58	-.05	-2.83
37	-3.01	-.05	-3.54
38	-3.44	-.05	-4.30
39	-3.88	-.06	-5.15
40	-4.32	-.06	-6.12
41	-4.78	-.06	-7.22
42	-5.23	-.07	-8.45
43	-5.66	-.07	-9.68
44	-6.09	-.08	-10.32
45	-6.53	-.08	-9.08
46	-7.16	-.08	-25.96
47	-3.22	.10	-31.59
48	-4.45	.07	-8.70
49	-4.55	.08	-7.80
50	-4.66	.09	-7.70
51	-4.79	.11	-7.74
52	-4.93	.12	-7.82
53	-5.10	.14	-7.94
54	-5.30	.16	-8.08
55	-5.55	.18	-8.25
56	-5.85	.21	-8.47
57	-6.23	.25	-8.78
58	-6.75	.29	-9.28
59	-7.47	.36	-10.14
60	-8.55	.45	-11.77
61	-10.30	.59	-15.24
62	-13.55	.85	-20.93
63	-21.55	1.44	-49.08

X-TRACTIONS

NO	A	B	C
1	-2.90	-.16	18.95
47	-2.43	-.26	78.08
48	1.53	.36	-15.76
49	.55	-.29	-26.73

Table 24 (cont'd.)

50	.48	.30	-14.44
51	.39	-.25	-3.42
52	.32	.24	1.21
53	.25	-.20	1.85
54	.19	.19	1.30
55	.14	-.14	.84
56	.09	.13	.72
57	.06	-.09	.83
58	.03	.07	1.07
59	.01	-.03	1.61
60	.01	.01	2.33
61	.04	.03	9.90
62	.08	-.05	11.68
63	1.06	.09	-58.67

INTERIOR X-DISP

NO	A	B	C
1	-.20	.00	-64.38
2	-.17	.00	4.74
3	-.18	.00	27.76
4	.19	.01	-.07
5	-.35	.00	11.42

INTERIOR Y-DISP

NO	A	B	C
1	-4.62	.12	-7.39
2	-2.70	.08	-3.76
3	-1.13	.06	.52
4	-2.74	.05	-4.44
5	-2.87	.15	-2.78

INTERIOR SXX

NO	A	B	C
1	.01	.01	1.64
2	-.07	.00	1.44
3	-.18	-.01	1.28
4	.29	.01	3.43
5	-.14	.00	.40

INTERIOR SXY

NO	A	B	C
1	-.66	-.04	-3.20
2	-.16	-.01	1.07
3	.86	.02	8.19
4	-2.37	-.10	-2.87
5	.22	.03	.65

Table 24 (cont'd.)

INTERIOR SY

NO	A	B	C
1	4.01	.15	15.22
2	3.45	.17	13.92
3	.62	.15	4.51
4	2.50	.11	9.04
5	5.02	.25	22.71

Table 25. Disk - 19 Nodes: X - Displacements

X-DISPLACEMENTS

NO	X	Y	UXA	UXB	UXC	EXACT
1	-.41620	-.89254	.09604	.09747	.09219	.12486
2	-.09671	-.98189	0.00000	0.00000	0.00000	0.00000
3	.22404	-.96087	-.08836	-.09208	-.10161	-.06721
4	.52101	-.83786	-.17181	-.17603	-.17864	-.15630
5	.76269	-.62592	-.24019	-.24563	-.24145	-.22881
6	.92341	-.34755	-.28573	-.29242	-.28136	-.27702
7	.98612	-.03228	-.30439	-.31165	-.29958	-.29583
8	.94416	.28641	-.29276	-.29985	-.28646	-.28325
9	.80199	.57470	-.25069	-.25682	-.24143	-.24060
10	.57470	.80199	-.18337	-.18732	-.17379	-.17241
11	.28641	.94416	-.09732	-.09753	-.08950	-.08592
12	-.03228	.98612	0.00000	0.00000	0.00000	0.00000
13	-.34754	.92341	.08575	.09300	.08594	.10426
14	-.62592	.76269	.16330	.16836	.15901	.18778
15	-.83786	.52102	.22274	.22891	.21336	.25136
16	-.96087	.22404	.25702	.26424	.24247	.28826
17	-.98189	-.09671	.26296	.27063	.24123	.29457
18	-.89254	-.41620	.23594	.24417	.20644	.26776
19	-.69636	-.69636	.17842	.18455	.15161	.20891

Table 26. Disk - 19 Nodes: Y - Displacements

Y-DISPLACEMENTS

NO	X	Y	UYA	UYB	UYC	EXACT
1	-.41620	-.89254	.23594	.24417	.22012	.26776
2	-.09671	-.98189	.26296	.27063	.25817	.29457
3	.22404	-.96087	.25702	.26424	.23543	.28826
4	.52101	-.83786	.22274	.22891	.19908	.25136
5	.76269	-.62592	.16330	.16836	.14050	.18778
6	.92341	-.34755	.08575	.09030	.07150	.10426
7	.98612	-.03228	0.00000	0.00000	0.00000	0.00000
8	.94416	.28641	-.09732	-.09753	-.11315	-.08592
9	.80199	.57470	-.18337	-.18732	-.19350	-.17241
10	.57470	.80199	-.25069	-.25682	-.25599	-.24060
11	.28641	.94416	-.29276	-.29985	-.29518	-.28325

Table 26 (cont'd.)

12	-.03228	.98612	-.30439	-.31165	-.30243	-.29583
13	-.34754	.92341	-.28573	-.29242	-.28109	-.27702
14	-.62592	.76269	-.24019	-.24563	-.23471	-.22881
15	-.83786	.52102	-.17181	-.17603	-.16457	-.15630
16	-.96087	.22404	-.08837	-.09208	-.08488	-.06721
17	-.98189	-.09671	0.00000	0.00000	0.00000	0.00000
18	-.89254	-.41620	.09604	.09747	.07830	.12486
19	-.69636	-.69636	.17842	.18455	.13606	.20891

Table 27. Disk - 19 Nodes: X - Traction

X-TRACTIONS

NO	X	Y	TXA	TXB	TXC	EXACT
1	-.41620	-.89254	.41620	.41620	.41620	.41620
2	-.09671	-.98189	.05623	.04803	.09908	.09671
3	.22404	-.96087	-.22404	-.22404	-.22404	-.22404
4	.52101	-.83786	-.52101	-.52101	-.52101	-.52101
5	.76269	-.62592	-.76269	-.76269	-.76269	-.76269
6	.92341	-.34755	-.92341	-.92341	-.92341	-.92341
7	.98612	-.03228	-.98612	-.98612	-.98612	-.98612
8	.94416	.28641	-.94416	-.94416	-.94416	-.94416
9	.80199	.57470	-.80199	-.80199	-.80199	-.80199
10	.57470	.80199	-.57470	-.57470	-.57470	-.57470
11	.28641	.94416	-.28641	-.28641	-.28641	-.28641
12	-.03228	.98612	.08018	.08478	.04518	.03228
13	-.34754	.92341	.34754	.34754	.34754	.34754
14	-.62592	.76269	.62592	.62592	.62592	.62592
15	-.83786	.52102	.83786	.83786	.83786	.83786
16	-.96087	.22404	.96087	.96087	.96087	.96087
17	-.98189	-.09671	.98189	.98189	.98189	.98189
18	-.89254	-.41620	.89254	.89254	.89254	.89254
19	-.69636	-.69636	.69636	.69636	.69636	.69636

Table 28. Disk - 19 Nodes: Y - Traction

Y-TRACTIONS

NO	X	Y	TYA	TYB	TYC	EXACT
1	-.41620	-.89254	.89254	.89254	.89254	.89254
2	-.09671	-.98189	.98189	.98189	.98189	.98189
3	.22404	-.96087	.96087	.96087	.96087	.96087
4	.52101	-.83786	.83786	.83786	.83786	.83786
5	.76269	-.62592	.62592	.62592	.62592	.62592
6	.92341	-.34755	.34755	.34755	.34755	.34755
7	.98612	-.03228	.08019	.08475	.18549	.03228
8	.94416	.28641	-.28641	-.28641	-.28641	-.28641
9	.80199	.57470	-.57470	-.57470	-.57470	-.57470
10	.57470	.80199	-.80199	-.80199	-.80199	-.80199
11	.28641	.94416	-.94416	-.94416	-.94416	-.94166

Table 28 (cont'd.)

12	-.03228	.98612	-.98612	-.98612	-.98612	-.98612
13	-.34754	.92341	-.92341	-.92341	-.92341	-.92341
14	-.62592	.76269	-.76269	-.76269	-.76269	-.76269
15	-.83786	.52102	-.52102	-.52102	-.52102	-.52102
16	-.96087	.22404	-.22404	-.22404	-.22404	-.22404
17	-.98189	-.09671	.05623	.04803	.04756	.09671
18	-.89254	-.41620	.41620	.41620	.41620	.41620
19	-.69636	-.69636	.69636	.69636	.69636	.69636

Table 29. Disk - 19 Nodes: Interior Values

INTERIOR X-DISP

NO	X	Y	UXA	UXB	UXC	EXACT
1	-.75000	0.00000	.19790	.20154	.17640	.22500
2	-.50000	0.00000	.12514	.12773	.10661	.15000
3	0.00000	0.00000	-.02036	-.02006	-.02803	0.00000
4	.50000	0.00000	-.16586	-.16801	-.16305	-.15000
5	.75000	0.00000	-.23854	-.24203	-.23132	-.22500
6	0.00000	.75000	-.01614	-.01534	-.01275	0.00000
7	0.00000	.50000	-.01862	-.01835	-.02011	0.00000
8	0.00000	-.50000	-.02141	-.02120	-.03115	0.00000
9	0.00000	-.75000	-.02309	-.02359	-.03178	0.00000
10	-.50000	.50000	.12698	.12932	.11774	.15000
11	.50000	.50000	-.16492	-.16710	-.15513	-.15000

INTERIOR Y-DISP

NO	X	Y	UYA	UYB	UYC	EXACT
1	-.75000	0.00000	-.02309	-.02359	-.03124	0.00000
2	-.50000	0.00000	-.02141	-.02120	-.03198	0.00000
3	0.00000	0.00000	-.02036	-.02006	-.02984	0.00000
4	.50000	0.00000	-.01862	-.01835	-.02799	0.00000
5	.75000	0.00000	-.01614	-.01534	-.02288	0.00000
6	0.00000	.75000	-.23854	-.24203	-.24701	-.22500
7	0.00000	.50000	-.16586	-.16801	-.17536	-.15000
8	0.00000	-.50000	.12514	.12773	.11918	.15000
9	0.00000	-.75000	.19790	.20154	.19559	.22500
10	-.50000	.50000	-.16602	-.16821	-.17369	-.15000
11	.50000	.50000	-.16492	-.16710	-.17396	-.15000

INTERIOR SXX

NO	X	Y	A	B	C	EXACT
1	-.75000	0.00000	-.97027	-.98360	-.99003	-1.00000
2	-.50000	0.00000	-.96936	-.98436	-.96725	-1.00000
3	0.00000	0.00000	-.96990	-.98602	-.95970	-1.00000
4	.50000	0.00000	-.97086	-.98694	-.97295	-1.00000
5	.75000	0.00000	-.96497	-.98748	-.97296	-1.00000
6	0.00000	.75000	-.97838	-.98944	-.98242	-1.00000
7	0.00000	.50000	-.97191	-.98757	-.97390	-1.00000

Table 29 (cont'd.)

8	0.00000	-.50000	-.96750	-.98468	-.95030	-1.00000
9	0.00000	-.75000	-.96429	-.98053	-.97728	-1.00000
10	-.50000	.50000	-.96944	-.97989	-.99931	-1.00000
11	.50000	.50000	-.97850	-.99558	-.95242	-1.00000

INTERIOR SKY

NO	X	Y	A	B	C	EXACT
1	-.75000	0.00000	.01565	.01243	-.01252	0.00000
2	-.50000	0.00000	.00521	.00561	.01081	0.00000
3	0.00000	0.00000	.00293	.00179	.00686	0.00000
4	.50000	0.00000	.00575	.00640	-.00157	0.00000
5	.75000	0.00000	.00570	.01358	.02050	0.00000
6	0.00000	.75000	.00570	.01358	.05688	0.00000
7	0.00000	.50000	.00575	.00640	.01720	0.00000
8	0.00000	-.50000	.00521	.00561	-.00616	0.00000
9	0.00000	-.75000	.01565	.01243	-.01394	0.00000
10	-.50000	.50000	.01015	.01084	.02086	0.00000
11	.50000	.50000	.00738	.01195	.04680	0.00000

INTERIOR SYX

NO	X	Y	A	B	C	EXACT
1	-.75000	0.00000	-.96429	-.98053	-.93358	-1.00000
2	-.50000	0.00000	-.96750	-.98468	-.94655	-1.00000
3	0.00000	0.00000	-.96990	-.98602	-.97341	-1.00000
4	.50000	0.00000	-.97191	-.98757	-.97297	-1.00000
5	.75000	0.00000	-.97838	-.98944	-.98667	-1.00000
6	0.00000	.75000	-.96497	-.98748	-.95095	-1.00000
7	0.00000	.50000	-.97086	-.98694	-.96699	-1.00000
8	0.00000	-.50000	-.96936	-.98436	-.99498	-1.00000
9	0.00000	-.75000	-.97027	-.98360	-1.01433	-1.00000
10	-.50000	.50000	-.95983	-.97670	-.92942	-1.00000
11	.50000	.50000	-.97850	-.99558	-.99591	-1.00000

Table 30. Disk - 19 Nodes: Percent Differences

X-DISPLACEMENTS

NO	A	B	C
1	23.08	21.94	26.17
3	-31.47	-37.00	-51.17
4	-9.92	-12.62	-14.29
5	-.498	-.735	-5.52
6	-3.14	-5.56	-1.56
7	-2.89	-5.35	-1.27
8	-3.36	-5.86	-1.13
9	-4.19	-6.74	-.35
10	-6.36	-8.65	-.80
11	-13.26	-13.51	-4.16
13	17.76	13.40	17.57

Table 30 (cont'd.)

14	13.03	10.34	15.32
15	11.39	8.93	15.12
16	10.84	8.33	15.89
17	10.73	8.13	18.11
18	11.88	8.81	22.90
19	14.59	11.66	27.43

Y-DISPLACEMENTS

NO	A	B	C
1	11.88	8.81	17.79
2	10.73	8.13	12.36
3	10.84	8.33	18.33
4	11.39	8.93	20.80
5	13.03	10.34	25.18
6	17.76	13.40	31.42
8	-13.26	-13.51	-31.69
9	-6.36	-8.65	-12.23
10	-4.19	-6.74	-6.40
11	-3.36	-5.86	-4.21
12	-2.89	-5.35	-2.23
13	-3.14	-5.56	-1.47
14	-4.98	-7.35	-2.58
15	-9.92	-12.62	-5.29
16	-31.47	-37.00	-26.28
17	100.00	100.00	100.00
18	23.08	21.94	37.29
19	14.59	11.66	34.87

INTERIOR X-DISP

NO	A	B	C
1	12.04	10.43	21.60
2	16.57	14.85	28.93
4	-10.57	-12.01	-8.70
5	-6.02	-7.57	-2.81
10	15.35	13.79	21.51
11	-9.95	-11.40	-3.42

INTERIOR Y-DISP

NO	A	B	C
6	-6.02	-7.57	-9.78
7	-10.57	-12.01	-16.90
8	16.57	14.85	20.55
9	12.04	10.43	13.07
10	-10.68	-12.14	-15.80
11	-9.95	-11.40	-15.97

Table 30 (cont'd.)

INTERIOR SXX

NO	A	B	C
1	2.97	1.64	1.00
2	3.06	1.56	3.28
3	3.01	1.40	4.03
4	2.91	1.31	2.71
5	3.50	1.25	2.70
6	2.16	1.06	1.76
7	2.81	1.24	2.61
8	3.25	1.53	4.97
9	3.57	1.95	2.27
10	3.06	2.01	.07
11	2.15	.44	4.76

INTERIOR SYX

NO	A	B	C
1	3.57	1.95	6.64
2	3.25	1.53	5.34
3	3.01	1.40	2.66
4	2.81	1.24	2.70
5	2.16	1.06	1.33
6	3.50	1.25	4.91
7	2.91	1.31	3.30
8	3.06	1.56	.50
9	2.97	1.64	-1.43
10	4.02	2.33	7.06
11	2.15	.44	.41

Table 31. Disk - 35 Nodes: X - Displacements

X-DISPLACEMENTS

NO	X	Y	UXA	UXB	UXC	EXACT
1	-.18499	-.97768	.05388	.05511	.05228	.05550
2	.00000	-.99619	0.00000	0.00000	0.00000	0.00000
3	.17299	-.98106	-.05166	-.05177	-.05979	-.05190
4	.34072	-.93612	-.10143	-.10203	-.10351	-.10222
5	.49810	-.86273	-.14803	-.14912	-.14748	-.14943
6	.64034	-.76313	-.19011	-.19167	-.18669	-.19210
7	.76313	-.64034	-.22642	-.22840	-.21993	-.22894
8	.86273	-.49810	-.25587	-.25819	-.24673	-.25882
9	.93612	-.34072	-.27756	-.2801	-.26555	-.28084
10	.98106	-.17299	-.29086	-.29359	-.27728	-.29432
11	.99619	.00000	-.29550	-.29816	-.28271	-.29886
12	.98106	.17299	-.29119	-.29369	-.27870	-.29432
13	.93612	.34072	-.27791	-.28025	-.26437	-.28084
14	.86273	.49810	-.25618	-.25829	-.24259	-.25882
15	.76313	.64034	-.22670	-.22849	-.21387	-.22894
16	.64034	.76313	-.19034	-.19175	-.17840	-.19210

Table 31 (cont'd.)

17	.49810	.86273	-.14820	-.14918	-.13809	-.14943
18	.34072	.93612	-.10154	-.10207	-.09378	-.10222
19	.17299	.98106	-.05169	-.05181	-.04715	-.05190
20	0.00000	.99619	0.00000	0.00000	0.00000	0.00000
21	-.17299	.98106	.05051	.05164	.05022	.05190
22	-.34072	.93612	.09975	.10167	.09623	.10222
23	-.49810	.86273	.14607	.14866	.13998	.14943
24	-.64034	.76313	.18796	.19115	.17875	.19210
25	-.76313	.64034	.22412	.22782	.21213	.22894
26	-.86273	.49810	.25345	.25755	.23865	.25882
27	-.93612	.34072	.27503	.27944	.25771	.28084
28	-.98106	.17299	.28820	.29280	.26888	.29432
29	-.99619	.00000	.29247	.29716	.27142	.29886
30	-.97768	-.18499	.28548	.29144	.26604	.29331
31	-.92164	-.37504	.26901	.27461	.24728	.27649
32	-.82906	-.55023	.24187	.24696	.21789	.24872
33	-.70359	-.70359	.20515	.20955	.17904	.21108
34	-.55023	-.82906	.16030	.16384	.13310	.16507
35	-.37504	-.92164	.10914	.11166	.09247	.11251

Table 32. Disk - 35 Nodes: Y - Displacements

Y-DISPLACEMENTS

NO	X	Y	UYA	UYB	UYC	EXACT
1	-.18499	-.97768	.28548	.29144	.26595	.29331
2	.00000	-.99619	.29247	.29716	.28391	.29886
3	.17299	-.98106	.28820	.29280	.26343	.29432
4	.34072	-.93612	.27503	.27945	.25045	.28084
5	.49810	-.86273	.25345	.25755	.29910	.25882
6	.64034	-.76313	.22412	.22782	.20108	.22894
7	.76313	-.64034	.18796	.19115	.16642	.19210
8	.86273	-.49810	.14607	.14866	.12742	.14943
9	.93612	-.34072	.09975	.10167	.08480	.10222
10	.98106	-.17299	.05051	.05164	.04168	.05190
11	.99619	.00000	0.00000	0.00000	0.00000	0.00000
12	.98106	.17299	-.05169	-.05181	-.05944	-.05190
13	.93612	.34072	-.10154	-.10207	-.10503	-.10222
14	.86273	.49810	-.14820	-.14918	-.15006	-.14943
15	.76313	.64034	-.19034	-.19175	-.19019	-.19210
16	.64034	.76313	-.22670	-.22849	-.22400	-.22894
17	.49810	.86273	-.25618	-.25829	-.25137	-.25882
18	.34072	.93612	-.27791	-.28025	-.27059	-.28084
19	.17299	.98106	-.29119	-.29368	-.28230	-.29432
20	.00000	.99619	-.29550	-.29816	-.28550	-.29886
21	-.17299	.98106	-.29086	-.29359	-.28035	-.29432
22	-.34072	.93612	-.27756	-.28013	-.26637	-.28084
23	-.49810	.86273	-.25587	-.25819	-.24460	-.25882
24	-.64034	.76313	-.22642	-.22840	-.21581	-.22894
25	0.76313	.64034	-.19011	-.19167	-.18035	-.19210
26	-.86273	.49810	-.14803	-.14912	-.14011	-.14943

Table 32 (cont'd.)

27	-.93612	.34072	-.10143	-.10203	-.09540	-.10222
28	-.98106	.17299	-.05166	-.05177	-.04847	-.05190
29	-.99619	.00000	0.00000	0.00000	0.00000	0.00000
30	-.97768	-.18499	.05388	.05511	.05124	.05550
31	-.92164	-.37504	.10914	.11166	.10496	.11251
32	-.82906	-.55023	.16030	.16384	.15235	.16507
33	-.70359	-.70359	.20515	.20955	.19281	.21108
34	-.5502	-.82906	.24187	.24697	.20781	.24872
35	-.37504	-.92164	.26901	.27461	.21729	.27649

Table 33. Disk - 35 Nodes: X - Traction

X-TRACTIONS

NO	X	Y	TXA	TXB	TXC	EXACT
1	-.18499	-.97768	.18499	.18499	.18499	.18499
2	.00000	-.99619	.00552	.00317	.06044	.00000
3	.17299	-.98106	-.17299	-.17299	-.17299	-.17299
4	.34072	-.93612	-.34072	-.34072	-.34072	-.34072
5	.49810	-.86273	-.49810	-.49810	-.49810	-.49810
6	.64034	-.76313	-.64034	-.64034	-.64034	-.64034
7	.76313	-.64034	-.76313	-.76313	-.76313	-.76313
8	.86273	-.49810	-.86273	-.86273	-.86273	-.86273
9	.93612	-.34072	-.93612	-.93612	-.93612	-.93612
10	.98106	-.17299	-.98106	-.98106	-.98106	-.98106
11	.99619	.00000	-.99619	-.99619	-.99619	-.99619
12	.98106	.17299	-.98106	-.98106	-.98106	-.98106
13	.93612	.34072	-.93612	-.93612	-.93612	-.93612
14	.86273	.49810	-.86273	-.86273	-.86273	-.86273
15	.76313	.64034	-.76313	-.76313	-.76313	-.76313
16	.64034	.7631	-.64034	-.64034	-.64034	-.64034
17	.49810	.86273	-.49810	-.49810	-.49810	-.49810
18	.34072	.93612	-.34072	-.34072	-.34072	-.34072
19	.17299	.98106	-.17299	-.17299	-.17299	-.17299
20	.00000	.99619	.00960	.00276	-.01894	.00000
21	-.17299	.98106	.17299	.17299	.17299	.17299
22	-.34072	.93612	.34072	.34072	.34072	.34072
23	-.49810	.86273	.49810	.49810	.49810	.49810
24	-.64034	.76313	.64034	.64034	.64034	.64034
25	-.76313	.64034	.76313	.76313	.76313	.76313
26	-.86273	.49810	.86273	.86273	.86273	.86273
27	-.93612	.34072	.93612	.93612	.93612	.93612
28	-.98106	.17299	.98106	.98106	.98106	.98106
29	-.99619	.00000	.99619	.99619	.99619	.99619
30	-.97768	-.18499	.97768	.97768	.97768	.97768
31	-.92164	-.37504	.92164	.92164	.92614	.92614
32	-.82906	-.55023	.82906	.82906	.82906	.82906
33	-.70359	-.70359	.70359	.70359	.70359	.70359
34	-.55023	-.82906	.55023	.55023	.55023	.55023
35	-.37504	-.92164	.37504	.37504	.37504	.37504

Table 34. Disk - 35 Nodes: Y - Traction

Y-TRACTIONS

NO	X	Y	TYA	TYB	TYC	EXACT
1	-.18499	-.97768	.97768	.97768	.97768	.97768
2	.00000	-.99619	.99619	.99619	.99619	.99619
3	.17299	-.98106	.98106	.98106	.98106	.98106
4	.34072	-.93612	.93612	.93612	.93612	.93612
5	.49810	-.86273	.86273	.86273	.86273	.86273
6	.64034	-.76313	.76313	.76313	.76313	.76313
7	.76313	-.64034	.64034	.64034	.64034	.64034
8	.86273	-.49810	.49810	.49810	.49810	.49810
9	.93612	-.34072	.34072	.34072	.34072	.34072
10	.98106	-.17299	.17299	.17299	.17299	.17299
11	.99619	.00000	.00960	.00275	.11302	.00000
12	.98106	.17299	-.17299	-.17299	-.17299	-.17299
13	.93612	.34072	-.34072	-.34072	-.34072	-.34072
14	.86273	.49810	-.49810	-.49810	-.49810	-.49810
15	.76313	.64034	-.64034	-.64034	-.64034	-.64034
16	.64034	.76313	-.76313	-.76313	-.76313	-.76313
17	.49810	.86273	-.86273	-.86273	-.86273	-.86273
18	.34072	.93612	-.93612	-.93612	-.93612	-.93612
19	.17299	.98106	-.98106	-.98106	-.98106	-.98106
20	.00000	.99619	-.99619	-.99619	-.99619	-.99619
21	-.17299	.98106	-.98106	-.98106	-.98106	-.98106
22	-.34072	.93612	-.93612	-.93612	-.93612	-.93612
23	-.49810	.86273	-.86273	-.86273	-.86273	-.86273
24	-.64034	.76313	-.76313	-.76313	-.76313	-.76313
25	-.76313	.64034	-.64034	-.64034	-.64034	-.64034
26	-.86273	.49810	-.49810	-.49810	-.49810	-.49810
27	-.98612	.34072	-.34072	-.34072	-.34072	-.34072
28	-.98106	.17299	-.17299	-.17299	-.17299	-.17299
29	-.99619	.00000	.00551	.00316	.00457	.00000
30	-.97768	-.18499	.18499	.18499	.18499	.18499
31	-.92164	-.37504	.37504	.37504	.37504	.37504
32	-.82906	-.55023	.55023	.55023	.55023	.55023
33	-.70359	-.70359	.70359	.70359	.70359	.70359
34	-.55023	-.82906	.82906	.82906	.82906	.82906
35	-.37504	-.92164	.92164	.92164	.92164	.92164

Table 35. Disk - 35 Nodes: Interior Values

INTERIOR X-DISP

NO	X	Y	UXA	UXB	UXC	EXACT
1	-.75000	0.00000	.22094	.2259	.13353	.22500
2	-.50000	0.00000	.14664	.14888	.08700	.15000
3	0.00000	0.00000	-.00179	-.00053	-.00619	0.00000
4	.50000	0.00000	-.15009	-.14991	-.09844	-.15000
5	.75000	0.00000	-.22426	-.22460	-.14488	-.22500
6	0.00000	.75000	-.00105	-.00027	-.00856	0.00000
7	0.00000	.50000	-.00139	-.00039	-.00798	0.00000

Table 35 (cont'd.)

8	0.00000	-.50000	-.00178	-.00052	-.00396	0.00000
9	0.00000	-.75000	-.00137	-.00040	-.00044	0.00000
10	-.50000	.50000	.14728	.14912	-.08554	.15000
11	.50000	.50000	-.14999	-.14986	-.10125	-.15000

INTERIOR Y-DISP

NO	X	Y	UYA	UYB	UYC	EXACT
1	-.75000	0.00000	-.00137	-.00039	-.00522	0.00000
2	-.50000	0.00000	-.00178	-.00052	-.00773	0.00000
3	0.00000	0.00000	-.00179	-.00053	-.00943	0.00000
4	.50000	0.00000	-.00139	-.00039	-.00890	0.00000
5	.75000	0.00000	-.00105	-.00027	-.00767	0.00000
6	0.00000	.75000	-.22426	-.22460	-.22755	-.22500
7	0.00000	.50000	-.15009	-.14991	-.15467	-.15000
8	0.00000	-.50000	.14664	.14888	.13703	.15000
9	0.00000	-.75000	.22094	.22359	.21340	.22500
10	-.50000	.50000	-.14983	-.14982	-.15251	-.15000
11	.50000	.50000	-.14999	-.14986	-.15515	-.15000

INTERIOR SXX

NO	X	Y	A	B	C	EXACT
1	-.75000	0.00000	-.99078	-.99593	-.97552	-1.00000
2	-.50000	0.00000	-.98928	-.99593	-.97486	-1.00000
3	0.00000	0.00000	-.98899	-.99594	-.97109	-1.00000
4	.50000	0.00000	-.98917	-.99601	-.97167	-1.00000
5	.75000	0.00000	-.98932	-.99610	-.97701	-1.00000
6	0.00000	.75000	-.99070	-.99651	-.97460	-1.00000
7	0.00000	.50000	-.99044	-.99644	-.97591	-1.00000
8	0.00000	-.50000	-.98722	-.99539	-.95302	-1.00000
9	0.00000	-.75000	-.98676	-.99531	-.94871	-1.00000
10	-.50000	.50000	-.99036	-.99644	-.97754	-1.00000
11	.50000	.50000	-.99073	-.99652	-.97310	-1.00000

INTERIOR SXY

NO	X	Y	A	B	C	EXACT
1	-.75000	0.00000	.00060	.00004	-.00594	0.00000
2	-.50000	0.00000	.00099	.00027	-.00388	0.00000
3	0.00000	0.00000	.00107	.00036	.00439	0.00000
4	.50000	0.00000	.00071	.00029	.00040	0.00000
5	.75000	0.00000	.00079	.00033	-.00450	0.00000
6	0.00000	.75000	.00079	.00033	.00919	0.00000
7	0.00000	.50000	.00071	.00029	.00319	0.00000
8	0.00000	-.50000	.00099	.00027	.00997	0.00000
9	0.00000	-.75000	.00060	.00004	-.00834	0.00000
10	-.50000	.50000	.00013	.00010	.00082	0.00000
11	.50000	.50000	.00147	.00053	.00677	0.00000

Table 35 (cont'd.)

INTERIOR SYI

NO	X	Y	A	B	C	EXACT
1	-.75000	0.00000	-.98676	-.99531	-.96770	-1.00000
2	-.50000	0.00000	-.98722	-.99539	-.96397	-1.00000
3	0.00000	0.00000	-.98899	-.99594	-.96913	-1.00000
4	.50000	0.00000	-.99044	-.99644	-.97358	-1.00000
5	.75000	0.00000	-.99070	-.99651	-.97341	-1.00000
6	0.00000	.75000	-.98932	-.99610	-.97538	-1.00000
7	0.00000	.50000	-.98917	-.99601	-.97121	-1.00000
8	0.00000	-.50000	-.98928	-.99593	-.98397	-1.00000
9	0.00000	-.75000	-.99078	-.99593	-1.02409	-1.00000
10	-.50000	.50000	-.98864	-.99578	-.96878	-1.00000
11	.50000	.50000	-.99073	-.99652	-.98002	-1.00000

Table 36. Disk - 35 Nodes: Percent Differences

X-DISPLACEMENTS

NO	A	B	C
1	2.92	.70	5.80
3	.45	.24	-15.21
4	.77	.19	-1.26
5	.94	.21	1.30
6	1.04	.22	2.82
7	1.10	.24	3.94
8	1.14	.24	4.67
9	1.17	.25	5.44
10	1.17	.25	5.79
11	1.12	.23	5.40
12	1.06	.22	5.31
13	1.04	.21	5.86
14	1.02	.20	6.27
15	.98	.19	6.58
16	.92	.18	7.13
17	.82	.16	7.59
18	.66	.14	8.25
19	.39	.18	9.14
21	2.68	.50	3.22
22	2.41	.54	5.85
23	2.25	.51	6.32
24	2.16	.50	6.95
25	2.10	.49	7.34
26	2.08	.49	7.79
27	2.07	.50	8.23
28	2.08	.52	8.64
29	2.14	.57	9.18
30	2.67	.64	9.30
31	2.71	.68	10.57
32	2.75	.70	12.29
33	2.81	.72	15.18

Table 36 (cont'd.)

34	2.89	.74	19.37
35	3.00	.76	17.82

Y-DISPLACEMENTS

NO	A	B	C
1	2.67	.64	9.33
2	2.14	.57	5.00
3	2.08	.52	10.50
4	2.07	.49	10.82
5	2.08	.49	11.48
6	2.10	.49	12.17
7	2.16	.50	13.37
8	2.25	.51	14.73
9	2.41	.54	17.04
10	2.68	.50	19.68
12	.39	.18	-14.54
13	.66	.14	-2.75
14	.82	.16	-.42
15	.92	.18	1.00
16	.98	.20	2.16
17	1.02	.20	2.88
18	1.04	.21	3.65
19	1.06	.22	4.08
20	1.12	.23	4.47
21	1.17	.25	4.75
22	1.17	.25	5.15
23	1.14	.24	5.50
24	1.10	.24	5.74
25	1.04	.22	6.12
26	.94	.21	6.24
27	.77	.19	6.67
28	.45	.25	6.60
30	2.92	.70	7.67
31	3.00	.76	6.72
32	2.89	.74	7.70
33	2.81	.72	8.65
34	2.75	.70	16.45
35	2.71	.68	21.41

INTERIOR X-DISP

NO	A	B	C
1	1.81	.63	40.65
2	2.24	.75	42.00
4	-.06	.06	34.37
5	.33	.18	35.61
10	1.82	.59	42.97
11	.01	.09	32.50

Table 36 (cont'd.)

INTERIOR Y-DISP

NO	A	B	C
6	.33	.18	-1.13
7	-.06	.06	-3.11
8	2.24	.75	8.65
9	1.81	.63	5.16
10	.11	.12	-1.67
11	.01	.09	-3.43

INTERIOR SXX

NO	A	B	C
1	.92	.41	2.45
2	1.07	.41	2.51
3	1.10	.41	2.89
4	1.08	.40	2.83
5	1.07	.39	2.30
6	.93	.35	2.54
7	.96	.36	2.41
8	1.28	.46	4.70
9	1.32	.47	5.13
10	.96	.36	2.25
11	.93	.35	2.69

INTERIOR SYX

NO	A	B	C
1	1.32	.47	3.23
2	1.28	.46	3.60
3	1.10	.41	3.09
4	.96	.36	2.64
5	.93	.35	2.66
6	1.07	.39	2.46
7	1.08	.40	2.88
8	1.07	.41	1.60
9	.92	.41	-2.41
10	1.14	.42	3.12
11	.93	.35	2.00

CHAPTER 5

CONCLUSIONS

The results from each problem favor case (b) as the best model. It is a closer approximation for linear elasticity since displacements are linear, but tractions are not, in general, piecewise continuous. Case (a), with its simple assumptions, is the next best approximation. It appears that an inaccurate assumption in displacement behavior is less damaging than an inaccurate traction assumption. The corner effect in case (c) is too pronounced to favor it over the other two cases.

It is possible to devise schemes for avoiding or reducing the corner effect. However, this will only add to the complexity of the input data or the model itself and, before taking that step, one should examine the benefits. This brings us to the ideas brought out in Chapter 1. Since the time of the first approximation methods, we have progressed to ever-increasing levels of sophistication. As we keep progressing, however, we should learn to use what we have more efficiently. That is what prompted this work and the results indicate that much can be learned about the applicability of our models through simple comparative studies.

APPENDIX

APPENDIX

COMPUTER CODE

```
program bem
C
parameter (nn=75)
parameter (mnn=2*nn)
parameter (mnn1=mnn+1)
parameter (mmm=50)
C
dimension x(nn),y(nn),xm(nn),ym(nn)
dimension rx(nn),ry(nn),s(nn)
dimension r(10),w(10),w1(10),w2(10)
dimension ua(mnn),ub(mnn),uc(mnn),ue(mnn)
dimension ta(mnn),tb(mnn),tc(mnn),te(mnn)
dimension uxa(mmm),uxb(mmm),uxc(mmm)
dimension uya(mmm),uyb(mmm),uyc(mmm)
dimension uxe(mmm),uye(mmm)
dimension soxa(mmm),soxb(mmm),soxc(mmm)
dimension sxya(mmm),sxyb(mmm),sxyc(mmm)
dimension syya(mmm),syyb(mmm),syyc(mmm)
dimension soxe(mmm),syxe(mmm),sxye(mmm)
dimension ibc(nn,2),bc(mnn),bcon(mnn),rhs(mnn)
dimension a(mnn,mnn),b(mnn,mnn),ucc(mnn,mnn)
dimension xf(mmm),yf(mmm)
C
character*70 title
C
open(unit=3,file='sol')
C
C OBTAIN INPUT DATA
C
write(*,*) 'THIS PROGRAM EMPLOYS THE DIRECT BOUNDARY ELEMENT'
write(*,*) 'METHOD TO SOLVE PLANE PROBLEMS OF LINEAR'
write(*,*) 'ELASTICITY'
write(*,*) ' '
C
write(*,*) 'DO YOU WANT TO FIND VALUES AT INTERIOR POINTS?'
write(*,*) ' '
write(*,*) ' 1 = YES'
write(*,*) ' 2 = NO'
write(*,*) ' '
write(*,*) 'ENTER THE NUMBER OF YOUR CHOICE'
read(*,*) ifield
```

```

C      write(*,*) '
C      write(*,*) 'ENTER A DESCRIPTION OF THE PROBLEM ON ONE LINE'
C      write(*,*) 'COLUMNS 1-70. (ENCLOSE IN QUOTES)'
C      read(*,*)title
C      write(*,*) '
C      write(*,*) 'ENTER THE APPROPRIATE NUMBER'
C      write(*,*) '    1 = PLANE STRESS'
C      write(*,*) '    2 = PLANE STRAIN'
C      read(*,*)iplane
C      write(*,*) '
C      write(*,*) 'ENTER THE NUMBER OF NODES'
C      read(*,*)n
C      write(*,*) '
C      write(*,*) 'ENTER POISSON'S RATIO'
C      read(*,*)pr
C      if(iplane.ne.1)then
C      pr=pr/(1.-pr)
C      else
C      endif
C      write(*,*) '
C      call bndry (n,x,y,xm,ym,rmx,rmy,s)
C
C      1  write(*,*) 'HOW MANY INTERIOR POINTS?'
C      read(*,*)mm
C      write(*,*) '
C      write(*,*) 'ENTER XF,YF ONE SET PER LINE'
C      do 5 i=1,mm
C      read(*,*)xf(i),yf(i)
C      5  continue
C
C      write(*,*) 'DO YOU WANT TO CHANGE THESE?'
C      write(*,*) '    1 = YES'
C      write(*,*) '    2 = NO'
C      read(*,*)ichange
C      write(*,*) '
C      if(ichange.eq.1)goto 1
C
C      nn=2*n
C
C      do 20 i=1,n
C      do 20 l=1,2
C      ibc(i,l)=0
C      20  continue
C
C      do 21 i=1,nn
C      bc(i)=0.
C      boon(i)=0.
C      21  continue
C

```

```

C BOUNDARY CONDITION PROGRAM
C
    call bdc(n,mm,pr,xm,ym,xf,yf,rmx,rny,ue,te,bc,ibc,bcon,uxe,
&    uye,sxoe,sxye,syye)
C
    write(*,*) 'ALL INPUT DATA RECEIVED'
    write(*,*) '
C
C INTEGRATION POINTS
C
    call ingpts(r,w,w1,w2)
C
C COMPUTE COEFFICIENT MATRICES A AND B
C
    do 30 l=1,3
C
C INITIALIZE MATRICES A AND B
C
    do 31 i=1,n
    bc(i)=bcon(i)
    do 31 j=1,n
    a(j,i)=0.
    b(j,i)=0.
31 continue
C
C ELEMENT SUBROUTINES
C
    if(l.eq.1)then
    write(*,*) 'COMPUTING FOR CASE A'
    write(*,*) '
    call casea(n,pr,x,y,xm,ym,rmx,rny,s,r,w,a,b)
    else if(l.eq.2)then
    write(*,*) 'COMPUTING FOR CASE B'
    write(*,*) '
    call caseb(n,pr,x,y,s,r,w,w1,w2,a,b)
    else
    write(*,*) 'COMPUTING FOR CASE C'
    write(*,*) '
    call casec(n,pr,x,y,s,r,w,w1,w2,a,b)
    endif
C
C POST-MULTIPLY BY GAMMA INVERSE TRANSPOSE
C
    if(l.eq.2)then
    do 32 i=1,n
    ii2=2*i
    ii1=ii2-1
    aa=-1.
    temp1=a(ii1,1)
    temp2=a(ii2,1)
    temp3=a(ii1,2)
    temp4=a(ii2,2)
C
    do 33 k=2,n

```



```

      kk2=2*k
      kk1=kk2-1
C
      a(ii1,1)=a(ii1,1)+a(ii1,kk1)*aa
      a(ii2,1)=a(ii2,1)+a(ii2,kk1)*aa
      a(ii1,2)=a(ii1,2)+a(ii1,kk2)*aa
      a(ii2,2)=a(ii2,2)+a(ii2,kk2)*aa
      aa=-aa
33  continue
C
      do 34 k=2,n
      kk2=2*k
      kk1=kk2-1
C
      temp5=a(ii1,kk1)
      temp6=a(ii2,kk1)
      temp7=a(ii1,kk2)
      temp8=a(ii2,kk2)
C
      a(ii1,kk1)=-a(ii1,kk1-2)+2.*temp1
      a(ii2,kk1)=-a(ii2,kk1-2)+2.*temp2
      a(ii1,kk2)=-a(ii1,kk2-2)+2.*temp3
      a(ii2,kk2)=-a(ii2,kk2-2)+2.*temp4
C
      temp1=temp5
      temp2=temp6
      temp3=temp7
      temp4=temp8
34  continue
C
32  continue
C
      else if(1.eq.3)then
      do 35 i=1,n
      ii2=2*i
      ii1=ii2-1
      aa=-1.
      temp1=a(ii1,1)
      temp2=a(ii2,1)
      temp3=a(ii1,2)
      temp4=a(ii2,2)
C
      temp11=b(ii1,1)
      temp12=b(ii2,1)
      temp13=b(ii1,2)
      temp14=b(ii2,2)
C
      do 36 k=2,n
      kk2=2*k
      kk1=kk2-1
C
      a(ii1,1)=a(ii1,1)+a(ii1,kk1)*aa
      a(ii2,1)=a(ii2,1)+a(ii2,kk1)*aa
      a(ii1,2)=a(ii1,2)+a(ii1,kk2)*aa

```

```

      a(ii2,2)=a(ii2,2)+a(ii2,kk2)*aa
C
      b(ii1,1)=b(ii1,1)+b(ii1,kk1)*aa
      b(ii2,1)=b(ii2,1)+b(ii2,kk1)*aa
      b(ii1,2)=b(ii1,2)+b(ii1,kk2)*aa
      b(ii2,2)=b(ii2,2)+b(ii2,kk2)*aa
      aa=-aa
36  continue
C
      do 37 k=2,n
      kk2=2*k
      kk1=kk2-1
C
      temp5=a(ii1,kk1)
      temp6=a(ii2,kk1)
      temp7=a(ii1,kk2)
      temp8=a(ii2,kk2)
C
      temp15=b(ii1,kk1)
      temp16=b(ii2,kk1)
      temp17=b(ii1,kk2)
      temp18=b(ii2,kk2)
C
      a(ii1,kk1)=-a(ii1,kk1-2)+2.*temp1
      a(ii2,kk1)=-a(ii2,kk1-2)+2.*temp2
      a(ii1,kk2)=-a(ii1,kk2-2)+2.*temp3
      a(ii2,kk2)=-a(ii2,kk2-2)+2.*temp4
C
      b(ii1,kk1)=-b(ii1,kk1-2)+2.*temp11
      b(ii2,kk1)=-b(ii2,kk1-2)+2.*temp12
      b(ii1,kk2)=-b(ii1,kk2-2)+2.*temp13
      b(ii2,kk2)=-b(ii2,kk2-2)+2.*temp14
C
      temp1=temp5
      temp2=temp6
      temp3=temp7
      temp4=temp8
C
      temp11=temp15
      temp12=temp16
      temp13=temp17
      temp14=temp18
37  continue
C
35  continue
C
      else
      endif
C
C RE-ORDER SYSTEM BASED ON KNOWN BOUNDARY CONDITIONS
C
      do 38 i=1,n
      do 38 k=1,2
      ii=2*(i-1)+k

```

```

        if(IBC(I,K).EQ.0)GOTO 38
        DO 39 J=1,NM
            TEMP=BC(J,II)
            B(J,II)=A(J,II)
            A(J,II)=TEMP
39      CONTINUE
38      CONTINUE
C
C DETERMINE THE KNOWN RIGHT HAND SIDE
C
        DO 40 I=1,NM
            RHS(I)=0.
40      CONTINUE
C
        DO 41 I=1,NM
            DO 41 J=1,NM
                RHS(I)=RHS(I)+B(I,J)*BC(J)
41      CONTINUE
C
C SOLVE FOR UNKNOWN BOUNDARY VALUES
C
        DO 42 I=1,NM
            DO 42 J=1,NM
                UCC(I,J)=A(I,J)
42      CONTINUE
C
        CALL GAUSS(UCC,RHS,NM)
C
        DO 43 I=1,N
            DO 43 K=1,2
                II=2*(I-1)+K
                IF(IBC(I,K).NE.1) GOTO 4
                TEMP=BC(II)
                BC(II)=RHS(II)
                RHS(II)=TEMP
43      CONTINUE
C
        DO 44 I=1,NM
            IF(L.EQ.1)THEN
                UA(I)=RHS(I)
                TA(I)=BC(I)
            ELSE IF(L.EQ.2)THEN
                UB(I)=RHS(I)
                TB(I)=BC(I)
            ELSE
                UC(I)=RHS(I)
                TC(I)=BC(I)
            ENDIF
44      CONTINUE
C
C COMPUTE INTERIOR VALUES
C
        IF(IFIELD.EQ.1)THEN
C

```

```

      if(1.eq.1)then
      call flda(n,mm,pr,x,y,r,w,w1,w2,ua,ta,xf,yf,uxa,uya,sxa,
&      sxya,syya)
      C
      else if(1.eq.2)then
      call fldb(n,mm,pr,x,y,r,w,w1,w2,ub,tb,xf,yf,uxb,uyb,sxb,
&      sxyb,syyb)
      C
      else
      call fldc(n,mm,pr,x,y,r,w,w1,w2,uc,tc,xf,yf,uxc,uyc,sxc,
&      sxyc,syyb)
      endif
      C
      else
      endif
      C
      30 continue
      C
      C OUTPUT
      C
      C TITLE AND INPUT DATA
      C
      write(3,100)
      write(3,105)
      write(3,*)title
      write(3,100)
      write(3,110)
      write(3,115)
      C
      write(3,120)n
      write(3,125)pr
      C
      if(iplane,eq.1)then
      write(3,130)
      else
      write(3,135)
      endif
      C
      C NODAL COORDINATES AND BOUNDARY CONDITIONS
      C
      write(3,200)
      write(3,205)
      do 50 i=1,n
50 write(3,210)i,x,(i),y(i),xm(i),ym(i),s(i),rx(i),ry(i)
      C
      write(3,215)
      C
      do 52 j=1,n
      i1=2*(j-1)+1
      i2=2*(j-1)+2
      bc1=boon(i1)
      bc2=boon(i2)
      k=1
      if(1bc(j,k).eq.1)then

```

```

    iprin1=0
    else
    iprin1=1
    endif
    k=2
    if(IBC(j,k).eq.1)then
    iprin2=1
    else
    iprin2=3
    endif
    iwrite=iprin1+1prin2
C
    if(iwrite.eq.1)then
    write(3,220)j,bc1,bc2
    else if(iwrite.eq.2)then
    write(3,225)j,bc1,bc2
    else if(iwrite.eq.3)then
    write(3,230)j,bc1,bc2
    else
    write(3,235)j,bc1,bc2
    endif
52  continue
    write(3,100)
C
C CALCULATED VALUES
C
    write(3,315)
C
    write(3,320)
    do 53 i=1,n
    i1=2*(i-1)+1
    write(3,322)i,xm(i),ym(i),ua(i1),ub(i1),uc(i1),ue(i1)
53  continue
    write(3,330)
    write(3,335)
    do 54 i=1,n
    i2=2*(i-1)+2
    write(3,322)i,xm(i),ym(i),ua(i2),ub(i2),uc(i2),ue(i2)
54  continue
    write(3,340)
    write(3,345)
    do55 i=1,n
    i=2*(i-1)+1
    write(3,322)i,xm(i),ym(i),ta(i1),tb(i1),tc(i1),te(i1)
55  continue
    write(3,350)
    write(3,355)
    do 56 i=,n
    i2=2*(i-1)+2
    write(3,322)i,xm(i),ym(i),ta(i2),tb(i2),tc(i2),te(i2)
56  continue
    write(3,100)
    write(3,360)
    write(3,365)

```

```

write(3,370)
do 57 i=1,mm
write(3,322)i,xf(i),yf(i),wza(i),wzb(i),wzc(i),wze(i)
57 continue
write(3,375)
write(3,380)
do 58 i=1,mm
write(3,322)i,xf(i),yf(i),uya(i),uyb(i),uyc(i),uye(i)
58 continue
write(3,385)
write(3,390)
do 59 i=1,mm
write(3,322)i,xf(i),yf(i),soza(i),sob(i),soxc(i),soxe(i)
59 continue
write(3,395)
write(3,390)
do 60 i=1,mm
write(3,322)i,xf(i),yf(i),sxya(i),sxyb(i),sxyc(i),sxye(i)
60 continue
write(3,400)
write(3,390)
do 61 i=1,mm
write(3,322)i,xf(i),yf(i),syza(i),syzb(i),syzc(i),syze(i)
61 continue
write(3,100)
C
C PERCENT DIFFERENCES
C
write(3,405)
write(3,315)
write(3,392)
do 70 i=1,n
i1=2*(i-1)+1
if(ue(i1).eq.0.)then
write(3,410)i
else
da=((ue(i1)-ua(i1))/ue(i1))*100.
db=((ue(i1)-ub(i1))/ue(i1))*100.
dc=((ue(i1)-uc(i1))/ue(i1))*100.
write(3,325)i,da,db,dc
endif
70 continue
C
write(3,330)
write(3,392)
do 71 i=1,n
i2=2*(i-1)+2
if(ue(i2).eq.0.)then
write(3,410)i
else
da=((ue(i2)-ua(i2))/ue(i2))*100.
db=((ue(i2)-ub(i2))/ue(i2))*100.
dc=((ue(i2)-uc(i2))/ue(i2))*100.
write(3,325)i,da,db,dc

```

```

endif
71 continue
C
write(3,340)
write(3,392)
do 72 i=1,n
  il=2*(i-1)+1
  if(te(il).eq.0.)then
    write(3,410)i
  else
    da=((te(il)-ta(il))/te(il))*100.
    db=((te(il)-tb(il))/te(il))*100.
    dc=((te(il)-tc(il))/te(il))*100.
    write(3,325)i,da,db,dc
  endif
72 continue
C
write(3,350)
write(3,392)
do 73 i=1,n
  i2=2*(i-1)+2
  if(te(i2).eq.0.)then
    write(3,410)i
  else
    da=((te(i2)-ta(i2))/te(i2))*100.
    db=((te(i2)-tb(i2))/te(i2))*100.
    dc=((te(i2)-tc(i2))/te(i2))*100.
    write(3,325)i,da,db,dc
  endif
73 continue
C
write(3,365)
write(3,392)
do 74 i=1,mm
  if(ux(i).eq.0.)then
    write(3,410)i
  else
    da=((ux(i)-uxa(i))/ux(i))*100.
    db=((ux(i)-uxb(i))/ux(i))*100.
    dc=((ux(i)-uxc(i))/ux(i))*100.
    write(3,325)i,da,db,dc
  endif
74 continue
C
write(3,375)
write(3,392)
do 75 i=1,mm
  if(uy(i).eq.0.)then
    write(3,410)i
  else
    da=((uy(i)-uya(i))/uy(i))*100.
    db=((uy(i)-uyb(i))/uy(i))*100.
    dc=((uy(i)-uyc(i))/uy(i))*100.
    write(3,325)i,da,db,dc
  endif

```

```

75  continue
C
    write(3,385)
    write(3,392)
    do 76 i=1,mm
        if(sxx(i).eq.0.)then
            write(3,410)i
        else
            da=((sxx(i)-sxxa(i))/sxx(i))*100.
            db=((sxx(i)-sxxb(i))/sxx(i))*100.
            dc=((sxx(i)-sxxc(i))/sxx(i))*100.
            write(3,325)i,da,db,dc
        endif
76  continue
C
    write(3,395)
    write(3,392)
    do 77 i=1,mm
        if(sxy(i).eq.0.)then
            write(3,410)i
        else
            da=((sxy(i)-sxya(i))/sxy(i))*100.
            db=((sxy(i)-sxyb(i))/sxy(i))*100.
            dc=((sxy(i)-sxyz(i))/sxy(i))*100.
            write(3,325)i,da,db,dc
        endif
77  continue
C
    write(3,400)
    write(3,392)
    do 78 i=1,mm
        if(syy(i).eq.0.)then
            write(3,410)i
        else
            da=((syy(i)-syya(i))/syy(i))*100.
            db=((syy(i)-syyb(i))/syy(i))*100.
            dc=((syy(i)-syyc(i))/syy(i))*100.
            write(3,325)i,da,db,dc
        endif
78  continue
C
C FORMATS
C
100  format(/,'_____')
105  format(' ')
110  format(/,30x,'INPUT DATA')
115  format(28x,' ')
120  format(/,'NUMBER OF NODES =',13)
125  format(/,'POISSON'S RATIO =',f7.4)
130  format(1,'PLANE STRESS')
135  format(/,'PLANE STRAIN')
200  format(/,'NODE AND ELEMENT INFORMATION')
205  format(/,'NO',4x,'X',9x,'Y',8x,'XM',7x,'YM',6x,'S',5x,'RNX',
&      5x,'RNY')

```



```

210 format( i2,f10.5,f10.5,f8.5,1x,f8.5,1x,f6.3,1x,f6.3,1x,f6.3)
215 format(/,"BOUNDARY CONDITIONS')
220 format( i3,1x,' U1=',f8.4,' U2=',f8.4)
225 format( i3,1x,' T1=',f8.4,' U2=',f8.4)
230 format( i3,1x,' U1=',f8.4,' T2=',f8.4)
235 format( i3,1x,' T1=',f8.4,' T2=',f8.4)
299 format(/,'***** CALCULATED RESULTS *****')
315 format(/,'X-DISPLACEMENTS')
320 format(/,'NO',4x,'X',9x,'Y',8x,'UXA',7x,'UXB',7x,'UXC',6x,
& 'EXACT')
322 format( i2,f10.5,f10.5,f10.5,f10.5,f10.5,f10.5)
325 format( i2,f7.2,2x,f7.2,2x,f7.2)
330 format(/,'Y-DISPLACEMENTS')
340 format(/,'X-TRACTIONS')
345 format(/,'NO',4x,'X',9x,'Y',8x,'TXA',7x,'TXB',7x,'TXC',6x,
& 'EXACT')
350 format(/,'Y-TRACTIONS')
355 format(/,'NO',4x,'X',9x,'Y',8x,'TYA',7x,'TYB',7x,'TYC',6x,
& 'EXACT')
360 format(/,'INTERIOR VALUES')
365 format(/,'INTERIOR X-DISP')
370 format(/,'NO',4x,'X',9x,'Y',8x,'UXA',7x,'UXB',7x,'UXC',6x,
& 'EXACT')
375 format(/,'INTERIOR Y-DISP')
380 format(/,'NO',4x,'X',9x,'Y',8x,'UYA',7x,'UYB',7x,'UYC',6x,
& 'EXACT')
385 format(/,'INTERIOR SXX')
390 format(/,'NO',4x,'X',9x,'Y',9x,'A',9x,'B',9x,'C',9x,'EXACT')
392 format(/,'NO',4x,'A',7x,'B',6x,'C')
395 format(/,'INTERIOR SXY')
400 format(/,'INTERIOR SY Y')
405 format(/,'PERCENT DIFFERENCE')
410 format( i2,1x,'***** ***** *****')
C
999 stop
end
subroutine bndry(n,x,y,xm,ym,rx,ry,s)
C
parameter (mn=75)
C
dimension xm(mn),ym(mn),rx(mn),ry(mn),s(mn)
dimension x(mn),y(mn)
C
istop=0
C
1 write(*,*)'ENTER THE TOTAL NUMBER OF BOUNDARY SEGMENTS.'
read(*,*)nb
nel=0. do 10 i=1,nb
ichange=0
99 write(*,90)i
90 format(/,'IS SEGMENT',i2,'?'
write(*,*)'
write(*,*)' 1. STRAIGHT'
write(*,*)' 2. CIRCULAR'

```

```

write(*,*)' 3. ELLIPTICAL'
write(*,*)'
read(*,*)ntype
C
write(*,*)'DO YOU WANT TO CHANGE THIS?'
write(*,*)'
write(*,*)' 1 = YES'
write(*,*)' 2 = NO'
read(*,*)ichange
write(*,*)'
if(ichange.eq.1)goto 99
C
if(ntype.eq.1)then
98 write(*,101)i
101 format(/,'ENTER THE FOLLOWING INFORMATION FOR SEGMENT ',i2)
write(*,102)
102 format(/,' BEG. NODE NO.,X(I),Y(I),X(J),Y(J),NO. OF
& ELEMENTS')
write(*,*)'
read(*,*)nbeg,xi,yi,xj,yj,ne
C
write(*,*)'DO YOU WANT TO CHANGE THIS?'
write(*,*)'
write(*,*)' 1 = YES'
write(*,*)' 2 = NO'
read(*,*)ichange
write(*,*)'
if(ichange.eq.1)goto 98
C
x(nbeg)=xi
y(nbeg)=yi
dx=xj-xi
dy=yj-yi
sx=dx/ne
sy=dy/ne
nel=ne-1
do 20 j=1,nel
k=nbeg+j
kl=k-1
x(k)=x(kl)+sx
y(k)=y(kl)+sy
20 continue
else if(ntype.eq.2)then
97 write(*,101)i
write(*,103)
103 format(/,' NBEG,XI,YI,XC,YC,R,THETA,NO.OF ELEMENTS')
write(*,104)
104 format(/,' (THETA=ARC IN DEGREES)')
write(*,*)'
read(*,*)nbeg,xi,yi,xc,yc,r,beta,ne
C
write(*,*)'DO YOU WANT TO CHANGE THIS?'
write(*,*)'
write(*,*)' 1 = YES'

```

```

write(*,*)' 2 = NO'
read(*,*)ichange
write(*,*)' '
if(ichange.eq.1)goto 97
C
write(*,*)' '
pi=4.*atan(1.)
theta=(beta*pi)/180.
phi=theta/ne
delx=(xi-xc)/r
dely=(yi-yc)/r
if(dely.ge.0.)then
alpha=acos(delx)
else
alpha=2.*pi-acos(delx)
endif
x(nbeg)=xi
y(nbeg)=yi
nel=ne-1
do 30 j=1,nel
k=nbeg+j
kl=k-1
kpl=k+1
alpha1=alpha+2.*phi
alpha=alpha+phi
x(k)=xc+r*cos(alpha)
y(k)=yc+r*sin(alpha)
x(kpl)=xc+r*cos(alpha1)
y(kpl)=yc+r*sin(alpha1)
30 continue
nbeg1=nbeg+1
else if(ntype.eq.3)then
96 write(*,101)i
write(*,105)
105 format(/,' NBEG,X(I),Y(I),ALPHA,A,B,THETA,NO. OF ELEMENTS')
WRITE(*,106)
106 format(/,'(CENTER AT ORIGIN ; THETA = ARC IN DEGREES)')
write(*,*)'(ALPHA = ANGLE TO FIRST POINT)'
read(*,*)nbeg,xi,yi,alpha,a,b,beta,ne
C
write(*,*)'DO YOU WANT TO CHANGE THIS?'
write(*,*)' '
write(*,*)' 1 = YES'
write(*,*)' 2 = NO'
read(*,*)ichange
write(*,*)' '
if(ichange.eq.1)goto 96
C
write(*,*)' '
pi=4.*atan(1.)
theta=(beta*pi)/180.
phi=theta/ne
x(nbeg)=xi
y(nbeg)=yi

```

```

nel=ne-1
a2=a*a
b2=b*b
top=a2*b2
do 40 j=1,nel
k=nbeg+j
k1=k-1
kp1=k+1
alpha=alpha+phi
bot=a2*sin(alpha)*sin(alpha)+b2*cos(alpha)*cos(alpha)
r2=top/bot
r=sqrt(r2)
x(k)=r*cos(alpha)
y(k)=r*sin(alpha)
40 continue
nbeg1=nbeg+1
else
write(*,*) 'AT THIS TIME I CANNOT GENERATE ELEMENTS FOR THIS'
write(*,*) 'TYPE OF BOUNDARY SEGMENT.'
goto 99
endif
nel=nel+ne
10 continue
write(*,*) 'THIS IS THE MESH'
write(*,*) 'NODE      X          Y          '
do 50 m=1,nel
write(*,503)m,x(m),y(m)
503 format(1x,i3,3x,f10.6,2x,f10.6)
50 continue
write(*,*) '
do 60 i=1,n
if(i.eq.1)then
im1=n
else
im1=i-1
endif
xm(i)=(x(i)+x(im1))/2.
ym(i)=(y(i)+y(im1))/2.
dx=x(i)-x(im1)
dy=y(i)-y(im1)
s(i)=sqrt(dx*dx+dy*dy)
if(ntype.eq.2)then
rnx(i)=xm(i)
rny(i)=ym(i)
else
rnx(i)=dy/s(i)
rny(i)=-dx/s(i)
endif
60 continue
C
70 return
end

```

subroutine bdc(n,mm,pr,xm,ym,xf,yf,rnx,rny,ue,te,bc,ibc,

```

&      bcon,uxe,uye,socx,sxye,syye)
C
      parameter (nn=75)
      parameter (nnn=2*nn)
      parameter (mmm=50)
C
      dimension xm(nn),ym(nn),xf(nn),yf(nn),rx(nn),ry(nn)
      dimension bc(mnn),ibc(nn,2),bcon(mnn)
      dimension ue(mnn),te(mnn)
      dimension uxe(mmm),uye(mmm),socx(mmm),sxye(mmm),syye(mmm)
C
      nn=2*n
C
100  write(*,*)'ENTER PROBLEM TYPE'
      write(*,*)'  1 = PURE EXTENSION'
      write(*,*)'  2 = RECTANGLE'
      write(*,*)'  3 = CIRCLE'
      read(*,*)iprob
      write(*,*)'
C
      if(iprob.eq.1)then
      do 10 i=1,n
      i1=2*(i-1)+1
      i2=2*(i-1)+2
      xm2=xm(i)*xm(i)
      ym2=ym(i)*ym(i)
      ym3=xm2*xm(i)
      ym3=ym2*ym(i)
C
      if(ym(i).eq.0.)then
      bc(i1)=0.
      bc(i2)=0.
      ibc(i,2)=1
      bcon(i1)=0.
      bcon(i2)=0.
      ue(i1)=-0.1*xm(i)
      ue(i2)=0.
      te(i1)=0.
      te(i1)=-1.
C
      else if(xm(i).eq.1.)then
      bc(i1)=0.
      bc(i2)=0.
      bcon(i1)=0.
      bcon(i2)=0.
      ue(i1)=-0.1
      ue(i2)=0.4*ym(i)
      te(i1)=0.
      te(i2)=0.
C
      else if(ym(i).eq.2.)then
      bc(i1)=0.
      bc(i2)=1.
      bcon(i1)=0.

```

```

      bcon(i2)=1.
      ue(i1)=-0.1*xm(i)
      ue(i2)=0.4*ym(i)
      te(i1)=0.
      te(i2)=1.
C
      else
      bc(i1)=0.
      bc(i2)=0.
      ibc(i,1)=1
      bcon(i1)=0.
      bcon(i2)=0.
      ue(i1)=0.
      ue(i2)=0.4*ym(i)
      te(i1)=0.
      te(i2)=0.
      endif
C
10  continue
C
      do 15 i=1,mm
C
      saxe(i)=0.
      syye(i)=1.
      sxye(i)=0.
      wxe(i)=-0.1*xf(i)
      uye(i)=0.4*yf(i)
15  continue
C
      else if(iprob.eq.2) then
      do 20 i=1,n
      i1=2*(i-1)+1
      i2=2*(i-1)+2
      xm2=xm(i)*xm(i)
      ym2=ym(i)*ym(i)
      xm3=xm2*xm(i)
      ym3=ym2*ym(i)
C
      if(ym(i).eq.0.) then
      bc(i1)=xm(i)
      bc(i2)=-0.45*xm2
      ibc(i,2)=1
      bcon(i1)=bc(i1)
      bcon(i2)=bc(i2)
      ue(i1)=(4.*xm(i)-xm3/12.)/2.5
      ue(i2)=(-1.125*xm2)/2.5
      te(i1)=xm(i)
      te(i2)=0.
C
      else if(xm(i).eq.1.) then
      bc(i1)=3.75+ym2/2.
      bc(i2)=0.5*ym(i)-1.
      bcon(i1)=bc(i1)
      bcon(i2)=bc(i2)

```

```

ue(i1)=(47./12.+0.5625*ym2-ym(i)/4.)/2.5
ue(i2)=(ym2/2.-ym3/8.-15.*ym(i)/16.-1.125)/2.5
te(i1)=ym2/2.+3.75
te(i2)=ym(i)/2.-1.
C
  else if(ym(i).eq.1.)then
    bc(i1)=-0.5*xm(i)
    bc(i2)=0.75
    bcon(i1)=bc(i1)
    bcon(i2)=bc(i2)
    ue(i1)=(69.*xm(i)/16.-xm3/12.)/2.5
    ue(i2)=(-5./8.-17.*xm2/16.)/2.5
    te(i1)=-0.5*xm(i)
    te(i2)=0.75
C
  else
    bc(i1)=0.
    bc(i2)=0.
    ibc(i,1)=1
    bcon(i1)=0.
    bcon(i2)=0.
    ue(i1)=0.
    ue(i2)=(ym2/2.-ym3/8.-ym(i))/2.5
    te(i1)=-ym2/2.-4.
    te(i2)=0.
  endif
C
20 continue
C
  do 25 i=1,mm
    xf2=xf(i)*xf(i)
    yf2=yf(i)*yf(i)
    xf3=xf2*xf(i)
    yf3=yf2*yf(i)
C
    sxoxe(i)=4.-xf2/4.+yf2/2.
    syye(i)=yf(i)-yf2/4.
    sxye(i)=xf(i)*yf(i)/2.-xf(i)
    uxoe(i)=(xf(i)*(4.-xf2/12.tyf2/2.-(yf(i)-yf2/4.)/4.))/2.5
    uye(i)=(yf2/2.-yf3/12.-yf(i)*(4.-xf2/4.+yf2/6.)/4.-1.125*
&    xf2)/2.5
25 continue
C
  else if(iprob.eq.3)then
C
    write(*,*)'ENTER ELEMENTS WHERE UX=0'
    read(*,*)ix1,ix2
    write(*,*)'
    write(*,*)'ENTER ELEMENTS WHERE UY=0'
    read(*,*)iy1,iy2
    write(*,*)'
C
    do 30 i=1,n
      i1=2*(i-1)+1

```

```

      i2=2*(I-1)+2
C
      if(i.eq.ix1.or.i.eq.ix2)then
        bc(i1)=0.
        bc(i2)=-rny(i)
        ibc(i,1)=1
        boon(i1)=bc(i1)
        boon(i2)=bc(i2)
C
      else if(i.eq.iy1.or.i.eq.iy2)then
        bc(i1)=-rmx(i)
        bc(i2)=0.
        ibc(i,2)=1
        boon(i1)=bc(i1)
        boon(i2)=bc(i2)
C
      else
        bc(i1)=-rmx(i)
        bc(i2)=1rny(i)
        boon(i1)=bc(i1)
        boon(i2)=bc(i2)
      endif
C
      ue(i1)=-0.3*rmx(i)
      ue(i2)=-0.3*rny(i)
      te(i1)=-rmx(i)
      te(i2)=-rny(i)
C
30    continue
C
      do 35 i=1,mm
        uxe(i)=-0.3*xf(i)
        uye(i)=-0.3*yf(i)
        soxe(i)=-1.
        syye(i)=-1.
        sxye(i)=0.
35    continue
C
      else
        goto 100
      endif
C
      write(*,*)'BOUNDARY CONDITION VECTORS'
      write(*,*)'
      write(*,115)
115    format( 'NO',4x,'BC(I1) ',4x,'BC(I2) ',4x,'IBC(I,1) ',4x,'IBC
&      (I,2) ')
      do 40 i=1,n
        i1=2*(i-1)+1
        i2=2*(i-1)+2
        write(*,120)i,bc(i1),bc(i2),ibc(i,1),ibc(i,2)
120    format( i2,4x,f6.3,4x,f6.3,7x,i1,11x,i1)
40    continue
C

```



```

write(*,*) '
write(*,*) 'ENTER ANY NUMBER TO CONTINUE'
read(*,*) igo
write(*,*) '
C
  return
  end

  subroutine ingpts(r,w,w1,w2)
C
  dimension r(10),w(10),w1(10),w2(10)
C
C POINTS AND WEIGHTS FOR NUMERICAL INTEGRATION
C
  r(1)=.97390652851717
  r(2)=.86506336668898
  r(3)=.67940956829902
  r(4)=.43339539412925
  r(5)=.14887433898163
  r(6)=r(5)
  r(7)=r(4)
  r(8)=r(3)
  r(9)=r(2)
  r(10)=r(1)
C
  w(1)=.066671344308688
  w(2)=.14945134915058
  w(3)=.21908636251598
  w(4)=.26926671931000
  w(5)=.29552422471475
  w(6)=w(5)
  w(7)=w(4)
  w(8)=w(3)
  w(9)=w(2)
  w(10)=w(1)
C
  do 10 l=1,10
  w1(l)=1.-r(l)
  w2(l)=1.r(l)
10 continue
C
  return
  end

  subroutine casea(n,pr,x,y,xm,ym,rx,ry,s,r,w,a,b)
C
  parameter (nn=75)
  parameter (mnn=2*nn)
C
  dimension x(nn),y(nn)
  dimension xm(nn),ym(nn),rx(nn),ry(nn),s(nn)
  dimension a(mnn,mnn),b(mnn,mnn),r(10),w(10)
C
C COMPUTE COEFFICIENT MATRICES

```

```

C
  nr=2*n
  pi=4.*atan(1.)
  c1=(1.+pr)
  c2=(1.-pr)
  c3=(3.+pr)
  c4=(3.-pr)
  c5=(1.+3.*pr)
C
  do 2 j=1,n
    jj2=2*j
    jj1=jj2-1
C
    if(j.eq.1) then
      jml=n
      jj2m2=nr
    else
      jml=j-1
      jj2m2=jj2-2
    endif
    jj1m2=jj2m2-1
C
    if(j.eq.n) then
      jpl=1
      jj2p2=2
    else
      jpl=j+1
      jj2p2=jj2+2
    endif
    jj1p2=jj2p2-1
C
    rn1=rnx(j)
    rn2=rny(j)
    ds=s(j)
    rn12=rn1*rn1
    rn22=rn2*rn2
C
    b(jj1,jj1)=(c1*rn22-c4*(log(0.5*ds)-1.))*ds/2.
    b(jj1,jj2)=1c1*rn1*rn2*ds/2.
    b(jj2,jj1)=b(jj1,jj2)
    b(jj2,jj2)=(c1*rn12-c4*(log(ds*0.5)-1.))*ds/2.
C
    dmm1=x(j)-xm(j)
    dmm2=y(j)-ym(j)
    c=dmm1*dmm1+dmm2*dmm2
C
    do 2 i=1,n
      if(i.eq.j) goto 2
      ii2=2*i
      ii1=ii2-1
C
      drml=xm(i)-xm(j)
      drn2=ym(i)-ym(j)
      aa=drml*drml+drn2*drn2

```

```

bb=-2.*(dmm1*dmm1+dmm2*dmm2)
C
do 3 l=1,10
rho=sqrt(aa+bb*r(l)+c*r(l)*r(l))
qx=(dmm1-dmm1*r(l))/rho
qy=(dmm2-dmm2*r(l))/rho
qx2=qx*qx
qy2=qy*qy
qx3=qx2*qx
qy3=qy2*qy
cl2=2.*cl
C

t11=(cl2*(dmm2*qx3+dmm1*qy3)+c2*dmm2*qx-c3*dmm1*qy)/rho
t12=(cl2*(dmm1*qx3-dmm2*qy3)-c3*dmm1*qx+c5*dmm2*qy)/rho
t21=(cl2*(dmm1*qx3-dmm2*qy3)-c5*dmm1*qx+c3*dmm2*qy)/rho
t22=(-cl2*(dmm2*qx3+dmm1*qy3)+c3*dmm2*qx-c2*dmm1*qy)/rho
C

u11=(cl*qx2-c4*log(rho))*ds/4.
u12=cl*qx*qy*ds/4.
u22=(cl*qy2-c4*log(rho))*ds/4.
C

a(ii1,jj1)=a(ii1,jj1)+w(l)*t11
a(ii1,jj2)=a(ii1,jj2)+w(l)*t21
a(ii2,jj1)=a(ii2,jj1)+w(l)*t12
a(ii2,jj2)=a(ii2,jj2)+w(l)*t22
C

b(ii1,jj1)=b(ii1,jj1)+w(l)*u11
b(ii1,jj2)=b(ii1,jj2)+w(l)*u12
b(ii2,jj1)=b(ii2,jj1)+w(l)*u12
b(ii2,jj2)=b(ii2,jj2)+w(l)*u22
C
3 continue
2 continue
C

do 4 i=1,n
ii2=2*i
ii1=ii2-1
do 4 k=1,n
if(k.eq.i)goto 4
kk2=2*k
kk1=kk2-1
C

a(ii1,ii1)=a(ii1,ii1)-a(ii1,kk1)
a(ii1,ii2)=a(ii1,ii2)-a(ii1,kk2)
a(ii2,ii1)=a(ii2,ii1)-a(ii2,kk1)
a(ii2,ii2)=a(ii2,ii2)-a(ii2,kk2)
4 continue
C

write(*,*)'CONSTANT MATRICES CALCULATED'
write(*,*)'
C

return
end

```

```

subroutine caseb(n,pr,x,y,s,r,w,w1,w2,a,b)
C
  parameter (nn=75)
  parameter (nnn=2*nn)
C
  dimension x(nn),y(nn),s(nn)
  dimension r(10),w(10),w1(10),w2(10)
  dimension a(nnn,nnn),b(nnn,nnn)
C
C COMPUTE COEFFICIENT MATRICES
C
  nn=2*n
  pi=4.*atan(1.)
  c1=(1.+pr)
  c12=c1*2.
  c2=(1.-pr)
  c3=(3.+pr)
  c4=(3.-pr)
  c5=(1.+3.*pr)
C
  do 2 j=1,n
    jj2=2*j
    jj1=jj2-1
C
    if(j.eq.1)then
      jml=n
      jj2m2=nn
    else
      jml=j-1
      jj2m2=jj2-2
    endif
    jj1m2=jj2m2-1
C
    if(j.eq.n)then
      jpl=1
      jj2p2=2
    else
      jpl=j+1
      jj2p2=jj2+2
    endif
    jj1p2=jj2p2-1
C
    dx=x(j)-x(jml)
    dy=y(j)-y(jml)
    ds=sqrt(dx*dx+dy*dy)
    rnx=dy/ds
    rny=-dx/ds
C
    b(jj1,jj1)=(c4*(1.-log(ds))+c1*rny*rny)*ds/2.
    b(jj1,jj2)=1c1*rnx*rny*ds/2.
    b(jj2,jj1)=b(jj1,jj2)
    b(jj2,jj2)=(c4*(1.-log(ds))+c1*rnx*rnx)*ds/2.
C

```

```

dx=x(jp1)-x(j)
dy=y(jp1)-y(j)
dss=sqrt(dx*dx+dy*dy)
rmx=dy/dss
rny=-dx/dss
C
b(jj1,jj1p2)=(c4*(1.-log(dss))+c1*rny*rny)*dss/2.
b(jj1,jj2p2)=-c1*rmx*rny*dss/2.
b(jj2,jj1p2)=b(jj1,jj2)
b(jj2,jj2p2)=(c4*(1.-log(dss))+c1*rmx*rmx)*dss/2.
C
xm=(x(j)+x(jm1))/2.
ym=(y(j)+y(jm1))/2.
dmm1=x(j)-xm
dmm2=y(j)-ym
o=dmm1*dmm1+dmm2*dmm2
C
do 2 i=1,n
ii2=2*i
ii1=ii2-1
C
drml=x(i)-xm
drml2=y(i)-ym
aa=drml*drml+drml2*drml2
bb=-2.*(drml*dmm1+drml2*dmm2)
C
do 3 l=1,10
rho=sqrt(aa+bb*r(l)+c*r(l)*r(l))
qx=(drml-dmm1*r(l))/rho
qy=(drml2-dmm2*r(l))/rho
qp2=qx*qx
qy2=qy*qy
qp3=qp2*qx
qy3=qy2*qy
C
t11=(c12*(dmm2*qp3+dmm1*qy3)+c2*dmm2*qx-c3*dmm1*qy)/(2.*rho)
t12=(c12*(dmm1*qp3-dmm2*qy3)-c3*dmm1*qx+c5*dmm2*qy)/(2.*rho)
t21=(c12*(dmm1*qp3-dmm2*qy3)-c5*dmm1*qx+c3*dmm2*qy)/(2.*rho)
t22=(-c12*(dmm2*qp3+dmm1*qy3)+c3*dmm2*qx-c2*dmm1*qy)/
& (2.*rho)
C
if(i.eq.j)then
C
a(ii1,jj1m2)=a(ii1,jj1m2)+w(1)*w1(1)*t11
a(ii1,jj2m2)=a(ii1,jj2m2)+w(1)*w1(1)*t21
a(ii2,jj1m2)=a(ii2,jj1m2)+w(1)*w1(1)*t12
a(ii2,jj2m2)=a(ii2,jj2m2)+w(1)*w1(1)*t22
C
else if(i.eq.jm1)then
C
a(ii1,jj1)=a(ii1,jj1)+w(1)*w2(1)*t11
a(ii1,jj2)=a(ii1,jj2)+w(1)*w2(1)*t21
a(ii2,jj1)=a(ii2,jj1)+w(1)*w2(1)*t12
a(ii2,jj2)=a(ii2,jj2)+w(1)*w2(1)*t22

```

```

C      else
C
C      a(ii1,jj1m2)=a(ii1,jj1m2)+w(1)*w1(1)*t11
C      a(ii1,jj2m2)=a(ii1,jj2m2)+w(1)*w1(1)*t21
C      a(ii2,jj1m2)=a(ii2,jj1m2)+w(1)*w1(1)*t12
C      a(ii2,jj2m2)=a(ii2,jj2m2)+w(1)*w1(1)*t22
C
C      a(ii1,jj1)=a(ii1,jj1)+w(1)*w2(1)*t11
C      a(ii1,jj2)=a(ii1,jj2)+w(1)*w2(1)*t21
C      a(ii2,jj1)=a(ii2,jj1)+w(1)*w2(1)*t12
C      a(ii2,jj2)=a(ii2,jj2)+w(1)*w2(1)*t22
C
C      endif
C
C      if(i.eq.j.or.1.eq.jm1)goto 3
C
C      u11=(c1*qp2-c4*log(rho))*ds/4.
C      u12=c1*qp*qy*ds/4.
C      u22=(c1*qy2-c4*log(rho))*ds/4.
C
C      b(ii1,jj1)=b(ii1,jj1)+w(1)*u11
C      b(ii1,jj2)=b(ii1,jj2)+w(1)*u12
C      b(ii2,jj1)=b(ii2,jj1)+w(1)*u12
C      b(ii2,jj2)=b(ii2,jj2)+w(1)*u22
C
C      3      continue
C      2      continue
C
C      COMPUTE DIAGONAL ENTRIES OF [A]
C
C      do 4 i=1,n
C      ii2=2*i
C      ii1=ii2-1
C      do 4 k=1,n
C      if(i.eq.i)goto4
C      kk2=2*k
C      kk1=kk2-1
C
C      a(ii1,ii1)=a(ii1,ii1)-a(ii1,kk1)
C      a(ii1,ii2)=a(ii1,ii2)-a(ii1,kk2)
C      a(ii2,ii1)=a(ii2,ii1)-a(ii2,kk1)
C      a(ii2,ii2)=a(ii2,ii2)-a(ii2,kk2)
C      4      continue
C
C      write(*,*) 'NONISOPARAMETRIC MATRICES CALCULATED'
C      write(*,*) ' '
C
C      return
C      end
C
C      subroutine casec(n,pr,x,y,s,r,w,w1,w2,a,b)
C
C      parameter (nn=75)

```

```

parameter (mn=2*nn)

C
dimension x(mn),y(mn),s(mn)
dimension r(10),w(10),w1(10),w2(10)
dimension a(mn,mn),b(mn,mn)

C
C COMPUTE COEFFICIENT MATRICES
C
nn=2*n
pi=4,*atan(1.)
c1=(1.+pr)
c12=c1*2.
c2=(1.-pr)
c3=(3.+pr)
c4=(3.-pr)
c5=(1.+3.*pr)

C
do 2 j=1,n
jj2=2*j
jj1=jj2-1

C
if(j.eq.1)then
jml=n
jj2m2=nn
else
jml=j-1
jj2m2=jj2-2
endif
jj1m2=jj2m2-1

C
if(j.eq.n)then
jpl=1
jj2p2=2
else
jpl=j+1
jj2p2=jj2+2
endif
jj1p2=jj2p2-1

C
dx=x(j)-x(jml)
dy=y(j)-y(jml)
ds=sqrt(dx*dx+dy*dy)
rmx=dy/ds
rmy=-dx/ds

C
b(jj1,jj1m2)=(c4*(0.5-log(ds))+c1*rmy*rmy)*ds/4.
b(jj1,jj2m2)=1c1*rmx*rmy*ds/4.
b(jj2,jj1m2)=b(jj1,jj2)
b(jj2,jj2m2)=(c4*(0.5-log(ds))+c1*rmx*rmx)*ds/4.

C
b(jj1,jj1)=(c4*(1.5-log(ds))+c1*rmy*rmy)*ds/4.
b(jj1,jj2)=-c1*rmx*rmy*ds/4.
b(jj2,jj1)=b(jj1,jj2)
b(jj2,jj2)=(c4*(1.5-log(ds))+c1*rmx*rmx)*ds/4.

```

```

C
dx=x(jp1)-x(j)
dy=y(jp1)-y(j)
dss=sqrt(dx*dx+dy*dy)
rmx_dy/dss
rny=-dx/dss

C
b(jj1,jj1)=b(jj1,jj1)+(c4*(1.5-log(dss))+c1*rny*rny)*dss/4.
b(jj1,jj2)=b(jj1,jj2)-c1*rmx*rny(dss/4.
b(jj2,jj1)=b(jj1,jj2)
b(jj2,jj2)=b(jj2,jj2)+(c4*(1.5-log(dss))+c1*rmx*rmx)*dss/4.

C
b(jj1,jj1p2)=(c4*(0.5-log(dss))+c1*rny*rny)*dss/4.
b(jj1,jj2p2)=-c1*rmx*rny(dss/4.
b(jj2,jj1p2)=b(jj1,jj2)
b(jj2,jj2p2)=(c4*(0.5-log(dss))+c1*rmx*rmx)*dss/4.

C
xm=(x(j)+x(jm1))/2.
ym=(y(j)+y(jm1))/2.
dmm1=x(j)-xm
dmm2=y(j)-ym
c=dmm1*dmm1+dmm2*dmm2

C
do 2 i=1,n
ii2=2*i
ii1=ii2-1

C
drm1=x(i)-xm
drm2=y(i)-ym
aa=drm1*drm1+drm2*drm2
bb=-2.*(drm1*dmm1+drm2*dmm2)

C
do 3 l=1,10
rho=sqrt(aa+bb*r(l)+c*r(l)*r(l))
qx=(drm1-dmm1*r(l))/rho
qy=(drm2-dmm2*r(l))/rho
qx2=qx*qx
qy2=qy*qy
qx3=qx2*qx
qy3=qy2*qy

C
t11=(c12*(dmm2*qx3+dmm1*qy3)+c2*dmm2*qx-c3*dmm1*qy)/(2.*rho)
t12=(c12*(dmm1*qx3-dmm2*qy3)-c3*dmm1*qx+c5*dmm2*qy)/(2.*rho)
t21=(c12*(dmm1*qx3-dmm2*qy3)-c5*dmm1*qx+c3*dmm2*qy)/(2.*rho)
t22=(-c12*(dmm2*qx3+dmm1*qy3)+c3*dmm2*qx-c2*dmm1*qy)/
& (2.*rho)
C
if(i.eq.j)then
C
a(ii1,jj1m2)=a(ii1,jj1m2)+w(1)*w1(1)*t11
a(ii1,jj2m2)=a(ii1,jj2m2)+w(1)*w1(1)*t21
a(ii2,jj1m2)=a(ii2,jj1m2)+w(1)*w1(1)*t12
a(ii2,jj2m2)=a(ii2,jj2m2)+w(1)*w1(1)*t22
C

```



```

      else if(i.eq.jm1)then
C
      a(ii1,jj1)=a(ii1,jj1)+w(1)*w2(1)*t11
      a(ii1,jj2)=a(ii1,jj2)+w(1)*w2(1)*t21
      a(ii2,jj1)=a(ii2,jj1)+w(1)*w2(1)*t12
      a(ii2,jj2)=a(ii2,jj2)+w(1)*w2(1)*t22
C
      else
C
      a(ii1,jj1m2)=a(ii1,jj1m2)+w(1)*w1(1)*t11
      a(ii1,jj2m2)=a(ii1,jj2m2)+w(1)*w1(1)*t21
      a(ii2,jj1m2)=a(ii2,jj1m2)+w(1)*w1(1)*t12
      a(ii2,jj2m2)=a(ii2,jj2m2)+w(1)*w1(1)*t22
C
      a(ii1,jj1)=a(ii1,jj1)+w(1)*w2(1)*t11
      a(ii1,jj2)=a(ii1,jj2)+w(1)*w2(1)*t21
      a(ii2,jj1)=a(ii2,jj1)+w(1)*w2(1)*t12
      a(ii2,jj2)=a(ii2,jj2)+w(1)*w2(1)*t22
C
      endif
C
      if(i.eq.j.or.i.eq.jm1)goto 3
C
      u11=(c1*qp2-c4*log(rho))*ds/8.
      U12=c1*qr*qy(ds/8.
      u22=(c1*qy2-c4*log(rho))*ds/8.
C
      b(ii1,jj1m2)=b(ii1,jj1m2)+w(1)*w1(1)*u11
      b(ii1,jj2m2)=b(ii1,jj2m2)+w(1)*w1(1)*u12
      b(ii2,jj1m2)=b(ii2,jj1m2)+w(1)*w1(1)*u12
      b(ii2,jj2m2)=b(ii2,jj2m2)+w(1)*w1(1)*u22
C
      b(ii1,jj1)=b(ii1,jj1)+w(1)*w2(1)*u11
      b(ii1,jj2)=b(ii1,jj2)+w(1)*w2(1)*u12
      b(ii2,jj1)=b(ii2,jj1)+w(1)*w2(1)*u12
      b(ii2,jj2)=b(ii2,jj2)+w(1)*w2(1)*u22
C
3      continue
2      continue
C
C COMPUTE DIAGONAL ENTRIES OF [A]
C
      do 4 i=1,n
      ii2=2*i
      ii1=ii2-1
      do 4 k=1,n
      if(k.eq.i)goto 4
      kk2=2*k
      kk1=kk2-1
C
      a(ii1,ii1)=a(ii1,ii1)-a(ii1,kk1)
      a(ii1,ii2)=a(ii1,ii2)-a(ii1,kk2)
      a(ii2,ii1)=a(ii2,ii1)-a(ii2,kk1)
      a(ii2,ii2)=a(ii2,ii2)-a(ii2,kk2)

```

```

4  continue
C
  write(*,*) 'ISOPARAMETRIC MATRICES CALCULATED'
  write(*,*) '          '
C
  return
  end

  subroutine gauss(ucc,rhs,n)
C
  parameter (nn=75)
  parameter (mnn=2*nn)
  parameter (mnn1=mnn+1)
C
  dimension ucc(mnn,mnn),rhs(mnn)
  dimension aug(mnn,mnn1)
C
  nml=nn-1
  npl=nn+1
C
C SET UP THE AUGMENTED MATRIX FOR AX=B
C
  do 2 i=1,nn
    do 1 j=1,nn
      aug(i,j)=ucc(i,j)
1    continue
      aug(i,npl)=rhs(i)
2    continue
C
C THE OUTER LOOP USES ELEMENTARY ROW OPERATIONS TO TRANSFORM THE
C AUGMENTED MATRIX INTO ECHELON FORM.
C
  do 5 i=1,nml
C
C SEARCH FOR THE LARGEST ENTRY IN COLUMN I, ROWS I THROUGH N.
C IPIVOT IS THE ROW INDEX OF THE LARGEST ENTRY.
C
    pivot=0.
    do 3 j=1,nn
      temp=abs(aug(j,i))
      if(pivot.ge.temp) go to 3
      pivot=temp
      ipivot=j
3    continue
      if(pivot.eq.0.) goto 13
      if(ipivot.eq.i) goto 5
C
C INTERCHANGE ROW I AND ROW IPIVOT.
C
    do 4 k=1,npl
      temp=aug(i,k)
      aug(i,k)=aug(ipivot,k)
      aug(ipivot,k)=temp
4    continue

```

```

C
C ZERO ENTRIES (I+1,I),(I+2,I),...,(N,I) IN THE AUGMENTED MATRIX.
C
5   ip1=i+1
   do 7 k=ip1,nm
     q=qug(k,i)/aug(i,i)
     aug(k,i)=0.
     do 6 j=ip1,np1
       qug(k,j)=a*aug(i,j)+aug(k,j)
6   continue
7   continue
8   continue
   if(aug(nm,nm).eq.0.) goto 13
C
C BACKSOLVE TO OBTAIN SOLUTION TO AX=B.
C
   rhs(nm)=aug(nm,np1)/aug(nm,nm)
   do 10 k=1,nm1
     q=0.
     do 9 j=1,k
       q=q+aug(nm-k,np1-j)*rhs(np1-j)
9   continue
     rhs(nm-k)=(aug(nm-k,np1)-q)/aug(nm-k,nm-k)
10  continue
C
C CALCULATE THE NORM OF THE RESIDUAL VECTOR,B-AX, SET IERROR=1
C AND RETURN.
C
   rsq=0.
   do 12 i=1,nm
     q=0.
     do 11 j=1,nm
       q=q+uoc(i,j)*rhs(j)
11  continue
     resi=rhs(i)-q
     rmag=abs(resi)
     rsq=rsq+rmag*rmag
12  continue
   rnorm=sqrt(rsq)
   ierror=1
C
   write(*,*)'SYSTEM OF EQUATIONS SOLVED'
   write(*,*)'
C
   return
C
C ABNORMAL RETURN—REDUCTION TO ECHELON FORM PRODUCES A ZERO ON
C THE DIAGONAL. THE MATRIX A MAY BE SINGULAR.
C
13  ierror=2
C
   write(*,*)'WARNING—MATRIX MAY BE SINGULAR!'
   write(*,*)'
   write(*,*)'ENTER ANY NUMBER TO CONTINUE'

```

```

      read(*,*)igoes
      write(*,*)'      '
C
      return
      end

      subroutine flda(n,mm,pr,x,y,r,w,w1,w2,ua,ta,xf,yf,uxa,uya,
&      soca,sxya,syya)
C
      parameter(mn=75)
      parameter(mrn=2*mn)
      parameter(mrn1=mrn+1)
      parameter(mmm=5)
C
      dimension x(mn),y(mn)
      dimension r(10,w(10,w1(10,w2(10)
      dimension ua(mrn),ta(mrn),fa(mrn)
      dimension xf(mmm),yf(mmm)
      dimension ul(5,mrn),ur(5,mrn)
      dimension uxa(mmm),uya(mmm)
      dimension soca(mmm),sxya(mmm),syya(mmm)
C
      mr=2*n
C
      pl=4,*atan(1.)
C
      c1=1.+pr
      c2=1.-pr
      c3=3.+pr
      c4=3.-pr
      c5=1.+3.*pr
C
      do 135 ii=1,mm
C
      do 136 i=1,mr
      do 136 k=1,5
      ul(k,i)=0.
      ur(k,i)=0.
136 continue
C
      do 137 j=1,n
      if(j.eq.1)then
      jml=n
      else
      jml=j-1
      endif
      jj2=2*j
      jj1=jj2-1
C
      if(j.eq.1)then
      jj2m2=mr
      else
      jj2m2=jj2-2
      endif

```

```

C      jj1m2=jj2m2-1
C      dx=x(j)-x(jm1)
C      dy=y(j)-y(jm1)
C      s=sqrt(dx*dx+dy*dy)
C      fa(jj1)=ta(jj1)*s
C      fa(jj2)=ta(jj2)*s
C      xmi=(x(j)+x(jm1))/2.
C      ymi=(y(j)+y(jm1))/2.
C      dmm1=x(j)-xmi
C      dmm2=y(j)-ymi
C      c=dmm1*dmm1+dmm2*dmm2
C      drml=xf(ii)-xmi
C      drm2=yf(ii)-ymi
C      aa=drml*drml+drm2*drm2
C      bb=-2.*(drml*dmm1+drm2*dmm2)
C      do 137 l=1,10
C      rho=sqrt(aa+bb*r(l)+c*r(l)*r(l))
C      rho2=rho*rho
C      qx=(drml-dmm1*r(l))/rho
C      qy=(drm2-dmm2*r(l))/rho
C      qx2=qx*qx
C      qy2=qy*qy
C      qx3=qx2*qx
C      qy3=qy2*qy
C      qx4=qx2*qx2
C      qy4=qy2*qy2
C      t11=2.*(2.*c1*(dmm2*qx3+dmm1*qy3)+c2*dmm2*qx-c3*dmm1*qy)/rho
C      t21=2.*(2.*c1*(dmm1*qx3-dmm2*qy3)-c5*dmm1*qx+c3*dmm2*qy)/rho
C      t12=2.*(2.*c1*(dmm1*qx3-dmm2*qy3)-c3*dmm1*qx+c5*dmm2*qy)/rho
C      t22=2.*(2.*c1*(-dmm2*qx3-dmm1*qy3)+c3*dmm2*qx-c2*dmm1*qy)
C      & /rho
C      ul(1,jj1)=ul(1,jj1)+w(1)*t11
C      ul(1,jj2)=ul(1,jj2)+w(1)*t21
C      ul(2,jj1)=ul(2,jj1)+w(1)*t12
C      ul(2,jj2)=ul(2,jj2)+w(1)*t22
C      u11=(-c4*log(rho)+c1*qx*qx)/2.
C      u12=c1*qx*qy/2.
C      u22=(-c4*log(rho)+c1*qy*qy)/2.
C      ur(1,jj1)=ur(1,jj1)+w(1)*u11
C      ur(1,jj2)=ur(1,jj2)+w(1)*u12
C      ur(2,jj1)=ur(2,jj1)+w(1)*u12
C      ur(2,jj2)=ur(2,jj2)+w(1)*u22
C      s111=4.*((8.*qx4-4.*qx2-1.)*dmm2-2.*qx*qy*(4.*qx2-1.)*dmm1)
C      & /rho2
C      s211=4.*(2.*qx*qy*(4.*qx2-1.)*dmm2-(8.*qx2*qy2-1.)*dmm1)

```

```

& /rho2
s221=4.*((8.*qx2*qy2-1.)*dmm2-2.*qx*qy((4.*qy2-1.)*dmm1)
& /rho2
s222=4.*(2.*qx*qy()4.*qy2-1.)*dmm2-(8,*qy4-4.*qy2-1.)*dmm1/
& /rho2
C
ul(3,jj1)=ul(3,jj1)+w(1)*s111
ul(3,jj2)=ul(3,jj2)+w(1)*s211
ul(r,jj1)=ul(4,jj1)+w(1)*s211
ul(4,jj2)=ul(4,jj2)+w(1)*s221
ul(5,jj1)=ul(5,jj1)+w(1)*s221
ul(5,jj2)=ul(5,jj2)+w(1)*s222
C
d111=(-2.*c1*qx3-c2*qx)/rho
d112=(8.*c1*qy3-c5*qy)/rho
d121=(2.*c1*qy3-c3*qy)/rho
d122=(2.*c1*qx3-c3*qx)/rho
d221=(2.*c1*qx3-c5*qx)/rho
d222=(-2.*c1*qy3-c2*qy)/rho
C
ur(3,jj1)=ru(3,jj1)+w(1)*d111
ur(3,jj2)=ur(3,jj2)+w(1)*d112
ur(4,jj1)=ur(4,jj1)+w(1)*d121
ur(4,jj2)=ur(4,jj2)+w(1)*d122
ur(5,jj1)=ur(5,jj1)+w(1)*d221
ur(5,jj2)=ur(5,jj2)+w(1)*d222
C
137 continue
C
uux=0.
uuy=0.
ssxx=0.
ssxy=0.
ssyy=0.
C
do 142 i=1,mn
uux=uux-ul(1,i)*ua(i)+ur(1,i)*fa(i)
uuy=uuy-ul(2,i)*us(i)+ur(2,i)*fa(i)
ssxx=ssxx+c1*ul(3,i)*ua(i)+ur(3,i)*fa(i)
ssxy=ssxy+c1*ul(4,i)*ua(i)+ur(4,i)*fa(i)
ssyy=ssyy+c1*ul(5,i)*ua(i)+ur(5,i)*fa(i)
142 continue
C
uux(ii)=uux/(8.*pi)
uuy(ii)=uuy/(8.*pi)
ssxx(ii)=ssxx/(8.*pi)
ssxy(ii)=ssxy/(8.*pi)
ssyy(ii)=ssyy/(8.*pi)
C
135 continue
C
return
end

```

```

      subroutine fldb(n,mm,pr,x,y,r,w,w1,w2,ub,tb,sf,yf,wdb,uyb,
&      socb,sxyb,syyb)
C
      parameter(mn=75)
      parameter(mrn=2*mn)
      parameter(mrn1=mrn+1)
      parameter(mmm=50)
C
      dimension x(mn),y(mn)
      dimension r(10),w(10),w1(10),w2(10)
      dimension ub(mrn),tb(mrn),fb(mrn)
      dimension xf(mmm),yf(mmm)
      dimension ul(5,mrn),ur(5,mrn)
      dimension wdb(mmm),uyb(mmm)
      dimension socb(mmm),sxyb(mmm),syyb(mmm)
      dimension temp1(5),temp2(5),temp3(5),temp4(5)
C
      nn=2*n
C
      pi=4.*atan(1.)
C
      c1=1.+pr
      c2=1.-pr
      c3=3.+pr
      c4=3.-pr
      c5=1.+3.*pr
C
      do 135 ii=1,mm
C
      do 136 i=1,mn
      do 136 k=1,5
      ul(k,i)=0.
      ur(k,i)=0.
136 continue
C
      do 137 j=1,n
      if(j.eq.1)then
      jml=n
      else
      jml=j-1
      endif
      jj2=2*j
      jj1=jj2-1
C
      if(j.eq.1)then
      jj2m2=mn
      else
      jj2m2=jj2-2
      endif
      jj1m2=jj2m2-1
C
      dx=x(j)-x(jml)
      dy=y(j)-y(jml)
      s=sqrt(dx*dx+dy*dy)

```

```

fb(jj1)=tb(jj1)*s
fb(jj2)=tb(jj2)*s
C
xmi=(x(j)+x(jm1))/2.
ymi=(y(j)+y(jm1))/2.
dmm1=x(j)-xmi
dmm2=y(j)-ymi
o=dmm1+dmm1+dmm2+dmm2
C
drml=xf(ii)-xmi
drn2=yf(ii)-ymi
aa=drml*drml+drn2*drn2
bb=-2.*(drml*dmm1+drn2*dmm2)
C
do 137 l=1,10
rho=sqrt(aa+bb*r(l)+c*r(l)*r(l))
rho2=rho*rho
qx=(drml-dmm1*r(l))/rho
qy=(drn2-dmm2*r(l))/rho
qx2=qx*qx
qy2=qy*qy
qx3=qx2*qx
qy3=qy2*qy
qx4=qx2*qx2
qy4=qy2*qy2
C
t11=(2.*c1*(dmm2*qx3+dmm1*qy3)+c2*dmm2*qx-c3*dmm1*qy)/rho
t21=(2.*c1*(dmm1*qx3-dmm2*qy3)-c5*dmm1*qx+c3*dmm2*qy)/rho
t12=(2.*c1*(dmm1*qx3-dmm2*qy3)-c3*dmm1*qx+c5*dmm2*qy)/rho
t22=(2.*c1*(-dmm2*qx3-dmm1*qy3)+c3*dmm2*qx-c2*dmm1*qy)/rho
C
ul(1,jj1m2)=ul(1,jj1m2)+w(1)*w1(1)*t11
ul(1,jj2m2)=ul(1,jj2m2)+w(1)*w1(1)*t21
ul(2,jj1m2)=ul(2,jj1m2)+w(1)*w1(1)*t12
ul(2,jj2m2)=ul(2,jj2m2)+w(1)*w1(1)*t22
C
ul(1,jj1)=ul(1,jj1)+w(1)*w2(1)*t11
ul(1,jj2)=ul(1,jj2)+w(1)*w2(1)*t21
ul(2,jj1)=ul(2,jj1)+w(1)*w2(1)*t12
ul(2,jj2)=ul(2,jj2)+w(1)*w2(1)*t22
C
u11=(-c4*log(rho)+c1*qx*qx)/2.
u12=c1*qx*qy/2.
u22=(-c4*log(rho)+c1*qy*qy)/2.
C
ur(1,jj1)=ur(1,jj1)+w(1)*u11
ur(1,jj2)=ur(1,jj2)+w(1)*u12
ur(2,jj1)=ur(2,jj1)+2(1)*u12
ur(2,jj2)=ur(2,jj2)+w(1)*u22
C
s111=2.*((8.*qx4-4.*qx2-1.)*dmm2-2.*qx*qy*(4.*qx2-2.)*dmm1)
& /rho2
s211=2.*(2.*qx*qy*(4.*qx2-1.)*dmm2-(8.*qx2*qy2-1.)*dmm1)
& /rho2

```



```

      s221=2.*(8.*qx2*qy2-1.)*dmm2-2.*qx*qy*(4.*qy2-1.)*dmm1)
& /rho2
      s222=2.*(2.*qx*qy*(4.*qy2-1.)*dmm2-(8.*qy4-4.*qy2-1.)*dmm1)
& /rho2
C
      ul(3,jj1m2)=ul(3,jj1m2)+w(1)*w1(1)*s111
      ul(3,jj2m2)=ul(3,jj2m2)+w(1)*w1(1)*s211
      ul(4,jj1m2)=ul(4,jj1m2)+w(1)*w1(1)*s211
      ul(4,jj2m2)=ul(4,jj2m2)+w(1)*w1(1)*s221
      ul(5,jj1m2)=ul(5,jj1m2)+w(1)*w1(1)*s221
      ul(5,jj2m2)=ul(5,jj2m2)+w(1)*w1(1)*s222
C
      ul(3,jj1)+ul(3,jj1)+w(1)*w2(1)*s111
      ul(3,jj2)+ul(3,jj2)+w(1)*w2(1)*s211
      ul(4,jj1)+ul(4,jj1)+w(1)*w2(1)*s211
      ul(4,jj2)+ul(4,jj2)+w(1)*w2(1)*s221
      ul(5,jj1)+ul(5,jj1)+w(1)*w2(1)*s221
      ul(5,jj2)+ul(5,jj2)+w(1)*w2(1)*s222
C
      d111=(-2.*c1*qx3-c2*qx)/rho
      d112=(2.*c1*qy3-c5*qy)/rho
      d121=(2.*c1*qy3-c3*qy)/rho
      d122=(2.*c1*qx3-c3*qx)/rho
      d221=(2.*c1*qx3-c5*qx)/rho
      d222=(-2.*c1*qy3-c2*qy)/rho
C
      ur(3,jj1)=ur(3,jj1)+w(1)*d111
      ur(3,jj2)=ur(3,jj2)+w(1)*d112
      ur(4,jj1)=ur(4,jj1)+w(1)*d121
      ur(4,jj2)=ur(4,jj2)+w(1)*d122
      ur(5,jj1)=ur(5,jj1)+w(1)*d221
      ur(5,jj2)=ur(5,jj2)+w(1)*d222
C
137 continue
C
C POST-MULTIPLY UL BY GAMMA TRANSPOSE INVERSE
C
      aa=-1
      do 138 l=1,5
        temp1(l)=ul(1,1)
        temp2(l)=ul(1,2)
138 continue
C
      do 139 k=2,n
        kk2=2*k
        kk1=kk2-1
C
        do 140 l=1,5
          ul(1,1)=ul(1,1)+ul(1,kk1)*aa
          ul(1,2)=ul(1,2)+ul(1,kk2)*aa
140 continue
        aa=-aa
139 continue
C

```

```

do 141 k=2,n
kk2=2*k
kk1=kk2-1
C
do 141 l=1,5
temp3(l)=ul(1,kk1)
temp4(l)=ul(1,kk2)
ul(1,kk1)=-ul(1,kk1-2)+2.*temp1(l)
ul(1,kk2)=-ul(1,kk2-2)+2.*temp2(l)
temp1(l)=temp3(l)
temp2(l)=temp4(l)
141 continue
C
uxx=0.
uyy=0.
ssxx=0.
ssxy=0.
ssyy=0.
C
do 142 i=1,mn
uxx=uxx-ul(1,i)*ub(i)+ur(1,i)*fb(i)
uyy=uyy-ul(2,i)*ub(i)+ur(2,i)*fb(i)
ssxx=ssxx+c1*ul(3,i)*ub(i)+ur(3,i)*fb(i)
ssxy=ssxy+c1*ul(4,i)*ub(i)+ur(4,i)*fb(i)
ssyy=ssyy+c1*ul(5,i)*ub(i)+ur(5,i)*fb(i)
142 continue
C
uxb(ii)=uxx/(8.*pi)
uyb(ii)=uyy/(8.*pi)
sxxb(ii)=ssxx/(8.*pi)
sxyb(ii)=ssxy/(8.*pi)
syxb(ii)=ssyy/(8.*pi)
C
135 continue
C
return
end

subroutine fldc(n,mm,pr,x,y,r,w,w1,w2,uc,tc,xf,yf,uxc,uyc,
&  sxxc,sxyc,syyc)
C
parameter(mn=75)
parameter(mrn=2*mn)
parameter(mrn1=mrn+1)
parameter(mmm=50)
C
dimension x(mn),y(mn)
dimension r(10),w(10),w1(10),w2(10)
dimension uc(mrn),tc(mrn),fc(mrn)
dimension xf(mmm),yf(mmm)
dimension ul(5,mrn),ur(5,mrn)
dimension uxc(mmm),uyc(mmm)
dimension sxxc(mmm),sxyc(mmm),syyc(mmm)
dimension temp1(5),temp2(5),temp3(5),temp4(5)

```

```

dimension temp11(5),temp12(5),temp13(5),temp14(5)
C
  nn=2*n
C
  pi=4.*atan(1.)
C
  c1=1.+pr
  c2=1.-pr
  c3=3.+pr
  c4=3.-pr
  c5=1.+3.*pr
C
  do 135 ii=1,nn
C
    do 136 i=1,nn
    do 136 k=1,5
      ul(k,i)=0.
      ur(k,i)=0.
136 continue
C
    do 137 j=1,n
      if(j.eq.1)then
        jml=n
      else
        jml=j-1
      endif
      jj2=2*j
      jj1=jj2-1
C
      if(j.eq.1)then
        jj2m2=nn
      else
        jj2m2=jj2-2
      endif
      jj1m2=jj2m2-1
C
      dx=x(j)-x(jml)
      dy=y(j)-y(jml)
      s=sqrt(dx*dx+dy*dy)
      fc(jj1)=tc(jj1)*s
      fc(jj2)=tc(jj2)*s
C
      xmi=(x(j)+x(jml))/2.
      ymi=(y(j)+y(jml))/2.
      dnm1=x(j)-xmi
      dnm2=y(j)-ymi
      o=dnm1*dnm1+dnm2*dnm2
C
      drml=xf(ii)-xmi
      drn2=yf(ii)-ymi
      aa=drml*drml+drn2*drn2
      bb=-2.*(drml*dnm1+drn2*dnm2)
C
      do 137 l=1,10

```

```

rho=sqrt(aa+bb*r(1)+c*r(1)*r(1))
rho2=rho*rho
qx=(dmm1-dmm1*r(1))/rho
qy=(dmm2-dmm2*r(1))/rho
qx2=qx*qx
qy2=qy*qy
qx3=qx2*qx
qy3=qy2*qy
qx4=qx2*qx2
qy4=qy2*qy2
C
t11=(2.*c1*(dmm2*qx3+dmm1*ay3)+c2*dmm2*qx-c3*dmm1*qy)/rho
t21=(2.*c1*(dmm1*qx3-dmm2*qy3)-c5*dmm1*qx+c3*dmm2*qy)/rho
t12=(2.*c1*(dmm1*qx3-dmm2*qy3)-c3*dmm1*qx+c5*dmm2*qy)/rho
t22=(2.*c1*(-dmm2*qx3-dmm1*qy3)+c3*dmm2*qx-c2*dmm1*qy)/rho
C
ul(1,jj1m2)=ul(1,jj1m2)+w(1)*w1(1)*t11
ul(1,jj2m2)=ul(1,jj2m2)+w(1)*w1(1)*t21
ul(2,jj1m2)=ul(2,jj1m2)+w(1)*w1(1)*t12
ul(2,jj2m2)=ul(2,jj2m2)+w(1)*w1(1)*t22
C
ul(1,jj1)=ul(1,jj1)+w(1)*w2(1)*t11
ul(1,jj2)=ul(1,jj2)+w(1)*w2(1)*t21
ul(2,jj1)=ul(2,jj1)+w(1)*w2(1)*t12
ul(2,jj2)=ul(2,jj2)+w(1)*w2(1)*t22
C
u11=(-c4*log(rho)+c1*qx*qx)/4.
u12=c1*qx*qy/4.
u22=(-c4*log(rho)+c1*qy*qy)/4.
C
ur(1,jj1m2)=ur(1,jj1m2)+w(1)*w1(1)*u11
ur(1,jj2m2)=ur(1,jj2m2)+w(1)*w1(1)*u12
ur(2,jj1m2)=ur(2,jj1m2)+w(1)*w1(1)*u12
ur(2,jj2m2)=ur(2,jj2m2)+w(1)*w1(1)*u22
C
ur(1,jj1)=ur(1,jj1)+w(1)*w2(1)*u11
ur(1,jj2)=ur(1,jj2)+w(1)*w2(1)*u12
ur(2,jj1)=ur(2,jj1)+w(1)*w2(1)*u12
ur(2,jj2)=ur(2,jj2)+w(1)*w2(1)*u22
C
s111=2.*((8.*qx4-4.*qx2-1.)*dmm2-2.*qx*qy*(4.*qx2-1.)*dmm1)
&
/rho2
s211=2.*(2.*qx*qy*(4.*qx2-1.)*dmm2-(8.*qx2*qy2-1.)*dmm1)
&
/rho2
s221=2.*((8.*qx2*qy2-1.)*dmm2-2.*qx*qy*(4.*qy2-1.)*dmm1)
&
/rho2
s222=2.*(2.*qx*qy*(4.*qy2-1.)*dmm2-(8.*qy4-4.*qy2-1.)*dmm1)
&
/rho2
C
ul(3,jj1m2)=ul(3,jj1m2)+w(1)*w1(1)*s111
ul(3,jj2m2)=ul(3,jj2m2)+w(1)*w1(1)*s211
ul(4,jj1m2)=ul(4,jj1m2)+w(1)*w1(1)*s211
ul(4,jj2m2)=ul(4,jj2m2)+w(1)*w1(1)*s221
ul(5,jj1m2)=ul(5,jj1m2)+w(1)*w1(1)*s221

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```

      ul(5,jj2m2)=ul(5,jj2m2)+w(1)*w1(1)*s222
C
      ul(3,jj1)=ul(3,jj1)+w(1)*w2(1)*s111
      ul(3,jj2)=ul(3,jj2)+w(1)*w2(1)*s211
      ul(4,jj1)=ul(4,jj1)+w(1)*w2(1)*s211
      ul(4,jj2)=ul(4,jj2)+w(1)*w2(1)*s221
      ul(5,jj1)=ul(5,jj1)+w(1)*w2(1)*s221
      ul(5,jj2)=ul(5,jj2)+w(1)*w2(1)*s222
C
      d111=(-2.*c1*qp3-c2*qx)/(rho*2.)
      d112=(2.*c1*qy3-c5*qy)/(rho*2.)
      d121=(2.*c1*qy3-c3*qy)/(rho*2.)
      d122=(2.*c1*qp3-c3*qx)/(rho*2.)
      d221=(2.*c1*qp3-c5*qx)/(rho*2.)
      d222=(-2.*c1*qy3-c2*qy)/(rho*2.)
C
      ur(3,jj1m2)=ur(3,jj1m2)+w(1)*w1(1)*d111
      ur(3,jj2m2)=ur(3,jj2m2)+w(1)*w1(1)*d112
      ur(4,jj1m2)=ur(4,jj1m2)+w(1)*w1(1)*d121
      ur(4,jj2m2)=ur(4,jj2m2)+w(1)*w1(1)*d122
      ur(5,jj1m2)=ur(5,jj1m2)+w(1)*w1(1)*d221
      ur(5,jj2m2)=ur(5,jj2m2)+w(1)*w1(1)*d222
C
      ur(3,jj1)=ur(3,jj1)+w(1)*w2(1)*d111
      ur(3,jj2)=ur(3,jj2)+w(1)*w2(1)*d112
      ur(4,jj1)=ur(4,jj1)+w(1)*w2(1)*d121
      ur(4,jj2)=ur(4,jj2)+w(1)*w2(1)*d122
      ur(5,jj1)=ur(5,jj1)+w(1)*w2(1)*d221
      ur(5,jj2)=ur(5,jj2)+w(1)*w2(1)*d222
C
137  continue
C
C POST-MULTIPLY UL AND UR BY GAMMA TRANSPOSE INVERSE
C
      aa=-1
      do 138 l=1,5
        temp1(l)=ul(l,1)
        temp2(l)=ul(l,2)
        temp11(l)=ur(l,1)
        temp12(l)=ur(l,2)
38  continue
C
      do 139 k=2,n
        kk2=2*k
        kk1=kk2-1
C
        do 140 l=1,5
          ul(l,1)=ul(l,1)+ul(l,kk1)*aa
          ul(l,2)=ul(l,2)+ul(l,kk2)*aa
          ur(l,1)=ur(l,1)+ur(l,kk1)*aa
          ur(l,2)=ur(l,2)+ur(l,kk2)*aa
140  continue
      aa=-aa
139  continue

```

```

C      do 141 k=2,n
        kk2=2*k
        kk1=kk2-1
C
        do 141 l=1,5
            temp3(l)=ul(1,kk1)
            temp4(l)=ul(1,kk2)
            temp13(l)=ur(1,kk1)
            temp14(l)=ur(1,kk2)
            ul(1,kk1)=ul(1,kk1-2)+2.*temp1(l)
            ul(1,kk2)=ul(1,kk2-2)+2.*temp2(l)
            ur(1,kk1)=ur(1,kk1-2)+2.*temp11(l)
            ur(1,kk2)=ur(1,kk2-2)+2.*temp12(l)
            temp1(l)=temp3(l)
            temp2(l)=temp4(l)
            temp11(l)=temp13(l)
            temp12(l)=temp14(l)
141    continue
C
        uux=0.
        uuy=0.
        ssxx=0.
        ssxy=0.
        ssyy=0.
C
        do 142 i=1,nm
            uux=uux-ul(1,i)*uc(i)+ur(1,i)*fc(i)
            uuy=uuy-ul(2,i)*uc(i)+ur(2,i)*fc(i)
            ssxx=ssxx+c1*ul(3,i)*uc(i)+ur(3,i)*fc(i)
            ssxy=ssxy+c1*ul(4,i)*uc(i)+ur(4,i)*fc(i)
            ssyy=ssyy+c1*ul(5,i)*uc(i)+ur(5,i)*fc(i)
142    continue
C
            usc(ii)=uux/(8.*pi)
            uyc(ii)=uuy/(8.*pi)
            sxxc(ii)=ssxx/(8.*pi)
            sxyc(ii)=ssxy/(8.*pi)
            syyc(ii)=ssyy/(8.*pi)
C
135    continue
C
        return
        end

```

List of References

1. Banerjee, P.K., and Butterfield, R., "Boundary Element Methods in Engineering Science," McGraw - Hill, 1981.
2. Segerlind, L.J., "Applied Finite Element Analysis," John Wiley and Sons, 1984.
3. Ugural, A.C., "Stresses in Plates and Shells," McGraw - Hill, 1981.
4. Atluri, S.N., "Computational Solid Mechanics (Finite Elements and Boundary Elements): Present Status and Future Directions," (4th International Conference on Applied Numerical Modelling Tainan, Taiwan, R.O.C.), Pentech Press, 1984.
5. Mikhlin, S.G., "Approximate Solutions of Differential and Integral Equation," Pergamon Press, 1965.
6. Cruse, T.A., "Numerical Solutions in Three Dimensional Elastostatics," International Journal of Solids and Structures, Vol. 5, pp. 1259 - 1274, Pergamon Press, 1969.
7. Cruse, T.A., "Some Classical Elastic Sphere Problems Solved Numerically by Integral Equations," Journal of Applied Mechanics, p. 272, 1972.
8. Cruse, T.A., "Application of the Boundary - Integral Equation Method to Three Dimensional Stress Analysis," Computers and Structures, Vol. 3, pp. 509 - 527, Pergamon Press, 1973.
9. Cruse, T.A., "An Improved Boundary - Integral Equation Method For Three Dimensional Elastic Stress Analysis," Computers and Structures, Vol. 4, pp. 741 - 754, Pergamon Press, 1974.
10. Brebbia, C.A., "The Boundary Element Method For Engineers," Pentech Press, 1978.
11. Brebbia, C.A. (ed), "Boundary Element Methods in Engineering," Springer - Verlag, 1982.
12. Brebbia, C.A., and Noye, B.J. (eds), "BETECH 85," Springer - Verlag, 1985.
13. Mackerle, J., and Andersson, T., "Boundary Element Software in Engineering," Advances in Engineering Software, Vol. 6, pp. 66 - 102, 1983.
14. Brebbia, C.A., and Walker, S., "Boundary Element Techniques in Engineering," Newnes - Butterworths, 1980.
15. Kitahara, M., "Boundary Integral Equation Methods in Eigenvalue Problems of Elastodynamics and Thin Plates," Elsevier, 1985, pp. 1 - 37.
16. Hromadka, T.V., and Lai, C., "The Complex Variable Boundary Element Method in Engineering Analysis," Springer - Verlag, 1986.
17. Manolis, G.D., and Banerjee, P.K., "Conforming Versus Non-Conforming Boundary Elements in Three Dimensional Elastostatics," International Journal of Numerical Methods in Engineering, Vol. 23, pp. 1885 - 1905, 1986.
18. Burgess, G., and Mahajerin, E., "A Comparison of the Boundary Element and Superposition Methods," Computers and Structures, Vol. 19, pp. 697 - 705, 1984.

