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APPLICATION AND ANALYSIS OF A
MICROSCOPE DIFFUSION CHAMBER

by

Keith D. Sherban

A THESIS

Submitted to
Michigan State University
in partial fulfillment of the requirements
for the degree of

MASTER OF SCIENCE

Department of Mechanical Engineering

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ABSTRACT

THE APPLICATION AND ANALYSIS OF A MICROSCOPE DIFFUSION CHAMBER

by

Keith D. Sherban

A microscope diffusion chamber has been used to determine the equilibrium and non-equilibrium osmotic response of individual cells. The chamber allowed the direct observation of a cell subjected to a change in concentration at a specified temperature. Cell systems used in this work were egg lecithin liposomes and human lymphocytes. For each cell system the normalized osmotically inactive volume, membrane hydraulic permeability (for five specific temperatures) and membrane activation energy have been determined.

The raw data generated were processed by a computer algorithm which used a parameter estimation technique to yield the best statistical estimate of the membrane permeability. The program was made "user friendly" by setting up the algorithm to run in menu format and converted to an IBM PC. In addition, the program also allowed the user to run simulations for sensitivity studies and the design of experiments.

A major finding/result is that the estimated parameters using this device and software matched previously reported results for egg lecithin liposomes and human lymphocytes. This suggests that the device and software can be applied successfully for determining water permeability of cell membranes, including temperature effects.

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ACKNOWLEDGEMENTS

I would like to express my appreciation to my advisor Dr. McGrath. I am grateful for his support, guidance and friendship.

I would like to thank my wife for her support, patients and never ending encouragement.

I am deeply grateful to the members of my family who have also patiently supported me.

I would like to thank John Tu, Mark Melkerson and Mosen Shabana of the Bioengineering Transport Lab for their help and guidance.

I would like to thank the Ostrom's for their support and the use of their computer systems.

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t Time
V Volume
V Partial
w Solute

NOMENCLATURE

A	Area
b	Estimated Parameter
C	Concentration
D	Diffusivity of Solute in Specified Medium
E _a	Activation Energy
H _d	Convective Mass Transfer Coefficient
J _i	Flux of Species i
L _{ij}	Phenomenological Coefficient
n	Number of Data Points
Q	Work Due to Heat
P	Cell Membrane Water Permeability
P _{est}	Estimated Permeability
p	Pressure
p	Number of Parameters
R	Gas Constant
R _c	Cell Radius - Predicted
R _m	Cell Radius - Measured
S	Entropy
S	Sum of the Squares Function
T	Temperature
t	Time
V	Volume
\bar{v}	Partial Molar Volume
w	Solute Permeability

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- c Cell
- D Diffusion
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- i Species i
- j Species j
- m Membrane
- p Pressure
- s Solute
- w Solvent
- 1 Dialysis Membrane Region
- 2 Sample Region
- 3 Inside the Cell of Interest

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GREEK NOMENCLATURE

β	Parameter
ϵ	Error
π	Osmotic Pressure
r	Molar Fraction
ϵ	Volume Fraction
σ	Reflection Coefficient
μ	Chemical Potential
Φ	Dissipation Function
θ	Standard Deviation
η	Predicted Parameter
ψ	Covariance of Errors

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CHAPTER 1

Introduction

1.1 Background and Motivation for Present Work

The cell is the most basic unit of living material. All biological organisms are composed of one or more of these fundamentally similar units. Understanding the reaction of a cell, due to an environmental change, is a concern of biologists and other scientists. One particular type of scientist, namely the cryobiologist, is interested in understanding what happens to a cell and its membrane as the cell is subjected to low temperatures. Since a cell is composed primarily of water (50-90%), the temperature of 0°C is of considerable interest: the freezing point of water (at atmospheric conditions). During the freezing process, it has been shown that the membrane of the cell becomes damaged or injured. It has been suggested that two distinct mechanisms of injury occur, and this has been formulated into the "two-factor" hypothesis of freezing injury.^[1] Specifically, at low rates of cooling, all ice formation is extracellular and injury is a direct result of osmotic stress. At high rates of cooling, cells are damaged by the nucleation of intracellular ice, and by its subsequent recrystallization during warming. An optimal recovery is then observed at an intermediate rate of cooling.^[2]

The important phenomenon of interest for this paper deals with the osmotic responses that occur during cooling and warming. The problem that will be addressed is the equilibrium and non-equilibrium osmotic behavior of a cell at a given temperature. To further explain, recall

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from above that during a low rate of cooling all ice formation is extracellular. As the extracellular water freezes, the cell begins to experience an increase in extracellular solute concentration which can be quite large, depending on the environmental/experimental conditions. The cell responds by expelling water from inside thus decreasing the cell volume. In other words, the cell is trying to increase its intracellular concentration in order to reestablish an equilibrium state. The cell suffers damage due to dehydration.

Typical techniques for determining the equilibrium osmotic behavior of cells includes one or more of the following undesirable characteristics: individual cells cannot be monitored; relatively large sample volumes are required; manipulation of the extracellular solute concentration is inconvenient and/or time consuming; rather extensive calibration procedures are required because the experimental technique is an indirect one.^[3] Optical techniques using light absorption and scattering have been used in stopped-flow spectrophotometers in order to determine the transient osmotic behavior of biological cells.^[4,5,6] This technique is indirect, requires relatively large sample volumes, subjects cells to substantial shearing stresses, and yields no information about individual cells, only the average.^[3]

With these undesirable characteristics in mind, J.J. McGrath developed the microscope diffusion chamber. The chamber attempts to provide the following ideal characteristics: (1) allows real time direct observation of individual cells in suspension, (2) requires small sample volumes (10-1000 microliters), (3) allows rapid change of extracellular concentrations (1-10 seconds), (4) allows repeated changes in

extracellular solutions, (5) allows temperature control of the medium, (6) allows the use of all standard microscope optical techniques, and (7) is simple and economical to construct and use.^[3] Although other microscope diffusion chambers have been developed, none have all the above characteristics, while the chamber developed by McGrath does.

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1.2 Statement of Objective

The work presented here is part of an ongoing study of the microscope diffusion chamber developed by J.J. McGrath and was conducted at the Bioengineering Transport Process Laboratory (BTPL) of Michigan State University. Previous work performed by S.P. Nowlen, S.M. Tu and M. Shabana, of the BTPL, initiated the testing and application of the diffusion chamber along with developing parameter estimation software to aid with data analysis. Their work consisted of using cell systems of liposomes and unfertilized hamster ova and was carried out at room temperature. The work in this thesis has accomplished the following: (1) extends the diffusion chamber capabilities to allow experiments to be run at different temperatures; (2) improves the software usability; (3) applies the diffusion chamber to the cell systems of liposomes and human lymphocytes; (4) uses the software to clarify previous results, and (5) uses the software to study the sensitivity of the estimated parameter (the membrane water permeability) with respect to a change in input parameters.

The first step toward these goals was to research and gather information about the work accomplished in the BTPL using the diffusion chamber. At the time, S.M. Tu was conducting experiments using liposomes as a cell system and developing a computer program to aid with data analysis. It was determined that the best way to gain an understanding of how the diffusion chamber operated was by trying to verify the results Tu obtained. This was accomplished by using liposomes under the same experimental conditions and analyzing the results using Tu's computer

program.

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Once this was accomplished, the next step was to adapt the experimental system to allow for experiments to be carried out at different temperatures. The diffusion chamber was already designed with this consideration in mind. It had a heat exchange channel running along the inside of the outer edge of the chamber body (see Figure 4.2.2). The device used to control the chamber's temperature was a refrigerated circulating bath. The bath was connected directly to the diffusion chamber's heat exchange channel. The bath's fluid was also used to control the temperature of the isotonic and hypertonic solutions (see Figure 4.3.1). Once the experimental system was set up, thermocouples and a digital display device were used to characterize the temperature distribution of the diffusion chamber and to monitor of the temperature at various points of the experimental system during an experimental run.

The computer program developed by Tu worked well, providing all of the data and the parameters were entered correctly. However, if something was not entered properly and/or the user encountered an error during run time, it was often difficult to locate the cause. The main thrust to improve the usability of the program was to have the program explain to the user what the program required and accomplished. To do this, the program was set up in a menu driven format which prompted the user for the necessary input. In addition, the program was also adapted so that it could be used with an IBM personal computer in conjunction with the graphical software PLOTIT. The original program resided on the PRIME 750, a minicomputer, available at the Case Center in the Engineering building at M.S.U.

The experimental work included conducting experiments using liposomes and lymphocytes as cell systems because results existed in literature for comparison. The types of experiments performed resulted in the data necessary to generate cell inactive volumes, membrane permeabilities and membrane activation energies for each cell system, with the exception of conducting experiments for the liposomes cell inactive volume. This work was previously performed by R. Callow of the BTPL. These results were compared with those reported by S.M. Tu and R. Callow for liposomes, and Porsche and Hempling for lymphocytes and were found to be in good agreement. Therefore this establishes validity of this approach.

Initially, the parameter estimation software was used to help clarify work previously done by M. Shabana using unfertilized hamster ova. When Shabana carried out his experiments and analyzed the data, the zero time was taken to be when the cell started to "respond", by visually detecting a fluctuation or shrinkage in the outer membrane of the cell. However, this is not the true zero time. By reexamining the recorded video tapes the delay time was approximated to be 6 seconds. Thus 6 seconds was added to each time interval for each set of data and new cell membrane permeabilities were estimated. Then these newly calculated permeabilities were compared to those calculated by Nowlen, using the same sets of data but different parameter estimation techniques, and were found to be in better agreement (see Appendix C for details).

The software was also applied to define the experimental conditions. By having an approximate value for the cell membrane permeability (from pervious work and published literature), the experimental conditions

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could be entered and the program could calculate a simulated volume time history for the cell. Based on the outcome of the volume time history, the experimental conditions could be adjusted to give a better or more desirable volume history. The criteria used to here was to have the cell radius shrink by 15% or more because this allowed for greater ease in measuring volume history.

The most obvious use and primary reason for creating the software was to enter the actual data from experimental runs to estimate a membrane permeability for an individual cell. This was done for each set of data obtained. The results are tabulated in Section 5.3, Tables 5.3.1 and 5.3.2.

Finally, the program was used for sensitivity studies. The sensitivity studies were performed to help give a better understanding of the results generated in this thesis. The question was asked, if the experimental conditions were similar to those encountered during experiments with liposomes and lymphocytes, thus giving similar results, what would happen to the estimated permeability if an input parameter was increased or decreased? By doing such a study, one could determine how "sensitive" the estimated parameter, in this case the cell permeability, was with respect to a change in a particular input parameter of interest. Thus estimates of experimental uncertainties could be made.

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CHAPTER 2

Analysis

2.1 System definition

A schematic representation of the diffusion chamber is given in Figure 2.1.1. Initially the cell specimen is placed into the diffusion chamber sample region and the bulk flow region is filled with the isotonic solution. At zero time, the bulk flow region is flushed with a continuous flow of hypertonic solution. As a result, a concentration boundary layer develops along the bottom surface of the dialysis membrane. Solute diffuses through the boundary layer, through the dialysis membrane and into the sample region. The cell responds osmotically to the concentration increase. The analysis presented here will model the solute diffusion process and the cell specimen's response, which has been incorporated into a computer program.

Schematic Representation of the Microscope Diffusion Chamber



Microscope
Objective

Schematic Representation of the Microscope Diffusion Chamber

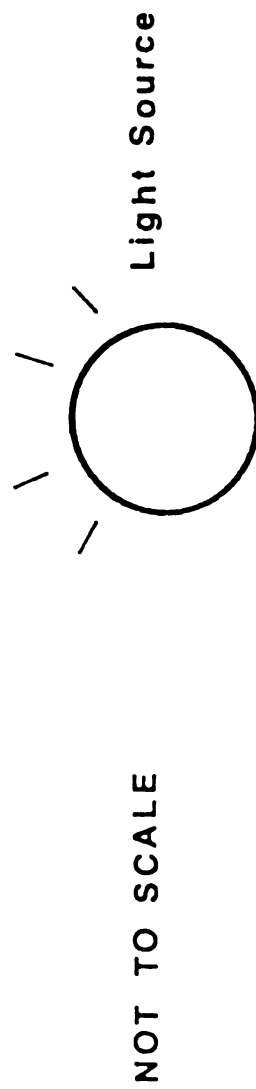
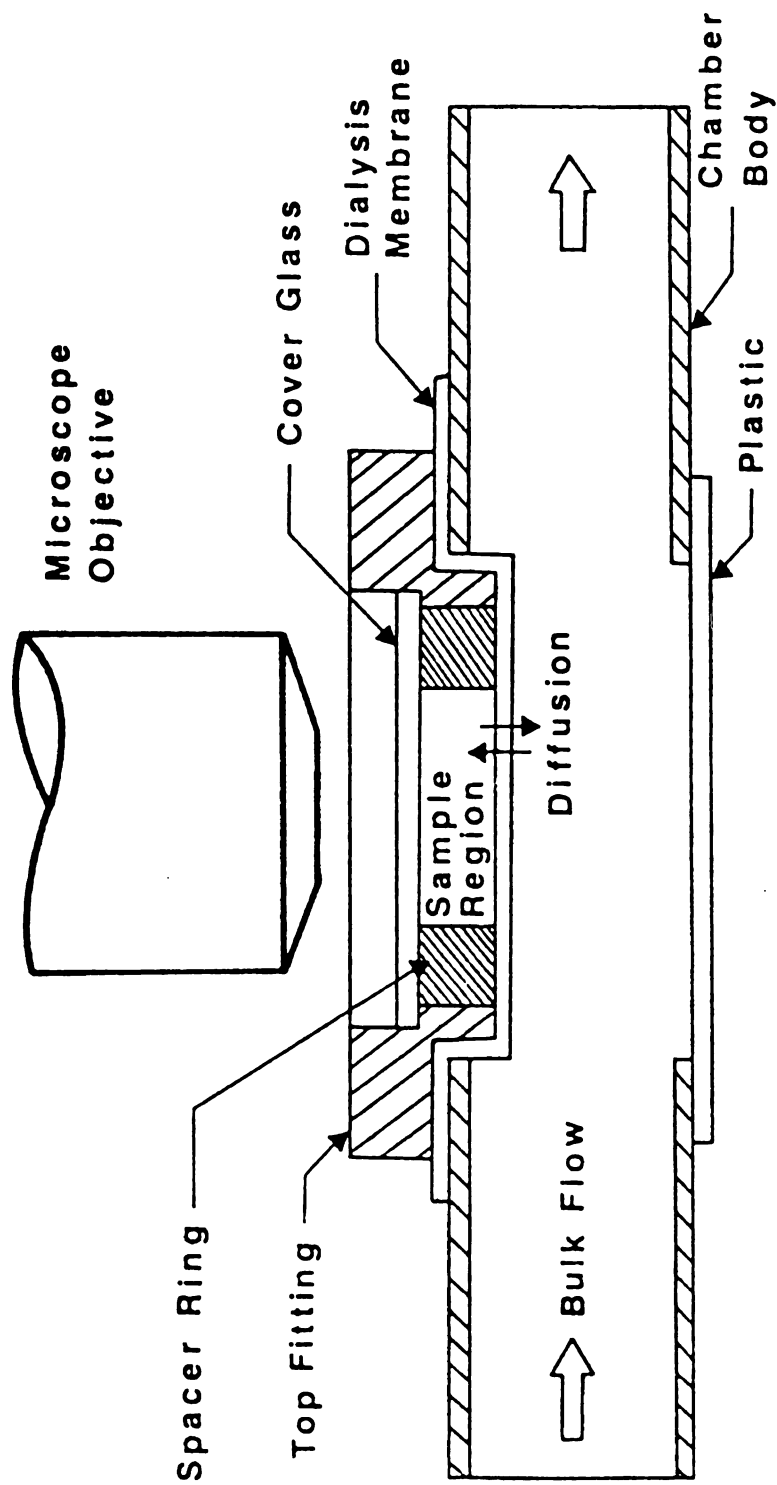


Figure 2.1.1.1

1.1 Model

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2.2 Modeling the system

The modeling of the system can be broken into two parts: the diffusion of the solute into the sample region and the osmotic response of the cell specimen.

2.2.1 The Concentration History

Since J.J. McGrath, in conjunction with S.M. Tu, has already extensively analyzed the solute concentration history of the microscope diffusion chamber, (see reference [7] in the bibliography), their approach and results will only be summarized here.

The assumptions used to model the solute concentration are as follows:[7]

- 1) one dimensional transient mass transfer (developing mass transfer boundary layer is accounted for with a mean coefficient, H_d).
- 2) a non-selective dialysis membrane, $\sigma = 0$ [8], (i.e. solute diffuses through the membrane as it would through free solution (except the diffusivity coefficient is lower).).
- 3) no net volume flow in the sample region of the diffusion chamber.
- 4) fully developed, steady state laminar hydrodynamic conditions in the bulk flow region.
- 5) the diffusion chamber is isobaric and isothermal.
- 6) constant mass diffusivities.
- 7) negligible solute velocities normal to the dialysis membrane.
- 8) the analysis does not account for the presence of cells in the sample region.

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$$\frac{\delta C_{s,1}}{\delta t}$$

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- 9) the bulk flow is assumed to step change from $C_{s,\infty}$ to C_f at the zero time.

The problem considered is therefore one-dimensional transient diffusion through two adjacent regions, one of which is bounded by an impermeable plane and the other by convective flow.^[7] A schematic representation of the basic system can be seen in Figure 2.2.1. The mathematics of the problem can be described by the following equations.

$$\frac{\delta C_{s,1}(X_1, t)}{\delta t} = D_1 \frac{\delta^2 C_{s,1}}{\delta X_1^2} \quad 0 \leq X_1 \leq L_1 \quad ; \quad t > 0 \quad (2.2.1)$$

$$\frac{\delta C_{s,2}(X_2, t)}{\delta t} = D_2 \frac{\delta^2 C_{s,2}}{\delta X_2^2} \quad 0 \leq X_2 \leq L_2 \quad ; \quad t > 0 \quad (2.2.2)$$

subject to the boundary conditions:

$$H_d [C_{s,\infty}(t) - C_{s,1}(0, t)] = -D_1 \frac{\delta C_{s,1}(0, t)}{\delta X_1} \quad (2.2.3)$$

$$C_{s,1}(L_1, t) = C_{s,2}(0, t) \quad (2.2.4)$$

$$D_1 \frac{\delta C_{s,1}(L_1, t)}{\delta X_1} = D_2 \frac{\delta C_{s,2}(0, t)}{\delta X_2} \quad (2.2.5)$$

$$\frac{\delta C_{s,2}(L_2, t)}{\delta X_2} = 0 \quad (2.2.6)$$

and the initial conditions:

$$C_{s,1}(X_1, 0) = C_i \quad (2.2.7)$$

$$C_{s,2}(X_2, 0) = C_i \quad (2.2.8)$$

$$C_{s,\infty} = C_i \quad : \quad t < 0 \quad (2.2.9)$$

The technique used to solve these equations, and calculate the concentration history, was the backwards finite difference approximation method. These equations were formulated into a subroutine, MBCON, in the program SENS. Refer to Appendices D and E for a listing of MBCON and SENS. It should also be noted that to solve these equations the solute diffusivity in free solution, D_2 , the solute diffusivity in the dialysis membrane, D_1 , and the convective mass transfer coefficient, H_d , must be

MEMORANDUM FOR THE DIRECTOR, BUREAU OF CHEMISTRY, U.S. DEPARTMENT OF AGRICULTURE
SUBJECT: ANALYSIS OF SAMPLES FROM THE
MEMPHIS REGION



Schematic of Diffusion Chamber with Relevant Parameters

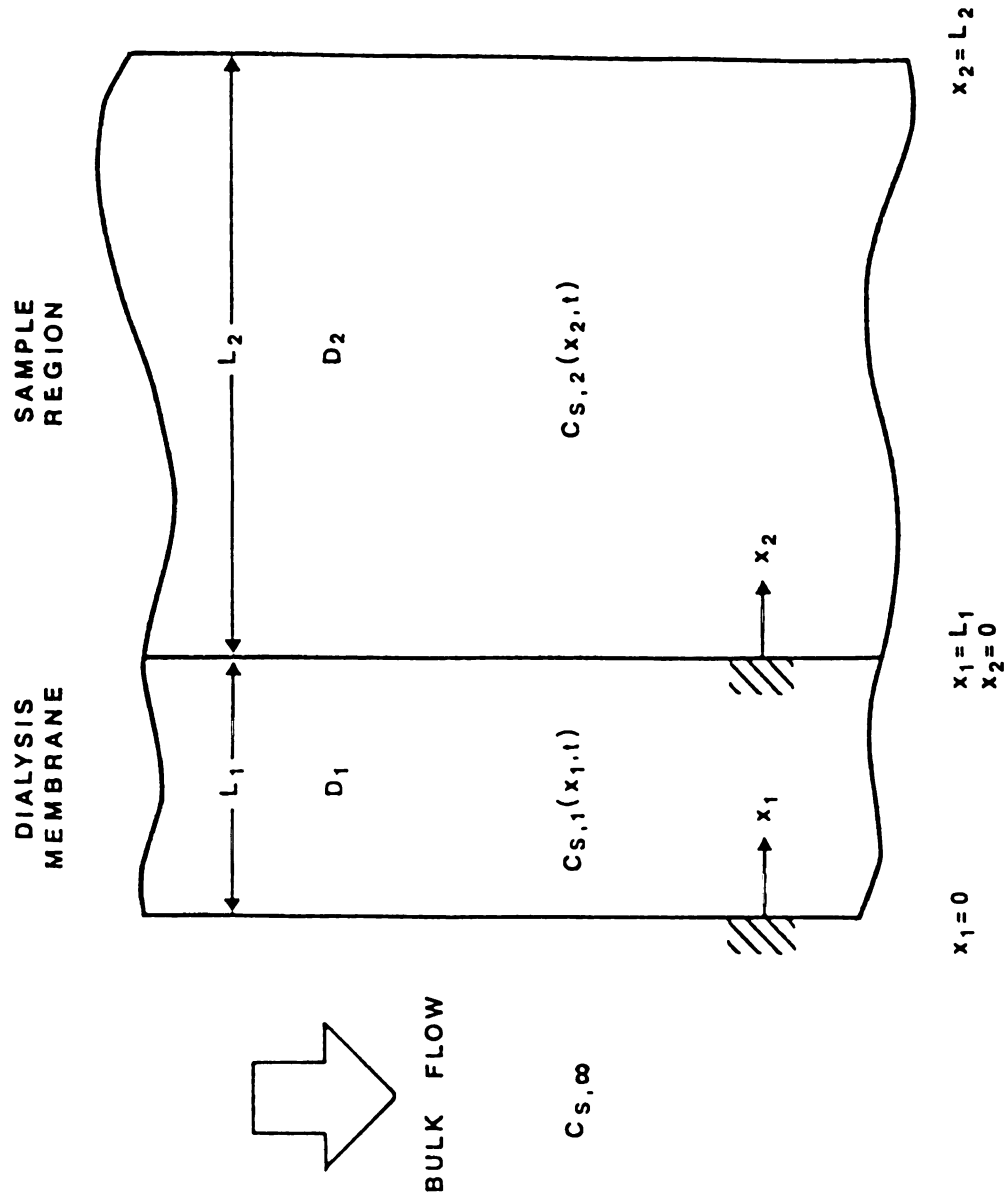


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known. The solute diffusivity in free solution can readily be found in an appropriate handbook (e.g. CRC Handbook of Chemistry and Physics). The solute diffusivity in the dialysis membrane has been claimed by the manufacture (ENKA AG, Product Group Membrana) to be approximately one tenth of the diffusion coefficient in free solution for compounds with a molecular weight of 300 or less.^[3] (For further discussion on the dialysis membrane refer to reference [3].) Therefore, the value used for the solute diffusivity in the dialysis membrane, throughout this work, was $D_1 = D_2 * 0.1$. The convective mass transfer coefficient used in this work was defined by J. Tu. He used an analogy from heat transfer developed by Kays and Crawford^[20]. By assuming 1) hydrodynamically fully developed flow in the bulk flow region, 2) a two dimensional parallel plate system and 3) no net volume flow in the sample region, he approximated the convective mass transfer coefficient to be $H_d = D_2 * 10000$ (which was also used though out this work).^[21]

2.2.2 The Kedem - Katchalsky Formulation

The approach used to solve for the osmotic response of a cell specimen is based on the principles developed in 1958 by Kedem and Katchalsky. Their model, the K-K Formulation, has come to be known as the classic model for membrane permeation using principles of irreversible thermodynamics^[9].

The development begins by considering the forces that cause the flows across the membrane. In 1931, L. Onsager related these flows and forces into equations called the "phenomenological equations". In general these equations are written as,

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$$\begin{aligned}
J_1 &= L_{11}X_1 + L_{12}X_2 + \dots + L_{1n}X_n \\
J_2 &= L_{21}X_1 + L_{22}X_2 + \dots + L_{2n}X_n \\
&\vdots \\
&\vdots \\
&\vdots \\
J_n &= L_{n1}X_1 + L_{n2}X_2 + \dots + L_{nn}X_n
\end{aligned} \tag{2.2.10}$$

Note that each flow, J_i ($i = 1$ to n), is influenced linearly by its conjugate force X_i and the nonconjugate forces X_j ($j \neq i$, $j=1$ to n), providing the "straight" coefficients, L_{ii} , and the "cross" or "coupling" coefficients, L_{ij} ($i \neq j$), differ from zero. Having dimensions of flow per unit force, $L_{ij} = (J_i/X_j)X_i$, the coefficients have general characteristics of conductances or mobility. In addition to developing these equations Onsager also discovered the matrix of coefficients to be symmetrical; in other words $L_{ik} = L_{ki}$ for $i \neq k$. It should be noted that this linearity holds only for sufficiently slow processes occurring when the system is not too far removed from a state of equilibrium. The choice of a force conjugate to the flow J_i is restricted by the requirement that the product J_iX_i has dimensions of the rate of entropy production or decrease in free energy with time.^[10] Thus this is the starting point of the thermodynamic description. The total rate of entropy change, dS/dt , is broken into the rate of entropy transfer between the system and its surroundings, d_eS/dt , and the rate of internal entropy production, d_iS/dt , which is generated by the irreversible processes occurring within the system.

$$\frac{dS}{dt} = \frac{d_eS}{dt} + \frac{d_iS}{dt} \tag{2.2.11}$$

If all process within a closed system occur reversibly, the rate of entropy change can be written as

$$\frac{d_e S}{dt} = \frac{1}{T} \frac{dQ}{dt} \quad (2.2.12)$$

where dQ is the heat gained, and T is the absolute temperature. However, if the system undergoes an irreversible change the rate of entropy change is written as

$$\frac{dS}{dt} = \frac{1}{T} \frac{dQ}{dt} + \frac{d_i S}{dt} \quad (2.2.13)$$

When dealing with irreversible processes in an isothermal system it is frequently convenient to consider the function Φ given by

$$\Phi = T \frac{d_i S}{dt} \quad (2.2.14)$$

which Lord Rayleigh called the dissipation function. The particular processes of interest for this paper are the movements of solute and water across a cell membrane. The system which will be considered (see Figure 2.2.2) consists of 1) two compartments separated by a membrane of thickness Δx and surface area A_c and 2) two solutions of the same solvent and solute, also separated by the membrane. The outer compartment is designated by ² and the inner compartment by ³.

The general dissipation function for the two component system of solvent and solute, for an isothermal system, is written as

$$\Phi = J_w X_w + J_s X_s \quad (2.2.15)$$

where w denotes the solvent and s denotes the solute. Focusing attention within the membrane of a volume element of unit area and thickness dx , the dissipation function becomes

The Two Compartment - Two Component System

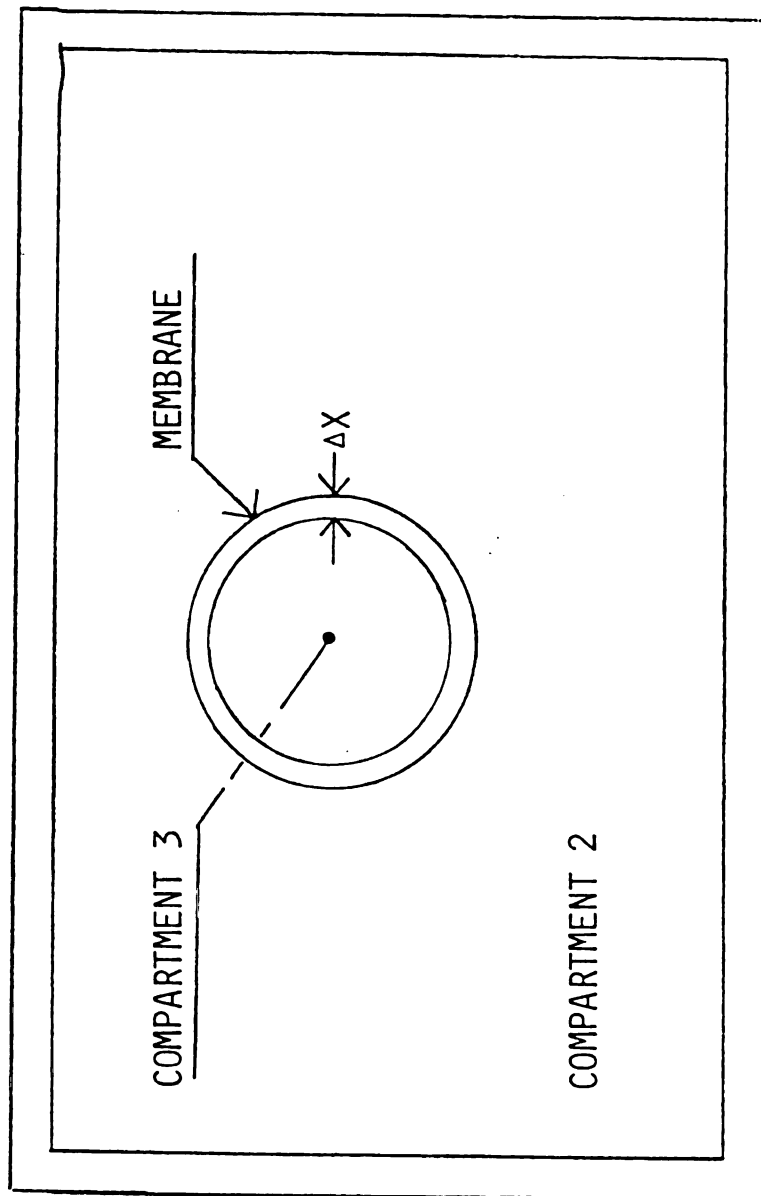


Figure 2.2.2

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$$\Phi = J_w \left[-\frac{d\mu_w}{dx} \right] + J_s \left[-\frac{d\mu_s}{dx} \right] \quad (2.2.16)$$

where μ denotes the chemical potential. Since J_w and J_s are independent of x we can integrate across the membrane from $x=0$ to $x=\Delta x$;

$$\Phi_m = J_w \int_0^{\Delta x} \left[-\frac{d\mu_w}{dx} \right] dx + J_s \int_0^{\Delta x} \left[-\frac{d\mu_s}{dx} \right] dx \quad (2.2.17)$$

Making the assumption that the chemical potentials at the surfaces of the membrane are the same as those in the adjacent solutions the dissipation function becomes

$$\Phi_m = J_w \Delta\mu_w + J_s \Delta\mu_s \quad (2.2.18)$$

where $\Delta\mu_w = \mu_{w,2} - \mu_{w,3}$ and $\Delta\mu_s = \mu_{s,2} - \mu_{s,3}$. If the solution is considered to be ideal, the chemical potential is approximated by

$$\Delta\mu_j = \bar{v}_j \Delta p + RT \Delta(\ln \gamma_j) \quad (j = w \text{ or } s) \quad (2.2.19)$$

where \bar{v} is the partial molar volume of j , Δp is the difference in pressure between the outer and inner compartment, γ the molar fraction of constituent j . To further simplify equation (2.2.19), we also assume both solutions dilute. This implies the volume fraction of solute is small, $\epsilon = C_s \bar{v}_s \ll 1$, thus

$$\Delta\mu_s = \bar{v}_s \Delta p + RT \frac{\Delta C_s}{\bar{C}_s} \quad (2.2.20)$$

where

$$\bar{C}_s = \frac{\bar{C}_{s,2}(x_2, t) + \bar{C}_{s,3}(t)}{2}$$

and

$$\Delta\mu_w = \bar{v}_w \Delta p + RT \frac{\Delta C_s}{\bar{C}_w} \quad (2.2.21)$$

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$$\bar{C}_w = \frac{1 - \epsilon}{\bar{v}_w} \approx \frac{1}{\bar{v}_w}$$

Introducing (2.2.19) and (2.2.23) into equation (2.2.18), the dissipation function becomes

$$\Phi_m = J_w (\bar{v}_w \Delta p - \frac{RT}{\bar{C}_w} \Delta C_s) + J_s (\bar{v}_w \Delta p + \frac{RT}{\bar{C}_s} \Delta C_s) \quad (2.2.22)$$

Rearranging Φ_m we get

$$\Phi_m = (J_w \bar{v}_w + J_s \bar{v}_s) \Delta p + \left(\frac{J_s}{\bar{C}_s} - \frac{J_w}{\bar{C}_w} \right) RT \Delta C_s \quad (2.2.23)$$

Note in equation (2.2.20) a new set of forces and flows represent the dissipation function. The new forces are the hydrostatic pressure, $\Delta p = X_p$ and the osmotic pressure, $RT \Delta C_s = X_D$. The new conjugate forces are the total volume flow per unit area,

$$J_v = J_w \bar{v}_w + J_s \bar{v}_s \quad (2.2.24)$$

and the velocity of solute relative to solvent,

$$J_D = \frac{J_s}{\bar{C}_s} - \frac{J_w}{\bar{C}_w} \quad (2.2.25)$$

which is called the exchange flow. Writing these new flows and forces in terms of phenomenological equations we get

$$J_v = L_p \Delta p + L_{pD} \Delta \pi \quad (2.2.26)$$

$$J_D = L_{Dp} \Delta p + L_D \Delta \pi \quad (2.2.27)$$

where $\Delta \pi = RT \Delta C_s$. Making use of Onsager's reciprocal relation, $L_{pD} = L_{Dp}$, equation (2.2.26) and (2.2.27) become

$$J_v = L_p \Delta p + L_{pD} \Delta \pi \quad (2.2.28)$$

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$$J_D = L_{pD}\Delta p + L_D\Delta\pi \quad (2.2.29)$$

To further clarify the significance of these equations, the phenomenological coefficients, L_p , L_D and L_{pD} , are transformed into other coefficients that allow for more convenient comparison with experimental data, w_s , \bar{U}_s and P .

Before deriving these new coefficients we must first look at the flows that are defined. Instead of studying the exchange flow, J_D , it would be more advantageous to study the solute flow J_s . By rearranging equations (2.2.24) and (2.2.25) and assuming $\bar{C}_w\bar{v}_w=1$

$$J_s = \frac{(J_s + J_D) \bar{C}_s}{(\bar{v}_s\bar{C}_s + 1)} \quad (2.2.30)$$

Also, by assuming the solution on both sides of the membrane dilute, $\bar{v}_s\bar{C}_s \ll 1$, (2.2.30) becomes

$$J_s = (J_v + J_D)\bar{C}_s \quad (2.2.31)$$

The first coefficient to be determined will be w_s , the solute permeability. To accomplish this experimentally, it is more convenient to have conditions of zero volume flow across the membrane, $J_v=0$. If a concentration difference exists across the membrane, a pressure difference can be applied such that $J_v=0$, according to equation (2.2.28). Rearranging (2.2.28) becomes

$$\Delta p = - \left[\frac{L_{pD}}{L_p} \right] \Delta\pi \quad (2.2.32)$$

Substituting equation (2.2.29) and (2.2.32) into (2.2.31) yields

$$J_s = \left[\frac{L_p L_D - L_{pD}^2}{L_p} \right] \bar{C}_s \Delta\pi \quad (2.2.33)$$

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The solute permeability is defined to be:

$$w_s = \left[\frac{L_p L_p - L_p D^2}{L_p} \right] \bar{C}_s \quad (2.2.34)$$

The second coefficient to be defined is the reflection coefficient, which was originally introduced by Staverman in 1951. This coefficient is defined by

$$\sigma_s = -\frac{L_p D}{L_p} = -\left[\frac{J_D}{J_V} \right]_{\Delta\pi=0} \quad (2.2.35)$$

Imposing similar conditions as described above, where $J_V=0$, (2.2.32) becomes

$$\Delta p = \sigma_s RT \Delta C_s$$

and rearranging

$$\sigma_s = \frac{\Delta p}{RT \Delta C_s} \quad (2.2.36)$$

The value of σ_s ranges between 0 and 1 where for an ideal semipermeable membrane $\sigma_s=1$. In other words, all of the solute is reflected. Thus, for $\sigma_s < 1$ implies only some of the solute is reflected.

Finally the last coefficient to be described is P, the membrane hydraulic permeability. This coefficient is defined letting

$$P = \frac{L_p RT}{\bar{v}_w} \quad (2.2.37)$$

where \bar{v}_w is the molar volume of the solvent.

By using these definition for w_s , σ_s and P, J_V and J_s can be written in a more useful form. Recall from (2.2.28)

$$J_V = L_p \Delta p + L_p D \Delta \pi$$

Substituting in (2.2.35) and (2.2.37), the volume flux becomes

$$J_V = \bar{v}_w P \left[\frac{\Delta p}{RT} - \sigma_s \Delta C_s \right] \quad (2.2.38)$$

Also, recall the solute flux, J_s , from (2.2.31)

$$J_s = (J_V + J_D) \bar{C}_s$$

By substituting (2.2.28), (2.2.29), (2.2.34) and (2.2.35) into (2.2.31) we get

$$J_s = \bar{C}_s (1 - \sigma_s) J_V + w_s \Delta \pi \quad (2.2.39)$$

Thus equations (2.2.38) and (2.2.39) are the equations commonly used to determine membrane characteristics and are known as the K-K formulation.

Summarizing the conditions for which these equations are valid are as follows:

- 1) The system is two compartment - two component
- 2) The system is in thermal equilibrium
- 3) The membrane is permeable to the solvent and may or may not be permeable to the solute.
- 4) The solutions are assumed to be ideal and dilute
- 5) The driving forces are considered to be sufficiently small such that a linear relation exists between the driving forces and the resulting flows.

2 . 2 . 3 The Volume Flow of a Cell

Recall from Figure 2.1.1, the cell specimen resides in the sample region of the diffusion chamber. As hypertonic solution is flushed into the bulk flow region the solute diffuses into the sample region and the cell responds osmotically. The equation that is most useful for describing the response of the cell is the equation of volume flow (2.2.38)

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$$J_v = \bar{v}_w P \left[\frac{\Delta p}{RT} - \sigma_s \Delta C_s \right]$$

To further simplify this equation we must take a closer look at the experimental conditions. As mentioned previously equation (2.2.38) implies that the volume flow across the cell membrane can be caused by a hydrostatic pressure difference, Δp , and/or a concentration difference ΔC_s . However with the experimental set up used in this work it is not likely for a hydrostatic pressure difference to exist across the membrane. Therefore Δp is assumed to be zero. Also the cell's membrane is assumed to be an ideal semipermeable membrane to the solute that were used which implies $\sigma_s=1$. Taking into account these assumptions, equation (2.2.38) can be rewritten as

$$J_v = -\bar{v}_w P \Delta C_s \quad (2.2.40)$$

This equation can be further simplified into a more useful form. First recognize that

$$J_v = \frac{1}{A_c(t)} \frac{dV_c(t)}{dt}$$

where $A_c(t)=4\pi R_c(t)^2$ for spherical systems (which was assumed), the surface area of the cell and $V_c(t)=(4/3)\pi R_c(t)^3$, the volume of the cell.

Therefore (2.2.40) can be rearranged into

$$\frac{dR_c(t)}{dt} = -\bar{v}_w P [C_{s,2}(X_2,t) - C_{s,3}(t)] \quad (2.2.41)$$

With the equation in this form the only unknowns are P and $C_{s,3}(t)$. $R_c(t)$, the radius of the cell, can be measured, \bar{v}_w , the partial molar volume of the solvent is a constant which can be found in the appropriate tables and $C_{s,2}(X_2,t)$ the concentration of solute outside the cell, is

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obtained for from the equations described in section 2.2.1. However, the concentration inside the cell $C_{s,3}(t)$ can be written in terms of the cell volume (which is related to the cell radius). This is accomplished by using the definition of concentration (written here in terms of molality):

$$C_s = \frac{\text{moles of solute}}{\text{volume of solvent}}$$

Letting $N_{s,3}$ represent the moles of solute inside the cell and $V_w(t)$ represent the volume of solvent inside the cell, the concentration is now written as

$$C_{s,3}(t) = \frac{N_{s,3}}{V_w(t)}$$

Note, $V_w(t)$ can be written as

$$V_w = V_c(t) - V_b$$

where $V_c(t)$ is the total volume of the cell and V_b is the "inactive volume". The inactive volume of the cell is that which is not "free" solvent of the cell, i.e. the solute, bound solvent and any cell organelle material. This parameter is a constant and can be determined experimentally (see Appendix A). Therefore, the concentration within the cell is

$$C_{s,3}(t) = \frac{N_{s,3}}{V_c(t) - V_b} \quad (2.2.42)$$

The initial concentration ($t=0$) within the cell is

$$C_i = \frac{N_{s,3}}{V_c(0) - V_b} \quad (2.2.43)$$

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Solving for $N_{s,3}$ and substituting into (2.2.42), the instantaneous concentration becomes

$$C_{s,3}(t) = C_i \left[\frac{V_c(0) - V_b}{V_c(t) - V_b} \right] \quad (2.2.44)$$

by substituting (2.2.44) into (2.2.41) we get

$$\frac{dR_c(t)}{dt} = -P\bar{v}_w \left[C_{s,2}(X_2, t) - C_i \left(\frac{V_c(0) - V_b}{V_c(t) - V_b} \right) \right] \quad (2.2.45)$$

Thus, the volume flow, J_v , has been written in a more convenient form which now describes the rate of change of the cell radius. This equation is also used in the program SENS. The method used to solve this equation was the numerical method of Runge-Kutta (4th order). Since the concentration history within the sample region is known as a function of position and time, \bar{v}_w is a constant (the partial molar volume of water), and V_b can be determined experimentally, the only unknown is P , the cell membrane hydraulic permeability, in equation (2.2.45).

2.3 The Estimation of Parameter P

As mentioned above in section 2.2.3 the membrane hydraulic permeability, P , is unknown and must be solved for. The method used to solve for the parameter P is a technique known as parameter estimation. Parameter estimation is a discipline that provides tools for the efficient use of data in the estimation of constants appearing in mathematical models and for aiding in modeling phenomena.^[11] Typically the solution to an equation is thought of as solving for the state of a system given the initial conditions, the boundary conditions and the constants, or parameters, which can be found in appropriate handbooks.

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However in many circumstances the parameter(s), in this case P, is (are) unknown. This is the problem that can be addressed using methods of parameter estimation.

It should be noted that there is more than one parameter estimation method available. This work involves using the ordinary least squares (OLS) method. This method, like the other estimation methods, attempts to minimize the error between the functional values generated by the mathematical model and the experimentally measured functional values, with respect to the parameter being estimated. The function used in the OLS method is

$$S = \sum_{i=1}^n (Y_i - \eta_i(\bar{\beta}))^2 \quad (2.3.1)$$

where n is the number of data points. S is referred to as the sum of the squares function. This equation states that the differences between the measured data values, Y_i , and the corresponding predicted values from the model, η_i , are squared and summed. The goal is to minimize S with respect to the vector of parameters, $\bar{\beta}$. This is accomplished by taking the derivative of S with respect to the parameters and setting it equal to zero.

$$\frac{\delta S}{\delta \bar{\beta}} = 0 \quad (2.3.2)$$

When the values of $\bar{\beta}$ are found that satisfy equation (2.3.2) the sum of squares function has been minimized. In some cases it is possible to have more than one set of parameters that satisfy (2.3.2) due to the presence of local minimums. The ultimate desire would be to find the

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global minimum. In general this is not a problem because most models that are well posed only have one minimum.

Using equation (2.3.1), the sum of squares function for this work is

$$S = \sum_{i=1}^n [R_{m_i}(t) - R_{c_i}(t)]^2 \quad (2.3.3)$$

where $R_{m_i}(t)$ is the experimentally measured radius and $R_{c_i}(t)$ is the predicted radius, using the model equation (2.2.45), at time t . Recall the procedure normally used to minimize (2.3.3) would be to set the derivative of S with respect to P equal zero and solve for P . However, the method used to minimize S , in the program SENS, was not as direct due to the difficulty of solving for $R_c(t)$ explicitly. Given a set of experimental data, (i.e. (t_i, R_{m_i}) for $i=1$ to n), S can be minimized by having a computer program, SENS, generate theoretical sets of data, as mentioned in section 2.2, for a likely range of P 's supplied by the user, which can be found in the published literature. Each set of data can then be plugged into (2.3.3) to calculate a S . The S with the smallest value, S_{\min} , corresponds to the set of data with the best curve fit of R v. s. t and the best estimate of the cell permeability, P_{est} .

Now that a method exists for estimating P , it would be beneficial to know how good of an estimate P_{est} is. This is accomplished by calculating the standard deviation of P_{est} . However, this is not an easy task because of the nonlinearity of S with respect to P . (S is said to be nonlinear in P if the sensitivity coefficient,

$$\frac{\delta S}{\delta P}$$

is a function of the parameter, $P^{[11]}$) To get around this, J. Beck formulated an approximate standard deviation by examining the covariance matrix of the parameters for models that are linear with respect to the parameters. To calculate the standard deviation of P we must start with the general sum of squares function for a linear model

$$S = (Y - X\beta)^T(Y - X\beta) \quad (2.3.4)$$

where $\eta = X\beta$ and

$$X = X_{jk}(i) = \frac{\delta \eta_j(i)}{\delta \beta_k}; \quad i=1, \dots, n; \quad j=1, \dots, n; \quad k=1, \dots, p$$

Taking the derivative of S with respect to β , setting the matrix of derivatives equal to zero and solving for $\beta=b$ we get

$$b = (X^T X)^{-1} X^T Y \quad (2.3.5)$$

By making the following assumptions

- 1) $\hat{Y}_i = \eta_i + \epsilon_i$; the error, ϵ_i , is in the measuring of Y_i and is additive,
- 2) $E(\epsilon_i) = 0$; the expected mean value of the error is zero, (the function $E(x)$ is the statistical function of the expected value of the variable x .)
- 3) Errorless independent variables,
- 4) Nonrandom parameters and no prior information regarding the parameters,

the covariance of (2.3.5) is

$$\text{cov}(b) = (X^T X)^{-1} X^T \psi X (X^T X)^{-1} \quad (2.3.6)$$

where $\psi = E(\epsilon \epsilon^T)$. Equation (2.3.6) can now be used to approximate the covariance matrix of the parameters for nonlinear models;

$$\text{cov}(b) \approx (X^T X)^{-1} X^T \phi X (X^T X)^{-1} \quad (2.3.7)$$

With the additional assumptions of

- 1) constant variance errors,
- 2) uncorrelated errors,
- 3) covariance matrix of errors is known to within a multiplicative constant,

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the estimate of (2.3.7) becomes

$$\text{cov}(\mathbf{b}) \approx (\mathbf{X}^T \mathbf{X})^{-1} s^2 ; \quad s^2 \approx \frac{(\mathbf{Y} - \hat{\mathbf{Y}})^T (\mathbf{Y} - \hat{\mathbf{Y}})}{(n - p)} \quad (2.3.8)$$

where n is the number of measurements, or data points, recorded, \mathbf{Y} is the experimental measured value, $\hat{\mathbf{Y}}$ is the predicted value and p is the number of parameters. Recall, in this work, there is only one parameter (P). Rewriting (2.3.8) for one parameter the covariance matrix simplifies to

$$\text{cov}(b) = V(b) \approx (\mathbf{X}^T \mathbf{X})^{-1} s^2 ; \quad s^2 \approx \frac{(\mathbf{Y} - \hat{\mathbf{Y}})^T (\mathbf{Y} - \hat{\mathbf{Y}})}{(n - 1)} \quad (2.3.9)$$

where $V(b)$ is the statistical function variance, which is related to the standard deviation by $\theta^2(P_{\text{est}}) = V(b)$, (where θ is the standard deviation). Therefore, applying (2.3.9) the square of the standard deviation becomes

$$\theta^2(P_{\text{est}}) \approx \frac{\sum_{i=1}^n [Rm_i(t) - Rc_i(t)]^2}{\sum_{i=1}^n \left[\frac{\delta Rc_i}{\delta P_{\text{est}}} \right]^2 (n-1)} \quad (2.3.10)$$

where $\delta Rc_i / \delta P_{\text{est}}$ is the so called sensitivity coefficient.

2.4 The Effect of Temperature on P. (The Activation Energy)

Several workers have studied the temperature dependence of the movement of water across cell membranes. The relationship used to describe this dependence obeys the classical Arrhenius type equation

$$P = k \exp[-\Delta E_a/RT] \quad (2.4.1)$$

where k is a constant (frequency factor) and E_a is the activation energy.

This equation can be rewritten as

$$\ln(P) = \ln(k) - \frac{\Delta E_a}{RT} \quad (2.4.2)$$

By plotting $\ln(P)$ v.s. $1/T$, the activation energy can be determined from the slope.

CHAPTER 3

The Parameter Estimation/Simulation Program, SENS

3.1 Introduction and Background (of J. Tu's Program)

As mentioned in Section 1.2, J. Tu developed a FORTRAN computer algorithm, SENS, to be used in conjunction with the microscope diffusion chamber system to estimate membrane water permeabilities. Specifically, the program was designed to estimate the permeability of a cell membrane or run a simulation (pseudo) experiment to see what would happen during an experiment under specified conditions. Prior to running the program the (actual or simulated) experimental data and parameters were entered into an input file. The input file was read by SENS and processed. The output consisted of four optional graphs (sent to the screen and a graphics file) and an output file containing tables. The first graph plotted the normalized concentration change, in the dialysis membrane and sample region, as a function of the normalized time. The second graph plotted the sensitivity coefficient, $\delta R_c / \delta P$, as a function of time. The third plot was the normalized cell volume as a function of time. The last graph plotted the sum of the squares function versus the permeability. The first table in the output file was the input data, the second a table containing the concentration distribution, in the dialysis membrane and the sample region, as a function of time, the third a table of the experimentally measured radius as function of time and finally the best statistical estimate of the membrane hydraulic permeability, the

standard deviation of the best estimate of the permeability and the corresponding minimum sum.

Tu's program worked quite well, providing all of the parameters and data were entered into the input file correctly. Therefore, the basic structure of his program was left intact i.e. the processing of the parameters and data. The major modifications made were at the input and output stages. The input stage was revised to allow the user an option of entering the necessary input by one of two ways: 1) a (modified) input file or 2) by answering the prompted questions. The output was arranged in a more logical manner and labelled more clearly as to what was being (graphically) plotted and what tables were being generated. Also, the best estimate of the permeability, the standard deviation and the minimum sum were sent to the screen and to two output files.

3.2 The Modified SENS

At first, the concept of making SENS user friendly seemed a relatively simple task. But during the modification process it was discovered that this would not be the case. The program grew 716 (FORTRAN) programming lines (which is about 24K) to 2002 programming lines (which is about 68K).

The most efficient way to describe how SENS works would be to look at the flow chart of SENS in Figure 3.2.1. The actual program can be found in Appendix D. In addition, sample output, of the four graphs describe in Section 3.1 and of one output file, can be seen in Figures 3.2.2 - 3.2.6. Note: this sample output is from actual experimental data for an experiment using a lymphocyte at 25°C.

Once the modifications were made, the next step was to convert SENS to an IBM Personal Computer.

Figure 3.2.1 - Flow Chart of SENS - PRIME Version

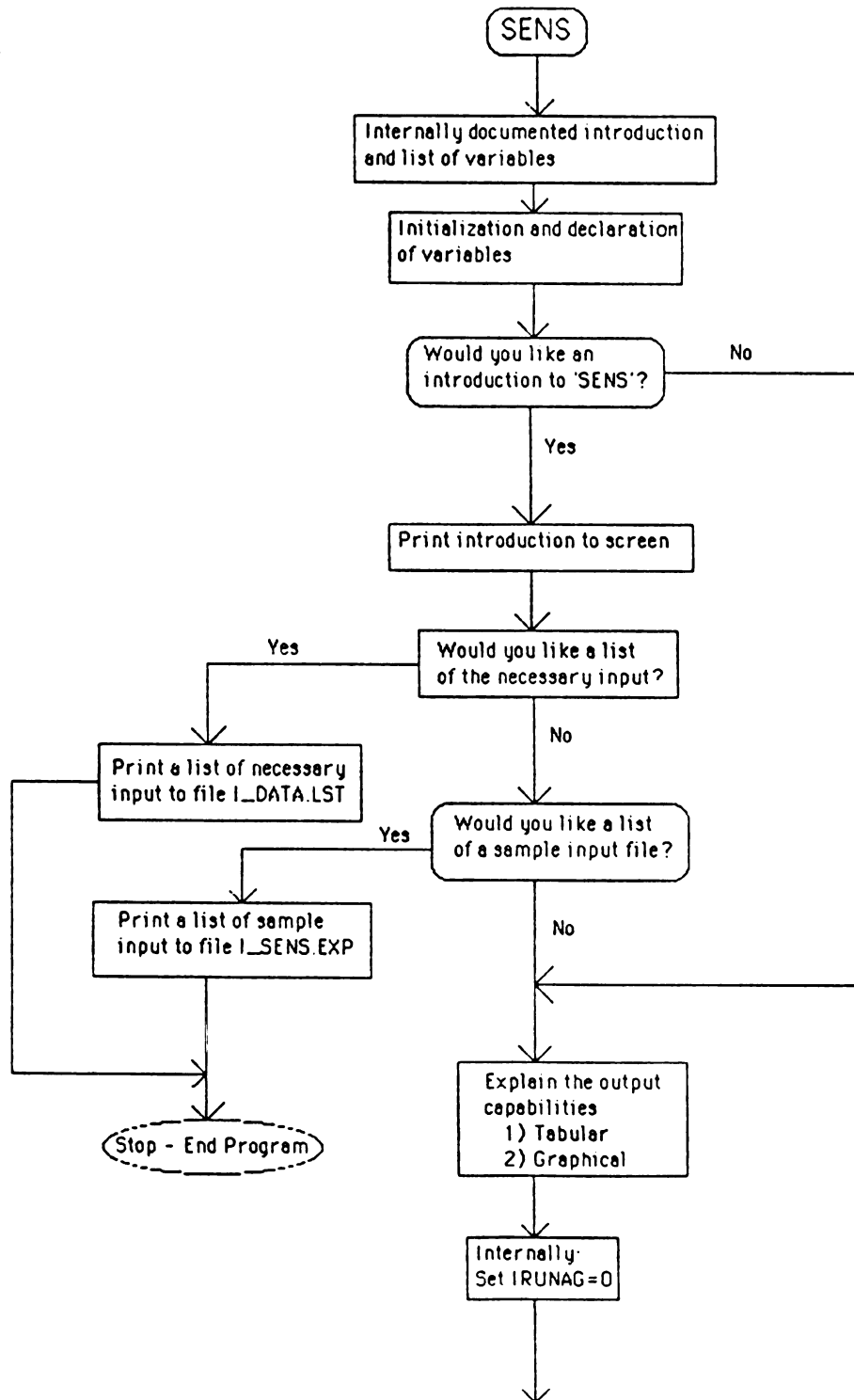


Figure 3.2.1 (cont'd.)

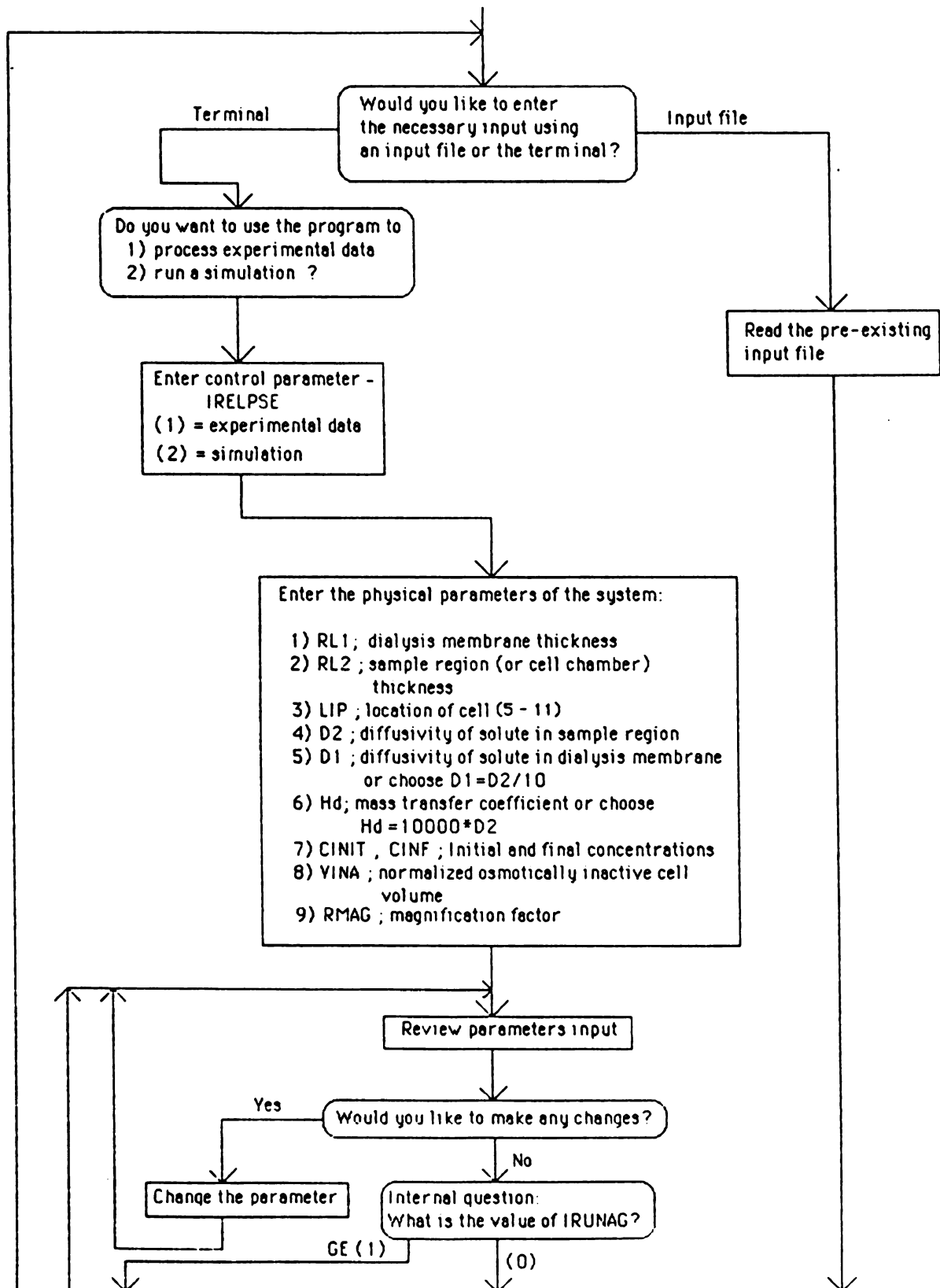


Figure 3.2.1 (cont'd)

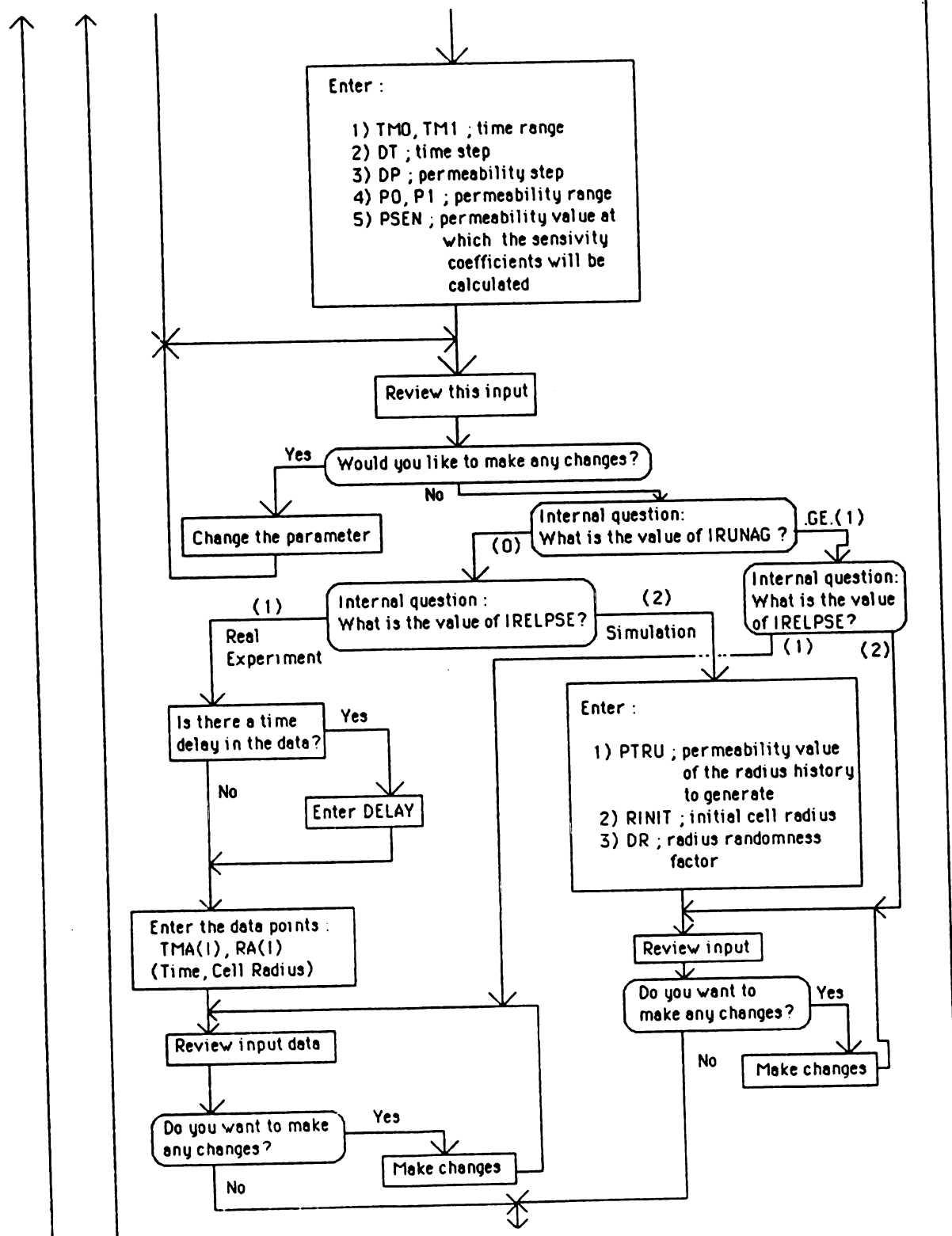


Figure 3.2.1 (cont'd.)

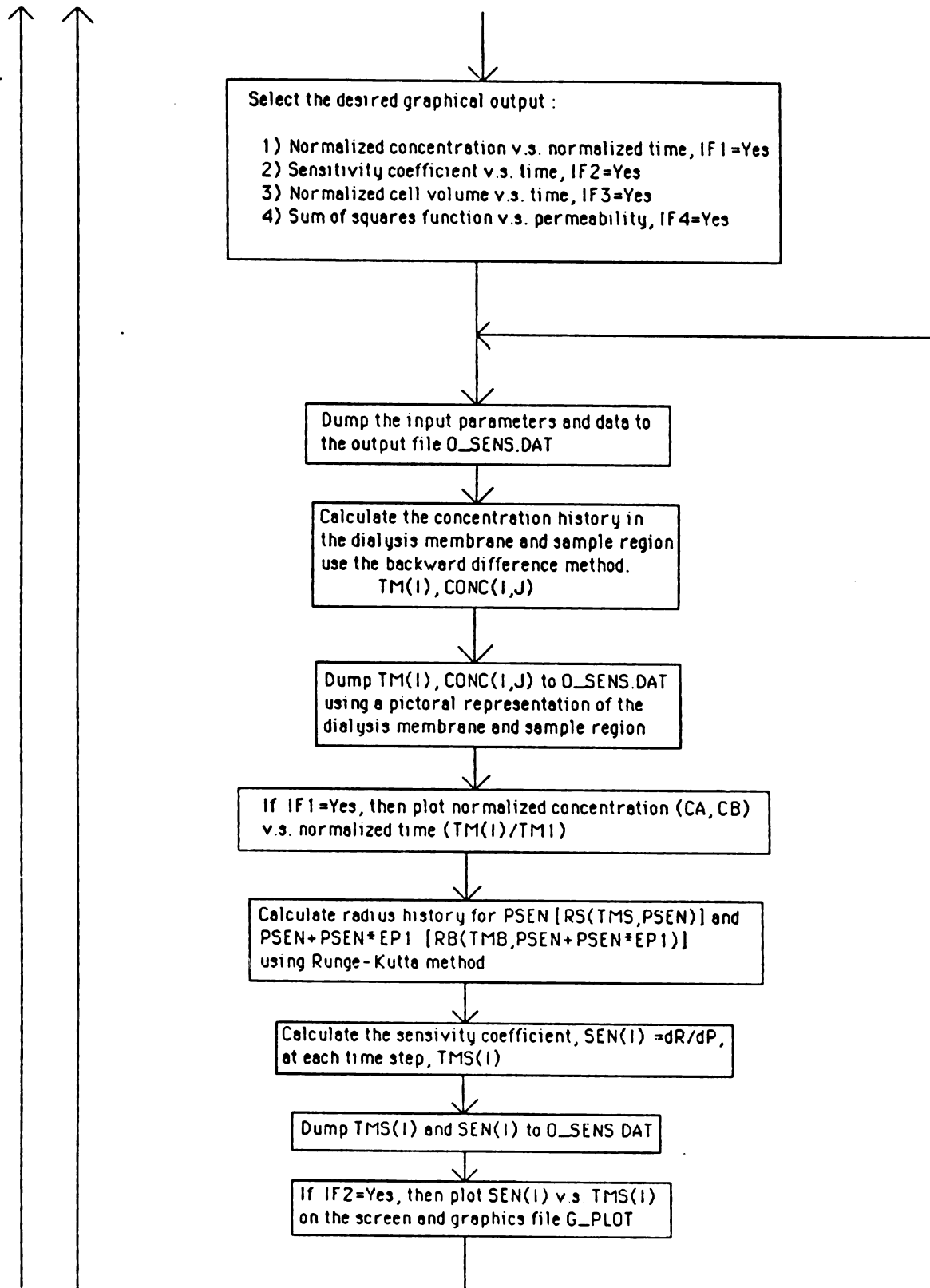


Figure 3.2.1 (cont'd)

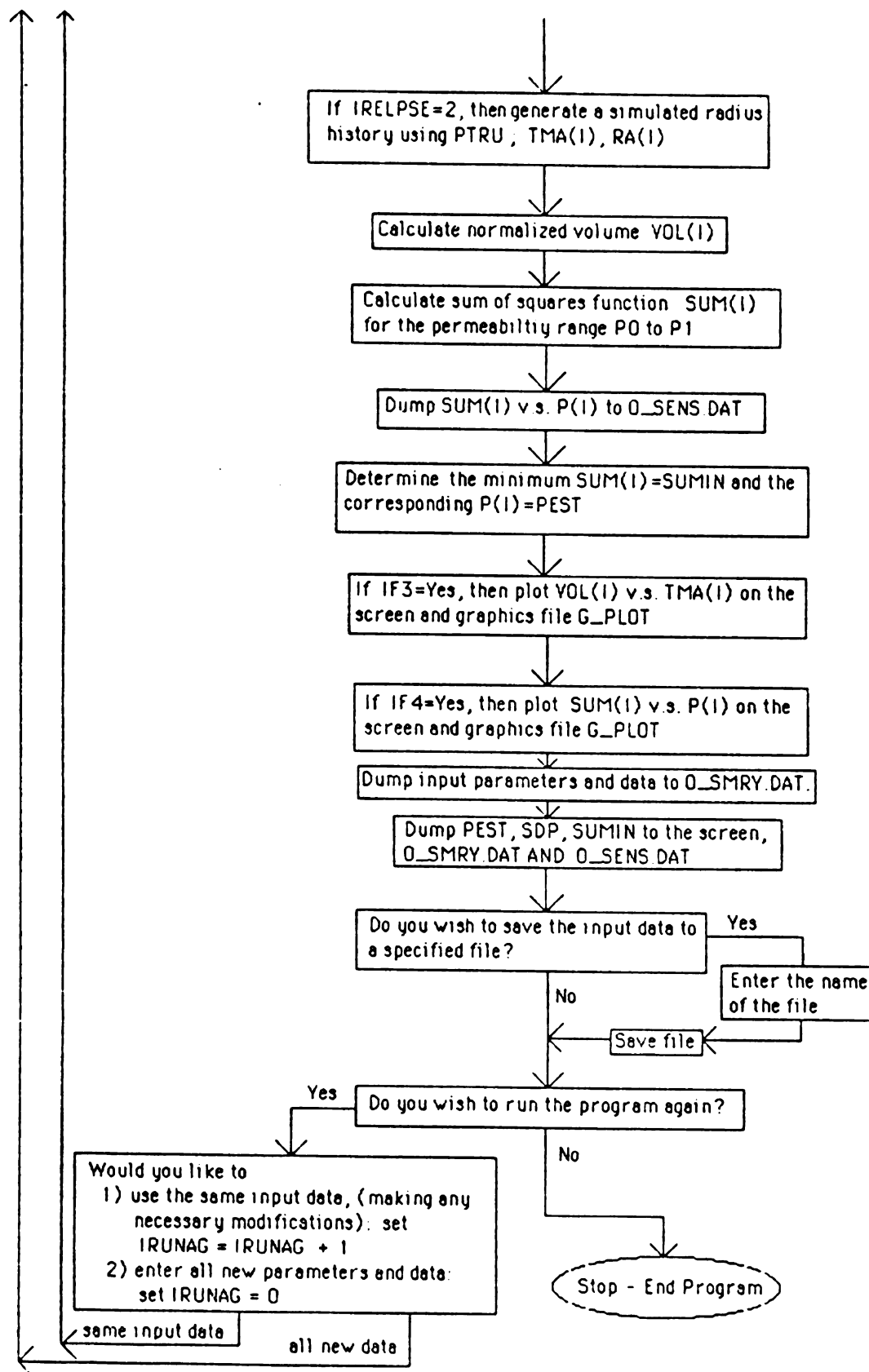


FIGURE 3.2.2 - Sample Output File of SENS - O_SMRY.DAT

***** THIS IS FILE O_SMRY.DAT *****

THE INPUT PARAMETERS AND DATA WERE:

THE VALUES ENTERED SO FAR ARE:

- 1) DIALYSIS MEMBRANE THICKNESS - .160E+02 MICRONS
- 2) CELL CHAMBER THICKNESS - .915E+02 MICRONS
- 3) LIPOSOME POSITION (5-11) - 5
- 4) DIFFUSIVITY IN CELL CHAMBER - .148E-08 M*M/SEC.
- 5) DIFFUSIVITY IN DIALYSIS MEMBRANE - .148E-09 M*M/SEC.
- 6) MASS TRANSFER COEFFICIENT - .148E-04
- 7) INITIAL CONCENTRATION - .291 OSMOLALITY
- 8) FINAL CONCENTRATION - .725 OSMOLALITY
- 9) INACTIVE VOLUME % - 34.70
- 10) MAGNIFICATION FACTOR - 11290.0

THE VALUES ENTERED ARE:

- 1) TIME STEP - 1.00 SEC.
- 2) TIME RANGE - .0 SEC. TO 60.0 SEC.
- 3) PERMEABILITY STEP - .10 MICRONS/SEC.
- 4) PERMEABILITY RANGE - .00 MICRONS/SEC. TO 15.00 MICRONS/SEC.
- 5) INVESTIGATING PERMEABILITY - 9.30 MICRONS/SEC.

THE DATA POINTS ENTERED WERE:

(INCLUDING THE TIME DELAY OF .0000 SEC.)

J	TIME(J) (SEC.)	RADIUS(J) (CENTIMETERS)
1	.20	4.69
2	1.40	4.69
3	3.00	4.65
4	4.40	4.65
5	7.60	4.61
6	11.80	4.52
7	13.90	4.43
8	15.30	4.38
9	18.40	4.34
10	22.00	4.25
11	26.60	4.16
12	31.40	4.12
13	37.60	4.07
14	51.80	4.03
15	54.30	3.99
16	58.90	3.99
17	.00	.00

FIGURE 3.2.2 (cont'd.)

***** THE RESULTING PERMEABILITY *****

THE LOCAL MINIMUM OCCURS AT P - 8.600 MICRONS/SEC.

THE STANDARD DEVIATION OF ESTIMATED P IS .267E+00 MICRONS/SEC.

THE MINIMUM VALUE OF SUM IS .004

Sample Graphical Output - Concentration v.s. Normalized Time

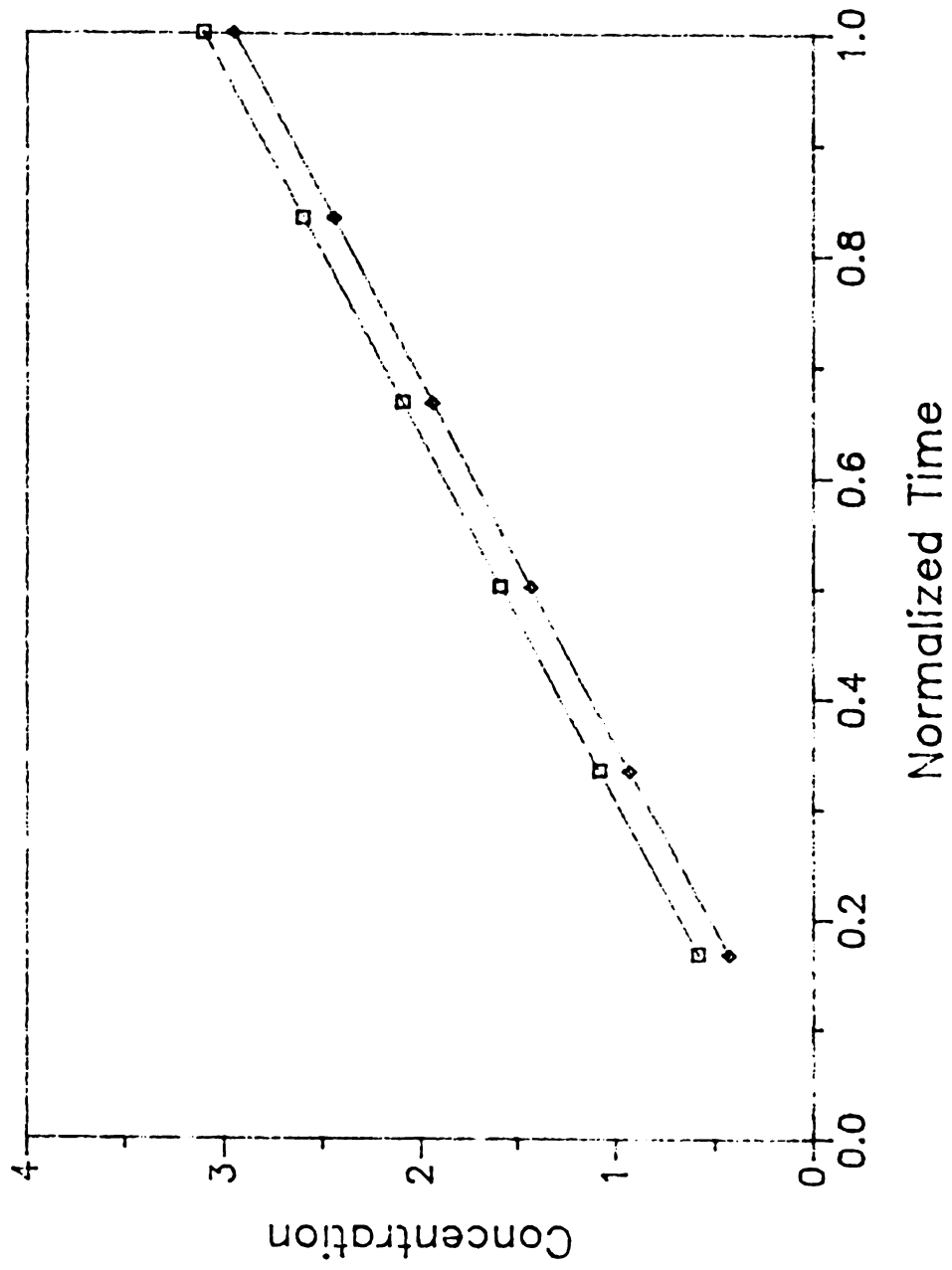


Figure 3.2.3

Sample Graphical Output - Sensitivity Coefficient v.s. Time

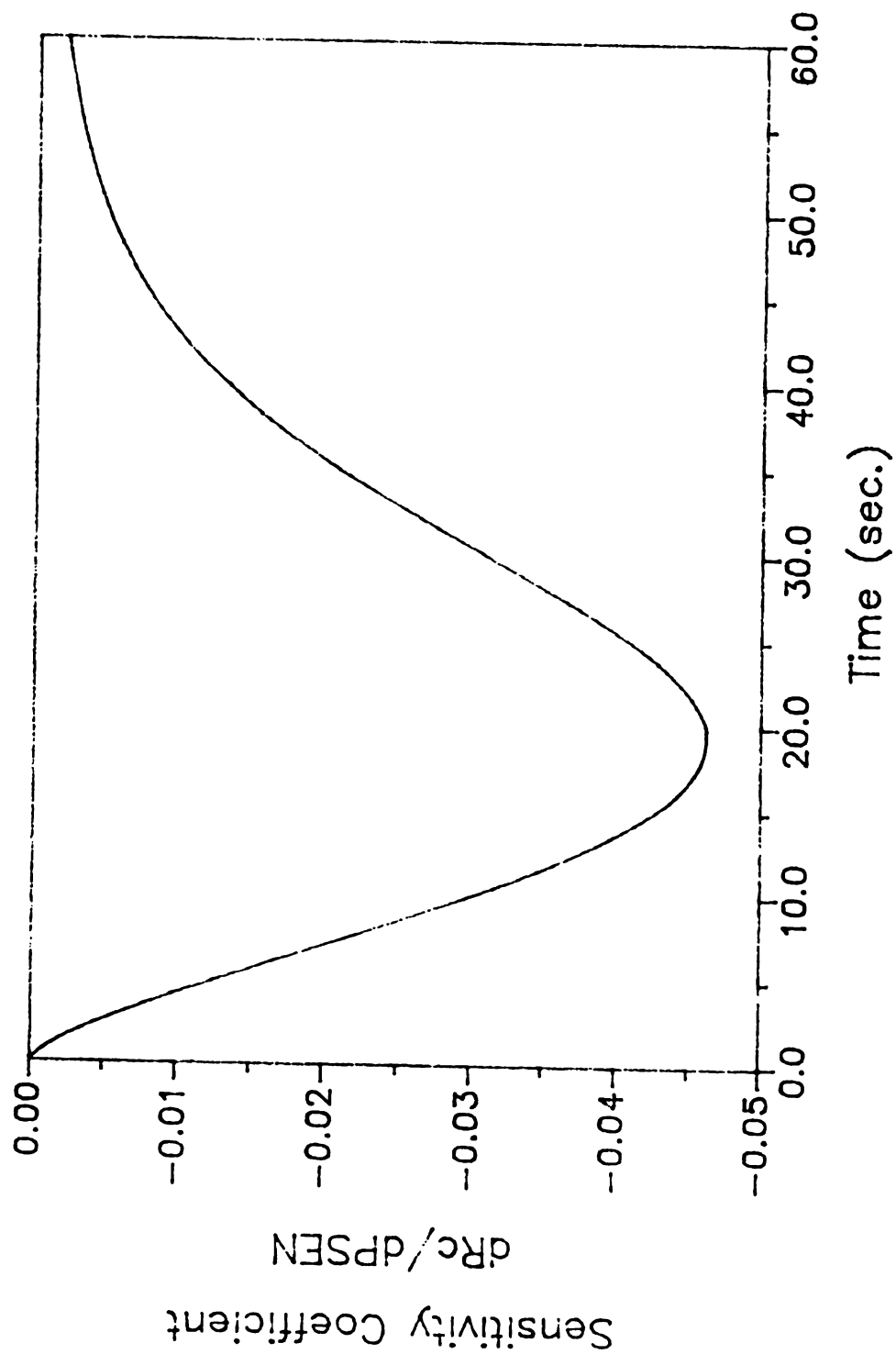


Figure 3.2.4

Sample Graphical Output - Normalized Cell Volume v.s. Time

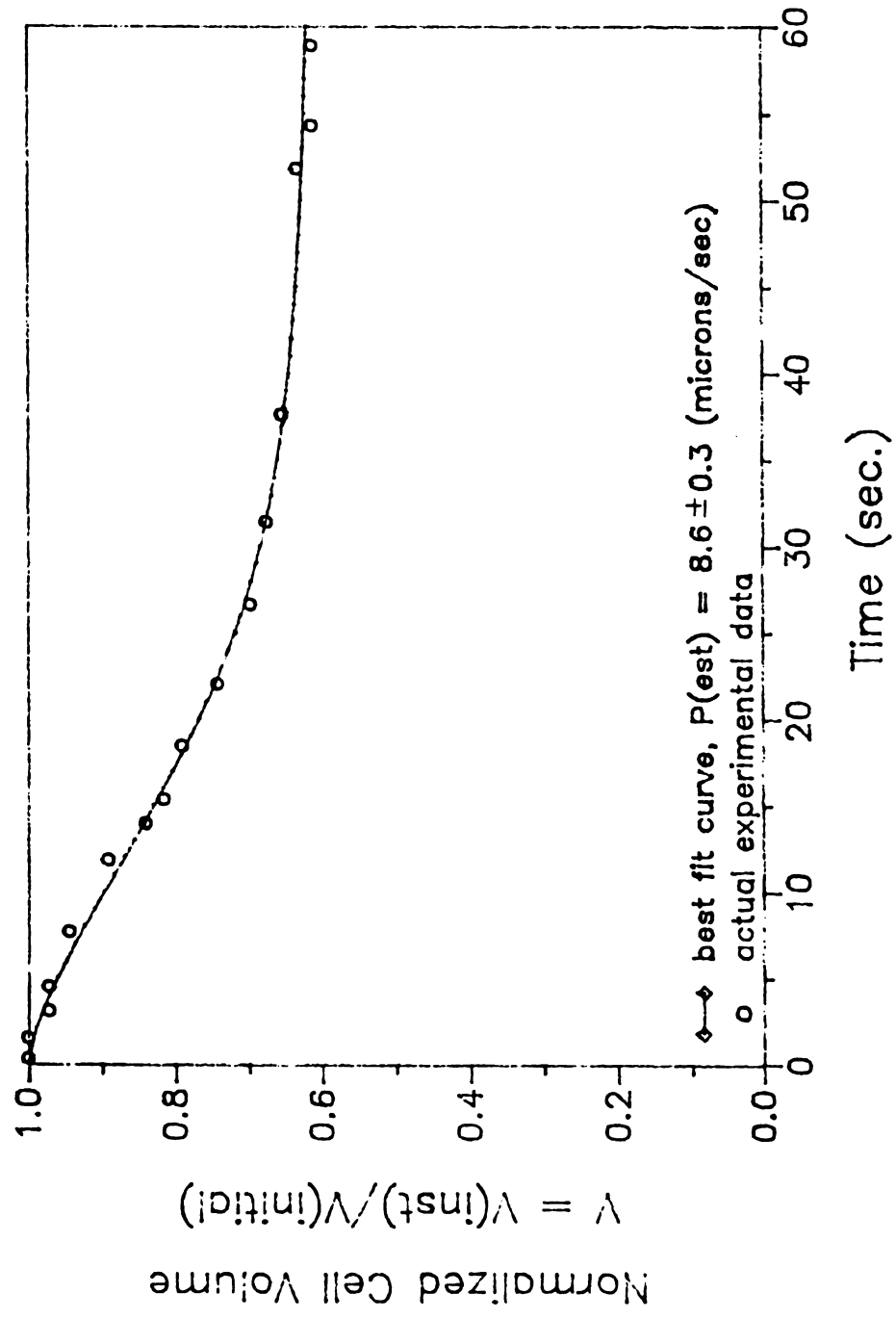


Figure 3.2.5

Sample Graphical Output - Sum of the Squares v.s. Permeability

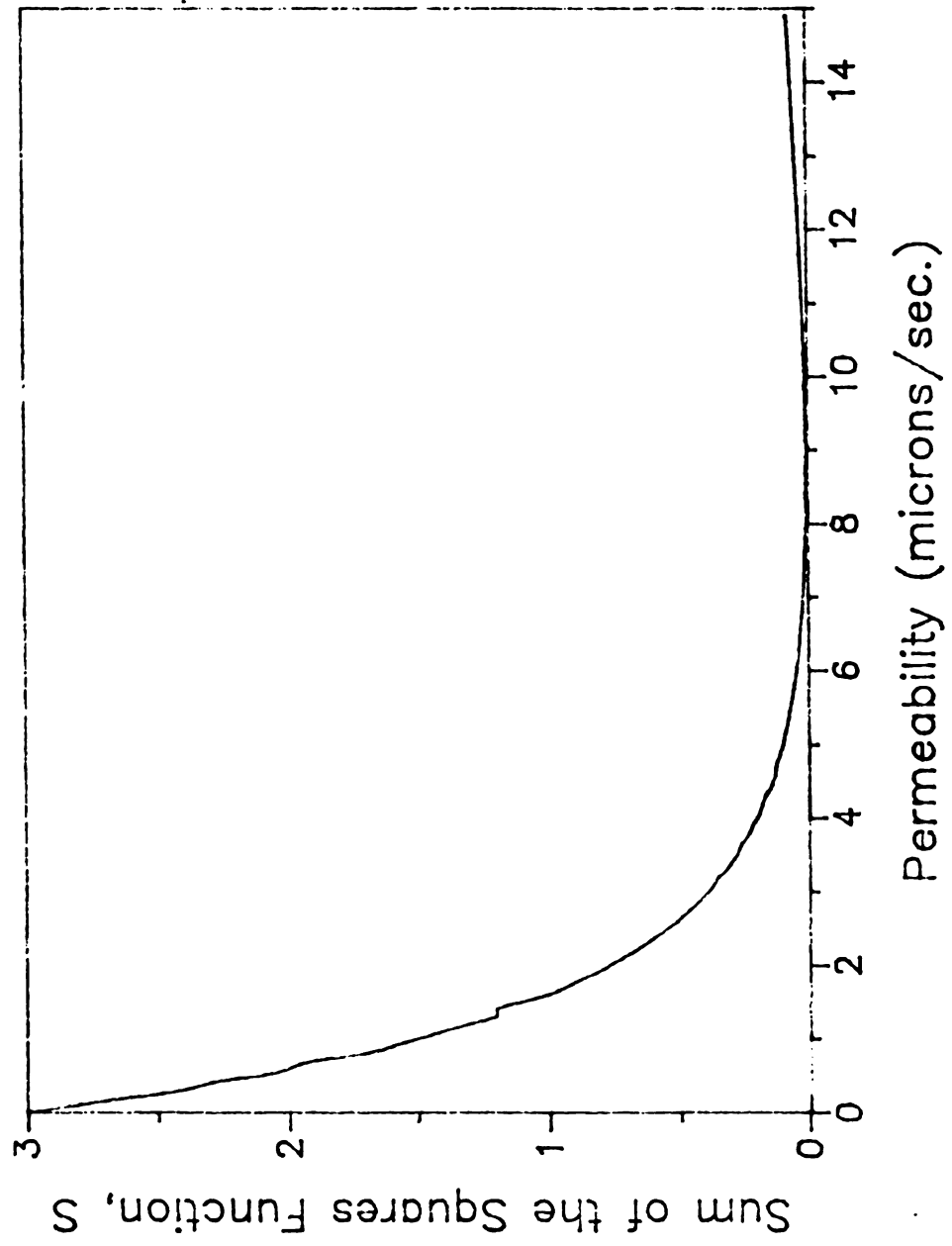


Figure 3.2.6

3.3 Converting SENS to the IBM PC

Before SENS was adapted to the IBM PC, the primary concern that needed to be addressed was which graphical software package should be used. Originally SENS resided on the PRIME, which allowed the use of the interactive graphical software, PRINTEX. The graphical software package that was chosen to be used with the converted SENS version was PLOTIT. PLOTIT was chosen because of its ease of use, the quality of graphs produced (using a Hewlett Packard Plotter) and its availability at the Engineering Computer Facility PC room.

Converting SENS from the PRIME to the IBM PC involved a two step process. First SENS was adapted to function as though it were on an IBM PC but was actually still on the PRIME. In other words, the interactive graphical programming code was stripped from the original version of SENS and replaced with code to generate four (optional) separate output files which could be used with PLOTIT (on the PRIME). Then once all the "bugs" were worked out SENS was converted to the IBM PC.

Another important consideration addressed was which FORTRAN compiler should be used. The compiler that was used was MICROSOFT FORTRAN. This compiler was chosen because the author was familiar with its operation and it seemed to have a good error detecting mechanism which was very helpful when SENS was converted.

Once the conversion process was completed, a sample input file was used as a test to make sure both versions yielded the same results. It should also be noted that after the conversion some minor programming changes were made to both versions resulting in the programs recorded in

Appendices D and E.

.

CHAPTER 4

Experimental Equipment and Procedures

4.1 Preparing Cells for Experimental Runs

The methods used to prepare the cells used in this work will now be described.

4.1.1 Preparing Egg Lecithin Liposomes

Before experiments using egg-lecithin liposomes were conducted, the liposomes, the isotonic sucrose solution and the hypertonic sucrose solution had to be prepared. The solutions were made by adding the proper amount of sucrose to a known amount of distilled water. The desired concentrations were 0.02 osmolality for the isotonic solution and 0.04 osmolality for the hypertonic solution. The concentrations were measured using an osmometer.

Once these solutions were made the liposome cells were prepared. 0.07 grams of the egg lecithin lipid was measured into a 25 ml erlenmeyer flask. Next, the lipid was dissolved using 25 ml of a 2:1 chloroform:methanol solution and a vortex mixer. Then 0.5 ml of this solution was pipetted into a 50 ml round bottom flask which was fastened to a rotavac and a vacuum was applied for approximately $\frac{1}{2}$ hour. The chloroform:methanol solution evaporated leaving a thin film of lipid dispersed on the bottom of the flask. The flask was detached and 10 ml of isotonic solution was gently added, being careful not to disturb the lipid film, and stoppered. The circulating bath, which had been

preheated to 60°C, was turned off, the flask was placed inside and steadied, and the bath was closed. This solution was left in the bath overnight and by morning a small cloud of lipid had formed on the bottom near the middle of the flask.

After a few tries, it was discovered that the best results for obtaining what was believed to be "unilamillar" vesicles was to use a pipetman, which was preadjusted to 18 μ l samples, and extract a sample from "near" the edge of the cloud.

4.1.2 Preparing Human Lymphocytes

Prior to conducting experiments using lymphocytes, whole blood was obtained and separated, and isotonic and hypertonic salt (sodium chloride) solutions were prepared. Again, these solutions were prepared in a similar fashion as those that were used in the liposome experiments. The desired concentrations for the lymphocyte experiments was 0.291 osmolality for the isotonic solution and 0.725 osmolality for the hypertonic solution. 0.291 osmolality was chosen for the isotonic solution because this is the approximate osmolality of human blood. 0.725 was chosen because by increasing the concentration 2.5 times allowed the final cell size to decrease about 40%, with respect to the initial cell volume, which allowed for greater ease in recording the change in the cell radius. Also, this was the approximate range used by Hempling and Porsche, which allowed for comparisons to be made. In addition to measuring the concentrations of the solution, the pH was also measured. The pH of the solutions ranged from 7.0 to 7.3. The pH measurements were made using an Orion pH electrode probe and meter.

The blood used was either obtained from the Red Cross in Lansing, Michigan or was drawn from the author by a medical technologist on campus. The blood was collected in vacuum tubes containing EDTA. Therefore the age of the drawn blood ranged between 1 and 24 hours old by the time the blood had undergone separation. Initially 3 ml of Histopaque-1077 (SIGMA DIAGNOSTICS) medium was placed in 15 ml test tube. Next 6 ml of blood was carefully layered on top of the medium. The tube was then placed into a swing-bucket centrifuge and set at 387 G's for 30 minutes. This resulted in four distinct layers. The top layer contained

primarily plasma and platelets, the next layer contained the desired lymphocyte cells, while the last two layers contained the medium and other blood cells (including red blood cells), respectively. The top layer was suctioned off to approximately 5 mm above the lymphocyte layer. Next the lymphocyte layer was pipetted off and placed into another 15 ml test tube. These cells were then washed with 5 ml of Bacto Hemagglutination buffer solution [(0512-33-2) DIFCO LABORATORIES] (PH 7.3 ± 0.1) and centrifuged at 387 G's for 10 minutes. The lymphocytes remained at the bottom of the tube while platelets were suspended in the buffer solution. The top layer of platelets was then suctioned off. This washing procedure was repeated two more times. Note, clumping sometimes occurred at any step of the washing. Clumping occurred approximately one out of every five separation attempts. Sometimes the clumps could be shook loose and sometimes the procedure was started over with another sample of blood because the clumps would not readily break apart. Finally, 0.8 ml of isotonic solution was added to the lymphocyte/platelet medium and stored at 4°C for an average of one hour.

4.2 Description of the Microscope Diffusion Chamber

List of parts:

- 1) Chamber body, with heat exchange ducts
- 2) Clear plastic bottom cover slip
- 3) Dialysis membrane, (Cuprophane M80, ENKA AG, Product Group Membrana)
- 4) Rubber membrane retaining ring
- 5) Top fitting
- 6) Top cover glass
- 7) Plastic membrane retainer

Schematic representations of the diffusion chamber are shown in Figure 4.2.1 and 4.2.2. The chamber body was made of copper to allow for effective heat transfer. There were two separate flow channels built into the chamber body. The inner bulk flow channel ran down into the entrance, near the middle area of the chamber body, across the bottom clear plastic cover slip and up and out the exit. This channel provided the introduction of the hypertonic solution during an experimental run. The outer flow channel ran along the outer edge of the chamber, in a square pattern, surrounding the inner channel region. This was the channel used to control the temperature of the diffusion chamber. The dialysis membrane separated the bulk flow region and the sample region. The membrane has a dual purpose: 1) absorbing the shear of the bulk flow region, thus keeping the cell specimen relatively stationary while 2) providing a mechanism for solute transport (i.e. diffusion). The rubber retaining ring held the dialysis membrane firmly to the top fitting, made of brass, and also provided a seal between the top fitting and the chamber body. The top cover glass was glued to the top fitting providing a solid stationary boundary. The area between the dialysis membrane and

Schematic Representation of the Microscope Diffusion Chamber

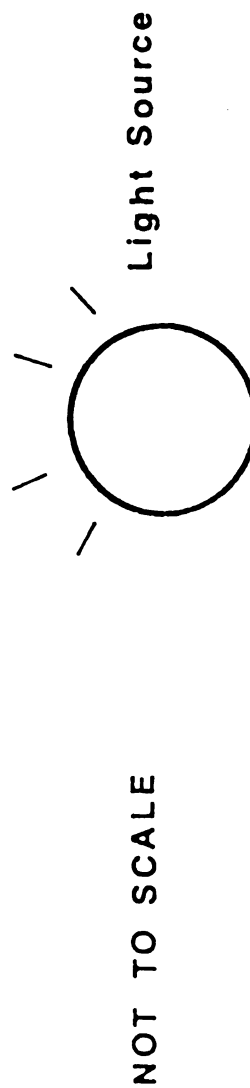
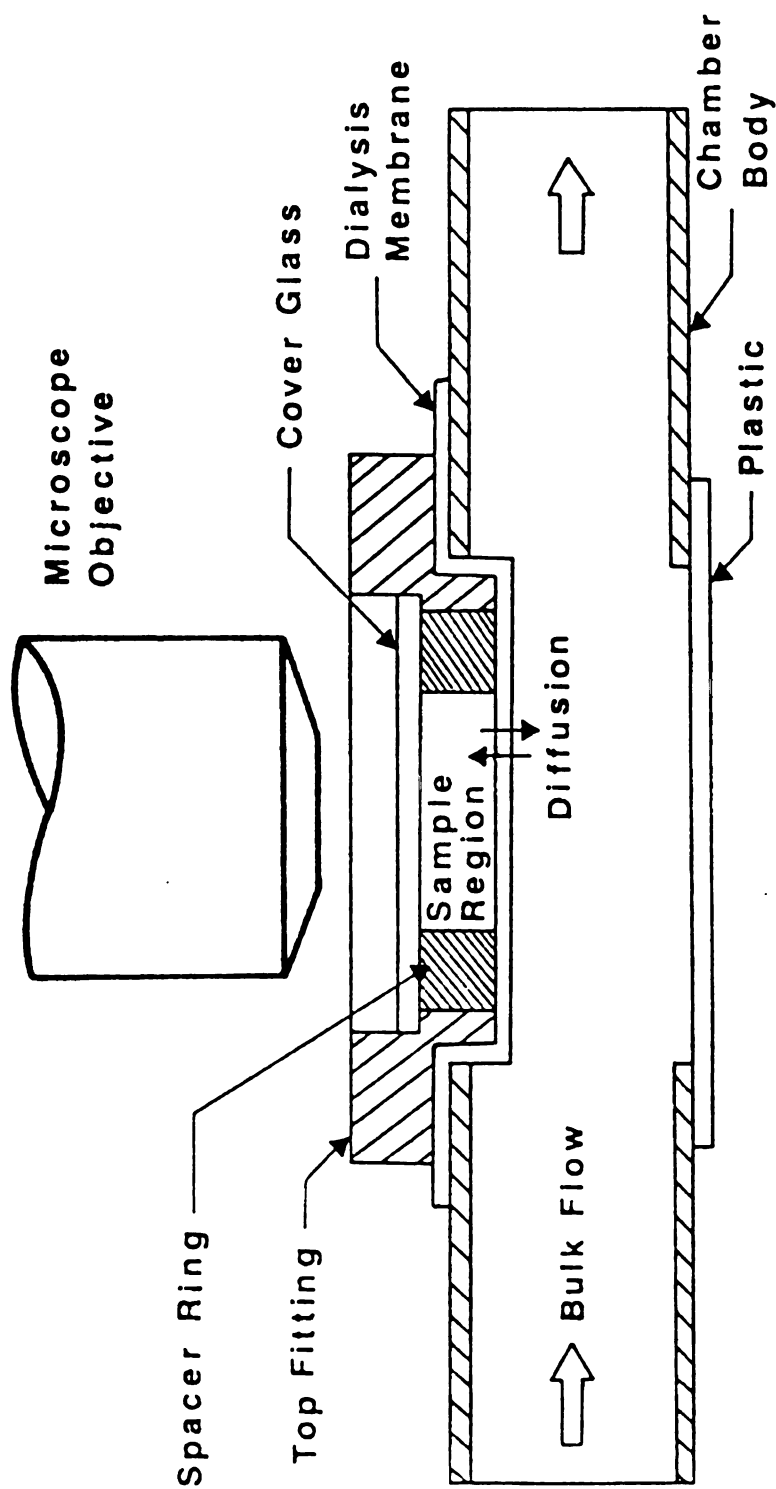
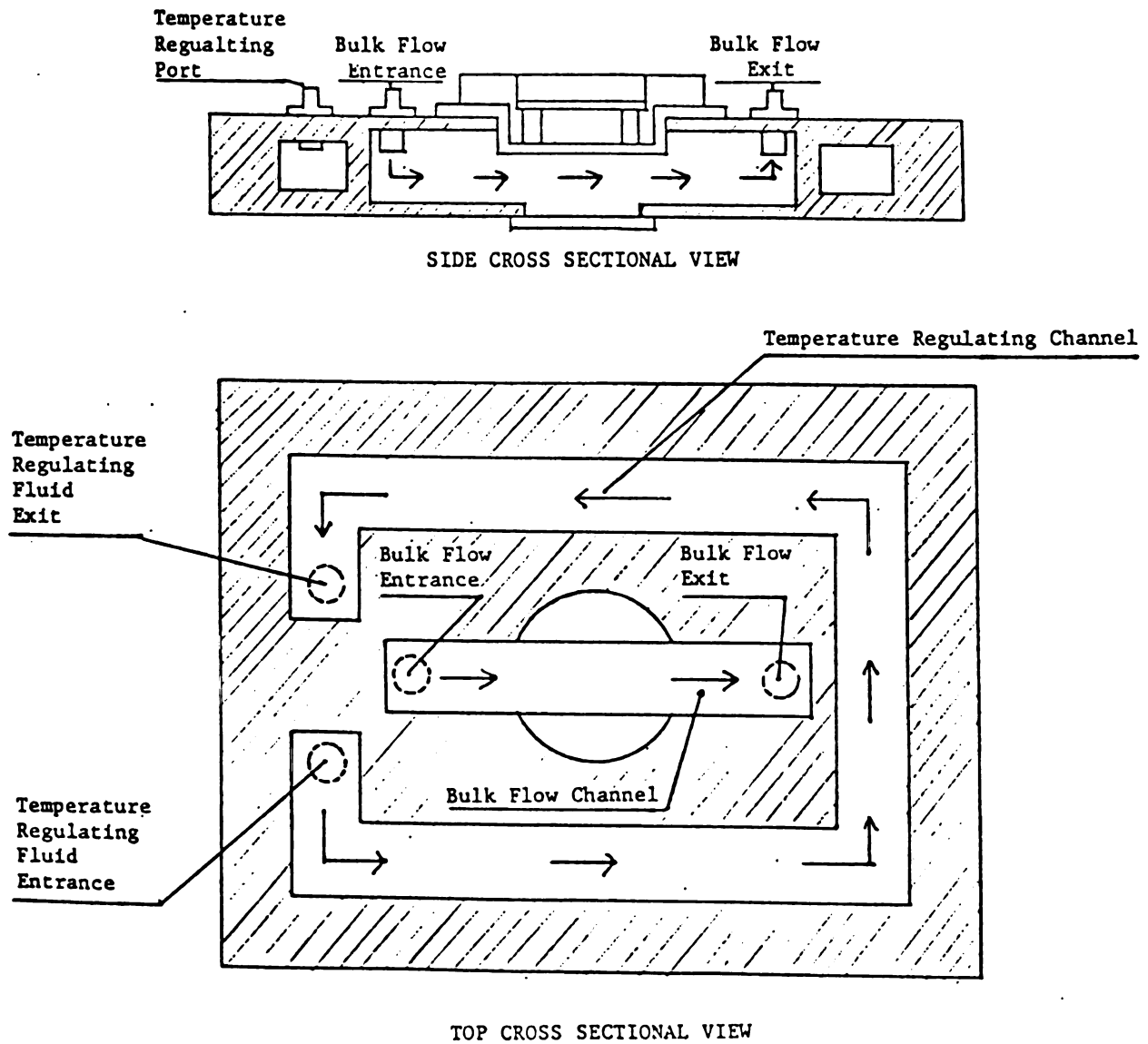


Figure 4.2.1

Figure 4.2.2 - Schematic Cross Sectional View of Microscope Diffusion Chamber



the top cover glass was called the sample region. This is where the cell specimen resided.

4.3 Description of the Overall Experimental System

List of Equipment Used During Experimental Runs

- 1) Microscope diffusion chamber
- 2) Microscope, (Ziess Universal Research D-7082)
- 3) Pumping system - isotonic and hypertonic solutions
- 4) Discharge beaker (1000 ml)
- 5) Pressurized air supply (Engineering Building)
- 6) Vibration damping table
- 7) Digital temperature display device, (OMEGA Digicator C)
- 8) Copper-Constantan thermocouples, (OMEGA Engineering, Inc., Model No. TT-T-24)
- 9) Endocal refrigerated circulating bath, (RTE-8DD, NESLAB)
- 10) Insulated Tub
- 11) Video monitor, (19" RCA Color Television)
- 12) Video camera, (Color JVC or Black and White)
- 13) Video cassette recorder (Sony- β I or Sony U-matic, VO-5600)
- 14) Video tape (Beta or 3/4")
- 15) Timer (Midwest Telecommunication)
- 16) Vacuum grease

After having isolated and prepared the cells of interest in the isotonic solution, the experimental system was set up. A schematic representation of the experimental system is shown in Figure 4.3.1. The system consisted primarily of three units: 1) the microscope diffusion chamber and pumping system, 2) the temperature control system and 3) the data recording equipment.

The microscope was set up on a vibration damping table. This table was used due to the focusing problems that occurred when the microscope was on a bench or counter top. Vibrations from other engineering labs were conducted throughout the building which caused a blurring effect when attempting to focus the microscope on a cell specimen.

First the microscope diffusion chamber body was placed on the specimen stage of the microscope and fastened. Next the electronic solenoid valves of the pumping system were connected to the specimen stage. Then

Schematic of the Overall System

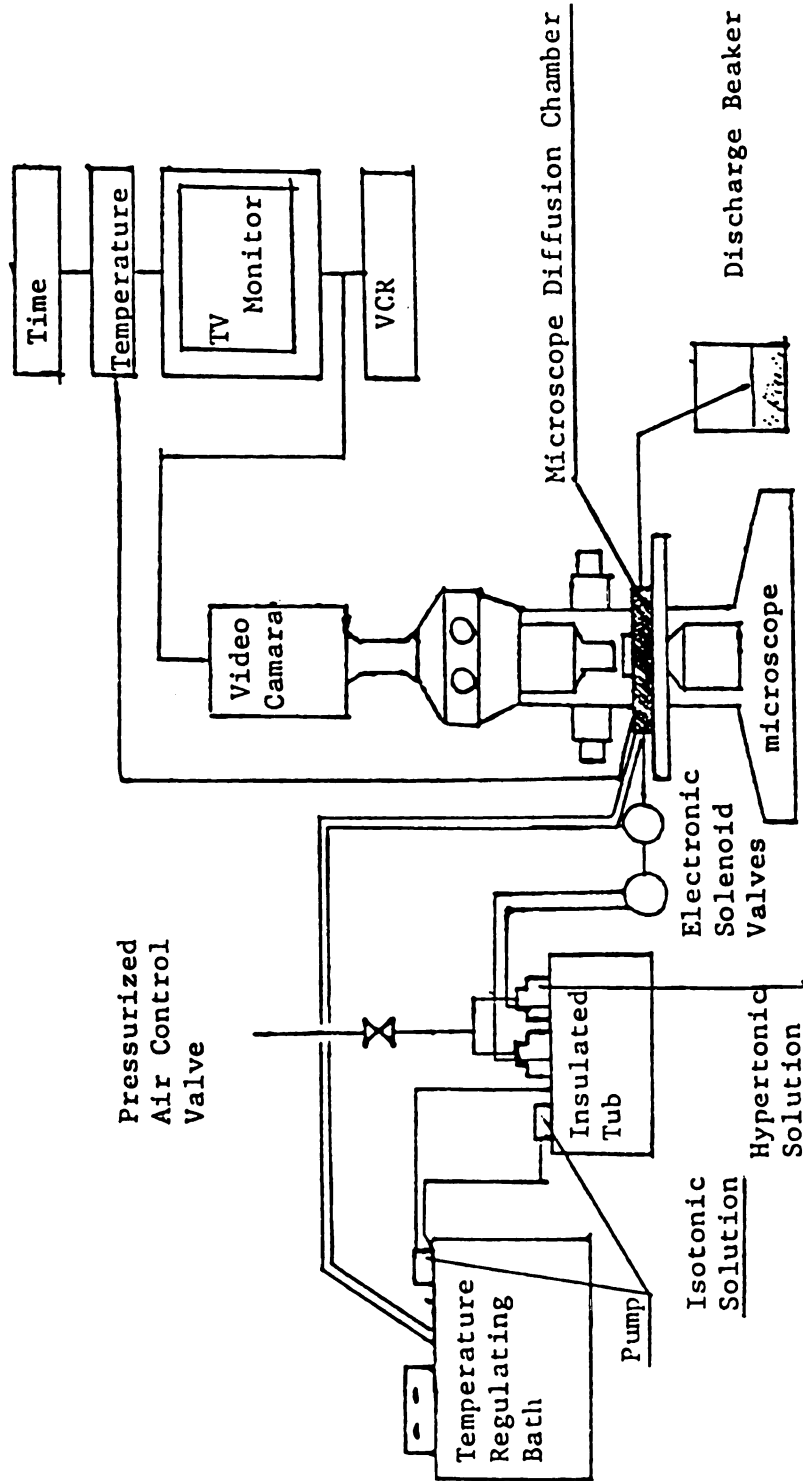


Figure 4.3.1

the pumping system was connected to the entrance for the inner bulk flow channel, a discharge hose was connected from the exit bulk flow port to a discharge beaker and the air supply was connected to the pumping system.

Subsequently the temperature control equipment was set up. The circulating bath was placed on a table next to the vibration damping table. The bath provided the fluid medium necessary to control the temperature of the diffusion chamber and the isotonic and hypertonic solution bottles. An internal circulating pump dispensed fluid to and from the diffusion chamber while two external pumps provided and removed the fluid necessary to heat/cool the solution bottles in the insulated tub. The hoses connected to the external entrance and exit ports of the diffusion chamber were insulated to minimized the heat transfer to/from the surrounding lab environment. As mentioned above, the solution bottles were placed in an insulated tub. The reason the solution bottles were placed in a separate tank, and not directly into the circulating bath, was to avoid vibration transfer from the compressor in the circulating bath to the solution bottles and ultimately to the sample region of the diffusion chamber. In addition, a series of thermocouples were used to monitor the temperature at various points of the experimental system. More specifically, the temperatures of the top fitting of the diffusion chamber, the fluid in the insulated tank, the fluid in the circulating bath, the fluid at the entrance of the inner bulk flow channel and the fluid in each solution bottle were monitored. Each of these thermocouples were connected to a digital temperature display device.

Finally the data recording equipment was set up. First the video camera was attached to the vertical tube on top of the microscope. The video cable from the camera was connected to timer. The timer projected a digital stop watch on the upper left corner of the video monitor. The timer cable was then connected to the video cassette recorder, which was connected to the video monitor.

4.4 Description of an Experimental Run

After the system was set up one or more experimental runs could be conducted. (It should be noted here that before any experiments were performed some preliminary tests were conducted, see Appendix B.) Initially the temperature controlling bath was started and allowed to equilibrate to a desired temperature. This included having the diffusion chamber, solution bottles and circulating fluid at approximately the same temperature. Typically these three temperatures were equal to within 0.5°C. During this temperature transient, the dialysis membrane was prepared. The membrane was shipped from the manufacture (ENKA) in sheets measuring 8½ x 11 inches, which were cut into 1½ x 2 inch sections and presoaked in isotonic solution for 30 minutes. After these preliminary steps were taken, hoses leading from the solution bottles were preflushed, using manual release valves, being careful to remove all air bubbles from the lines. Next, the top fitting was removed and the chamber body was flushed with isotonic solution. The top fitting was then inverted, cover glass facing up, and an 18 µl sample, containing the cell specimen, was pipetted on to the center of the glass. Then a section of presoaked dialysis membrane was placed across the membrane retainer. Extra care was taken in handling the dialysis membrane being careful not to rip it. The membrane was then carefully lowered on to the top fitting using the plastic membrane retainer. Holding the membrane retainer in place, the rubber O-ring was applied to the fitted groove in the top fitting. This O-ring held the membrane firmly in place. Next, a small amount of vacuum grease was applied to the O-ring and then the top fitting was placed into the chamber body. Note, at this point it was

also very important to make sure no air bubbles were present in the bulk flow region. Air bubbles in the bulk flow region would cause a pulsing motion during an experimental run. The microscope was next focused on the sample region. Then the pumping system was turned on flushing the isotonic solution through the bulk flow region. This allowed for the operator to check for air bubbles and any leaks before the hypertonic solution was introduced thus "preserving" the cell specimen. The isotonic solution was shut off and a search for a desirable specimen was conducted. Once a cell was located the sample region thickness (RL2) and cell position (LIP) were determined. The sample chamber thickness was calculated using the grid marks on the fine adjustment focusing knob. Each grid mark was calculated to be $1.5 \mu\text{m}$ deep. (This measurement was performed by J. Tu). The number of grid marks counted between the top cover glass and the dialysis membrane gave an approximate sample region thickness. Note in the analysis it was assumed that the sample region thickness remained constant, however in practice the sample region thickness sometimes increased, on the average, 5 - 7%. Therefore an average thickness was used based on the initial and final sample region thicknesses. Also, the cell position was noted by counting the number of grid marks from the dialysis membrane or the top cover glass. Again, in the analysis the cell position was assumed constant; however in practice the cell sometimes moved, on average 5%. Therefore an average cell position was used based on the initial and final cell position. After these calculation were made the isotonic solution was started again, final focusing adjustment were made and the video recorder was started. At the desired time ($t=0$), the timer was started and the switch for the

hypertonic solution was engaged, which also cut the supply of isotonic solution. Note, the reason hypertonic solution was started while the isotonic solution was flowing, and not from a dead start, was because the shock from a dead start sometimes caused the cell to move out of the plane of focus. The transition from flowing isotonic to hypertonic was less abrupt. The cell response was recorded for a length of time based upon calculations made using the simulation mode of the data reduction program using reasonable estimates of anticipated permeability. At the end of the time duration, the pumping system, timer and video recorder were stopped.

At this point the experimental system could be set up for another run or solution bottles could be exchanged and the system started up again, further reducing the cell size.

4.5 Description of Data Measurements

After each run or after a set of runs, the data measurements were made. It should be noted that all experimental runs had a time delay. This was due to the small piece of tubing which connected the flow and the diffusion chamber bulk flow entrance port. In the description above, it was mentioned that a timer was started at the time the hypertonic solution was switched on. At that moment, the solution in the connecting tube still had isotonic solution in it. Based upon the length of the tube, the tube diameter and the flow rate of the hypertonic solution, a "time delay" was calculated (at the beginning of each experimental day). The time delay did not need to be subtracted here because the program SENS allowed the user to have a time delay (DELAY) subtracted from the data if necessary. The typical time delay was between 2.2 seconds and 3.1 seconds with an average of 2.7 seconds.

The recorded video tape was played back and using the pause function the time of the timer and cell radius was recorded. The number of data points collected was about 20 to 30 for each cell. It should also be noted here that during the play back of the tape, measuring the cell radius was sometimes a difficult task for three reasons: 1) the cell sometimes fluctuated such that the outer membrane of the cell was no longer spherical in shape, particularly when experiments using liposomes were conducted, (note: this fluctuation tended to diminish as the temperature at which the experiment was conducted was decreased), 2) the cell outer membrane was not clearly defined on the TV monitor, and 3) the pause function for the VCR, particularly the SONY Beta machine, caused the projected image on the TV monitor to vibrate slightly. These effects

will be studied in Sections 6.2.7 and 6.3.7. It should also be noted that when experiments using lymphocytes were conducted no distinction was made between T-cells and B-cells (which could obviously lead to a variability in the results presented in this paper).

The temperature was also recorded for each experimental run by using a copper-constantan thermocouple which was placed on the top fitting. During an experimental run the temperature sometimes changed slightly, particularly if the temperature of the experiment was removed from room temperature. However, this temperature change, on average, was no more than 1.5°C (which occurred when the temperature of the experimental run was either at 10°C or 37°C).

4.6 Types of Experiments Performed

As described previously, the experimental system was set up either to do multiple experiments with different cells, at the same experimental conditions, or to use the same cell and subject it to different experimental conditions, e.g. continue to increase or decrease the extracellular concentration or temperature. Using these two basic configurations the normalized osmotically inactive volume of the cell, the cell membrane water permeability and the cell membrane water permeability activation energy could be determined.

To obtain the inactive volume of a cell, the cell was initially subjected to the isotonic solution and the radius of the cell was recorded. Then the cell was subjected to an increase in concentration and allowed to come to an equilibrium cell volume. The cell radius was again recorded for this new specified concentration. Next the original isotonic solution was replaced by another solution with an even higher concentration with which the cell had equilibrated. This procedure was repeated until the cell had undergone five increases in concentration. The inactive volume of the cell was obtained by developing a Boyle-Van't Hoff plot (see Appendix A).

To obtain the permeability of a cell type at a specified temperature, the cell was initially subjected to the isotonic solution at this specified temperature. At desired time a hypertonic solution was introduced and the radius history of the cell was recorded as mentioned in Section 4.5. The parameter characterizing the system and the measured data were entered into SENS and an estimated permeability was formulated.

To obtain the activation energy of a cell type, experiments were performed at five different temperatures. At any given temperature, five individual permeabilities were recorded and averaged to generate a mean permeability. Recall by plotting the natural logarithm of the mean permeability as a function of the inverse absolute temperature the activation energy was obtained.

CHAPTER 5

The Experimental Results and Discussion

5.1 Introduction

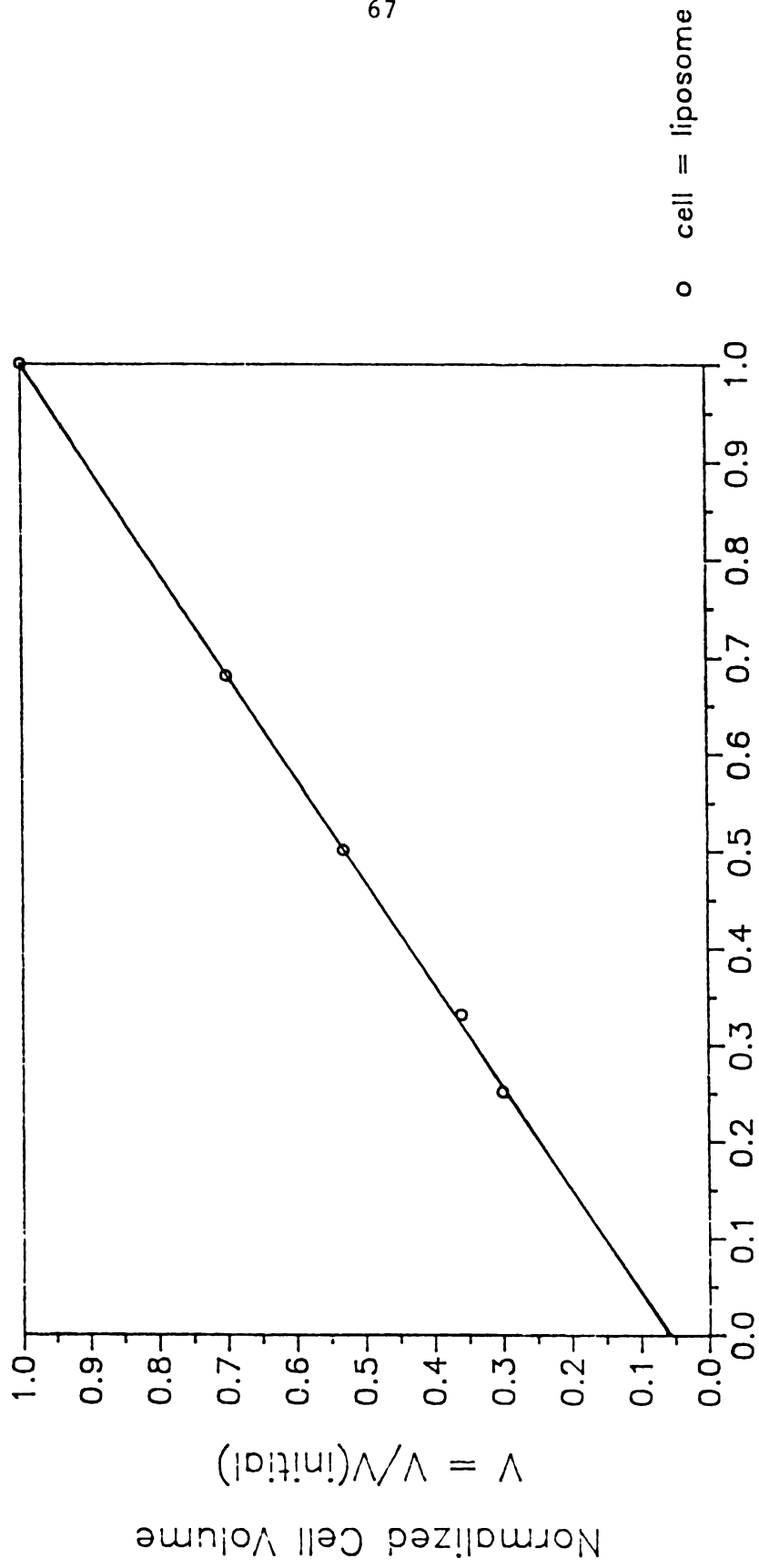
As mentioned previously, the objective of these experiments was to apply the microscope diffusion chamber to cell systems that had previously been examined by other scientists. The results obtained from the diffusion chamber would then be compared with the results of these other scientists. The specific parameters that were compared were the normalized osmotically inactive cell volume, cell membrane water permeability and cell membrane activation energy. The cells systems tested were egg-lecithin liposomes and human lymphocytes.

5.2 The Normalized Osmotically Inactive Cell Volume

The normalized osmotically inactive cell volume of egg-lecithin liposomes was not determined as a part of this work. Experiments using the diffusion chamber were performed by R. Callow [18] of the BTPL, using similar experimental conditions. The normalized osmotically inactive volume reported by Callow was 6.0%. Therefore, this was the values used to determine the liposome cell membrane permeability and activation energy, (see Figure 5.2.1 for a schematic of Callow's results).

The normalized osmotically inactive volume for human lymphocytes was determined to be $\hat{V}_b = 34.7\%$. See Figure 5.2.2 for the graphs of \hat{V}_{cell} v.s. $1/C_s$. This result is in good agreement with the inactive volumes published by Hempling [14] (32.0%) and Porsche [15] (36.9%) (see Table 5.2.1). Therefore this inactive volume (34.7%) was used to formulate the membrane permeability and activation energy for lymphocytes.

Normalized Cell Volume v.s. Normalized Inverse Concentration -
Liposome



Normalized Inverse Concentration

Figure 5.2.1

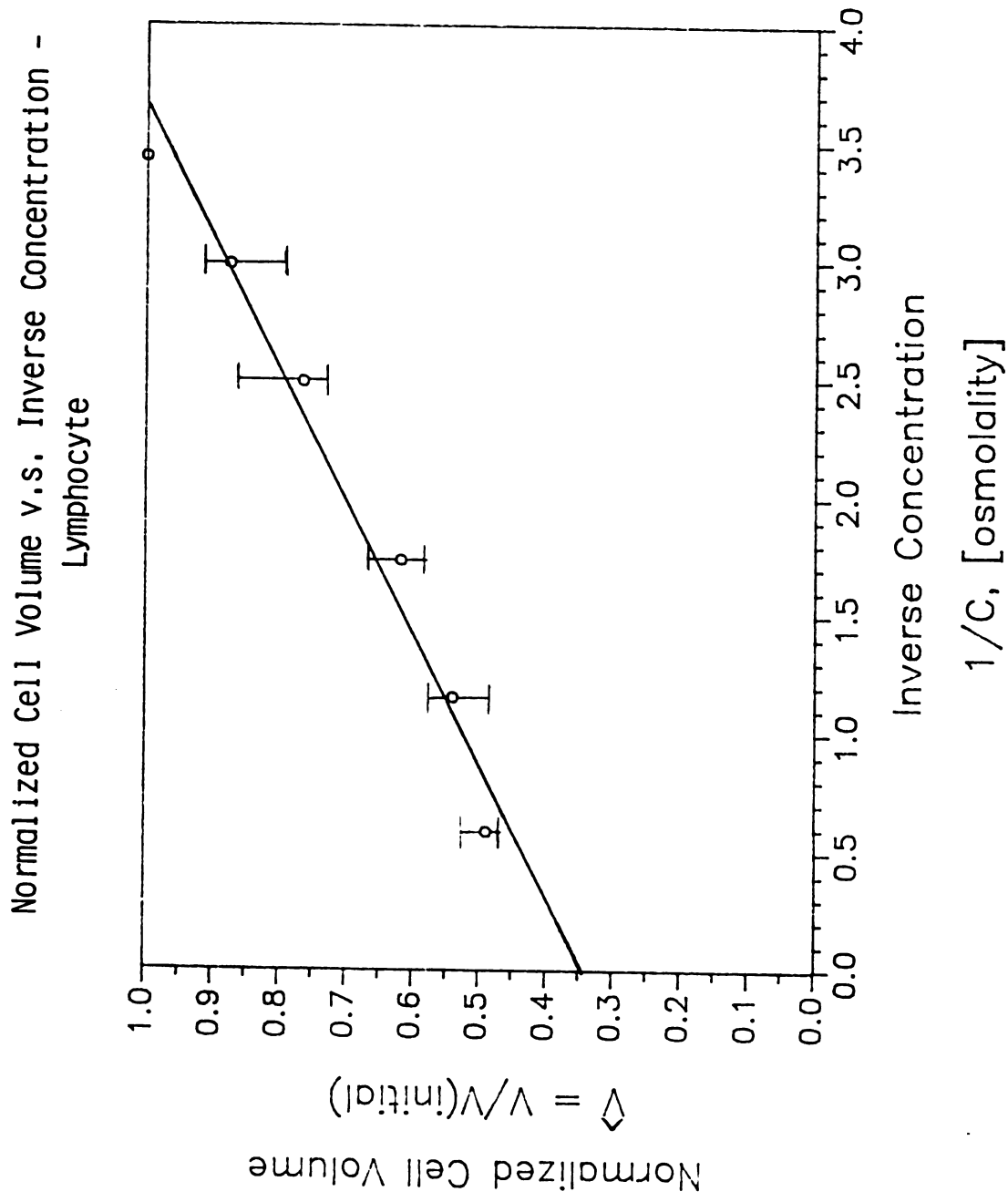


Figure 5.2.2

TABLE 5.2.1 - Normalized Osmotically Inactive Cell Volume

cell type: human lymphocyte

<u>Investigator</u>	<u>Normalized Volume (%)</u>
Hempling	32.0
Porshce	36.9
Sherban (*)	34.7

5.3 The Cell Membrane Water Permeability

The membrane water permeability was calculated for 25 individual liposome cells and 25 individual lymphocyte cells. The temperatures at which the permeability was generated were 10°C, 16°C, 25°C, 30°C and 37°C for liposomes and 10°C, 16°C, 25°C, 30°C and 35°C for lymphocytes, five at each temperature. These results are summarized in Tables 5.3.1 and 5.3.2. The mean permeability at each temperature is also recorded.

A comparison can be made between the permeability calculated at 25°C from this work and the work published by other scientists, for both liposomes and lymphocytes (see Table 5.3.3). For example, Boroske [12] reported the mean permeability (P_m) for egg-lecithin liposomes to be $41 \pm 4.9 \mu\text{m/sec}$, Callow [13] reported $P_m = 40.5 \pm 8.4 \mu\text{m/sec}$, Melkerson [13] reported $P_m = 41.0 \pm 3.1 \mu\text{m/sec}$ and Tu [7] reported $P_m = 39.0 \pm 3.3 \mu\text{m/sec}$. The mean permeability generated for this work was $40.2 \pm 6.9 \mu\text{m/sec}$. This is in excellent agreement with the mean permeability reported by the above investigators.

For the case of the lymphocyte, a similar comparison can be made. Hempling [14] reported the mean permeability at 25°C to be $10.4 \pm 0.45 \mu\text{m/sec}$, while Porshce [15] reported $P_m = 4.2 \pm 0.42 \mu\text{m/sec}$ at 25°C. The mean permeability calculated for this work was $9.3 \pm 1.9 \mu\text{m/sec}$ at 25°C. This is in good agreement with the permeability reported by Hempling. However, there seems to be a discrepancy with the resulting mean permeability reported by Porshce. By reviewing the paper published by Porshce it was discovered that she devised a method to directly measure the concentration change within the sample region of a diffusion chamber similar to the one developed by McGrath. The solute she used was sodium

chloride and the dialysis membrane had a wetted thickness of 20 μm . Her system was also similar in that there was a time delay of approximately 1 second due to the hypertonic solution front passing from the (switched) valve to the chamber. Based on the information she reported in reference [15] it was concluded that she treated the sample region (cell chamber) as a "lumped" system. The thickness the sample region during these concentration measurements was never specified. When the concentration measurements were made she discovered that the concentration-time history could be approximated by an exponential function. She calculated the time constants with and with out a dialysis membrane to be $\tau=2.08$ sec and $\tau=1.48$ sec, respectively. Therefore, she claimed the dialysis membrane only played a secondary role as it did not cause much addition to the delay and that the deviation from a step-like behavior seemed to be caused mostly by a disturbance of the concentration profile due to turbulence on its way toward the cell chamber. These results also indicated that 95% of the final concentration was reached after about 5.6 seconds, when the cell has not yet started to shrink, and 99% was reached after 8.6 seconds. In addition, she also stated that the zero time was defined when shrinkage of more that 2% was detected. However, she did realize that an under estimate of the delay time would result in an underestimate of the membrane permeability. Based on the above argument she concluded that the approximation of the measured concentration-history by a step function impose at the corrected zero time seemed therefore justified. These same experimental conditions that Porsche used were entered into SENS, (i.e. wetted dialysis membrane thickness = 20 μm , sample region thickness = 100 μm , the sodium chloride diffusivity

in free solution, $D_2 = 1.49 \times 10^{-9} \text{ m}^2/\text{sec}$ (at 25°C), the sodium chloride diffusivity in the dialysis membrane, $D_1 = 0.1 \cdot D_2$, the convective mass transfer coefficient, $H_d = 10000 \cdot D_2$, the initial concentration = .310 osmol and the final concentration = 0.478 osmol), to see what the 95% and 99% concentration-time history results would be. Note, two assumptions were made in this analysis since these parameters were not specified; specifically, the sample region thickness was estimated at $100 \text{ } \mu\text{m}$ and the concentration readings were taken at the surface of the dialysis membrane in the sample region, $LIP=5$. This analysis showed the 95% concentration reading did not occur until approximately 45 seconds, while the 99% concentration reading did not occur until approximately 85 seconds. Consequently Porsche's analysis would lead to an underestimated membrane permeability. Therefore, this is probably the cause for the discrepancy.

Note in Tables 5.3.1 and 5.3.2 two types standard deviations are recorded: 1) the individual standard deviation for a single cell at a specific temperature and 2) the standard deviation for the "population" of cells at a specified temperature. The results show that the standard deviation was less for an individual cell than for the population of cells, at a specified temperature. Therefore it can be concluded that there is a variation among the population.

Another way to look at it would be that for these cell types (liposomes and lymphocytes) a given cell will have a specific cell membrane permeability and that this membrane permeability will vary from cell to cell (at a specified temperature). This result was not anticipated for the liposome study but was not surprising for the lymphocyte study because no distinction was made between B and T cells.

Another interesting observation was the ratio of the standard deviation, both individual and population, to the resulting mean permeability. These results show this ratio for the liposomes ranged from 0.005 to 0.11 and on the average was 0.04 (for individual cells), while this ratio for the lymphocytes ranged from 0.03 to 0.10 and on the average was 0.05 (for individual cells). This ratio was higher for the population because of the variance in population (0.14 for liposomes, on the average and 0.17 for lymphocytes, on the average). There did not appear to be any apparent patterns or trends.

TABLE 5.3.1 - Permeability Results for Liposomes

solute: sucrose
concentration: 0.02 - 0.04 osmolality

Temperature (C°)	Permeability ($\mu\text{m}/\text{sec}$)	Standard Deviation (S.D.) (for an individual cell) ($\mu\text{m}/\text{sec}$)	S.D./Pm
10	25.4	2.6	0.11
10	26.5	1.6	0.07
10	22.0	0.6	0.03
10	24.2	0.5	0.02
10	21.9	0.5	0.02
16	27.7	1.7	0.06
16	32.0	0.7	0.02
16	33.2	1.0	0.03
16	30.4	1.6	0.05
16	32.2	1.6	0.05
25	39.0	0.7	0.02
25	37.2	2.4	0.06
25	38.0	1.4	0.03
25	45.9	0.2	0.005
25	41.0	1.0	0.02
30	65.6	3.7	0.06
30	62.0	4.1	0.06
30	66.0	3.4	0.05
30	64.8	2.8	0.04
30	70.3	3.0	0.05
37	92.5	2.1	0.02
37	104.2	1.9	0.02
37	95.8	8.5	0.09
37	95.8	3.9	0.04
37	94.1	3.5	0.04

TABLE 5.3.1 (cont'd.)

Average Permeability For Each Specified Temperature			
Temperature (C°)	Permeability, Pm ($\mu\text{m}/\text{sec}$)	Standard Deviation, S.D. _p (for population) ($\mu\text{m}/\text{sec}$)	S.D. _p /Pm
10	24.0	4.1	0.17
16	30.7	4.8	0.16
25	40.2	6.9	0.17
30	65.7	6.0	0.09
37	96.5	9.1	0.09

TABLE 5.3.2 - Permeability Results for Lymphocytes

solute: sodium chloride
 concentration: 0.291 - 0.725 osmolality

Temperature (C°)	Permeability ($\mu\text{m}/\text{sec}$)	Standard Deviation (S.D.) ($\mu\text{m}/\text{sec}$)	S.D./Pm
10	2.7	0.1	0.04
10	3.0	0.1	0.04
10	2.8	0.1	0.04
10	2.7	0.1	0.04
10	2.7	0.1	0.04
16	5.1	0.1	0.02
16	4.0	0.1	0.02
16	4.3	0.3	0.07
16	4.4	0.2	0.04
16	5.2	0.3	0.07
25	8.6	0.3	0.03
25	9.2	0.5	0.05
25	8.2	0.3	0.03
25	10.2	0.5	0.05
25	10.3	0.3	0.03
30	17.5	1.4	0.09
30	16.4	1.1	0.07
30	15.4	1.0	0.06
30	17.9	1.4	0.09
30	14.5	0.9	0.06
35	23.9	1.3	0.05
35	24.5	2.5	0.10
35	25.8	1.9	0.08
35	22.7	1.2	0.05
35	26.9	2.0	0.08

TABLE 5.3.2 (cont'd.)

Average Permeability For Each Specified Temperature			
Temperature (C°)	Permeability, Pm ($\mu\text{m}/\text{sec}$)	Standard Deviation, S.D. _p (for population) ($\mu\text{m}/\text{sec}$)	S.D. _p /Pm
10	2.8	0.3	0.11
16	4.6	1.1	0.24
25	9.3	1.9	0.20
30	16.3	2.8	0.17
35	24.8	3.3	0.13

TABLE 5.3.3 - Comparison of Permeability Results

cell type: egg lecithin liposomes
 temperature: 25°C
 solute: sucrose

<u>Investigator</u>	<u>Concentration (osmolality)</u>	<u>Mean Permeability ($\mu\text{m}/\text{sec}$)</u>	<u>N</u>
Boroske	0.0 - 0.04	41.1 ± 4.9	13
Callow	0.0 - 0.02	40.5 ± 8.4	23
	0.0 - 0.04		
Melkerson	0.0 - 0.04	41.0 ± 3.1	6
Tu	0.02 - 0.04	39.0 ± 3.3	9
Sherban (*)	0.02 - 0.04	40.2 ± 6.9	5

cell type: human lymphocytes
 temperature: 25°C
 solute: sodium chloride

<u>Investigator</u>	<u>Concentration (osmolality)</u>	<u>Mean Permeability ($\mu\text{m}/\text{sec}$)</u>	<u>N</u>
Hempling	0.315 - 0.600	10.4 ± 0.45	?
Porshce	0.310 - 0.478	4.2 ± 0.42	?
Sherban (*)	0.291 - 0.725	9.3 ± 1.9	5

Note: N is the number of cells used to determine the mean permeability.

5.4 The Cell Membrane Water Permeability Activation Energy

From the permeability data accumulated, the cell membrane activation energy was formulated for both egg-lecithin liposomes and human lymphocytes. Each activation energy, ΔE_a , was obtained from the slope of the lines in Figures 5.4.1 and 5.4.2. The activation energy resulting from this work, $\Delta E_a=8.9$ Kcal/mole, for egg-lecithin liposomes compared well with those published by other scientists. Specifically, Blok [16] reported 9.5 Kcal/mole, while Reeves [17] cited 8.25 Kcal/mole. In addition, the activation energy calculated from this work for human lymphocytes was 15.1 Kcal/mole. This result was in good agreement with the activation energy reported by Hempling, $\Delta E_a=14.1$ Kcal/mole. However, the activation energy reported by Porsche, $\Delta E_a=3.4$ Kcal/mole, did not compare well. She reported that her result was in good agreement with the results reported by Hempling in reference [23], i.e. the activation energy for lymphoid cells was 4.4 Kcal/mole, while the activation energy for tumor cells was 5.7 Kcal/mole. Yet, the activation energies reported by Hempling in reference [23] ranged between 13 and 18 Kcal/mole, rather than 4.4 and 5.7 Kcal/mole. Therefore it is difficult to make a comparison. These results are summarized in Table 5.4.1.

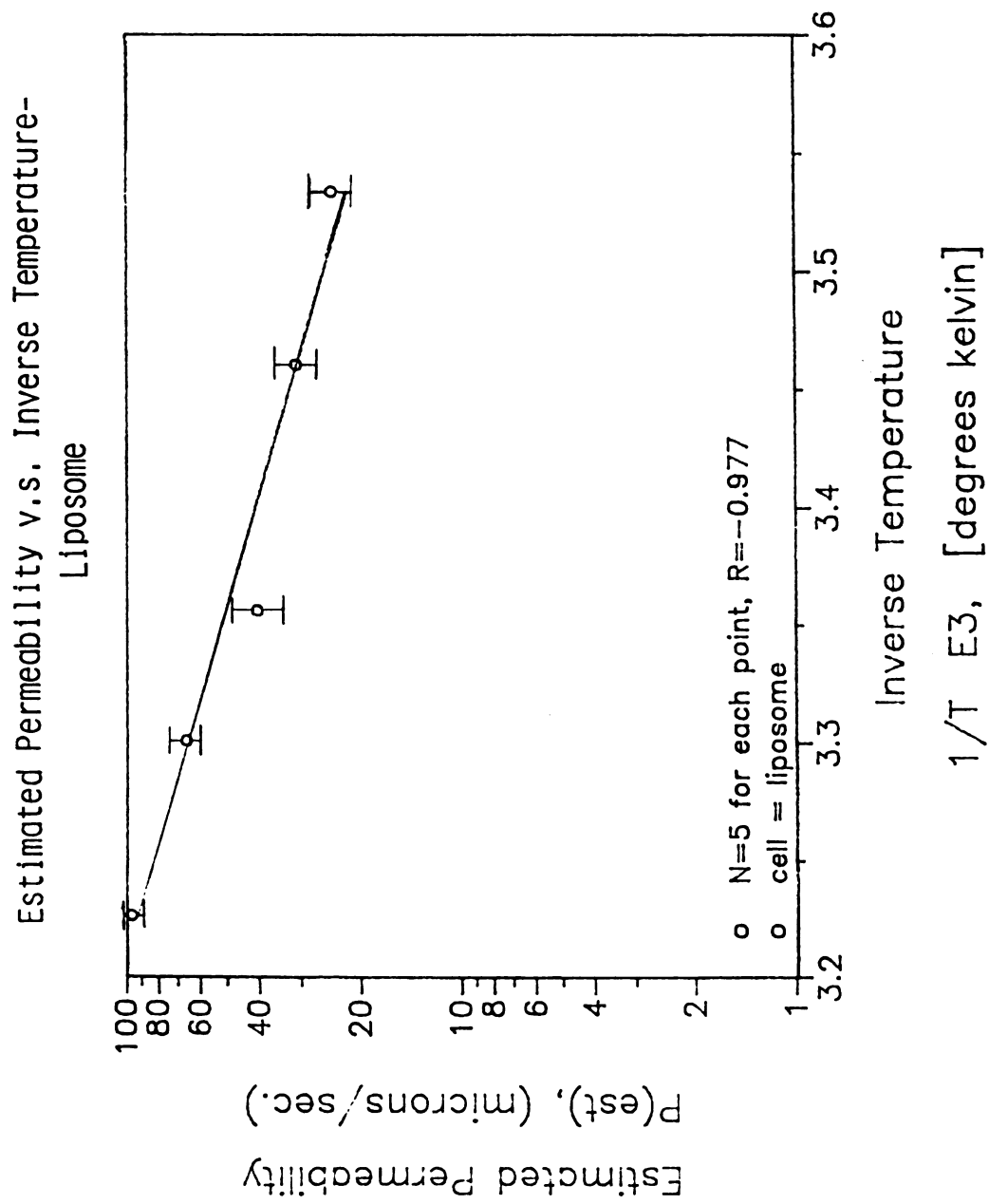


Figure 5.4.1

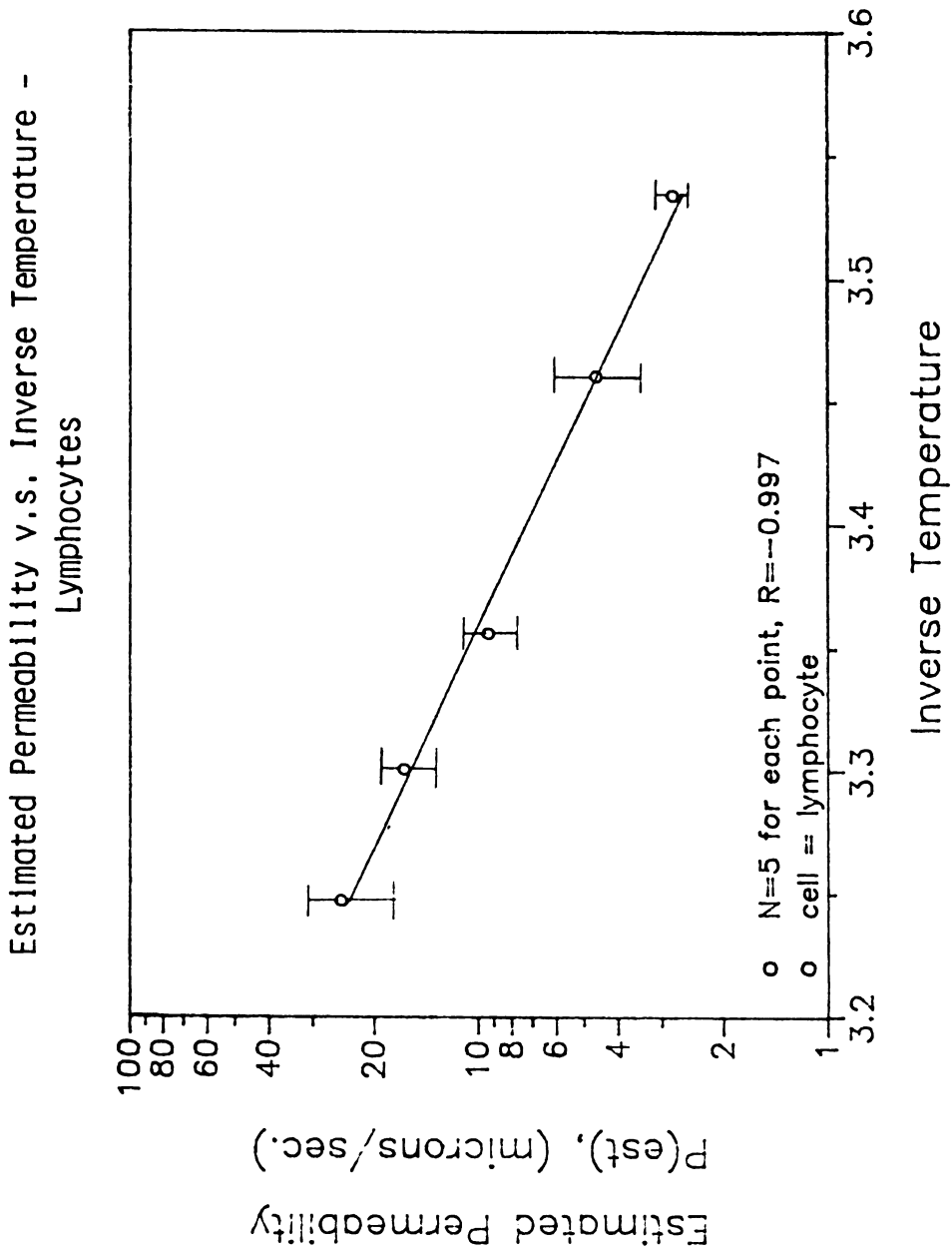


Figure 5.4.2

TABLE 5.4.1 - Activation Energy Results

cell type: egg lecithin liposomes

<u>Investigator</u>	<u>Activation Energy (kcal/mole)</u>
Blok	9.5
Reeves	8.25
Sherban (*)	8.9

cell type: human lymphocytes

<u>Investigator</u>	<u>Activation Energy (kcal/mole)</u>
Hempling	14.1
Porsche	3.4
Sherban (*)	15.1

(*) - Results from this thesis

CHAPTER 6

Sensitivity Studies

6.1 Introduction

As mention in the objective statement of this thesis (Section 1.2), the program SENS was used to study the sensitivity of the estimated parameter with respect to a change in input parameters. This can more clearly be stated by asking a key question. Specifically, what effect would an under or over specified input parameter, which describes some aspect of the experimental conditions, have on the resulting estimated permeability, standard deviation and minimum sum produced by SENS? The approach used to answer this question will be termed "sensitivity studies". Since there are an infinite number of possible experimental cases which could be studied, this discussion will be limited to two "base" cases, which are relevant to the work presented in this paper. From the study of these base cases some basic trends can be seen and some generalized statements can be made. The two cases presented here involve one for a liposome and one for a lymphocyte, both at room temperature. Also, only those input parameters that could possibly have a value different from the base case were studied. In other words, a value that was specified for an input parameter for which there was confidence (for that being the actual value) was not studied. More specifically, the wetted dialysis membrane thickness (RL1), the diffusivity of the solute in free solution (D2), the magnification factor (RMAG) and the initial and final concentrations (CINIT and CINF) were not investigated.

6.2 The Liposome Base Case

The experimental conditions which were used to describe the base case for the liposome were conditions commonly encountered in the lab when experiments were performed at room temperature, i.e. 25°C. Initially SENS was used, in the simulation mode, to generate a radius history of a liposome which had an estimated permeability of 39.9 $\mu\text{m}/\text{sec}$. The experimental conditions specified were as follows, (unless otherwise specified):

TABLE 6.2.1 - The Liposome Base Case

cell type: liposome
solute: sucrose
temperature: 25°C

<u>Variable</u>	<u>Description of Variable</u>	<u>Specified Value</u>
RL1	Wetted dialysis membrane thickness	16 μm
RL2	Sample region thickness	100 μm
LIP	Cell position in sample region	5
D2	Diffusivity of solute in free solution	$0.521 \times 10^{-9} \text{ m}^2/\text{sec}$
D1	Diffusivity of solute in dialysis membrane	$D2 \times 0.1$
Hd	Mass Transfer coefficient	$D2 \times 10000$
VINA	Normalized osmotically inactive volume	6.0%
RINIT	Initial cell radius	10 μm
DR	Imposed randomness factor	0.0 μm
RMAG	Magnification factor	1
CINIT	Initial (isotonic) concentration	0.02 osmol
CINF	Final (hypertonic) concentration	0.04 osmol
DP	Permeability step	0.1 $\mu\text{m}/\text{sec}$
DT	Time step	2.5 sec
TM0	Starting time	0.0 sec
TM1	End time	500 sec
DELAY	Time delay	0.0 sec

The resulting estimated permeability generated was $39.9 \pm 0.000 \mu\text{m}/\text{sec}$ (with a minimum sum of 0.000). This generated data was then reentered, using the (real) experimental parameter estimation mode, to yield a permeability of $39.9 \pm 0.037 \mu\text{m}/\text{sec}$ (with a minimum sum of 0.000). Note, when comparing the standard deviations there appears to be a discrepancy. However, only the first three significant figures of a calculated radius, $R_{c_i}(t)$, were stored and the rest were truncated. Therefore, when this radius history generated, in the simulation mode, reentered into SENS, in the (real) experimental parameter estimation mode, the absolute value of the difference between the simulated (pseudo) radius and the predicted radius was greater than zero.

In each of the following sections (6.2.1 through 6.2.8) an input parameter was varied (by increasing and then decreasing the value of the parameter) to investigate the effect that this variation would have on the resulting estimated permeability and standard deviation. Only one input parameter was varied at a time and no other changes were made. The resulting estimated permeability, standard deviation and minimum sum have been tabulated for each varied input parameter. In addition, the varied parameter has been plotted versus the resulting estimated permeability (for most cases) or the standard deviation.

In the last section (6.2.9) the question was asked, what would be the effect on the membrane activation energy of the liposome if the activation energy of the dialysis membrane was changed? The results are tabulated in Table 6.2.10. This is important because if the activation energy of the dialysis membrane reported by the manufacture is not

correct, it could have a dramatic effect on the results presented in this thesis. The magnitude of this difference would determine the severity.

6.2.1 The Effect of Varying D₁TABLE 6.2.2 - The Effect of Varying D₁

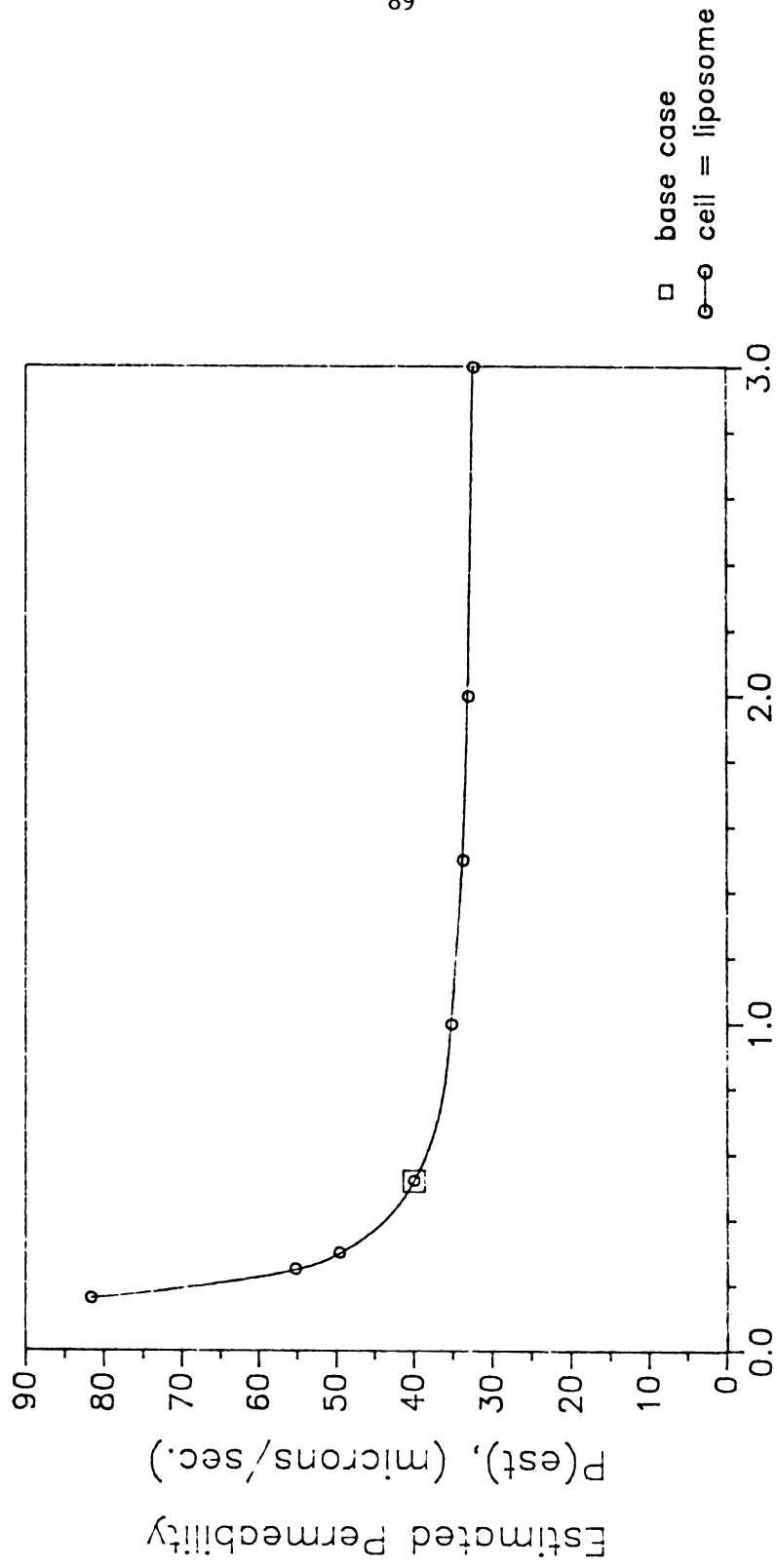
D ₁ E10 (m ² /sec)	Permeability and Standard Deviation (μm/sec)	Minimum Sum
10.0	31.3 ± 0.400	0.077
3.0	32.2 ± 0.348	0.054
2.0	32.9 ± 0.311	0.040
1.5	33.6 ± 0.274	0.029
1.0	35.1 ± 0.201	0.014
* 0.521	39.9 ± 0.037	0.000
0.3	49.5 ± 0.225	0.006
0.25	55.2 ± 0.286	0.006
0.16	81.6 ± 0.832	0.013

* - original base case

The results show (Table 6.2.2 and Figure 6.2.1) that the estimated permeability was inversely related to D₁ in a non-linear way. For example, by doubling D₁ the estimated permeability decreased approximately 10%, while increasing D₁ by a factor of 20 only decreased P(est) another 10%, (i.e a total of 20% more than the base case). However, decreasing D₁ by a factor of 2 increases P(est) by almost 40% and decreasing D₁ by a factor of 4 increase D₁ by over 200%. Therefore the value of the sucrose diffusivity in the dialysis membrane was on the border line of being critically important and not so important. That is to say that if D₁ was under estimated the resulting estimated permeability, P(est), would increase dramatically, while if D₂ was over estimated P(est) would not have a major effect. Thus it would be desirable to increase D₁ by some means. The manufacture (ENKA) has claimed that the solute diffusivity in the dialysis membrane is equivalent to the permeability of the membrane, P_{mem} times the wetted

membrane thickness, Δx , (i.e. $D_1 = P_{\text{mem}} \cdot \Delta x$). Therefore if the permeability of the membrane was increased, (possibly by making the dialysis membrane out of a more permeable substance), the effect D_1 would have on $P(\text{est})$ would be diminished. Note, the maximum value D_1 could ever be, which would not be very likely, would be the same value of the diffusivity of sucrose in free solution (in this case water) $5.21\text{E-}10 \text{ m}^2/\text{sec}$ (at 25°C).

P(est) v.s. D_1 - Liposome



D_1 E10, (meters**2/sec.)
Figure 6.2.1

6.2.2 The Effect of Varying Hd

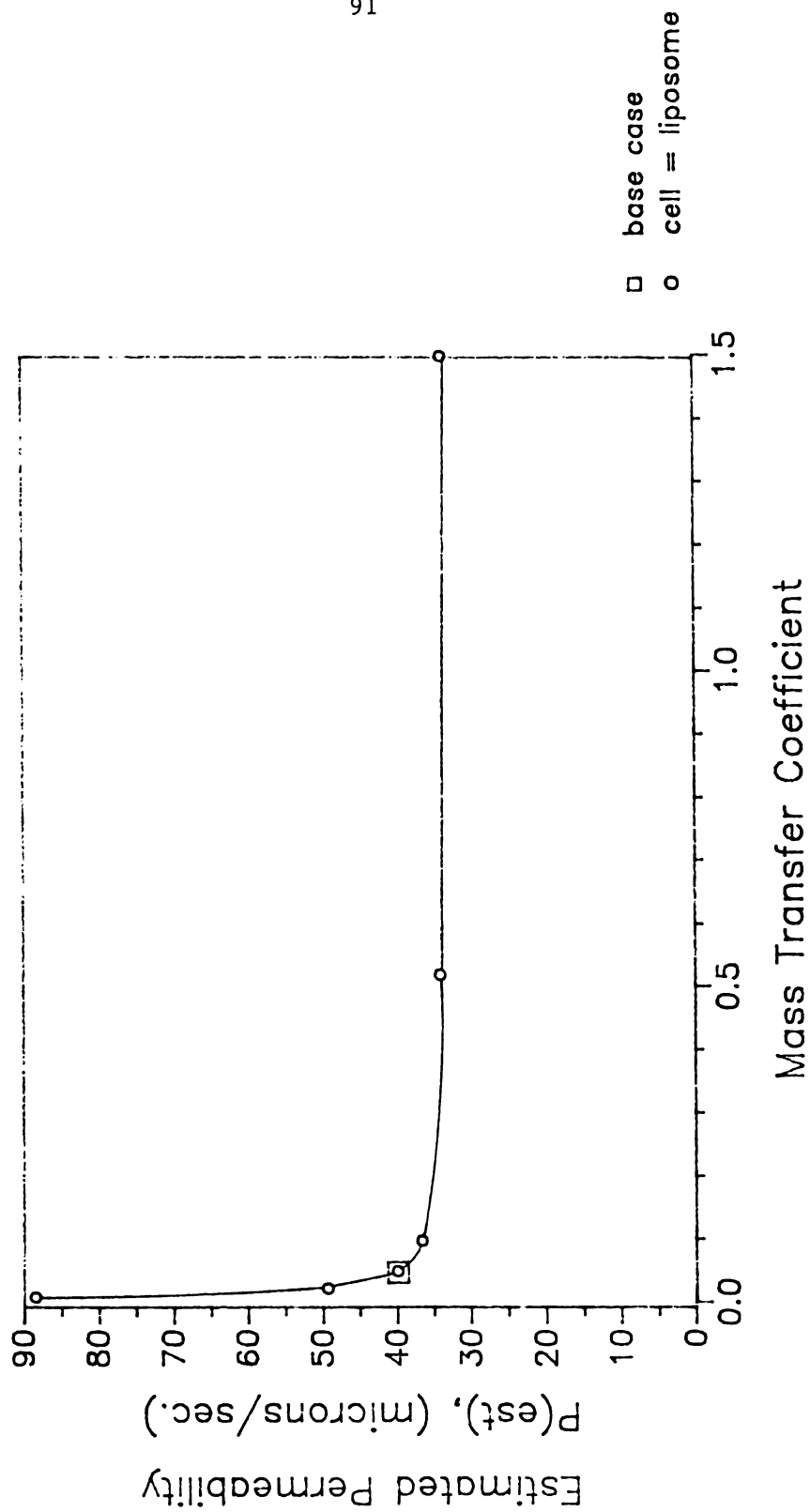
TABLE 6.2.3 - The Effect of Varying Hd

Hd E5 (m/sec)	Permeability and Standard Deviation (μ m/sec)	Minimum Sum
15.0	33.6 ± 0.272	0.029
5.21	34.0 ± 0.254	0.024
1.0	36.6 ± 0.138	0.006
* 0.521	39.9 ± 0.037	0.000
0.25	49.3 ± 0.214	0.005
0.11	88.5 ± 1.372	0.027

* - original base case

These results (Table 6.2.3 and Figure 6.2.2) show that the convective mass transfer coefficient was also inversely related to $P(\text{est})$ in a non-linear way. Similarly, when Hd was doubled, $P(\text{est})$ decreased approximately 8%, while when Hd was decreased by a factor of 2, $P(\text{est})$ increased by approximately 25%. Physically what this meant was that when Hd was decreased, the concentration boundary layer developing on the surface of the dialysis membrane, in the bulk flow region, was becoming large and visa versa, (i.e. when Hd was increased, the concentration boundary layer was becoming small). Obviously it would be more desirable to decrease the concentration boundary layer, thus minimizing the importance of correctly estimating Hd, with respect to estimating the membrane permeability. Experimental Hd can be increased by increasing the flow rate in the bulk flow region.

P(est) v.s. Hd - Liposome



Hd E4, (meters/sec.)

Figure 6.2.2

6.2.3 The Effect of Varying RL2

TABLE 6.2.4 - The Effect of Varying RL2

RL2 (μm)	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
10	28.4 ± 0.562	0.206
50	32.7 ± 0.283	0.034
75	36.1 ± 0.129	0.005
* 100	39.9 ± 0.037	0.000
150	49.0 ± 0.090	0.001
200	59.2 ± 0.699	0.028
250	68.8 ± 2.092	0.145
300	76.7 ± 4.088	0.372

* - original base case

For the above case, the relationship that exists between the sample region thickness and $P(\text{est})$ appears to be slightly non-linear (see Figure 6.2.3) and was directly proportional. At first glance one might expect that there should not be much of an effect here because the cell was at the surface of the dialysis membrane; therefore the cell should be experiencing the same increase in extracellular concentration no matter what the sample region thickness. However, the developing concentration boundary layer, at the surface of the dialysis membrane, and dialysis membrane must also be taken into account. For example, let's say the sample region thickness was small and at the beginning of an experiment the bulk flow region was flushed with a hypertonic solution, thus creating a step change in concentration in the bulk flow region. The developing concentration gradient inside the sample region would be short lived and the sample region can essentially be treated as a lumped

system. On the other hand if the sample region thickness was infinitely large, a concentration gradient would always exist; therefore the cell in the sample region, even though it's at the surface of the dialysis membrane, would never experience the final hypertonic solution concentration. Looking at Figure 6.2.3 the curve appears to almost have an S shape where the "ends" of the S will eventually approach asymptotes. These two asymptotes are the two limiting cases discussed above. In most of the experiments performed in this thesis the value of RL2 was usually between 50 and 150 microns, which, for this case, could decrease $P(\text{est})$ by 20% and increase $P(\text{est})$ by 20%, respectively. Ideally RL2 should be made as small as possible (with respect to the cell diameter) because this would decrease the concentration gradient across the sample region thus decreasing the likelihood of incorrectly estimating RL2. However, this was not an easy task to accomplish because the presoaked dialysis membrane always has some unknown amount of isotonic solution on its surface, which adds to the volume of the sample region. Note liposome position was 5 (at the surface of the dialysis membrane) for all of the above data sets.

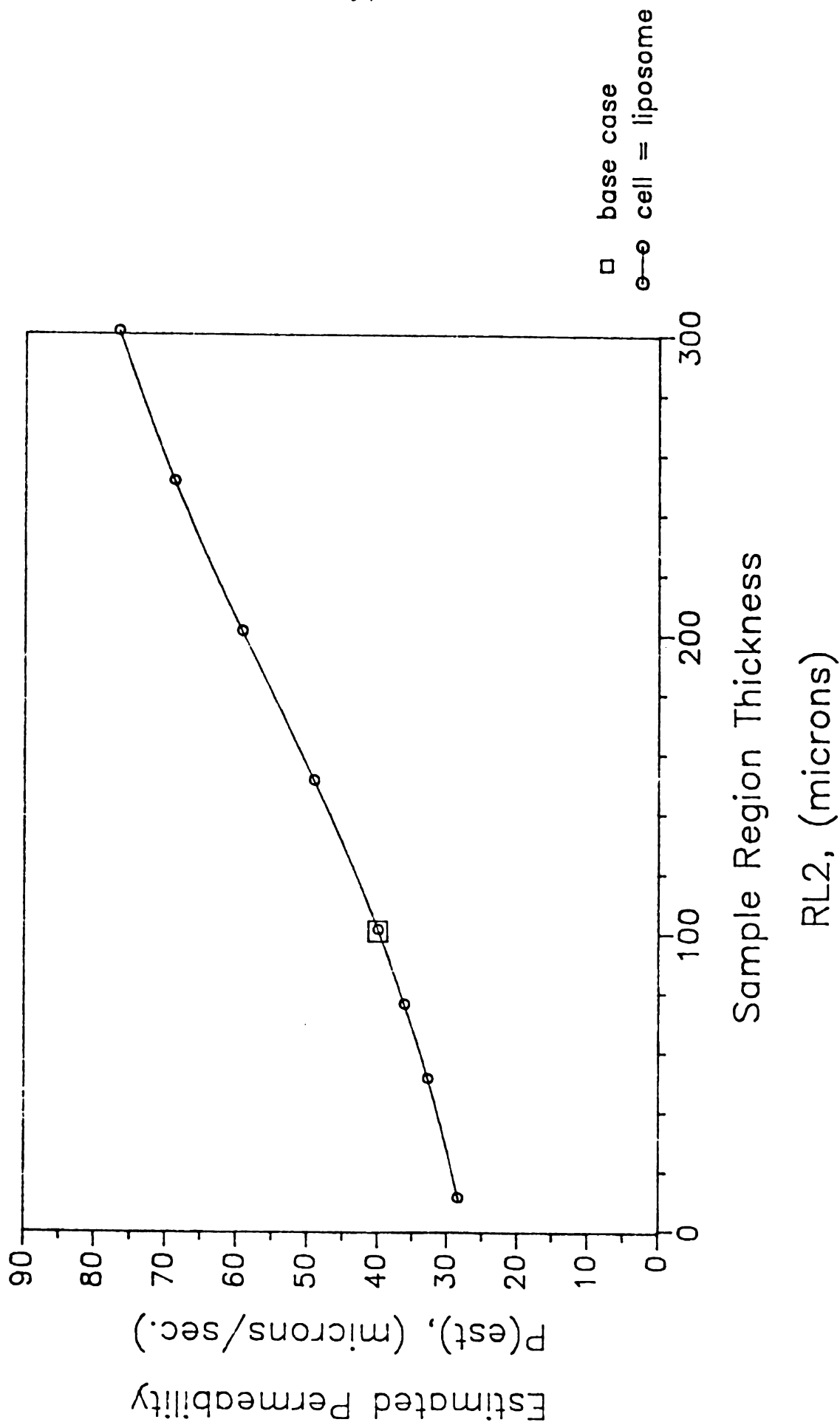


Figure 6.2.3

6.2.4 The Effect of Varying LIP

TABLE 6.2.5 - The Effect of Varying LIP

LIP	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
5	37.7 ± 0.198	0.010
6	38.6 ± 0.122	0.061
7	39.4 ± 0.061	0.001
** 8	40.1 ± 0.045	0.000
9	40.5 ± 0.072	0.001
10	40.8 ± 0.096	0.002
11	40.9 ± 0.105	0.002

** : The base case was modified here in order to have the cell position be in the middle, i.e. LIP=8, instead of 5.

The results in Table 6.2.5 show that the liposome position was directly proportional to $P(\text{est})$ via an approximate linear relationship. Clearly from this investigation of the effect of the cell position in the sample region the estimated permeability did not change significantly (see Figure 6.2.4) and would not be considered an important effect (for this case). By mistakenly perceiving the cell to be at the middle position (LIP=8) when the cell really was at the surface of the dialysis membrane or at the surface of the top cover glass only decreases $P(\text{est})$ by 6% or increases $P(\text{est})$ by 2%, respectively. Note, this trend, of RL2 not greatly effecting $P(\text{est})$, would continue if RL2 were decreased. However, if RL2 were increased LIP would play a more significant role because of the developing concentration gradient in the sample region. Therefore, this would be another good reason to keep RL2 as small as possible.

P(est) v.s. LIP - Liposome

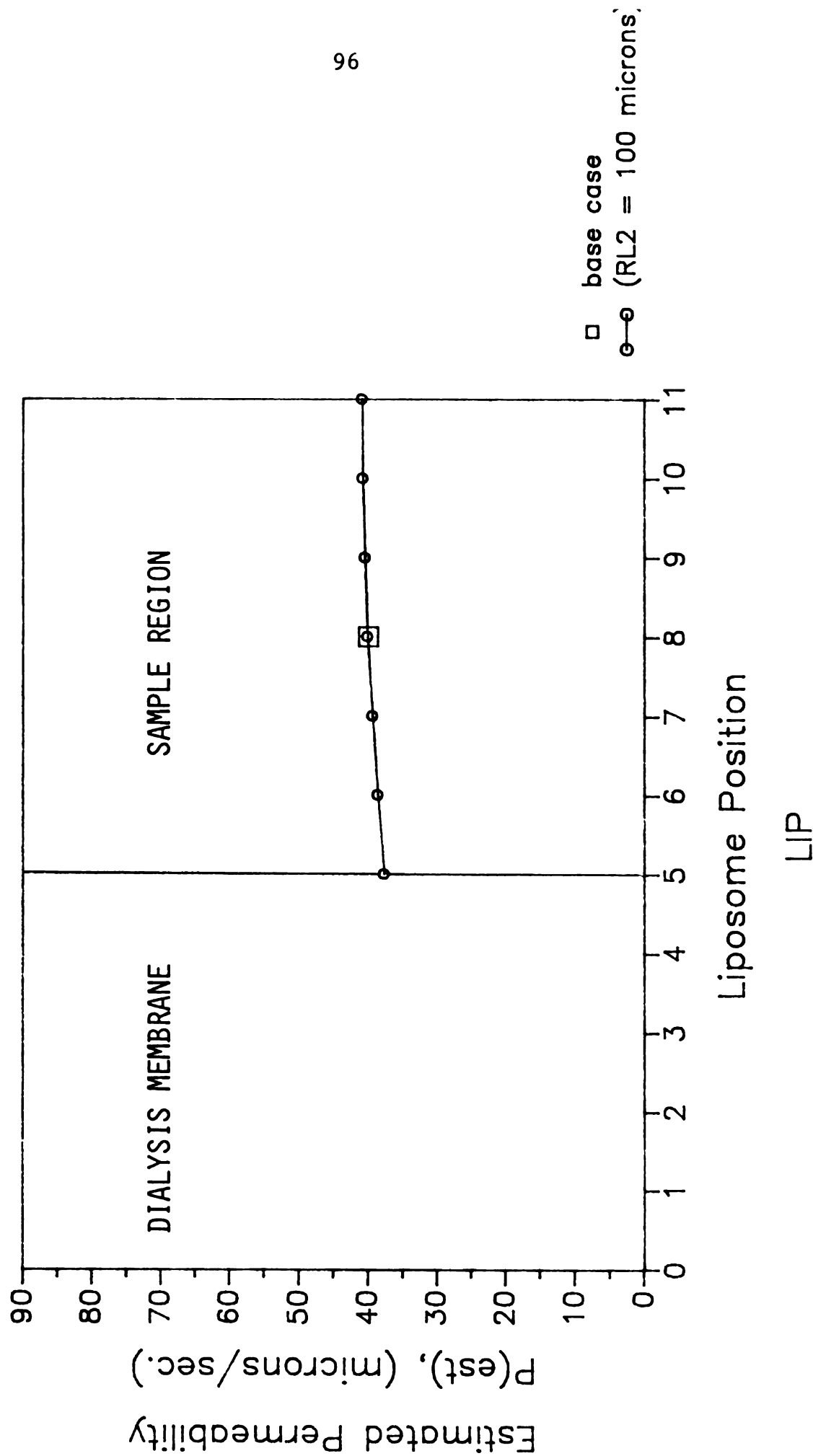


Figure 6.2.4

6.2.5 The Effect of Varying VINA

TABLE 6.2.6 - The Effect of Varying VINA

VINA (%)	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
0.0	35.7 ± 0.632	0.158
3.0	37.7 ± 0.381	0.044
* 6.0	39.9 ± 0.037	0.000
10.0	42.9 ± 0.811	0.100
15.0	46.5 ± 2.420	0.588
20.0	50.0 ± 4.930	1.472
30.0	56.5 ± 13.90	4.863

* - original base case

The results from this study show that the normalized osmotically inactive volume of a cell was directly proportional to $P(\text{est})$ in a linear fashion (see Figure 6.2.5). Decreasing VINA by a factor of 2 decreases the estimated permeability by about 5% and increasing VINA by a factor of 2 increases $P(\text{est})$ by about 13%. Therefore an inaccurate VINA only has a small to moderate effect on $P(\text{est})$.

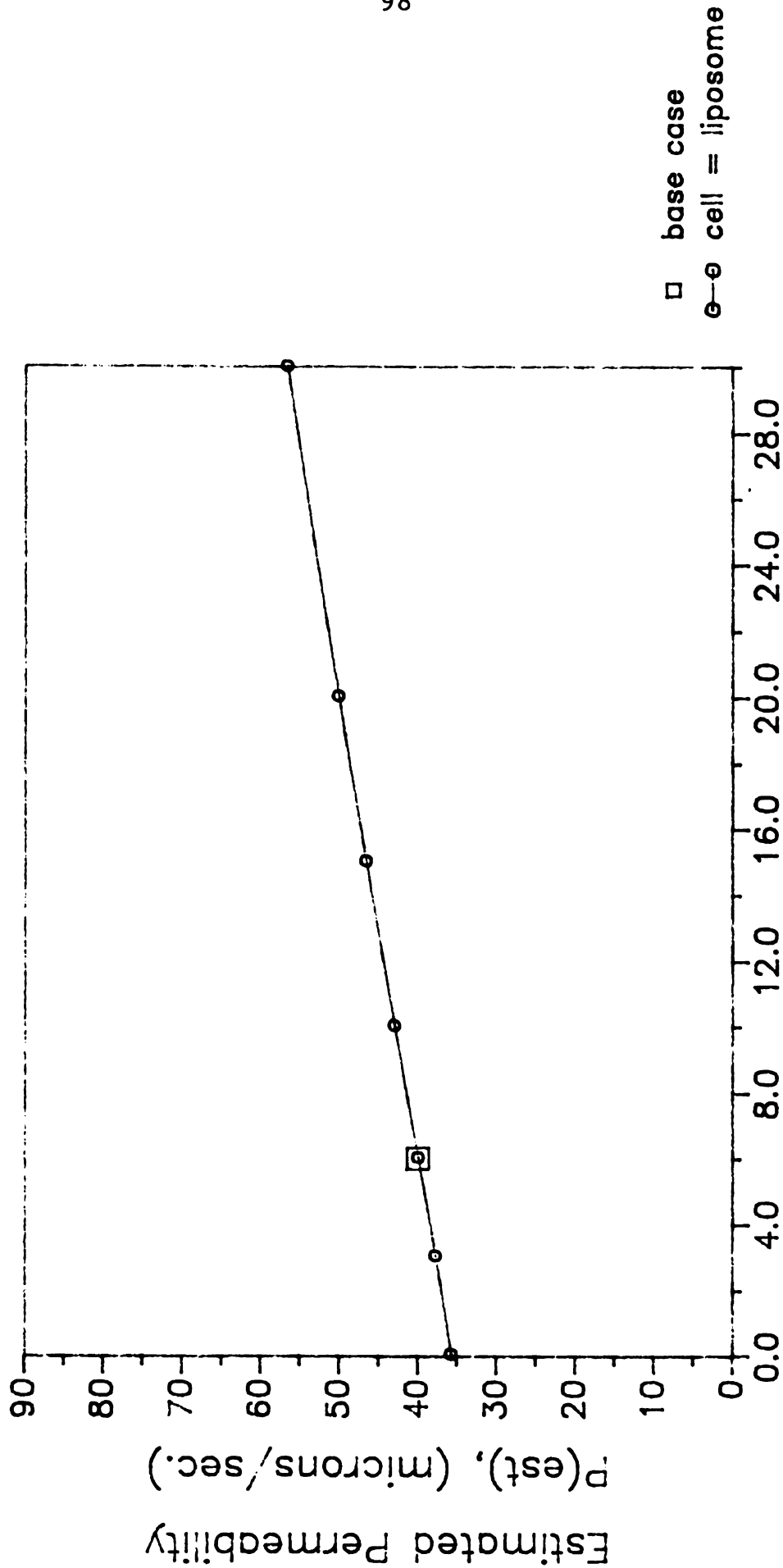


Figure 6.2.5

6.2.6 The Effect of Varying DELAY

TABLE 6.2.7 - The Effect of Varying DELAY

DELAY (sec)	Permeability and Standard Deviation ($\mu\text{m/sec}$)	Minimum Sum
0.0	38.9 ± 0.110	0.003
1.0	39.2 ± 0.080	0.002
2.0	39.6 ± 0.054	0.001
** 3.0	39.9 ± 0.037	0.000

** : The base case was modified here because during an actual experimental run there was a time delay (DELAY - defined in Section 4.5) when the hypertonic solution was started, (due to the time it took for the hypertonic solution to travel from the electronic solenoid switch valve to the bulk flow region under the dialysis membrane). Based on the volumetric flow rate of the hypertonic solution, an average time delay was calculated to be about 2.7 sec. A time delay of 3.0 sec. was chosen for the new base case to allow for a little extract delay in case the flow rate decreased.

The results from this study show the DELAY was directly and nearly linearly related to $P(\text{est})$. By not accounting for a time delay when the data was recorded $P(\text{est})$ would only be underestimated approximately 3%. Therefore, relationship that exists between the time delay and $P(\text{est})$ does appear to be critically important (for this case) because the slope of the line in Figure 6.2.6 is very small.

P(est) v.s. DELAY - Liposome

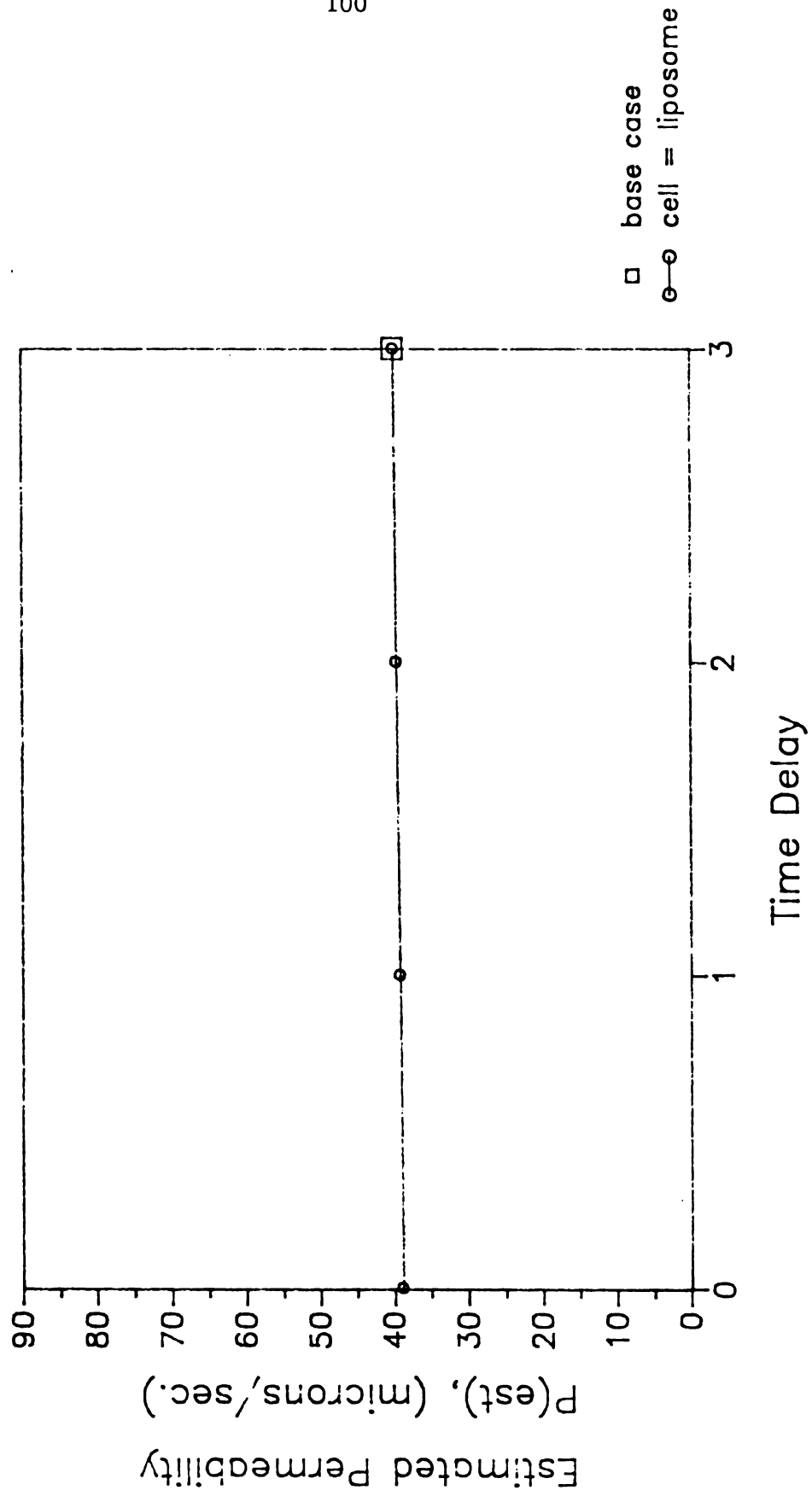


Figure 6.2.6

6.2.7 The Effect of Varying DR

TABLE 6.2.8 - The Effect of Varying DR

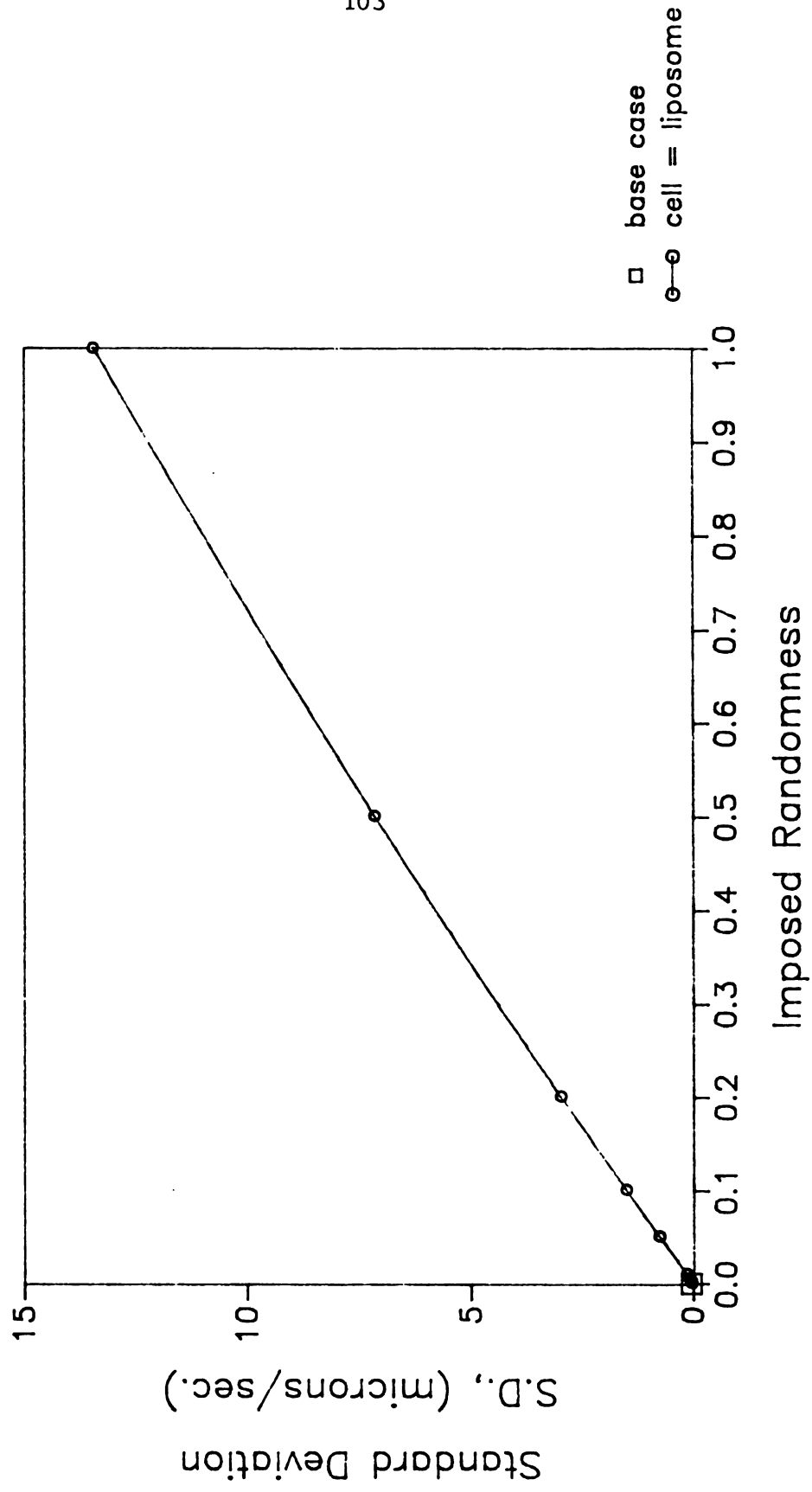
	DR (μm)	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
*	0.000	39.9 ± 0.037	0.000
	0.001	40.0 ± 0.040	0.000
	0.005	40.0 ± 0.083	0.002
	0.01	39.8 ± 0.152	0.005
	0.05	39.8 ± 0.768	0.134
	0.1	39.6 ± 1.513	0.524
	0.2	39.2 ± 2.983	2.105
	0.5	38.0 ± 7.144	13.260
	1.00	36.5 ± 13.43	52.895

* - original base case

The results from this study show that $P(\text{est})$ was not greatly effected by DR, while the standard deviation increased linearly as DR increased (see Figure 6.2.7). Recall from Figure 3.2.1, p.31 that DR was defined to be the radius randomness factor. DR was implemented into SENS to impose a (pseudo) randomness factor on the generated radius history of a cell. This randomness factor was meant to incorporate the uncertainties mentioned in Section 4.5, (i.e. the fluctuations of the outer membrane of the cell and/or measurement errors that may have occurred. An attempt was made to estimate the maximum magnitude of this inaccuracy. Based on the TV monitor screen size, the video camera used and the lens in the microscope the cell was magnified 5080 times. The uncertainty in measuring the cell radius was estimate by approximating the range the cell radius could be. For example, a cell with a $20 \mu\text{m}$ diameter would measure 10.16 cm in the TV monitor. Based upon the

apparent thickness of the membrane projected on the screen and the "steadiness" of the cell on the screen, which vibrated slightly on the screen when the pause function was used, the uncertainty was approximated to be ± 0.1 cm which corresponds to $0.1 \mu\text{m}$ uncertainty in the cell radius.

S.D. v.s. DR - Liposome



DR, (microns)

Figure 6.2.7

6.2.8 The Effect of the Number of Data Points

TABLE 6.2.9 - The Effect of the Number of Data Points

# of points	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
4	51.4 ± 2.85	0.006
6	49.4 ± 5.63	0.064
10	46.6 ± 3.74	0.088
15	42.4 ± 3.25	0.242
20	40.0 ± 2.48	0.305
25	39.3 ± 2.06	0.350
30	39.2 ± 1.77	0.375
35	39.3 ± 1.65	0.422
40	39.4 ± 1.57	0.527
45	39.4 ± 1.45	0.570
50	39.5 ± 1.38	0.644
100	39.6 ± 0.93	1.151

Note: All of the input parameters used for this case were the same as described for the base case except DR was set at $0.1 \mu\text{m}$. The rationale for using $0.1 \mu\text{m}$ for DR was described in Section 6.2.7, (i.e. this was the best estimate for the uncertainty when the cell radius measured). If DR was kept at $0.0 \mu\text{m}$ the result would always be $P(\text{est}) = 39.9 \mu\text{m}/\text{sec}$, S.D. = $0.0 \mu\text{m}/\text{sec}$ and the SUMIN = 0.000. It should also be noted that the data points used for each of the above cases were equally spaced within the 0 - 500 sec time interval.

The above results appear to show that the number of data points, used to generate a $P(\text{est})$, was related to the estimated permeability in a non-linear way. The estimated permeability started at $51.4 \mu\text{m}/\text{sec}$ and decreased until the number of data points was approximately 30, where $P(\text{est})$ appears to level off around $39.5 \mu\text{m}/\text{sec}$ (see Figure 6.2.8). Intuitively one would think that $P(\text{est})$ would oscillate about $39.9 \mu\text{m}/\text{sec}$ when only a few data points were used and then level off, at approximately $39.9 \mu\text{m}/\text{sec}$, as the number of points was increased. It

should also be noted that it did not take very many points to get a reasonably good estimate for the membrane permeability - approximately 15 points or so. Also, recall from Section 4.5 that the number of data points recorded for each experiment conducted was about 20 - 30.

The above results also show that the standard deviation was inversely related to the number of points, with the exception of the case for the number of points equal to 4. When the standard deviation was plotted as a function of the inverse square root of the number of points the relationship was approximately linear, (if the case for the number of points equal to 4 was ignored), (see Figure 6.2.9). This was expected based on the relationship between the number of data points and the standard deviation given by equation (2.3.10).

Finally the number of data points was found to be related to the minimum sum in an increasingly linear manner (see Figure 6.2.10). This was also anticipated based on the relationship described in equation (2.3.3).

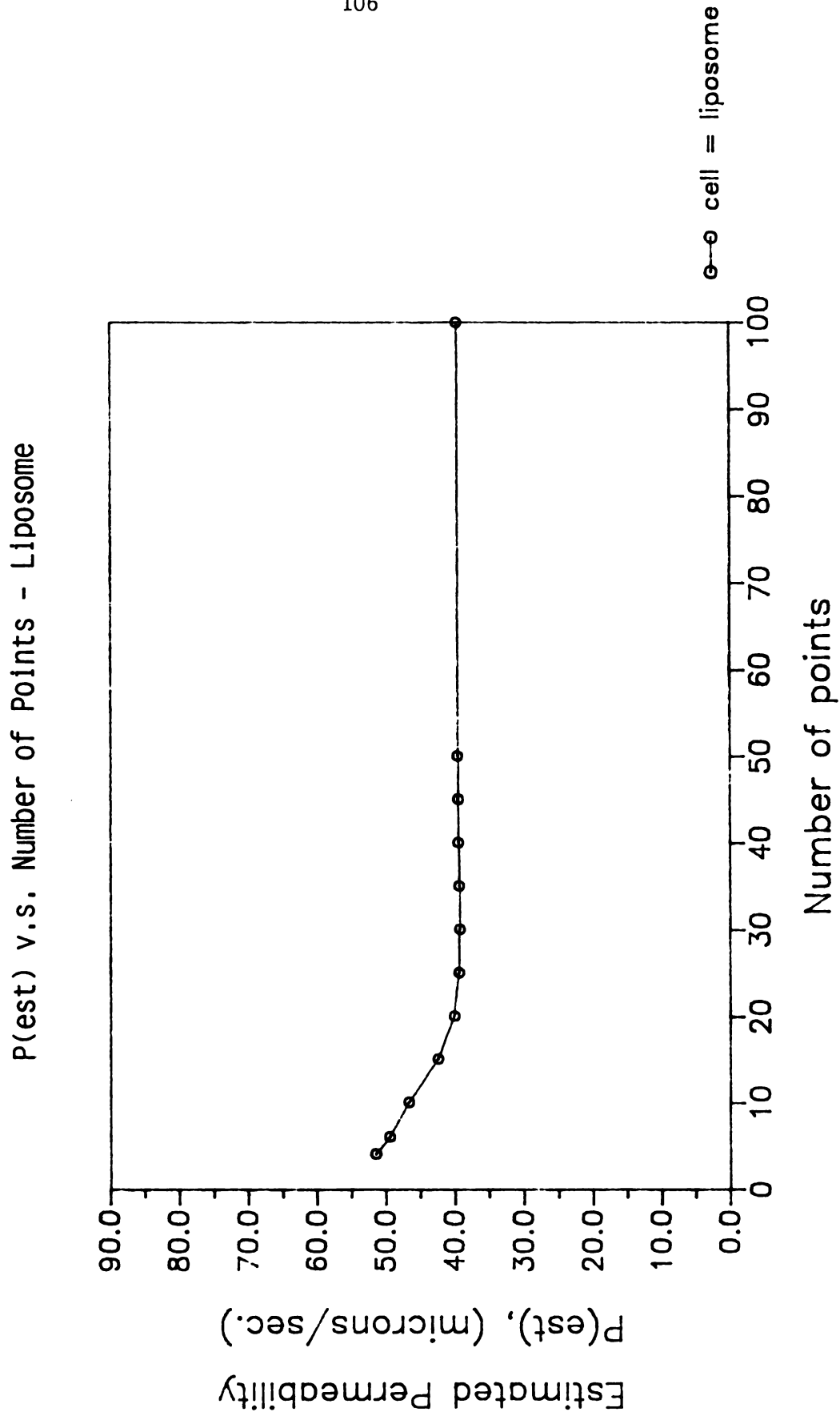


Figure 6.2.8

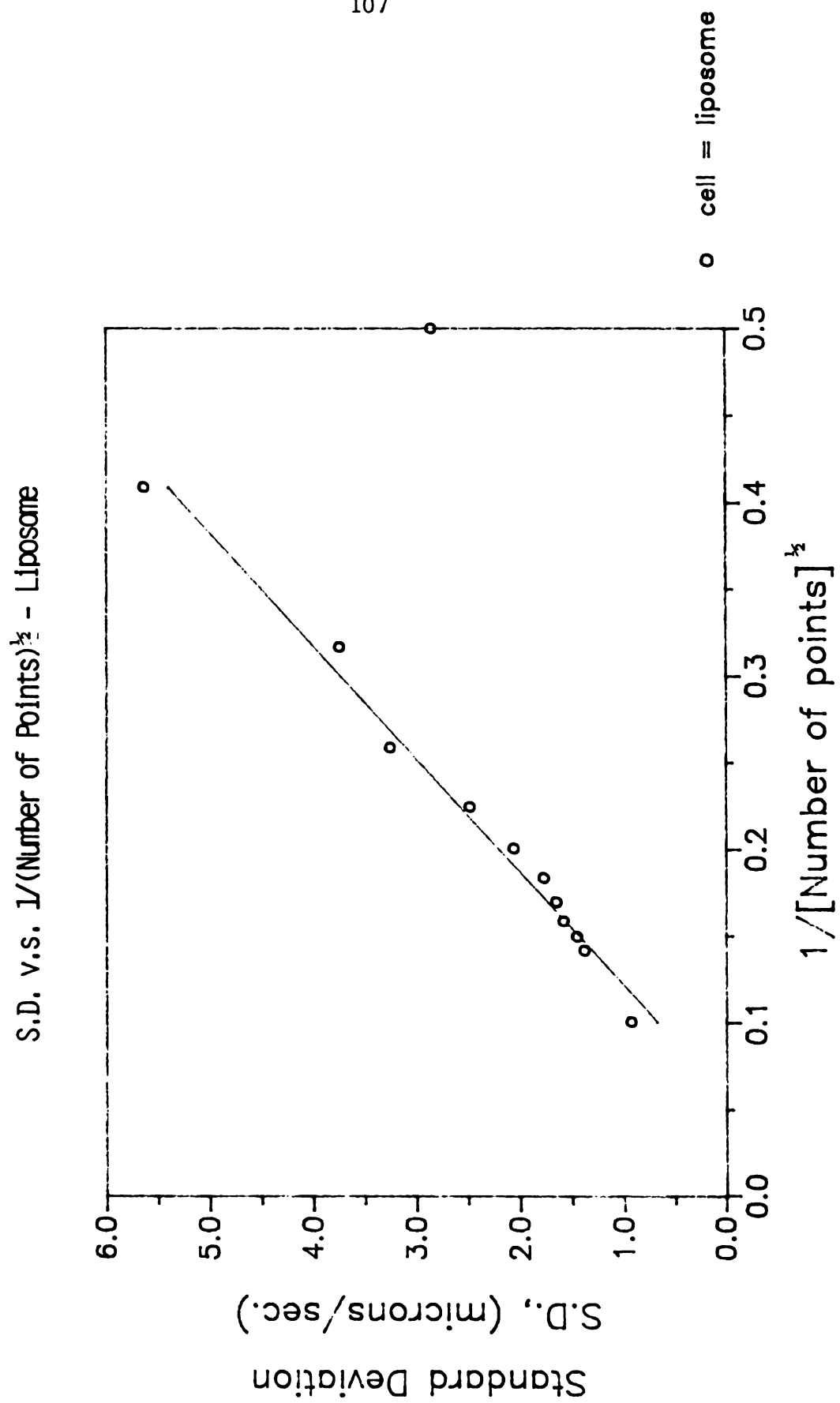


Figure 6.2.9

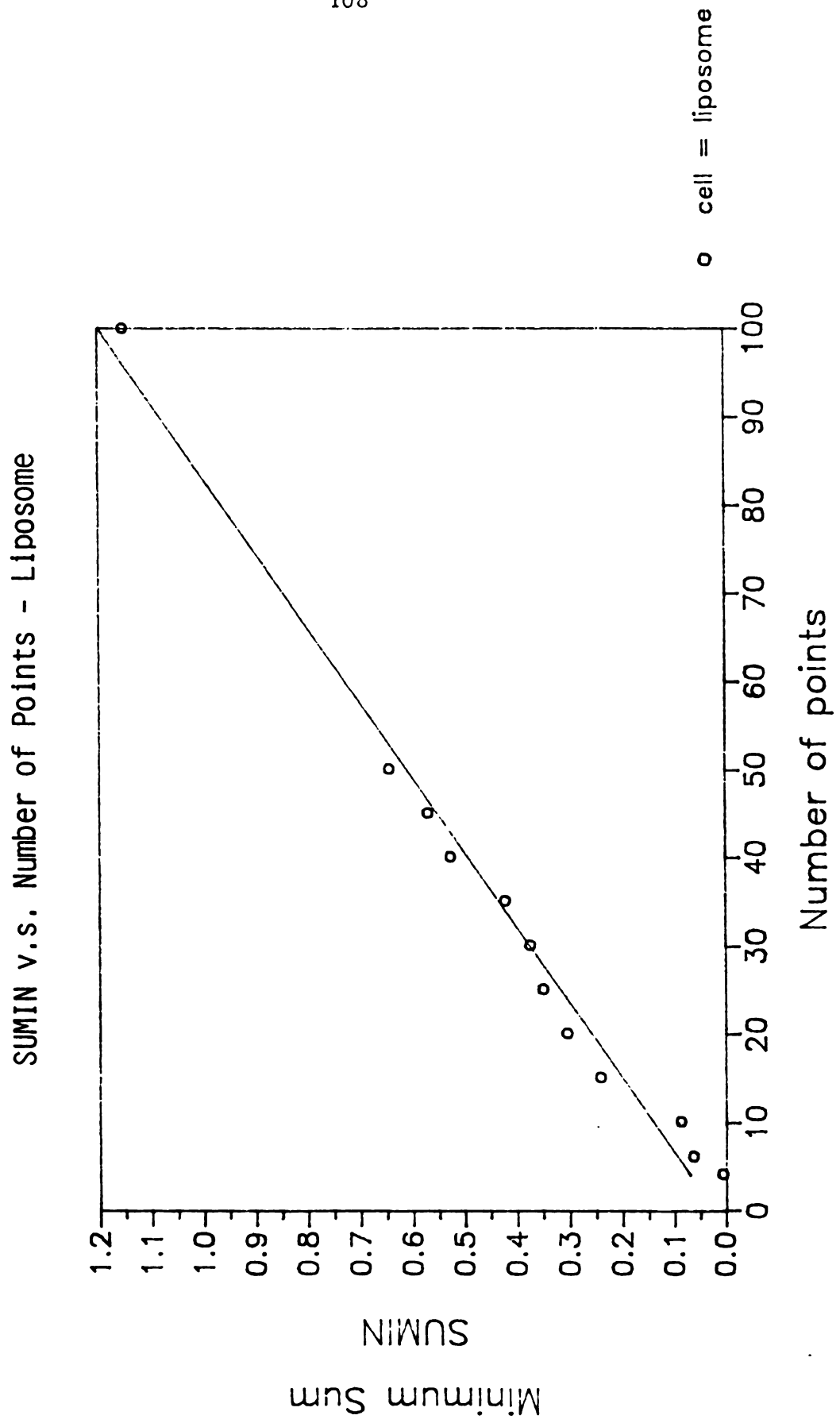


Figure 6.2.10

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6.2.9 The Effect of Varying E_a of the Dialysis Membrane on the E_a of the Cell

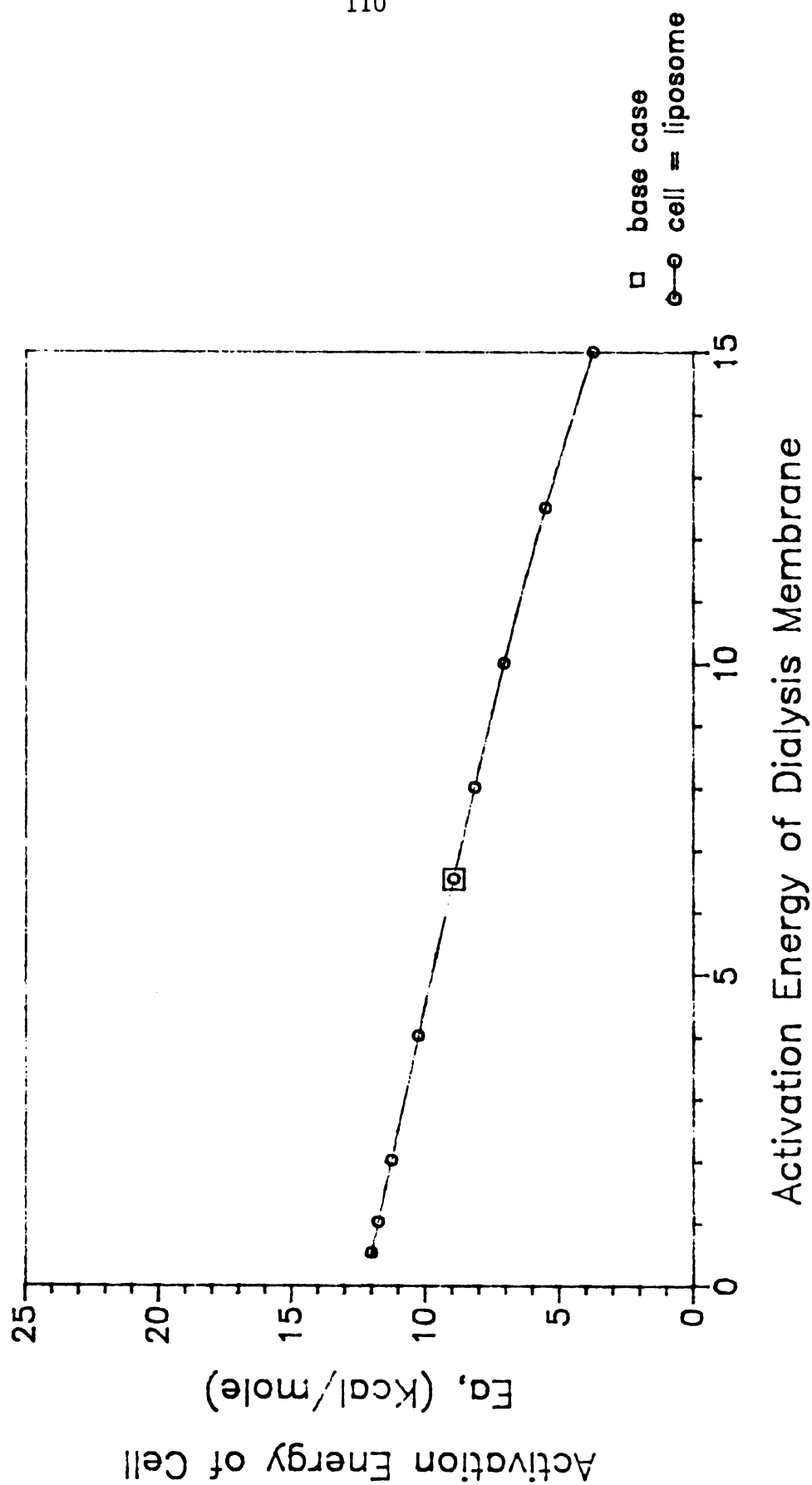
TABLE 6.2.10 - The Effect of Varying E_a of the Dialysis Membrane on the E_a of the Cell

<u>E_a, Dialysis Membrane (Kcal/mole)</u>	<u>E_a, Liposome Membrane (Kcal/mole)</u>
0.5	12.0
1.0	11.7
2.0	11.2
4.0	10.2
* 6.53	8.9
8.0	8.1
10.0	7.0
12.5	5.5
15.0	3.7

* - original base case

This investigation shows that the relationship between the two membrane activation energies was slightly non-linear and inversely proportional (see Figure 6.2.11). What this study suggested was that if the manufacturer incorrectly stated the temperature effects, i.e. the activation energy, with respect to the dialysis membrane, then the activation energy reported in this work for the liposome would have to be reevaluated. However, this is not likely but it is possible. The original base case dialysis membrane E_a was 6.53 Kcal/mole. This data was obtained from the manufacture (ENKA) and was published in reference [3].

$E_a(\text{Cell})$ v.s. $E_a(\text{Dialysis Membrane})$ - Liposome



E_a , (Kcal/mole)

Figure 6.2.11

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6.3 The Lymphocyte Base Case

The experimental conditions used for the lymphocyte base case are shown below in Table 6.3.1. The conditions specified were also commonly encountered conditions when experiments were performed using lymphocytes at 25°C. Again, SENS was used in the simulation mode to generate a radius history for a cell with an estimated permeability of 9.3 $\mu\text{m}/\text{sec}$.

TABLE 6.3.1 - The Lymphocyte Base Case

cell type: lymphocyte
solute: sodium chloride
temperature: 25°C

<u>Variable</u>	<u>Description of Variable</u>	<u>Specified Value</u>
RL1	Wetted dialysis membrane thickness	16 μm
RL2	Sample region thickness	100 μm
LIP	Cell position in sample region	5
D2	Diffusivity of solute in free solution	$1.483 \times 10^{-9} \text{ m}^2/\text{sec}$
D1	Diffusivity of solute in dialysis membrane	$D2 \times 0.1$
Hd	Mass Transfer coefficient	$D2 \times 10000$
VINA	Normalized osmotically inactive volume	34.7%
RINIT	Initial cell radius	5.5 μm
DR	Imposed randomness factor	0.0 μm
RMAG	Magnification factor	1
CINIT	Initial (isotonic) concentration	0.291 osmol
CINF	Final (hypertonic) concentration	0.725 osmol
DP	Permeability step	0.1 $\mu\text{m}/\text{sec}$
DT	Time step	1.0 sec
TMO	Starting time	0.0 sec
TM1	End time	100 sec
DELAY	Time delay	0.0 sec

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When these parameters and generated radius history data were reentered into SENS, in the (real) experimental parameter estimation mode, the resulting permeability was $9.3 \pm 0.042 \mu\text{m/sec}$ (with a minimum sum of 0.000).

The approach used to investigate the input parameter of interest was the same approach as described for the liposome base case in Sections 6.2.1 through 6.2.9, (i.e. only the input parameter of interest was varied and any deviation from this approach was specifically stated). The results were also tabulated and graphs were produced where appropriate.

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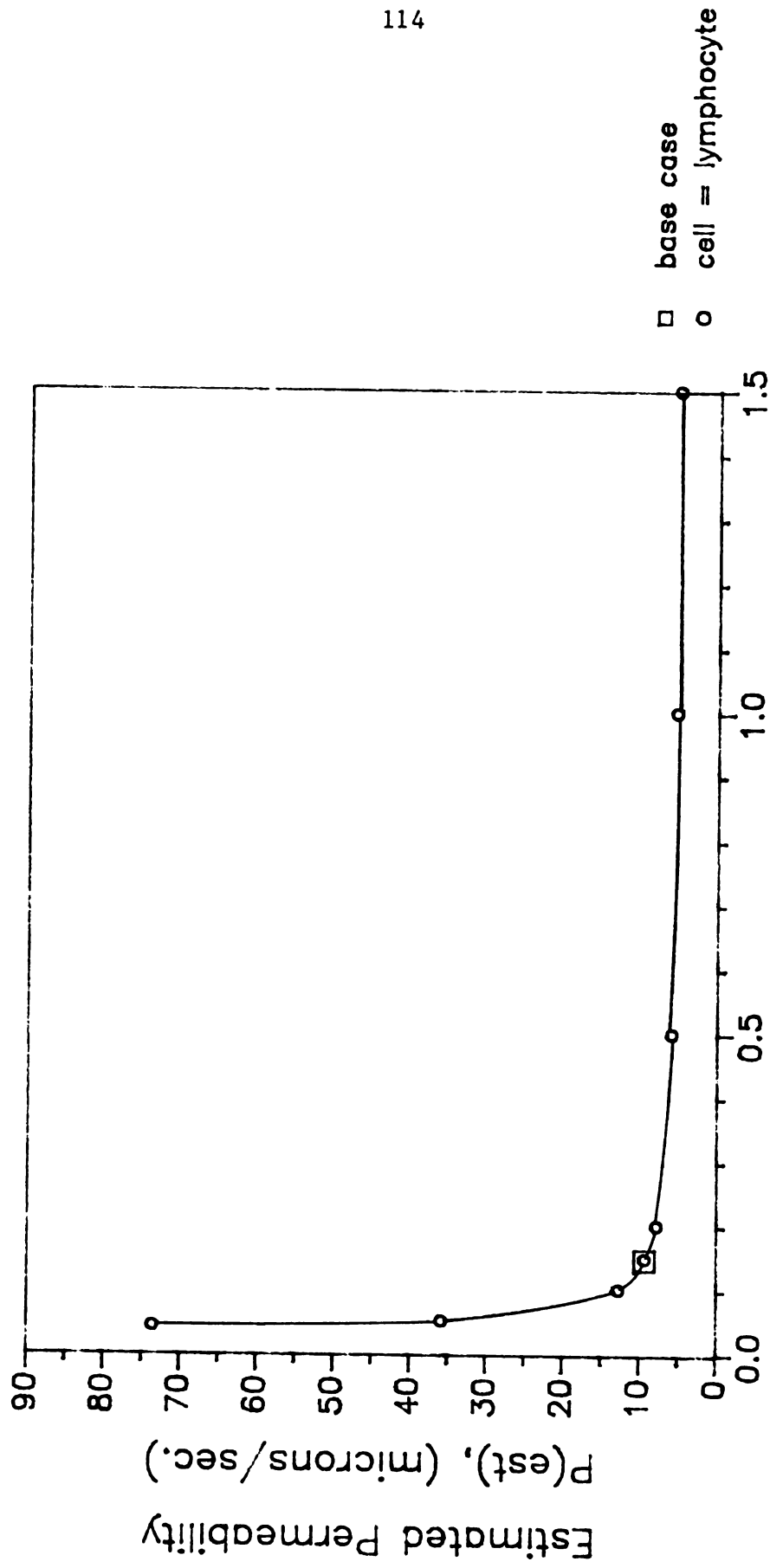
6.3.1 The Effect of Varying D₁TABLE 6.3.1 - The Effect of Varying D₁

D ₁ E9 (m ² /sec)	Permeability and Standard Deviation (μm/sec)	Minimum Sum
1.5	5.2 ± 0.055	0.002
1.0	5.4 ± 0.060	0.002
0.5	5.9 ± 0.070	0.002
0.2	7.8 ± 0.068	0.001
* 0.148	9.3 ± 0.042	0.000
0.1	12.7 ± 0.348	0.004
0.05	35.8 ± 11.38	0.106
0.04	73.5 ± 63.06	0.211

* - original base case

The results show that the estimated permeability was inversely related to D₁ in a non-linear way (see Figure 6.3.1). When D₁ was doubled P(est) decreased approximately 30%, while when D₁ was increased by a factor of 10 P(est) only decreased another 14%. When the value of D₁ was half the base case the estimated permeability increased approximately 250%. Therefore, a similar conclusion that was made in 6.2.1 can be made here also, i.e. the value used for D₁ was on the border line of being critically important. Also the goal here would be to either increase the dialysis membrane permeability, thus diminishing the effect D₁ has on P(est). The maximum value D₁ could have would be the same for the sodium chloride diffusivity in water, 1.48E-9 m²/sec (at 25°C), however this would not be very realistic.

P(est) v.s. D_1 - Lymphocyte



Diffusivity of Sodium Chloride
in Dialysis Membrane

$D_1 E_9$, (meters²/sec.)
Figure 6.3.1

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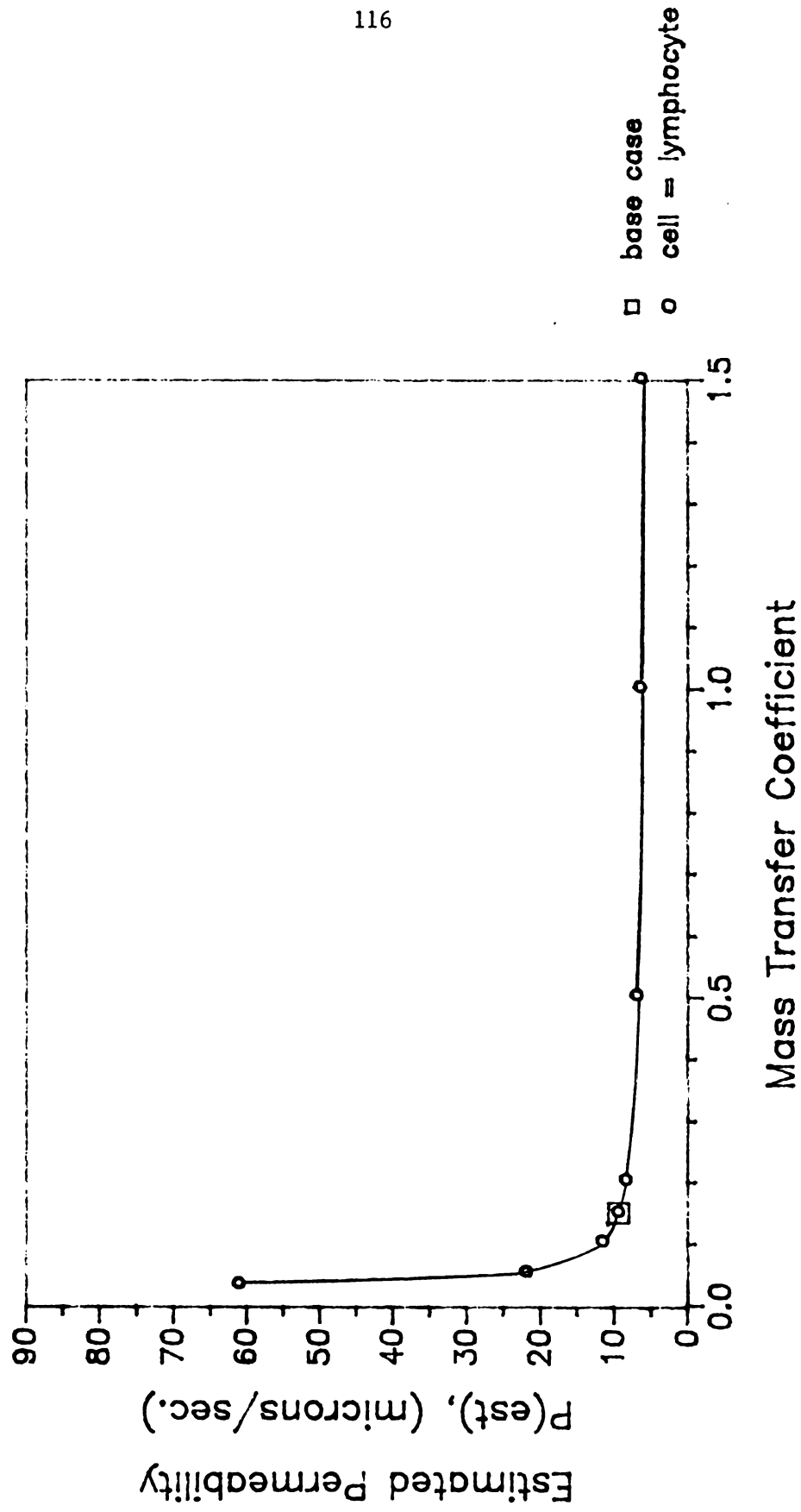
6.3.2 The Effect of Varying H_d TABLE 6.3.2 - The Effect of Varying H_d

H_d E4 (m/sec)	Permeability and Standard Deviation (μ m/sec)	Minimum Sum
1.5	6.3 ± 0.075	0.002
1.0	6.4 ± 0.076	0.002
0.5	6.8 ± 0.078	0.002
0.2	8.3 ± 0.060	0.001
* 0.148	9.3 ± 0.042	0.000
0.1	11.4 ± 0.192	0.002
0.05	21.8 ± 2.920	0.044
0.03	61.0 ± 43.80	0.205

* - original base case

The result from this study show that the estimated permeability was inversely related to the mass transfer coefficient in a non-linear manner also (see Figure 6.3.2). For example, increasing H_d by a factor of 2 decreased $P(\text{est})$ 15%, while decreasing H_d by a factor of 2 increased $P(\text{est})$ 194%. Again, as was mentioned Section 6.2.2, to minimize the importance of accurately estimating H_d by increasing the bulk flow rate.

P(est) v.s. Hd - Lymphocyte



Hd E4, (meters/sec.)

Figure 6.3.2

6 . 3.3 The Effect of Varying RL2

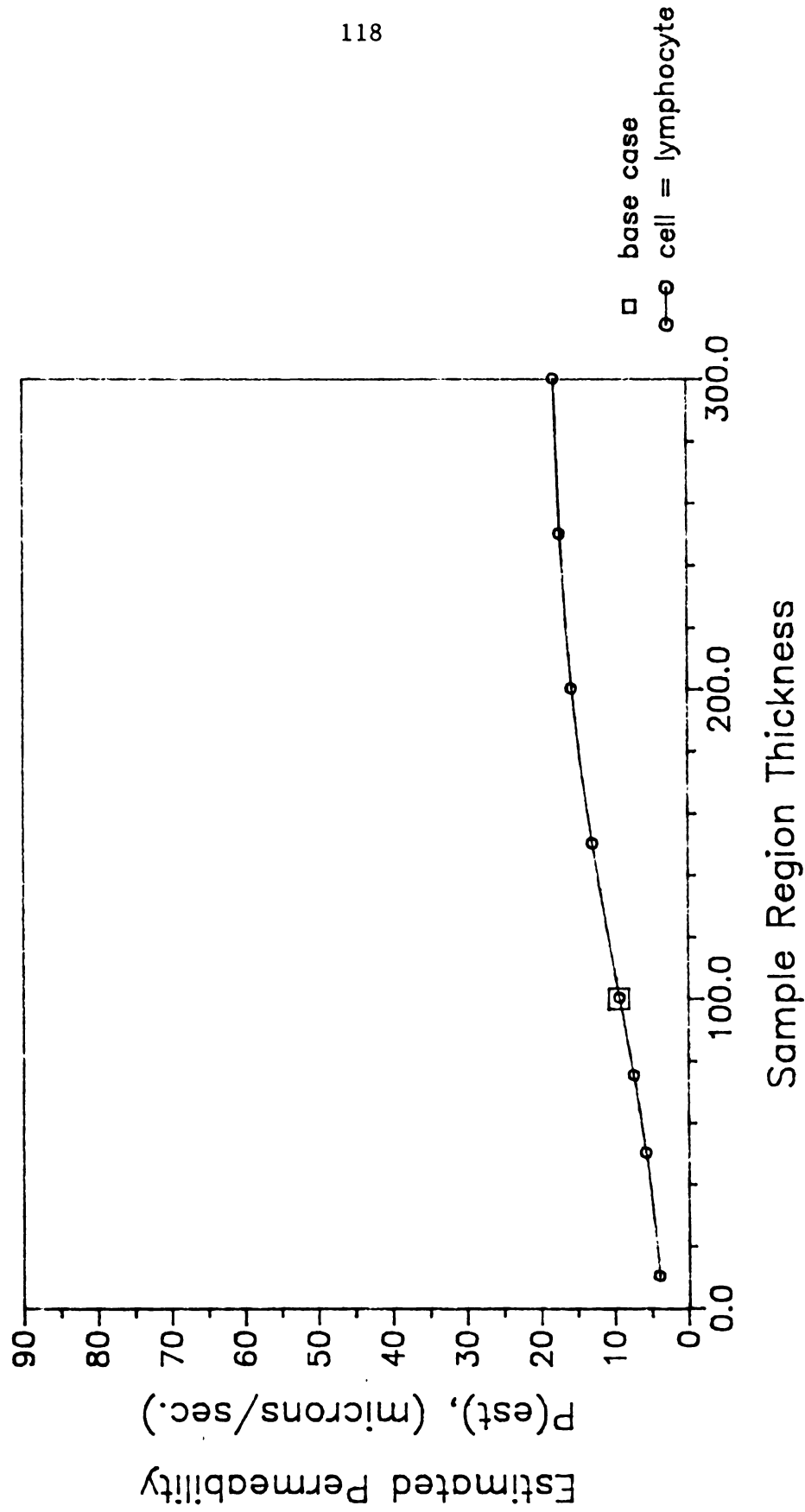
TABLE 6.3.3 - The Effect of Varying RL2

RL2 (μm)	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
10	4.0 ± 0.039	0.002
50	5.8 ± 0.097	0.005
75	7.4 ± 0.112	0.003
* 100	9.3 ± 0.042	0.000
150	12.9 ± 0.786	0.020
200	15.7 ± 2.261	0.082
250	17.3 ± 2.716	0.163
300	18.1 ± 5.070	0.242

* — original base case

The results show the RL2 was proportionally related to $P(\text{est})$ in a slightly non-linear way. Recall from Section 6.2.3 the two extreme cases of a small RL2, which resulted in treating the sample region as a lumped system, and of a large RL2, which resulted in a infinite concentration gradient in the sample region. These two extreme cases cause the curve in Figure 6.3.3 to approach two asymptotes at about $P(\text{est})=4 \mu\text{m}/\text{sec}$, for a small RL2, and about $P(\text{est})=20 \mu\text{m}/\text{sec}$, for larger RL2. Again, the approximate range that was used when experiments were conducted was between $50 \mu\text{m}$, which would decrease $P(\text{est})$ by 38% if RL2 had been underestimated, and $150 \mu\text{m}$, which would increase $P(\text{est})$ by 39% if RL2 has been overestimated.

P(est) v.s. RL2 - Lymphocyte



RL2, (microns)

Figure 6.3.3

6.3.4 The Effect of Varying LIP

Note, investigating LIP for the lymphocyte case will not be necessary because the author was very certain that the position of the lymphocytes that were tested were always next to the dialysis membrane. Therefore the position was LIP = 5 for all five lymphocyte experiments for all five temperature ranges.

6.3.5 The Effect of Varying VINA

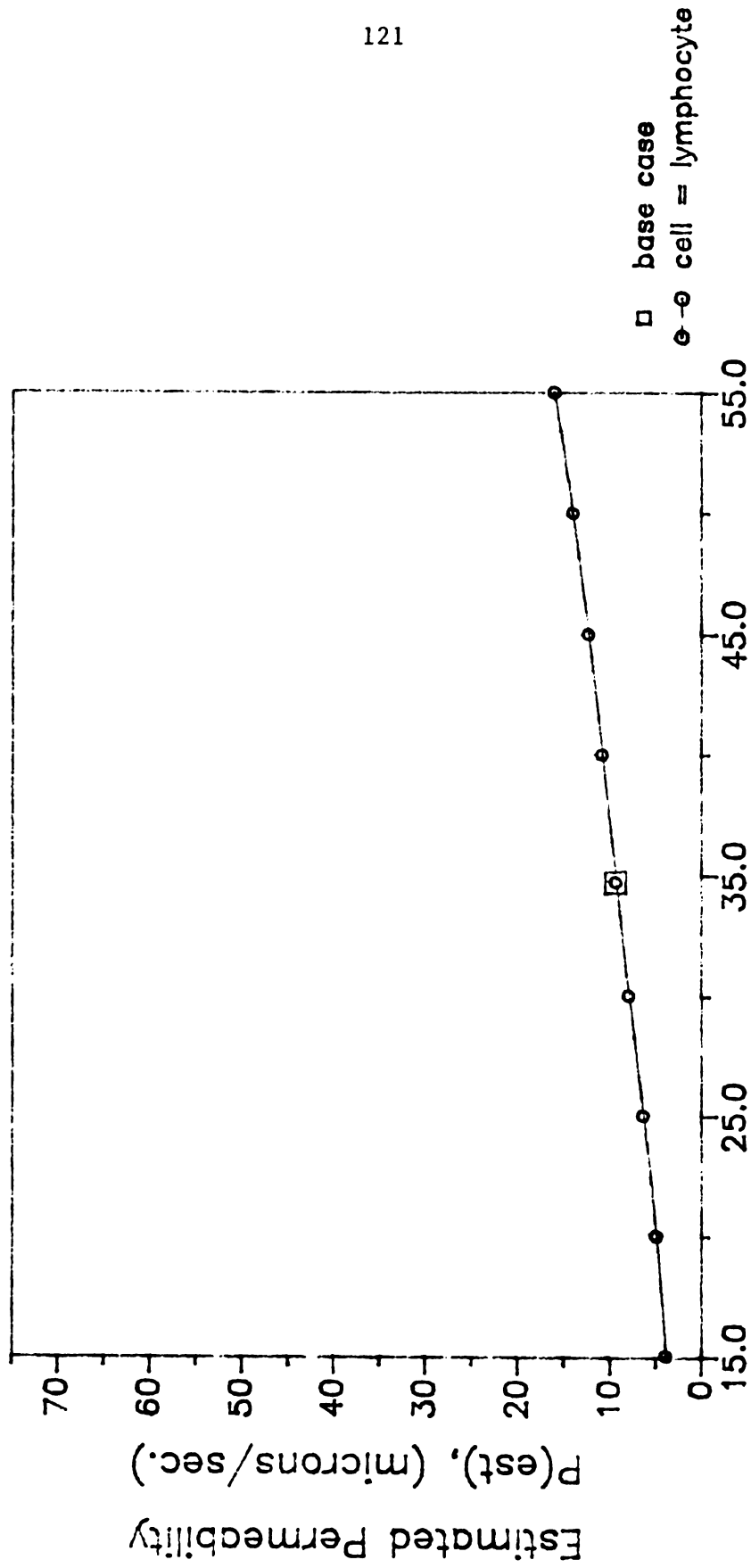
TABLE 6.3.5 - The Effect of Varying VINA

VINA (%)	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
15.0	3.9 ± 0.389	0.626
20.0	4.9 ± 0.515	0.444
25.0	6.3 ± 0.616	0.229
30.0	7.9 ± 0.510	0.059
* 34.7	9.3 ± 0.042	0.000
40.0	10.8 ± 1.307	0.081
45.0	12.3 ± 3.702	0.310
50.0	14.0 ± 8.100	0.688
55.0	16.0 ± 16.20	1.211

* - original base case

The relationship that resulted between VINA and $P(\text{est})$ in this study was directly proportional and approximately linear (see Figure 6.3.4). It should be noted that the curve in Figure 5.2.2, which the normalized osmotically inactive cell volume obtained, appears to slightly non-linear. If one were to trace a spline curve through the points and extrapolate the curve to the y-axis the resulting \hat{V}_b would approximately 45% which would increase the resulting permeability to $12.3 \mu\text{m}/\text{sec}$. However, this \hat{V}_b was not used in order to handle the resulting data the same as other investigators. To clarify this more experiments should be conducted.

P(est) v.s. VINA - Lymphocyte



Normalized Osmotically Inactive Cell Volume

$VINA, [\hat{V}_b = V_b/V(\text{initial})] \times 100$

Figure 6.3.4

6.3.6 The Effect of Varying DELAY

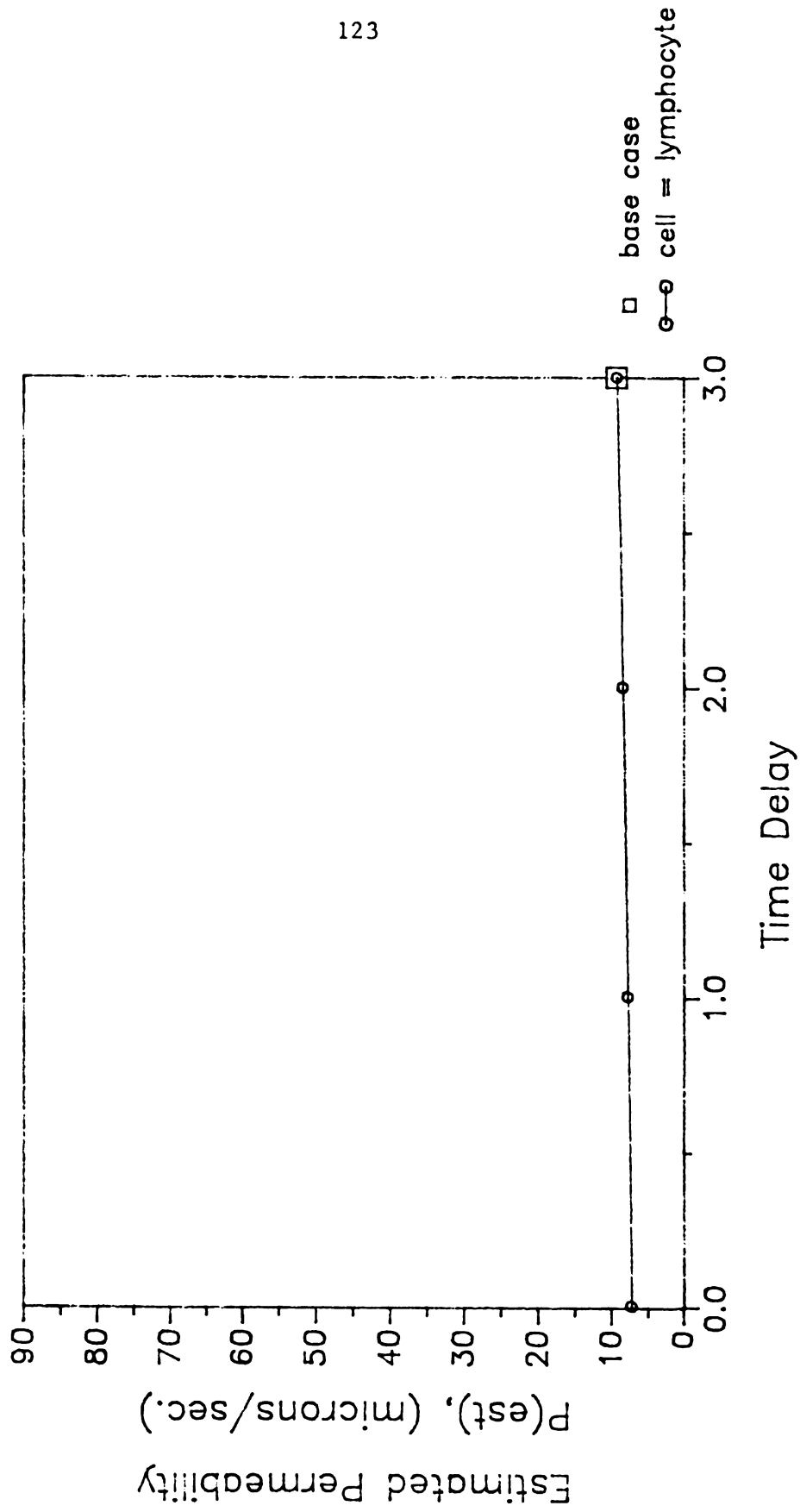
TABLE 6.3.6 - The Effect of Varying Delay

DELAY (sec)	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
0.0	7.3 ± 0.150	0.005
1.0	7.8 ± 0.114	0.002
2.0	8.5 ± 0.072	0.001
** 3.0	9.3 ± 0.043	0.000

** : The base case was modified here because during an actual experimental run there was a time delay (DELAY) when the hypertonic solution was started, (due to the time it took for the hypertonic solution to travel from the electronic solenoid valve to the bulk flow entrance port). Base upon the volumetric flow rate of the hypertonic solution, an average time delay was calculated to be about 2.7 sec. A time of 3.0 was chosen for the new base case to allow for a little extract delay in case the flow rate decreased.

The results from this study show that DELAY was directly proportional and approximately linearly related to $P(\text{est})$ (see Figure 6.3.5). Therefore, under estimating the delay time would result in under estimating the membrane permeability. For example, if the delay time of 3.0 seconds was not accounted for when the data was recorded, (which would imply a delay time of 0.0 seconds), $P(\text{est})$ would be under estimated by approximately 22%.

P(est) v.s. DELAY - Lymphocyte



DELAY, (sec.)

Figure 6.3.5

6.3.7 The Effect of Varying DR

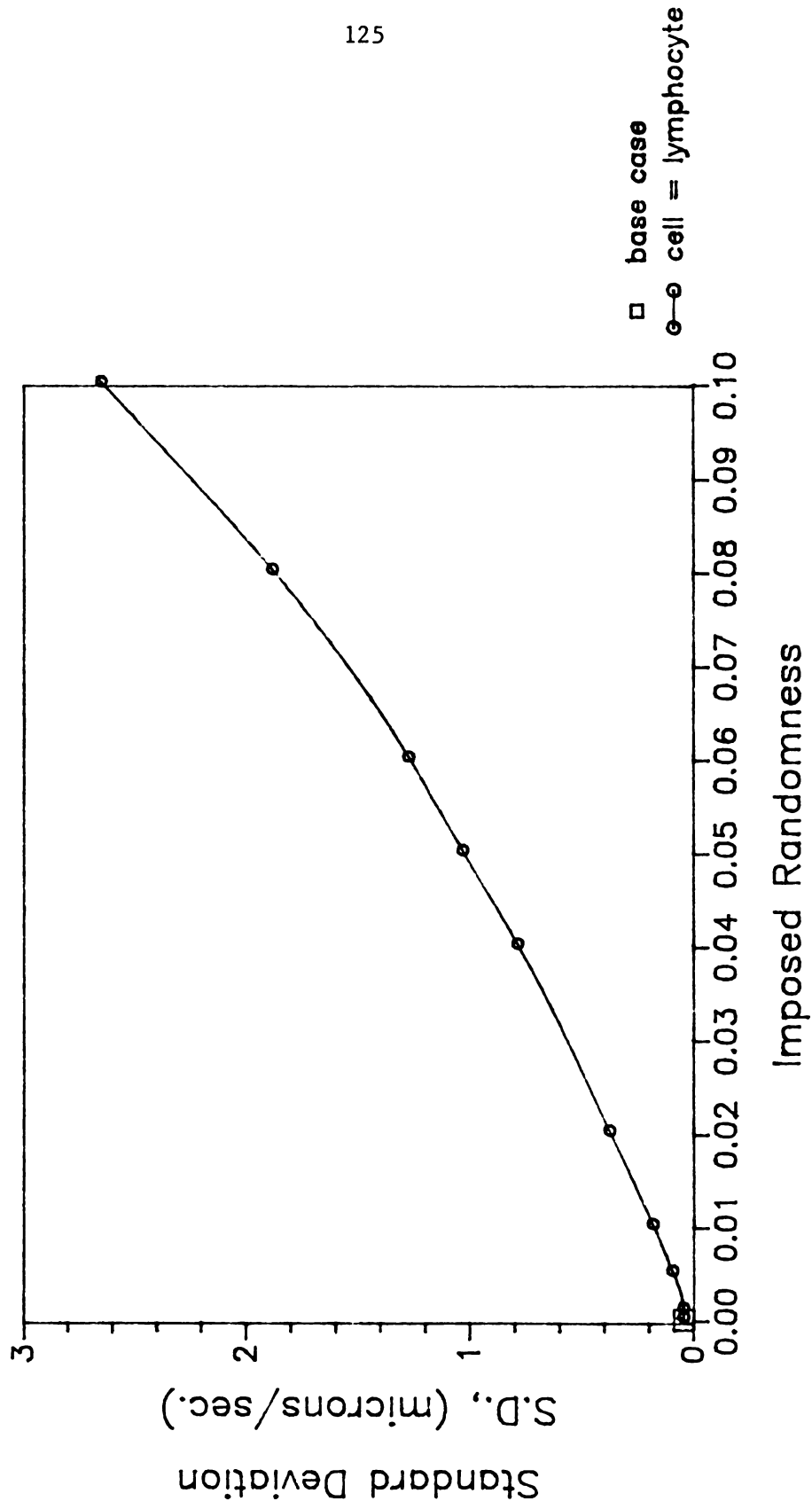
TABLE 6.3.7 - The Effect of Varying DR

	DR (μm)	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
*	0.000	9.3 ± 0.042	0.000
	0.001	9.3 ± 0.042	0.000
	0.050	9.4 ± 0.091	0.001
	0.010	9.4 ± 0.180	0.003
	0.020	8.9 ± 0.373	0.014
	0.040	9.9 ± 0.784	0.055
	0.050	9.0 ± 1.030	0.085
	0.060	10.4 ± 1.270	0.123
	0.080	11.1 ± 1.880	0.218
	0.100	10.0 ± 2.650	0.338

* - original base case

The results from this study show that the estimated permeability, for the most part, was not greatly effected as the imposed randomness, DR, was increased, while the standard deviation increased, non-linearly, as DR was increased (see Figure 6.3.6). As mentioned in Section 6.2.7 an attempt was made to estimate the maximum possible inaccuracy obtained when measuring the cell radius (after an experimental run). This same approach was used to determine the likely range of uncertainty for the lymphocyte case also. The uncertainty in measuring the cell radius for this case was $\pm 0.04 \mu\text{m}$.

S.D. v.s. DR - Lymphocyte



DR, (microns)

Figure 6.3.6

6.3.8 The Effect of the Number of Data Points

TABLE 6.3.8 - The Effect of the Number of Data Points

# of points	Permeability and Standard Deviation ($\mu\text{m}/\text{sec}$)	Minimum Sum
4	12.0 ± 1.76	0.003
6	12.0 ± 1.37	0.011
10	11.8 ± 1.29	0.014
15	11.3 ± 1.29	0.033
20	10.7 ± 1.02	0.044
25	10.0 ± 0.81	0.055
30	9.5 ± 0.65	0.060
35	9.3 ± 0.58	0.071
40	9.2 ± 0.55	0.084
45	9.1 ± 0.50	0.091
50	9.1 ± 0.47	0.103
100	9.2 ± 0.32	0.184

Note: All of the input parameters used for this case were the same as described for the base case except DR was set at $0.04 \mu\text{m}$. This approach was based on the rational described in Section 6.2.8 and the uncertainty approximation made in Section 6.3.7. Also the number of data points used for each of the above cases were equally space with the 0 - 100 sec time range.

These results suggest that the estimated permeability was related to the number of data points recorded in a non-linear fashion. The estimated permeability started at about $12.0 \mu\text{m}/\text{sec}$ for a few points and decreased as the number of points was increased until the number of points reached about 30, where $P(\text{est})$ began steady at about $9.2 \mu\text{m}/\text{sec}$ (see Figure 6.3.7). Recall from section 4.5 that the number of data points recorded for each experimental run was 20 - 30.

Also from the above results, the standard deviation was related to the number of data points recorded in a decreasing non-linear manner, (as the number of points increased). Again as was mentioned in Section 6.2.8, if the

case where the number of data points equalled 4 was ignored, the standard deviation was then approximately linearly related to the inverse square root of the number of data points (see Figure 6.3.8), which was to be expected based on equation (2.3.10).

The relationship between the number of points and the minimum was approximately linear, which was also expected based on equation (2.3.3) (see Figure 6.3.9).

P(est) v.s. Number of Points - Lymphocyte

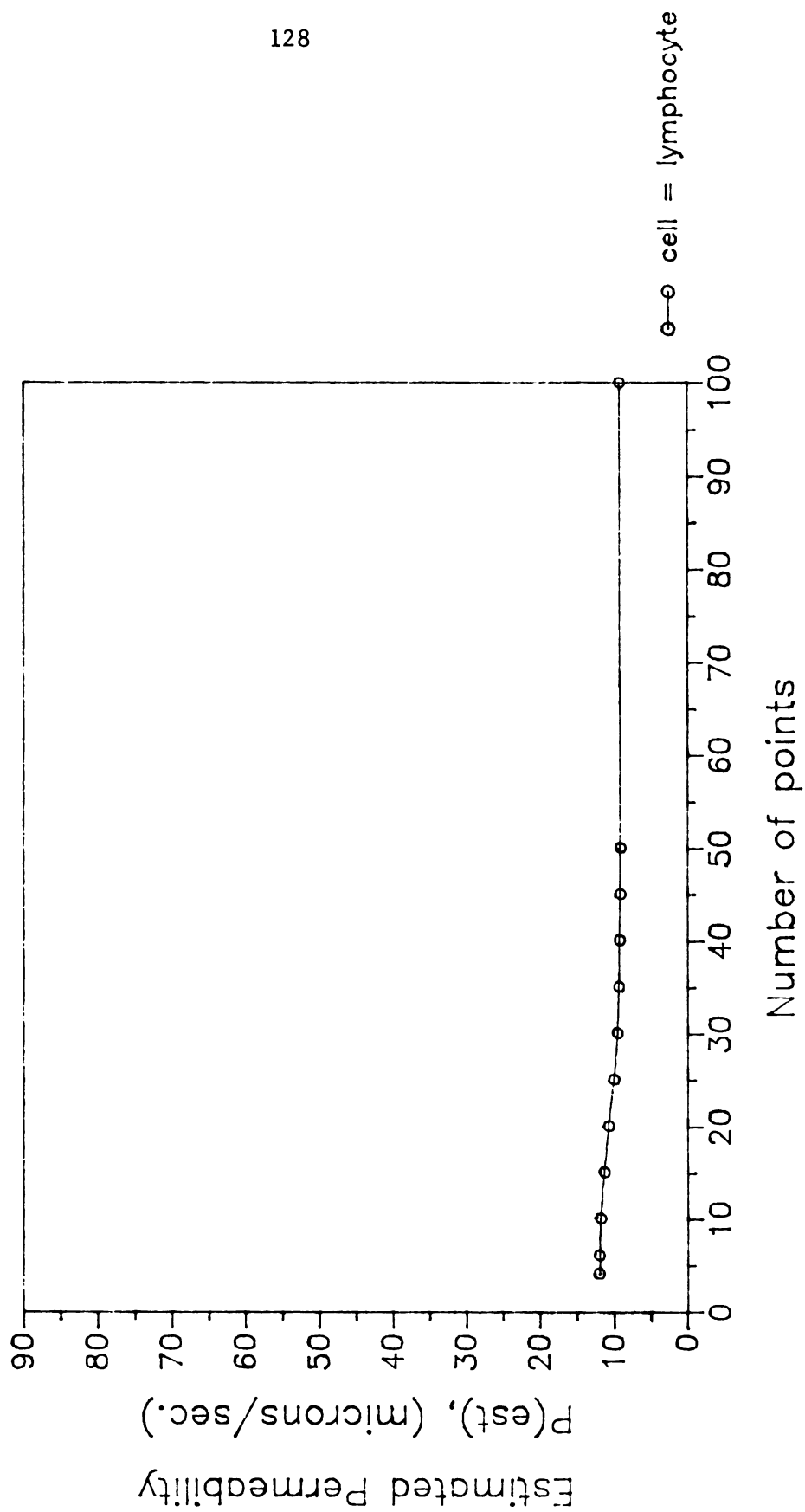


Figure 6.3.7

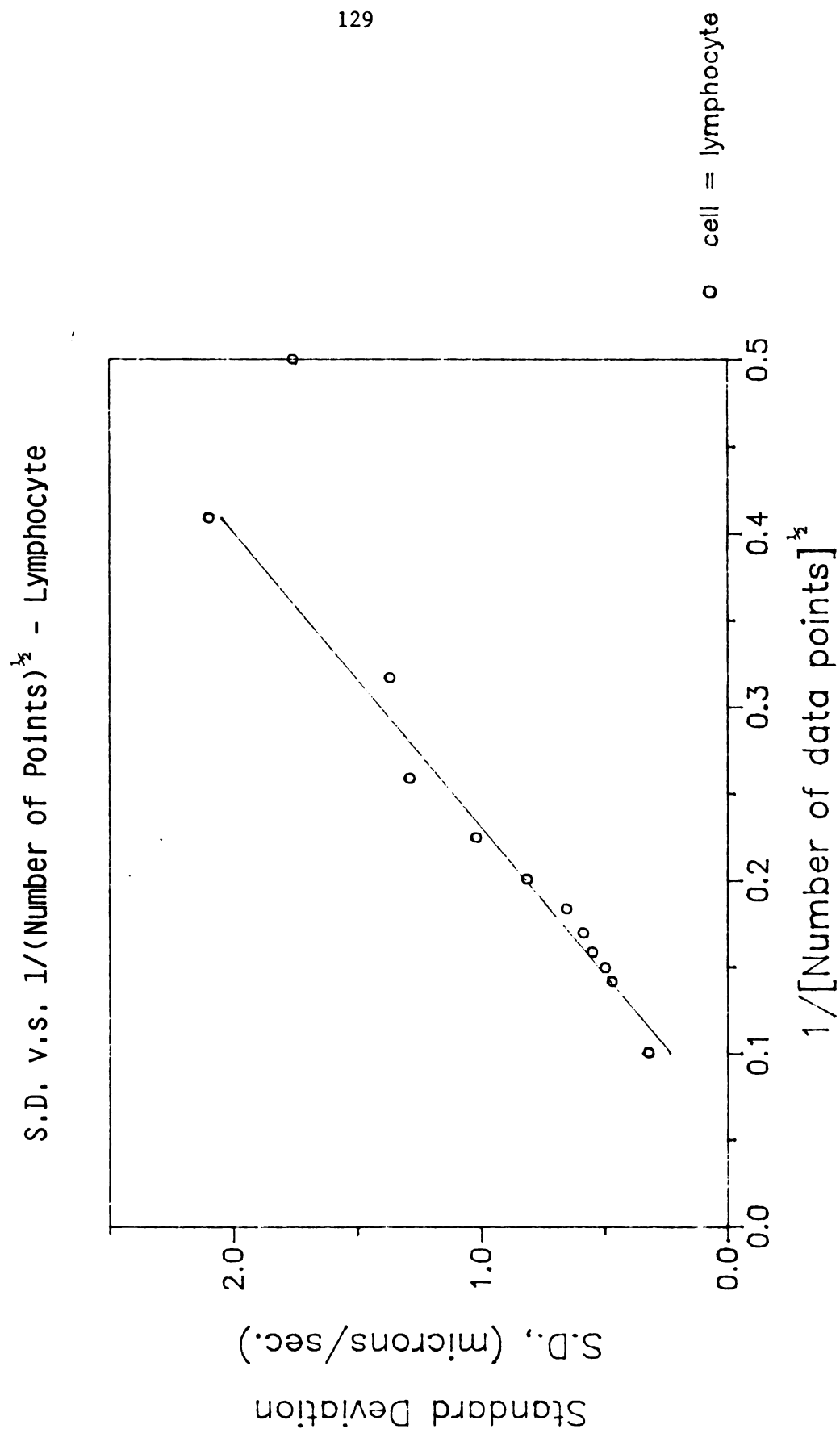


Figure 6.3.8

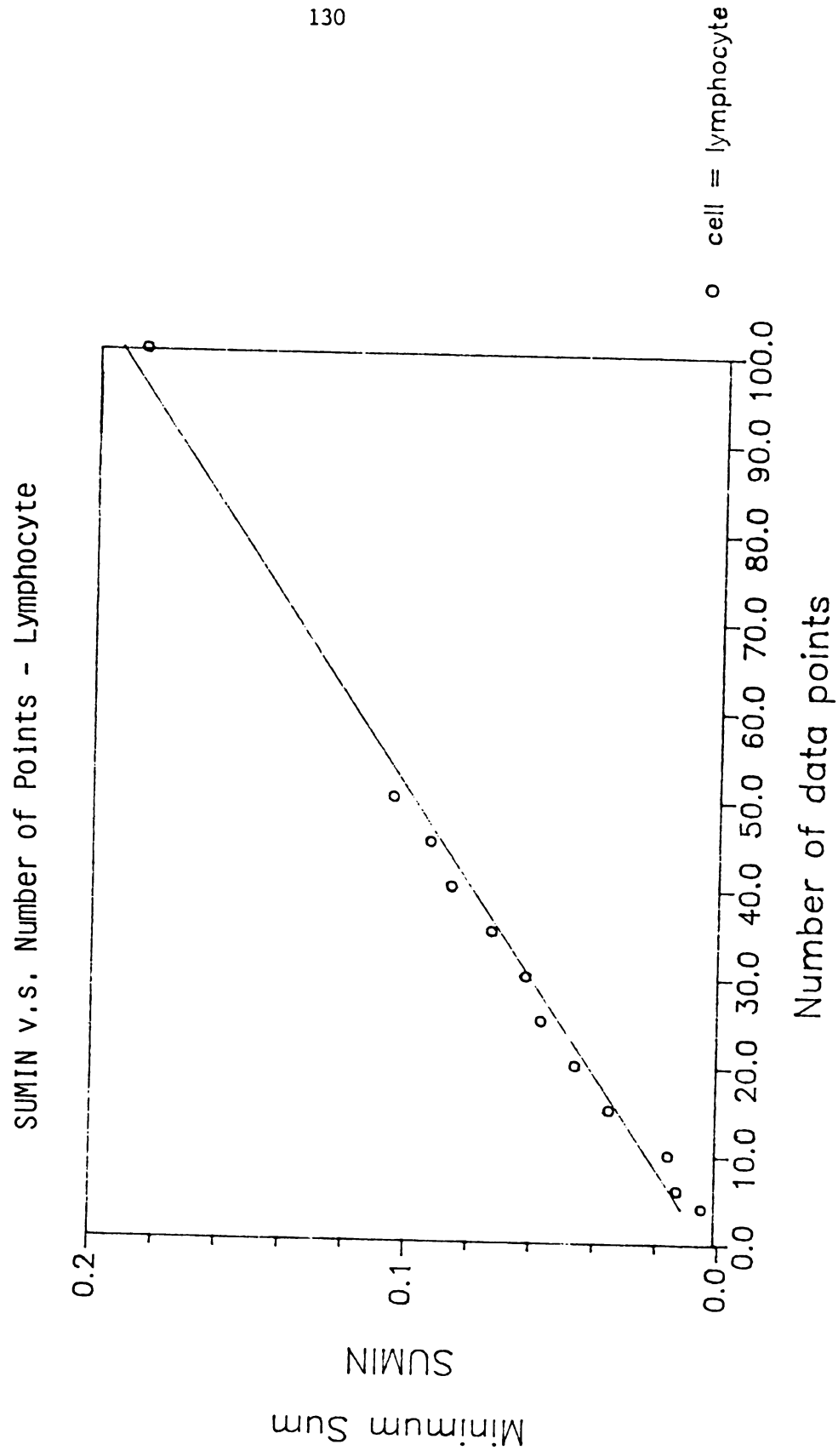


Figure 6.3.9

6.3.9 The Effect of Varying Ea of the Dialysis Membrane on the Ea of the Cell

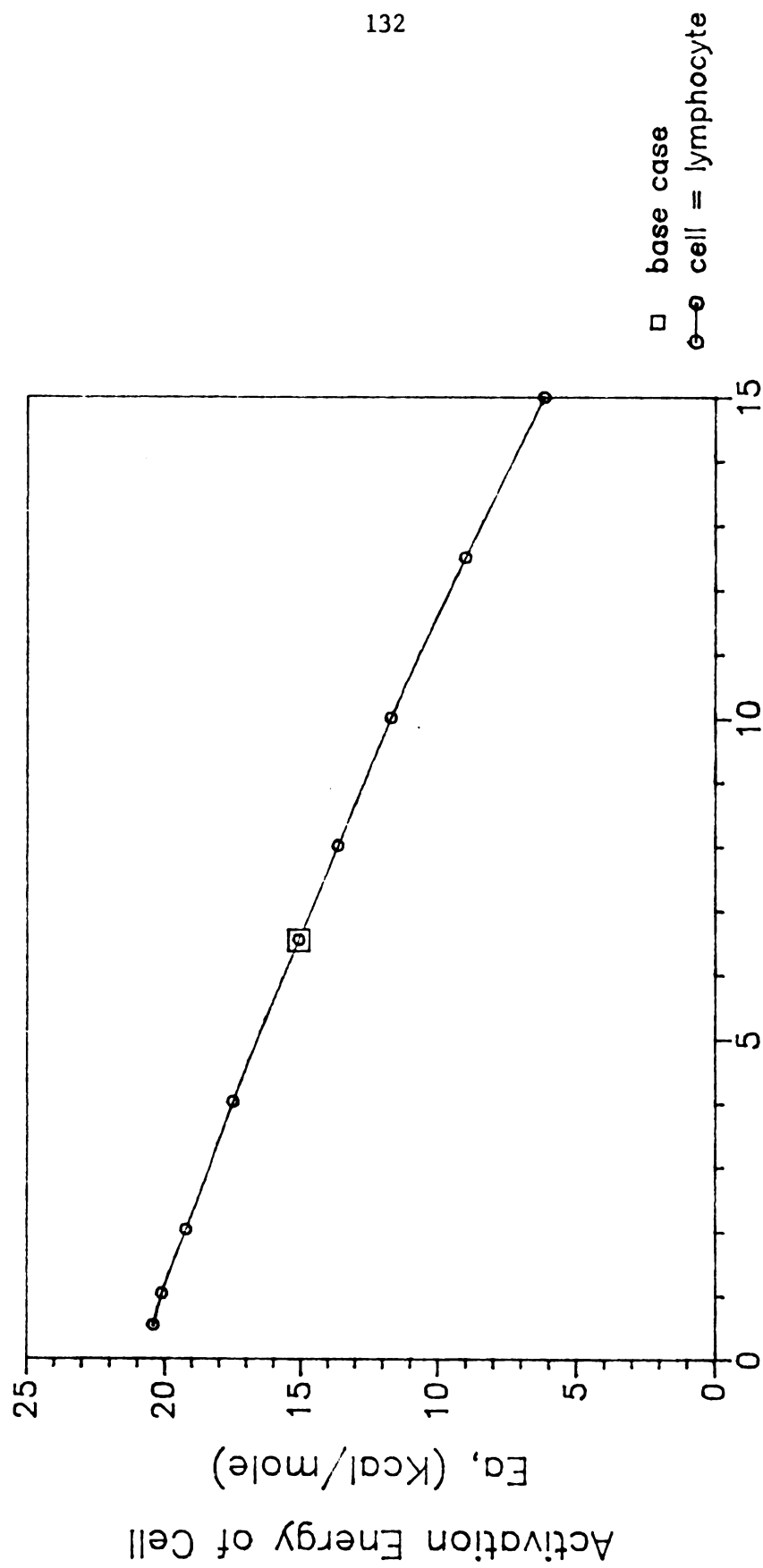
TABLE 6.3.9 - The Effect of Varying Ea of the Dialysis Membrane
on the Ea of the Cell

<u>Ea, Dialysis Membrane</u> <u>(Kcal/mole)</u>	<u>Ea, Liposome Membrane</u> <u>(Kcal/mole)</u>
0.5	20.4
1.0	20.1
2.0	19.2
4.0	17.5
* 6.53	15.1
8.0	13.6
10.0	11.7
12.5	9.0
15.0	6.2

* - original base case

The results for this study suggest the two membrane activation energies were inversely proportional and slightly non-linear in relation to one another (see Figure 6.3.10). Similarly, as mention in Section 6.2.9, if the manufacturer misstated the activation energy for the dialysis membrane then the resulting cell membrane activation energies would be effected.

$E_a(\text{Cell})$ v.s. $E_a(\text{Dialysis Membrane})$



$E_a, (\text{Kcal/mole})$

Figure 6.3.10

6.4 Discussion of Sensitivity Studies - Ranking Input Parameters

For the most part the sensitivity studies in Sections 6.2 and 6.3 produced similar results, when comparing the respective (general) shapes of the curves, (e.g. Figure 6.2.1 and 6.3.1, etc.). Each input parameter that was questioned effected the estimated membrane permeability to some degree. This section will rank the importance of correctly estimating input parameters, from most to least in terms of its "potential" to effect estimated membrane permeability (for the two cases studied).

Clearly the input parameters which could effect the estimated permeability the most are H_d and D_1 (see Figures 6.2.1, 6.2.2, 6.3.1 and 6.3.2). This can be explained by studying the resistance of the solute flow through the boundary layer, dialysis membrane and sample region, which can be written as $1/H_d$, RL_1/D_1 and RL_2/D_2 , respectively. (Recall that H_d was the convective mass transfer coefficient, RL_1 was the thickness of the wetted dialysis membrane, D_1 was the solute diffusivity in the dialysis membrane, RL_2 was the thickness of the sample region and D_2 was the solute diffusivity in free solution.) Calculating these resistances, $1/H_d=0.625$, $RL_1/D_1=1.0$ and $RL_2/D_2=0.625$ (for the base case). Therefore, whenever H_d or D_1 was decreased its corresponding resistance became the dominant resistance to the solute flow and when ever H_d or D_1 was increased the resistance to solute flow in that area diminished.

The input parameter which probably had the next most influence on $P(\text{est})$ was RL_2 , the sample chamber thickness (see Figures 6.2.3 and 6.3.3). This can also be explained by studying the resistance to solute flow. As mentioned

above, when the resistance to solute flow was changed, $P(\text{est})$ would then be effected. More specifically, when RL2 was increased the resistance to solute flow was increased and when RL2 was decreased the resistance to solute flow was decreased, in the sample region.

Following RL2 would be VINA, the normalized osmotically inactive cell volume (see Figures 6.2.5 and 6.3.4). This parameter was determined by performing osmotic equilibrium experiments. It was observed that each cell that was tested had its own osmotically inactive volume, which wasn't too different for the average value used. The osmotically inactive cell volume that was used for the liposome and lymphocyte experiments was average based on a sample of the population.

The parameter with the next most influence, which wasn't a single input parameter, was the number of data points used to estimate the membrane permeability.

The last two input parameters that were studied were the time delay, DELAY, and the cell position in the diffusion chamber, LIP. Varying these parameters did not have much of an effect on $P(\text{est})$ (for these cases). However, the time delay could have a substantial effect on $P(\text{est})$ if the time duration of an experimental run is very short (less than about 15 seconds). LIP would only become important if the sample region thickness was large where a substantial concentration gradient could develop.

CHAPTER 7

Conclusions

Based upon the results of this work the following conclusions can be made:

- 1) The two preparation techniques used to prepare egg-lecithin liposomes and human lymphocytes can produce good yields, thus providing a good population from which a cell specimen can be chosen.
- 2) The microscope diffusion chamber system can effectively be used to produce reliable data for calculating the equilibrium osmotic response of liposomes and human lymphocytes because it is relatively simple to task a cell in some isotonic solution and expose it to a series of step-wise increases in concentration.
(Note: the cell is allowed to come to an equilibrium volume after each step increase in concentration.) The cell system test in this work was human lymphocytes which yielded a normalized osmotically inactive cell volume of 34.7%. This normalized osmotically inactive volume was in good agreement with inactive volumes reported by other scientists. Therefore, the author believes the microscope diffusion chamber could be applied to other cell systems to determine their respective normalized osmotically inactive cell volume.
- 3) The microscope diffusion chamber system, in conjunction with the computer algorithm SENS, can be used to determine the dynamic non-

equilibrium osmotic response of egg-lecithin liposomes and human lymphocytes, (i.e. the cell membrane water permeability), at a specified temperature. The cell membrane water permeabilities determined for this work compared well with permeabilities published by other scientists. Specifically, the mean permeability calculated at 25°C for egg-lecithin liposomes was 40.2 $\mu\text{m}/\text{sec}$ and for human lymphocytes was 9.3 $\mu\text{m}/\text{sec}$. Based on these results the author believes that the diffusion chamber, along with SENS, can be used to determine the membrane water permeability for other cell systems with similar membrane characteristics and could probably be applied to cell systems with even higher membrane permeabilities. However, there may be an upper limit, with respect to the permeability, at which the diffusion chamber may not produce reliable results.

- 4) Because the microscope diffusion chamber can be used at different temperatures, the data produced by the microscope diffusion chamber system can be used to determine the effect of temperature with respect to the membrane permeability, i.e. the activation energy. Based on the experiments conducted, for this work, it was discovered the cell membrane permeability for both liposomes and lymphocytes have a strong dependence on temperature. This temperature dependence was quantified into an activation energy. The activation energies calculated, for liposomes and lymphocytes, were in good agreement with activation energies published by other scientists, (8.9 Kcal/mole for egg-lecithin liposomes and 15.1 Kcal/mole for human lymphocytes). Based on these results the

author believes that the activation energy for other cell systems can successfully be determined.

- 5) Egg-lecithin liposomes represent a good model system for equilibrium and non-equilibrium osmotic studies because of the similar behavior observed as compared to using a living cell system, i.e. the osmotic shrinkage of liposomes is consistent with the irreversible thermodynamic model developed by Kedem and Katchalsky. As mentioned, the liposomes used for this work were egg-lecithin in composition. Liposomes of other compositions could be used in the diffusion chamber to determine the effect of the membrane composition with respect to the cell membrane permeability.
- 6) Human lymphocytes also behaved in a manner consistent with the irreversible thermodynamic model and represent a good "hearty" cell system to study, i.e. lymphocytes hold up well under adverse conditions like increases in concentration.
- 7) The original version of SENS developed by J. Tu was an excellent starting point for developing a user friendly program. The program can easily be used by a user who has a general working knowledge of the microscope diffusion chamber system.
- 8) The computer program SENS is a useful tool for setting up experimental conditions. For example, if an investigator wishes to know the approximate time duration of an experimental run, the preliminary experimental conditions can be entered and the normalized cell volume can be observed, (which will come to some equilibrium volume). At the point when the cell has reached 99% of

its new volume is the approximate time duration of an experimental run.

- 9) The computer program SENS can effectively be used to study the effect of under or over estimating an input parameter with respect to the resulting estimated membrane permeability. Thus a particularly "sensitive" parameter can be identified and procedures can be implemented to carefully estimate this parameter.

CHAPTER 8

Suggestions for Future Work

The following suggestions are made for future work regarding the design of the experimental system and the cell systems tested with the microscope diffusion chamber.

- 1) Redesign the pumping system used with the diffusion chamber system to allow for more solution bottles to be accessible at one time. The present design of the system only allows for only two solution bottles to be used at a time. If a third (or fourth, or fifth, etc.) solution were to be introduced, it would have to be changed manually. By having five or more solution bottles readily accessible the equilibrium osmotic response could more easily be studied, i.e. the normalized osmotically inactive volume could more easily be obtained.
- 2) Interface the switch which turns on the pumping system could also be interfaced with the timer so that only one switch is necessary to start an experiment. The present design of the microscope diffusion chamber system has two separate switches, one to start the hypertonic solution and one to start the timer, which take two hands to start. In the mean time the focusing knob on the microscope needs to have continual minor adjustments made. Having a single switch would make this process easier.

- 3) Incorporate electronically controlled valves to allow the solution lines leading from the solution bottle to the electronic solenoid valve to be preflushed. This would allow for more easily controlling the temperature of the incoming solution and any air bubbles in the solution lines to escape.
- 4) Make the bulk flow region thinner to allow for greater ease in focusing the microscope condenser, which would result in a sharper image project (and therefore video taped). The present design of the diffusion chamber is such that the microscope condenser has to be smashed into the plastic on the bottom of the diffusion chamber.
- 5) Modify to the diffusion chamber to allow more systematic control of the sample region thickness.
- 6) Develop a better method of recording the cell radius (or volume) history. This could be done by using an image analysis equipment which can more accurately calculate the dynamic volume change of the cell as it is exposed to the hypertonic solution.
- 7) Devise a method to verify the number of bilipid layers when liposomes are used. Presently the method used to determine the number of bilipid layers is based on the contrast of the liposome projected on the screen.
- 8) Incorporate into the modelling, of the membrane water permeability, the effect of internal and external solute concentration. The concentration dependence was not mentioned, or studied, in this work but has been shown by other investigators to have an effect.
- 9) Also incorporate into the modelling the estimation of the individual cell osmotically inactive volume, in addition to the

cell membrane water permeability. This would result in a more accurate estimate of the membrane permeability.

- 10) Do experiments to characterize the dialysis membrane permeability, thus verifying the results of the manufacturer. As was shown in the sensitivity studies the accurately knowing the solute diffusivity in the dialysis membrane, which is related to the membrane permeability by $P_{mem} \Delta x = D_1$, is extremely important.
- 11) Devise a method to study the convective mass transfer coefficient and accurately determine its value. Also recall from the sensitivity studies that accurately knowing the convective mass transfer coefficient could be extremely important.
- 12) Apply the microscope diffusion chamber system to other cell systems, particularly cells with higher membrane water permeabilities, to determine if there are any problems in accurately estimating the membrane permeability. The microscope diffusion chamber system may produce misleading results if the cell has a high membrane water permeability. To further explain, if the dialysis membrane doesn't allow the passage of solute into the sample region fast enough, (in other words the dialysis membrane is too rate limiting with respect to solute transport), the resulting volume history may lead to an inaccurate membrane permeability.

APPENDICES

APPENDIX A

The Normalized Osmotically Inactive Volume

Van't Hoff was the first to study and develop the laws to osmotic equilibrium. His work was further expanded and applied to living cells by Boyle and Van't Hoff. The result has come to be known as the Boyle-Van't Hoff law, which has a form analogous to the perfect gas law ($PV=nRT$):

$$\pi V_w = \text{constant} \quad (\text{A-1})$$

where V_w represents the volume of solvent (water) and π represents the osmotic pressure. This law states that if the intracellular solution can be considered ideal and if all of the solvent can be considered "free" or osmotically active then the osmotic pressure is inversely proportional to the osmotic pressure, or extracellular concentration. However, for many cell systems not all of the solvent can be considered free. In 1932 Lucké and McCutcheon developed a relationship to compensate for the non-free solvent and anything else within the cell that can be considered non-solvent. This non-free solvent non-solvent volume is termed the "osmotically inactive cell volume".

The modified Boyle-Van't Hoff law, corrected for the osmotically inactive volume, may then be stated as

$$\pi(V_{\text{cell}} - V_b) = \pi^0(V_{\text{cell}}^0 - V_b) \quad (\text{A-3})$$

where π is the osmotic pressure, (the extracellular and intracellular osmotic pressures are equal at equilibrium), V_{cell} is the total volume of the cell and V_b is the osmotically inactive volume. The superscript

values correspond to a reference initial states.[McGrath, Heat Trans...]

Dividing (A-3) by the initial cell volume, V_{cell}^0 , and rearranging, the modified Boyle-Van't Hoff law becomes

$$\hat{V}_{\text{cell}} = \frac{\pi^0}{\pi}(1 - \hat{V}_b) + \hat{V}_b \quad (\text{A-4})$$

where $\hat{V}_{\text{cell}} = V_{\text{cell}}/V_{\text{cell}}^0$ (the normalized cell volume) and $\hat{V}_b = V_b/V_{\text{cell}}^0$ (the normalized osmotically inactive cell volume). Therefore by plotting \hat{V}_{cell} v.s. $1/\pi$ the normalized osmotically inactive volume can be found from the intercept when $1/\pi$ equals zero or from the slope $\pi^0(1 - \hat{V}_b)$ since both π^0 is known.

Appendix B

Preliminary Testing and Set Up of Experimental Equipment

The magnification calibrations were necessary because a cell, which appeared on the video monitor, was not only magnified by the lenses in the microscope but was also magnified by the video camera and the video monitor. These calibrations were performed using a Petroff-Haussen Bacteria Counter. The counter had etches of a specific distance apart marked on the surface of the glass. After focusing the microscope, the length between the two etch marks projected on the video monitor was measured. The ratio of the measured projected image and the known specific distance on the bacteria counter resulted in a magnification factor, RMAG. The results of these calibrations are summarized in Table B.1. It should be noted here that the that SENS allowed the user to enter the radius history measured from the video monitor, providing RMAG was also entered.

In addition, before conducting any experiments the temperature distribution of the diffusion chamber was investigated. These tests were conducted to determine what temperature the controller (i.e. refrigerated circulating bath) needed to be set at in order to obtain the desired temperature at the cell chamber. The investigated temperature settings of the circulating bath were 0.0°C, 8.9°C, 21.1°C, 30.6°C, 35.2°C 50.8°C and 60.7°C. The resulting temperatures detected at the top fitting are summarized in Table B.2 and Figure B.1.

TABLE B.1 - Magnification Calibration

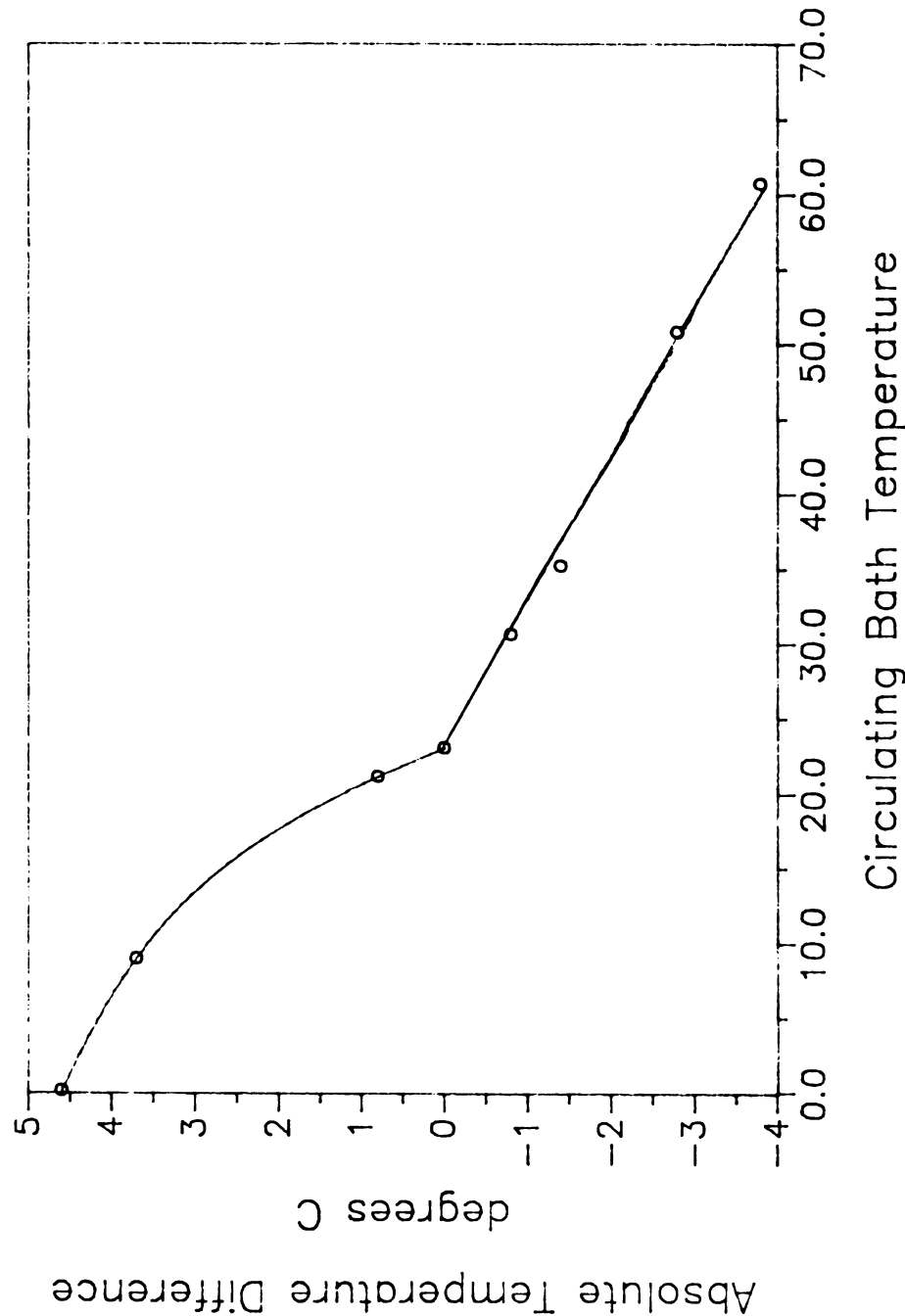
<u>Camera</u>	<u>Objective Power</u>	<u>Optavar Power</u>	<u>μm/mark</u>	<u>Magnification, RMAG</u>
Color	25	1.25	3.846	3175
Color	25	1.6	3.125	4064
Color	25	2.0	2.500	5080
Color	40	1.25	2.632	4683
Color	40	1.6	2.083	5994
Color	40	2.0	1.695	7492
Black/White	25	1.25	3.846	4750
Black/White	25	1.6	3.125	4064
Black/White	25	2.0	2.500	7600
Black/White	40	1.25	2.632	7005
Black/White	40	1.6	2.083	8968
Black/White	40	2.0	1.695	11209

TABLE B.2 - Temperature Bath Measurements

Room Temperature = 23°C
 (Note: All temperature are recorded in °C)

<u>Circulating Bath Temperature</u>	<u>Temperature of Top Fitting</u>	<u>Difference</u>
0.0	4.6	4.6
8.9	12.6	3.7
21.1	21.9	0.8
23.0	23.0	0.0
30.6	29.8	-0.8
35.2	33.8	-1.4
50.8	48.0	-2.8
60.7	56.9	-3.8

Temperature Bath Measurements



degrees C

Figure B.1

APPENDIX C

As mentioned in section 1.2 SENS was used to clarify previous results generated by M. Shabana using the microscope diffusion chamber. The cell system he used was unfertilized hamster ova. After Shabana gathered the experimental data he used a method devised by Terwilliger and Solomon [19] to calculate the membrane water permeability, P_{MS} [22]. To help clarify this results his data was reentered into SENS to generate a new permeability, P_{SENS} . The results are summarized in Table C.1.

TABLE C.1 - Summary of Shabana's Results

cell type: unfertilized hamster ova
initial concentration: 0.3 osmol (NaCl)
temperature: 25°C

<u>Exp. #</u>	<u>Final Concentration (osmol)</u>	<u>P_{MS} ($\mu\text{m}/\text{sec}$)</u>	<u>P_{SENS} ($\mu\text{m}/\text{sec}$)</u>
1	0.5	18.38	28.1 ± 1.6
2	0.5	21.26	51.3 ± 5.6
5	0.5	22.40	33.0 ± 3.4
6	0.5	20.75	42.8 ± 3.6
7	0.5	21.86	61.0 ± 13.0
3	0.8	20.35	28.1 ± 3.0
4	0.8	17.21	24.8 ± 1.7
8	0.8	16.96	15.2 ± 1.5
9	0.8	14.72	33.1 ± 2.0
10	0.8	18.64	36.4 ± 3.6
11	0.8	18.26	31.9 ± 1.8
12	1.5	17.68	35.3 ± 4.0
13	1.5	15.89	37.2 ± 5.6
14	1.5	15.36	22.3 ± 1.6
15	1.5	15.21	33.2 ± 4.5
16	1.76	17.05	29.3 ± 2.9
17	1.76	14.62	29.5 ± 2.4
18	1.76	?	25.1 ± 3.7
19	1.76	16.14	28.2 ± 3.1

APPENDIX D

SENS - The Prime Version Fortran Source Code

PROGRAM SENS

```

C-----
C   THIS PROGRAM INCLUDES THE COMPUTER MODEL FOR THE
C   DIFFUSION CHAMBER AND THE PARAMETER ESTIMATION FOR FINDING
C   PERMEABILITY OF A CELL INSIDE THE CELL CHAMBER OF THE
C   DIFFUSION CHAMBER.
C
C   THIS PROGRAM CONSISTS OF 1 MAIN PROGRAM AND 8 SUBROUTINES
C   AND 4 FUNCTIONS. THEY ALL ARE INSIDE THE FILES 'SENS',
C   'PAR.COUT', 'PLOT'. THE INPUT FILENAME IS SPECIFIED BY THE USER
C   AND THE NUMERICAL OUTPUT FILENAMES ARE 'O_SENS.DAT' AND 'O_SMRY.DAT',
C   AND THE GRAPHICAL OUTPUT FILENAME IS 'G_PLOT'
C
C   THE INPUT FORM REQUIRED IS AS FOLLOW
C
C   RL1: THICKNESS OF DIALYSIS MEMBRANE (M)
C
C   RL2: THICKNESS OF CELL CHAMBER (M)
C
C   LIP: APPROXIMATE LOCATION OF THE LIPOSOME (FROM 5 TO 11)
C
C   D1: DIFFUSIVITY OF SOLUTE INSIDE DIALYSIS MEMBRANE (M*M/SEC)
C
C   D2: DIFFUSIVITY OF SOLUTE INSIDE CELL CHAMBER (M*M/SEC)
C
C   CINIT: INITIAL CONCENTRATION (OSM)
C
C   CINF: FINAL CONCENTRATION (OSM)
C
C   H: MASS TRANSFER COEFF. (APPROXIMATELY 10000*D2)
C
C   IPRINT: NUMERICAL DATA OUTPUT FREQUENCY. (EVERY IPRINT*DT
C           SEC. PRINTS THE CONC. DIST. ON OUTPUT FILE)
C
C   IF1: CONTROL THE OUTPUT OF CONC. CHANGE INSIDE THE CELL
C        CHAMBER
C
C   IF2: CONTROL THE OUTPUT OF SENSITIVITY COEFF. VERSUS TIME
C
C   IF3: CONTROL THE OUTPUT OF NORMALIZED VOLUME RESPONSE
C        VERSUS TIME
C
C   IF4: CONTROL THE OUTPUT OF SUM OF ERROR OF SQUARE VERSUS
C        PERMEABILITY
C
C        (THE VALUES FOR ABOVE INTEGER OPTIONS ARE 1-YES, 0-NO)
C
C   IRELPS: OPTION FOR EXPERIMENTAL DATA INPUT 1-REAL-EXPERIMENT
C                                                  2-PSUESO-EXPERIMENT
C
C   IMICCEN: OPTION FOR ENTERING DATA IN 1-MICRONS 2-CENTIMETERS
C

```

C TMO, TM1: SETTING THE TIME RANGE ON THE PLOTS (SEC.)
 C
 C DT: TIME STEP FOR PROCEEDING THE CALCULATION (SEC.)
 C (NOTE: IF DT IS SET TOO LARGE, THE RESULT WILL FLUCTUATE.
 C IN THIS CASE, REDUCE THE SIZE OF DT AND TRY AGAIN.
 C THIS IS DUE TO THE UNSTABLE OF THE NUMERICAL METHOD.)
 C
 C DELAY: TIME DELAY SUBTRACTED FROM TIME ARRAY TM(I)
 C
 C CABO, CAB1: WINDOW OF THE Y-DIRECTION ON FIRST GRAPH.
 C (UNLESS NECESSARILY, SET THE VALUES AS 0. AND 5.)
 C
 C PSEN: THE PERMEABILITY VALUE AT WHICH WE INVESTIGATE THE
 C SENSITIVITY COEFF. (P'S EFFECT ON R'S CHANGE)
 C
 C SEN0, SEN1: SETTING THE RANGE FOR THE SENSITIVITY COEFF. PLOT
 C
 C PTRU: THE PERMEABILITY VALUE WITH WHICH THE PROGRAM GENERATES
 C PSUDO-EXPERIMENTAL DATA (R(TM,PTRU)).
 C
 C DT1: THE TIME STEP FOR THE PSUDO-EXPT'L DATA DURING TMO TO
 C TM01. (SEC.)
 C
 C TM01: THE PARTITION BETWEEN TWO DIFFERENT TIME STEPS RANGE.
 C (YOU CAN ASK THE PROGRAM TO GENERATES PSUDO-EXPT'L DATA
 C WITH TWO DIFFERENT INCREMENT IN TIME FOR TWO TIME
 C RANGE.)
 C
 C DT2: THE TIME STEP FOR THE PSUDO-EXPT'L DATA DURING TM01
 C TO TM1. (SEC.)
 C
 C
 C RINIT: INITIAL RADIUS (CM)
 C
 C VINA: INACTIVE VOLUME (%)
 C
 C RMAG: THE MAGNIFICATION OF THE MICROSCOPE
 C
 C DR: MAGNITUDE FOR THE PSEUDO-RANDOMNESS IMPOSED ON THE
 C PREDICTED RADIUS RESPONSE (CM)
 C
 C PO,P1: PERMEABILITY RANGE FOR THE FOURTH PLOT (MICRON/SEC.)
 C
 C DP: INCREMENT OF PERMEABILITY IN CALCULATING SUM OF ERROR OF
 C SQUARE FOR EACH P VALUE
 C
 C SUM0, SUM1: RANGE FOR THE FOURTH PLOT
 C
 C
 C OUTPUT CONFIGURATION OF 'O_SENS.DAT':
 C
 C (1) INPUT DATA

```

C          (2) PRINT CONC. DIST. OF THE SYSTEM AS A FUNCTION OF
C          TIME.
C          (3) SENSITIVITY COEFF. CORESPOND TO PSEN.
C          (4) THE ESTIMATED PERMEABILITY (LOCAL MINIMUM ON SUM
C          VERSUS P GRAPH)
C          (5) THE STANDARD DEVIATION OF THIS ESTIMATED P
C
C  OUTPUT CONFIGURATION OF 'O_SUMR.DAT':
C
C          (1) SUMMARY OF INPUT PARAMETERS AND DATA
C          (2) SUMMARY OF RESULTING PERMEABILITY, STANDARD DEVIATION
C          AND MINIMUM SUM
C
C  OUTPUT CONFIGURATION OF THE GRAPHICS FILE G_PLOT CAN BE
C  ONE OR MORE OF THE FOLLOWING:
C
C          (1) CONCENTRATION V.S. DIMENSIONLESS TIME
C          (2) SENSITIVITY COEFFICIENTS V.S. TIME
C          (3) NORMALIZED VOLUME V.S. TIME
C          (4) SUM OF SQUARE OF ERRORS V.S. PERMEABILITY
C
C-----
C  INITIALIZATION AND DECLARATIONS
C-----
C  PARAMETER (N3-301,II-2,N1-301,N4-301,EP1-0.01)
C  DIMENSION TMA(N3),TMB(N3),RA(N3),RB(N3),SEN(N3),SUM(N1),P(N1)
C  DIMENSION VOLC(N3),VOLA(N3),TMS(N3),RS(N3),RC(N3),RSAVE(N3)
C  CHARACTER*1 ICHANG, IGRAPH, IMORE, IAGAIN, IANOTH, ISAVE
C  CHARACTER*1 IMISTAK, IFIRST, IQUIT, IDEL
C  CHARACTER*11 XMICCEN,PROBLEM
C  CHARACTER*10 NAMFIL,ISENS
C  COMMON /C1/IPRINT,IF1,A1(II),A2(II),CAB0,CAB1
C  COMMON /C2/RINIT,VINA,DT,TM1,COUT(N4)
C  COMMON /C3/RL1,RL2,LIP,D1,D2,CINIT,CINF,H
C  EXTERNAL FCT0,F
C-----
C  EXPLANATION TO THE USER WHAT THE PROGRAM DOES.
C-----
C  IBACK = 0
C  IRUNAG=0
C  IOPNAG=0
C  IMISTAK = 'N'
2000 CONTINUE
C  WRITE(1,*)
C  WRITE(1,*)'WOULD YOU LIKE AN EXPLAINATION OF THIS PROGRAM, '
C  WRITE(1,*)'(SENS), (Y/N)?'
C  READ(1,'(A1)') IFIRST
C  CALL IYESNO(IFIRST)
C  IF(IFIRST.EQ.'N') GO TO 2002
C  WRITE(1,*)
C  WRITE(1,*)' WELCOME TO THE PROGRAM SENS. THIS PROGRAM WILL '
C  WRITE(1,*)'ALLOW THE USER TO (1) ANALYZE THE DATA OBTAINED USING '

```

```

WRITE(1,*)'THE MICROSCOPE DIFFUSION CHAMBER I.E. PARAMETER '
WRITE(1,*)'ESTIMATION OF THE PERMEABILITY OF A CELL OR (2) RUN '
WRITE(1,*)'A SIMULATION (PSEUDO) EXPERIMENT TO SEE WHAT MIGHT '
WRITE(1,*)'TO A CELL UNDER SPECIFIED CONDITIONS.'

C-----
C      OPTION TO HAVE A LIST OF THE NECESSARY PARAMETERS SENT TO
C      'I_DATA.LST'
C-----

WRITE(1,*)'  IF THIS IS THE FIRST TIME YOU HAVE USED THIS '
WRITE(1,*)'PROGRAM AND YOU WANT TO ENTER DATA FROM A REAL '
WRITE(1,*)'EXPERIMENT YOU MAY WANT TO OBTAIN A LIST OF THE '
WRITE(1,*)'PARAMETERS AND DATA NECESSARY TO RUN THE PROGRAM.'
WRITE(1,*)
WRITE(1,*)'WOULD YOU LIKE TO DO THIS, (Y/N)?'
READ(1,'(A1)') IFIRST
CALL IYESNO(IFIRST)
IF(IFIRST.EQ.'Y') THEN
  OPEN(13,FILE='I_DATA.LST')
  WRITE(1,*)
  WRITE(1,*)'THE LIST OF THE NECESSARY INPUT TO RUN THE PROGRAM'
  WRITE(1,*)'WILL BE IN FILE I_DATA.LST. THE PROGRAM WILL'
  WRITE(1,*)'STOP NOW. HAVE I_DATA.LST PRINT AT THE PRINTER.'
  WRITE(13,*)
  WRITE(13,*)'THE PARAMETES AND DATA NEEDED TO RUN THE PROGRAM'
  WRITE(13,*)'ARE:'
  WRITE(13,*)
  WRITE(13,*)'1) DIALYSIS MEMBRANE THICKNESS (RL1), MICRONS.'
  WRITE(13,*)'2) CELL CHAMBER THICKNESS (RL2), MICRONS.'
  WRITE(13,*)'3) DIFUSSIVITY OF SOLUTE IN MEMBRANE (D1), '
  WRITE(13,*)'          - METERS*METERS/SEC.'
  WRITE(13,*)'4) DIFUSSIVITY OF SOLUTE IN FREE SOLUTION (D2), '
  WRITE(13,*)'          - METERS*METERS/SEC.'
  WRITE(13,*)'5) MASS TRANSFER COEFFICIENT (H).'
  WRITE(13,*)'6) INITIAL CONCENTRATION (CINIT), OSMOLALITY.'
  WRITE(13,*)'7) FINAL CONCENTRATION (CINF), OSMOLALITY.'
  WRITE(13,*)'8) INACTIVE VOLUME (VINA), %'
  WRITE(13,*)'9) MAGNIFICATION FACTOR (RMAG).'
  WRITE(13,*)'10) TIME STEP (DT), SEC.'
  WRITE(13,*)'11) STARTING TIME (TMO), SEC.'
  WRITE(13,*)'12) ENDING TIME (TM1), SEC.'
  WRITE(13,*)'13) TIME DELAY (DELAY), SEC.'
  WRITE(13,*)'14) PERMEABILITY STEP (DP), MICRONS/SEC.'
  WRITE(13,*)'15) PERMEABILITY AT WHICH INVESTIGATE THE '
  WRITE(13,*)'      SENSITIVITY COEFFICIENTS (PSEN), MICRONS/SEC.'
  WRITE(13,*)'16) THE DATA POINTS: TIME (TMA(I)), SEC. AND '
  WRITE(13,*)'          RADIUS (RA(I)), MICRONS OR '
  WRITE(13,*)'          CENTIMETERS.'
  WRITE(13,*)
  WRITE(13,*)'      (NOTE: YOU ONLY NEED THE DATA POINTS IF YOU'
  WRITE(13,*)'      ARE USING THE PARAMETER ESTIMATION OPTION,'
  WRITE(13,*)'      I.E. A REAL EXPERIMENT.)'
  CLOSE(13)

```


C-----
C
C-----

C-----
C
C-----

```

        GO TO 600
    ENDIF
C-----
C   EXPLAINING THE OPTION TO ENTER DATA USING KEYBOARD OR AN INPUT FILE
C-----
    WRITE(1,*)
    WRITE(1,*)'  THIS PROGRAM WILL ALLOW YOU TO ENTER THE DATA '
    WRITE(1,*)'USING THE TERMINAL/KEYBOARD OR A PRE-EXISTING INPUT'
    WRITE(1,*)'FILE SET UP BY THE USER.  AN EXAMPLE OF AN INPUT FILE'
    WRITE(1,*)'CAN BE SEEN BY QUITTING THIS PROGRAM AND PRINTING'
    WRITE(1,*)'I_SENS.EXP AT THE PRINTER.  DO YOU WISH TO QUIT AND '
    WRITE(1,*)'PRINT THE EXAMPLE (Y/N)?'
    READ(1,'(A1)') IQUIT
    CALL IYESNO(IQUIT)
C-----
C   IF IQUIT IS YES THE PROGRAM WILL GENERATE I_SENS.EXP AND QUIT.
C-----
    IF (IQUIT.EQ.'Y') THEN
        OPEN(12,FILE='I_SENS.EXP')
        WRITE(12,*)'THIS IS THE EXAMPLE INPUT FILE I_SENS.EXP FOR THE'
        WRITE(12,*)'PROGRAM SENS.FOR.  THE PROGRAM WILL READ THE DATA'
        WRITE(12,*)'ALINING THE VALUES UNDER THE LEFT MOST CHARACTER.'
        RL1 = 16.
        RL2 = 100.
        LIP = 9
        D1 = 5.21E-11
        D2 = 5.21E-10
        H = 5.21E-6
        CINIT = 0.02
        CINF = 0.04
        VINA = 6.
        RMAG = 5080.
        DT = 5.0
        TMO = 0.0
        TM1 = 500.0
        DELAY = 0.0
        DP = 2.
        PO = 0.
        P1 = 100.
        PSEN = 40.
        RINIT = 7.7
        PTRU = 40.0
        DR = 0.01
        TM01 = 500.0
        DT1 = 5.
        DT2 = 5.0
        IRELPSE = 1
        IMICCEN = 2
        IF1 = 1
        IF2 = 1
        IF3 = 1
        IF4 = 1
    
```

```

      IPRINT = 10.
      CAB0 = 0.0
      CAB1 = 5.0
      SEN0 = -0.1
      SEN1 = 0.0
      VOLO = 0.0
      VOL1 = 1.0
      SUM0 = 0.0
      SUM1 = 100.0
      P0 = 0.0
      P1 = 100.0
      ICOUNT = 40
      RA(1) = 7.7
      TMA(1) = 0.0
      DO 1100 I = 2,40
          TMA(I) = TMA(I-1) + 10.
          RA(I) = RA(I-1) - 0.05
1100      CONTINUE
          GO TO 331
      ENDIF
C-----
C      EXPLAINING THE INPUT AND OUTPUT OPTIONS
C-----
      WRITE(1,*)
      WRITE(1,*)'  THE PROGRAM WILL ALSO ALLOW THE USER TO VIEW THE'
      WRITE(1,*)'RESULTS BY 1) TABLES AND/OR 2) GRAPHICALLY.  THE'
      WRITE(1,*)'TABLES GENERATED CAN BE FOUND IN A FILE CALLED'
      WRITE(1,*)'"O_SENS.DAT".  A SUMMARY OF THE INPUT PARAMETERS AND'
      WRITE(1,*)'DATA CAN BE FOUND IN "O_SMRY.DAT".  THE GRAPHICAL '
      WRITE(1,*)'OUTPUT WILL BE DISPLAYED ON THE SCREEN AND STORED'
      WRITE(1,*)'IN A GRAPHICS FILE G_PLOT.'
      WRITE(1,*)'THE USER MUST THEN USE "PRINTX" TO GENERATE A'
      WRITE(1,*)'PRINTED COPY, (NOTE: THE FIRST GRAPHICS FILE WILL'
      WRITE(1,*)'START ON PAGE 2 !!).  THE PLOTS THAT CAN BE GENERATED'
      WRITE(1,*)'ARE:'
      WRITE(1,*)
      WRITE(1,*)'  1) CONCENTRATION V.S. DIMENSIONLESS TIME'
      WRITE(1,*)'  2) SENSITIVITY COEFFICIENTS V.S. TIME'
      WRITE(1,*)'  3) NORMALIZED VOLUME V.S. TIME'
      WRITE(1,*)'  4) SUM OF SQUARE OF ERRORS V.S. PERMEABILITY'
      WRITE(1,*)
      WRITE(1,*)'YOU ARE NOW READY TO START THE PROGRAM.'
2002  CONTINUE
      WRITE(1,*)
      WRITE(1,*)'DO YOU WISH TO ENTER THE DATA USING (1) THE TERMINAL'
      WRITE(1,*)'OR (2) A PRE-EXISTING INPUT FILE, (ENTER 1 OR 2)?'
      WRITE(1,*)
      READ(1,*,ERR=2000) ITERINP
      CALL IONETWO(ITERINP)
      IF(ITERINP.EQ.2) THEN
          WRITE(1,*)
          WRITE(1,*)'PLEASE ENTER THE NAME OF THE INPUT FILE TO BE '

```

C

C-

C

C

C-

20

210

210

210

```

        WRITE(1,*)'USED, (ENTER NO MORE THAN 10 CHARACTERS).'
```

```

        READ(1,'(A10)') ISENS
        CALL CHANNAM(ISENS)
        WRITE(1,*)
        WRITE(1,*)'OKAY, THE PROGRAM IS CRUNCHING.'
```

```

        GO TO 2999
    ENDIF
C
    IPRINT = 10
C-----
C    PROMPTING THE USER TO ENTER THE REQUIRED DATA AND PARAMETERS
C    NEEDED TO RUN THE PROGRAM.
C-----
2005  CONTINUE
        WRITE(1,*)
        WRITE(1,*)'DO YOU WISH TO (1) ENTER DATA FROM A REAL EXPERIMENT'
        WRITE(1,*)'OR (2) USE THE PROGRAM FOR A SIMULATION (PSEUDO-'
        WRITE(1,*)'EXPERMINT), (ENTER 1 OR 2)?'
        WRITE(1,*)
        READ(1,*,ERR=2005) IRELPSE
        CALL IONETWO(IRELPSE)
2100  CONTINUE
        WRITE(1,*)'ENTERING THE PHYSICAL PARAMETERS OF THE SYSTEM:'
        WRITE(1,*)
        WRITE(1,*)'PLEASE ENTER THICKNESS OF THE DIALYSIS MEMBRANE, '
        WRITE(1,*)'(MICRONS).'
```

```

        WRITE(1,*)
        READ(1,*,ERR=2100) RL1
        WRITE(1,*)
2105  CONTINUE
        WRITE(1,*)'PLEASE ENTER THE THICKNESS OF THE CELL CHAMBER,'
        WRITE(1,*)'(MICRONS).'
```

```

        WRITE(1,*)
        READ(1,*,ERR=2105) RL2
        WRITE(1,*)
2106  CONTINUE
        WRITE(1,*)'PLEASE ENTER THE CELL POSITION, (5-11).'
```

```

        WRITE(1,*)'(SEE THE DIAGRAM BELOW FOR BETTER UNDERSTANDING.)'
        WRITE(1,*)
        WRITE(1,*)'      DIALYSIS MEMBRANE                CELL CHAMBER'
```

```

        WRITE(1,*)'| | | | | | | | | | | |'
        WRITE(1,*)'| B | | | | | | | | | |'
        WRITE(1,*)'| U | | | | | | | | | |'
        WRITE(1,*)'| L | | | | | | | | | |'
        WRITE(1,*)'| K | | | | | | | | | |'
        WRITE(1,*)'| 1 2 3 4 5 6 7 8 9 10 11'
        WRITE(1,*)'| F | | | | | | | | | |'
        WRITE(1,*)'| L | | | | | | | | | |'
        WRITE(1,*)'| O | | | | | | | | | |'
        WRITE(1,*)'| W | | | | | | | | | |'
        WRITE(1,*)'| | | | | | | | | | |'
        WRITE(1,*)

```

```

      READ(1,*,ERR=2106) LIP
      WRITE(1,*)
2110  CONTINUE
      WRITE(1,*)'PLEASE ENTER THE DIFFUSIVITY OF THE SOLUTE INSIDE'
      WRITE(1,*)'THE CELL CHAMBER, (METERS*METERS/SEC.), D2.'
      WRITE(1,*)
      READ(1,*,ERR=2110) D2
      WRITE(1,*)
2120  CONTINUE
      WRITE(1,*)'DO YOU WISH TO ENTER (1) SEPARATE VALUES FOR THE'
      WRITE(1,*)'DIFFUSIVITY OF THE SOLUTE INSIDE THE DIALYSIS'
      WRITE(1,*)'MEMBRANE (METERS*METERS/SEC.), D1, AND THE MASS'
      WRITE(1,*)'TRANSFER COEFFICIENT, H, OR (2) USE PRESET'
      WRITE(1,*)'VALUES OF D1-D2/10 AND H=10000*D2?'
      WRITE(1,*)
      READ(1,*,ERR=2120) ISEPPRE
      CALL IONETWO(ISEPPRE)
      IF(ISEPPRE.EQ.1) THEN
2130  CONTINUE
          WRITE(1,*)'PLEASE ENTER D1 (METERS*METERS/SEC.).'
          WRITE(1,*)
          READ(1,*,ERR=2130) D1
          WRITE(1,*)
2140  CONTINUE
          WRITE(1,*)'PLEASE ENTER H, (METERS*METERS/SEC.)'
          WRITE(1,*)
          READ(1,*,ERR=2140) H
      ELSE IF (ISEPPRE.EQ.2) THEN
          D1 = D2/10.0
          H = 10000.*D2
      ENDIF
2150  CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE INITIAL AND FINAL CONCENTRATION, '
      WRITE(1,*)'CINIT CINF, (OSMOLALITY). (ENTER BOTH VALUES AND'
      WRITE(1,*)'SEPARATE WITH A SPACE.)'
      WRITE(1,*)
      READ(1,*,ERR=2150) CINIT, CINF
2160  CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE INACTIVE VOLUME (%).'
      WRITE(1,*)
      READ(1,*,ERR=2160) VINA
      WRITE(1,*)
2170  CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE MAGNIFICATION FACTOR. (USE 5080 0 '
      WRITE(1,*)'EXACT CELL SIZE ENTER 1.0.)'
      WRITE(1,*)
      READ(1,*,ERR=2170) RMAG
      WRITE(1,*)

```

```

2180  CONTINUE
      WRITE(1,*)
      WRITE(1,2190) RL1,RL2,LIP,D2,D1,H,CINIT,CINF,VINA,RMAG
2190  FORMAT(1X,'THE VALUES ENTERED SO FAR ARE:',/,
. 1X,'1) DIALYSIS MEMBRANE THICKNESS = ',E11.3,' MICRONS',/,
. 1X,'2) CELL CHAMBER THICKNESS = ',E11.3,' MICRONS',/,
. 1X,'3) LIPOSOME POSITION (5-11) = ',I2,/,
. 1X,'4) DIFFUSIVITY IN CELL CHAMBER = ',E11.3,' M*M/SEC.',/,
. 1X,'5) DIFFUSIVITY IN DIALYSIS MEMBRANE = ',E11.3,' M*M/SEC.',/,
. 1X,'6) MASS TRANSFER COEFFICIENT = ',E11.3,' ',/,
. 1X,'7) INITIAL CONCENTRATION = ',F7.3,' OSMOLALITY',/,
. 1X,'8) FINAL CONCENTRATION = ',F7.3,' OSMOLALITY',/,
. 1X,'9) INACTIVE VOLUME % = ',F5.2,/,
. 1X,'10) MAGNIFICATION FACTOR = ',F7.1,/)
      WRITE(1,*)'DO YOU WISH TO CHANGE ANY OF THEM, (Y/N)?'
      READ(1,'(A1)') ICHANG
      CALL IYESNO(ICHANG)
      IF(ICHANG.EQ.'Y') THEN
2210  CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE NUMBER BESIDE THE PARAMETER'
      WRITE(1,*)'YOU WISH TO CHANGE, (1-10). '
      READ(1,*,ERR=2210) NCHANG
2215  CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE NEW VALUE.'
      IF(NCHANG.EQ.1) THEN
          READ(1,*,ERR=2215) RL1
      ELSE IF(NCHANG.EQ.2) THEN
          READ(1,*,ERR=2215) RL2
      ELSE IF(NCHANG.EQ.3) THEN
          READ(1,*,ERR=2215) LIP
      ELSE IF(NCHANG.EQ.4) THEN
          READ(1,*,ERR=2215) D2
      ELSE IF(NCHANG.EQ.5) THEN
          READ(1,*,ERR=2215) D1
      ELSE IF(NCHANG.EQ.6) THEN
          READ(1,*,ERR=2215) H
      ELSE IF(NCHANG.EQ.7) THEN
          READ(1,*,ERR=2215) CINIT
      ELSE IF(NCHANG.EQ.8) THEN
          READ(1,*,ERR=2215) CINF
      ELSE IF(NCHANG.EQ.9) THEN
          READ(1,*,ERR=2215) VINA
      ELSE IF(NCHANG.EQ.10) THEN
          READ(1,*,ERR=2215) RMAG
      ELSE IF(NCHANG.LE.0.OR.NCHANG.GE.11) THEN
          CALL INCORRES
          GO TO 2210
      ENDIF
      GO TO 2180
    ENDIF
  ENDIF

```

```

IF(IRUNAG.GE.1.OR.IMISTAK.EQ.'Y') GO TO 2235
WRITE(1,*)
WRITE(1,*)'IN ORDER FOR THE PROGRAM TO RUN THE USER'
WRITE(1,*)'MUST ALSO ENTER THE FOLLOWING DATA:'
2220 CONTINUE
WRITE(1,*)
WRITE(1,*)'THE TIME RANGE OF THE EXPERIMENT, TMO TM1, (SEC.),'
WRITE(1,*)'(NOTE: PLEASE MAKE SURE TM1 IS GREATER THAN THE '
WRITE(1,*)'TIME OF THE LAST DATA POINT TO BE ENTERED AND ENTER '
WRITE(1,*)'BOTH VALUES WITH A SPACE BETWEEN THEM.)'
READ(1,*,ERR=2220) TMO, TM1
2223 CONTINUE
WRITE(1,*)
WRITE(1,*)'THE TIME STEP, DT, (SEC.). (NOTE: THIS TIME STEP IS'
WRITE(1,*)'USED FOR NUMERICAL INTEGRATION - CHOOSE DT SUCH THAT'
WRITE(1,*)'DT .GE. (TM1-TMO)/301 , TO PREVENT ARRAY OVERFLOW.)'
READ(1,*,ERR=2223) DT
2225 CONTINUE
WRITE(1,*)
WRITE(1,*)'THE PERMEABILITY STEP, DP, (MICRONS/SEC.) (NOTE: '
WRITE(1,*)'CHOOSE DP SUCH THAT DP .GE. (THE MAGINTUE OF THE'
WRITE(1,*)'PERMEABILITY RANGE UNDER INVESTIGATION)/301 TO'
WRITE(1,*)'PREVENT ARRAY OVERFLOW.)'
READ(1,*,ERR=2225) DP
2230 CONTINUE
WRITE(1,*)
WRITE(1,*)'THE PERMEABILITY RANGE UNDER INVESTIGATION, P0 P1,'
WRITE(1,*)'(MICRONS/SEC.). (NOTE: ENTER BOTH VALUES WITH A'
WRITE(1,*)'SPACE BETWEEN THEM.)'
READ(1,*,ERR=2230) P0, P1
2231 CONTINUE
WRITE(1,*)
WRITE(1,*)'THE PERMEABILITY VALUE AT WHICH THE SENSITIVITY'
WRITE(1,*)'COEFFICIENT WILL BE EVALUATED, PSEN, (MICRONS/SEC.) '
READ(1,*,ERR=2230) PSEN
2235 CONTINUE
WRITE(1,*)
WRITE(1,2240) DT,TMO,TM1,DP,P0,P1,PSEN
2240 FORMAT(1X,'THE VALUES ENTERED ARE:',/,
. 1X,'1) TIME STEP - ',F7.2,' SEC.',/,
. 1X,'2) TIME RANGE - ',F8.1,' SEC.', ' TO ',F8.1,' SEC.',/,
. 1X,'3) PERMEABILITY STEP - ',F7.2,' MICRONS/SEC.',/,
. 1X,'4) PERMEABILITY RANGE - ',F7.2,' MICRONS/SEC.', ' TO '
. ,F7.2,' MICRONS/SEC.',/,
. 1X,'5) INVESTIGATING PERMEABILITY - ',F7.2,' MICRONS/SEC.',/)
WRITE(1,*)'DO YOU WISH TO CHANGE ANY OF THEM, (Y/N)?'
READ(1,'(A1)') ICHANG
CALL IYESNO(ICHANG)
IF(ICHANG.EQ.'Y')THEN
2245 CONTINUE
WRITE(1,*)
WRITE(1,*)'PLEASE ENTER THE NUMBER BESIDE THE PARAMETER'

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WRITE(1,*)'YOU WISH TO CHANGE, (1-5). '
READ(1,*,ERR=2245) NCHANG
2246 CONTINUE
WRITE(1,*)
WRITE(1,*)'PLEASE ENTER THE NEW VALUE(S). '
READ(1,*,ERR=2246)
IF(NCHANG.EQ.1) THEN
    READ(1,*,ERR=2246) DT
ELSE IF(NCHANG.EQ.2) THEN
    WRITE(1,*)'(BOTH TMO AND TM1 - SEPARATE WITH A SPACE)'
    READ(1,*,ERR=2246) TMO, TM1
ELSE IF(NCHANG.EQ.3) THEN
    READ(1,*,ERR=2246) DP
ELSE IF(NCHANG.EQ.4) THEN
    WRITE(1,*)'(BOTH P0 AND P1 - SEPARATE WITH A SPACE)'
    READ(1,*,ERR=2246) P0, P1
ELSE IF(NCHANG.EQ.5) THEN
    READ(1,*,ERR=2246) PSEN
ELSE IF(NCHANG.LE.0.OR.NCHANG.GE.6) THEN
    CALL INCORRES
    GO TO 2246
ENDIF
GO TO 2235
ENDIF
C
IF(IRELPS.EQ.1) THEN
    IF(IRUNAG.GE.1.OR.IMISTAK.EQ.'Y') THEN
2248 CONTINUE
        WRITE(1,*)
        WRITE(1,*)'DO YOU WISH TO (1) ENTER ALL NEW DATA POINTS'
        WRITE(1,*)'OR (2) REVIEW THE PREVIOUS DATA POINTS,'
        WRITE(1,*)'(Y/N)?'
        READ(1,*,ERR=2248) INR
        CALL IONETWO(INR)
        IF(INR.EQ.2) GO TO 2261
        IF(INR.EQ.1) THEN
            I=0
            WRITE(1,*)
            GO TO 2250
        ENDIF
    ENDIF
    I = 0
    WRITE(1,*)
    WRITE(1,*)'SINCE YOU HAVE CHOSEN THE REAL-EXPERIMENTAL'
    WRITE(1,*)'OPTION YOU MUST NOW ENTER THE DATA POINTS.'
2250 CONTINUE
    WRITE(1,*)'BEFORE ENTERING THE DATA, IS THERE A TIME'
    WRITE(1,*)'DELAY THAT YOU WOULD LIKE TO HAVE SUBTRACTED'
    WRITE(1,*)'FROM THE TIME ARRAY YOU WILL BE ENTERING,'
    WRITE(1,*)'(Y/N)?'
    READ(1, '(A1)') IDEL
    CALL IYESNO(IDEL)

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IF(IDEL.EQ.'N') THEN
  DELAY = 0.0
ELSE IF(IDEL.EQ.'Y') THEN
2251  CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE TIME DELAY TO BE SUBTRACTED,'
      WRITE(1,*)'(SEC.)'
      READ(1,*,ERR=2251) DELAY
      WRITE(1,2252) DELAY
2252  FORMAT(/,' THE TIME DELAY THAT WILL BE SUBTRACTED IS ',
          F7.4,' SEC. ',/,/,', DO YOU WISH TO CHANGE IT, (Y/N)?')
      READ(1,'(A1)') ICHANG
      CALL IYESNO(ICHANG)
      IF(ICHANG.EQ.'Y') GO TO 2251
ENDIF
WRITE(1,*)
WRITE(1,*)'DO YOU WISH TO ENTER THE RADIUS USING UNITS'
WRITE(1,*)'OF (1) MICRONS OR (2) CENTIMETERS?'
2253  READ(1,*,ERR=2253) IMICCEN
      CALL IONETWO(IMICCEN)
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE DATA POINTS,'
      IF(IMICCEN.EQ.1)THEN
        WRITE(1,*)'TIME(I) (SEC.)  RADIUS(I) (MICRONS)'
      ELSE IF(IMICCEN.EQ.2) THEN
        WRITE(1,*)'TIME(I) (SEC.)  RADIUS(I) (CENTIMETERS)'
      ENDIF
      WRITE(1,*)'(ENTER BOTH VALUES AND SEPARATE WITH A SPACE.)'
      WRITE(1,*)'(NOTE:  ENTER 0.0 0.0 FOR THE LAST DATA POINT.) '
      WRITE(1,*)
2255  I = I+1
      WRITE(1,2256) I
2256  FORMAT(1X,'ENTER POINT ',I3)
2257  READ(1,*,ERR=2257) TMA(I), RA(I)
      IF((TMA(I).GT.0.).AND.(RA(I).GT.0.)) TMA(I)=TMA(I)-DELAY
      IF(I.EQ.1) RAMAX = RA(I)
      IF(I.GE.2.AND.RA(I).GT.RAMAX) RAMAX = RA(I)
      IF((TMA(I).GT.0.).OR.(RA(I).GT.0.)) GO TO 2255
      ICOUNT = I-1
      IF(TM1.LE.TMA(ICOUNT)) THEN
        WRITE(1,*)
        WRITE(1,*)'PLEASE MAKE SURE THE TIME, LIMIT TM1 IS'
        WRITE(1,*)'LARGER THAN THE TIME OF THE LAST DATA POINT.'
        WRITE(1,*)'IF YOU DO NOT CHANGE THIS THE PROGRAM WILL STOP.'
        WRITE(1,*)'(RELAX YOU WILL HAVE A CHANCE TO CHANGE IT.)'
        WRITE(1,*)
2260  CONTINUE
      WRITE(1,*)'THE NEXT TABLE WILL SHOW YOU THE POINTS YOU HAVE'
      WRITE(1,*)'JUST ENTERED.  IF YOU HAVE ENTERED MORE THAN 20'
      WRITE(1,*)'POINTS THE TABLE WILL STOP SPOOLING EVERY 20 POINTS'
      WRITE(1,*)'TO ALLOW YOU TO REVIEW THE POINTS ENTERED.  MAKE'

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WRITE(1,*) 'A NOTE OF WHICH POINT YOU WISH TO CHANGE OR'
WRITE(1,*) 'INSERT AND PRESS [RETURN] TO CONTINUE NOTE, YOU'
WRITE(1,*) 'YOU WILL ONLY BE ABLE TO CHANGE ONE POINT AT'
WRITE(1,*) 'A TIME.'
WRITE(1,*) '(NOW PRESS [RETURN] TO CONTINUE.)'
READ(1, '(A1)') ICHANG
2261 CONTINUE
WRITE(1,*)
WRITE(1,*) 'THE DATA POINTS YOU HAVE ENTERED ARE: '
WRITE(1,2259) DELAY
2259 FORMAT(' (INCLUDING THE SUBTRACTED TIME DELAY OF ',
          F10.4, ' SEC.))')
WRITE(1,*)
WRITE(1,*) ' J          TIME(J)          RADIUS(J)'
IF(IMICCEN.EQ.1) THEN
WRITE(1,*) '          (SEC.)          (MICRONS)'
ELSE IF(IMICCEN.EQ.2) THEN
WRITE(1,*) '          (SEC.)          (CENTIMETERS)'
ENDIF
DO 2265 J=1, ICOUNT+1
    WRITE(1,2263) J, TMA(J), RA(J)
2263 FORMAT(1X, I3, 5X, F8.2, 5X, F8.2)
    IF((J/20)*20.EQ.J) THEN
        WRITE(1,*)
        WRITE(1,*) 'PRESS [RETURN] TO CONTINUE.'
        READ(1, '(A1)') ICHANG
    ENDIF
2265 CONTINUE
IF(IBACK.EQ.1) GO TO 2281
WRITE(1,*)
WRITE(1,*) 'DO YOU WISH TO CHANGE OR INSERT ANY OF THE POINTS,'
WRITE(1,*) '(Y/N)?'
READ(1, '(A1)') ICHANG
CALL IYESNO(ICHANG)
IF(ICHANG.EQ.'Y') THEN
2266 CONTINUE
    WRITE(1,*)
    WRITE(1,*) 'ENTER (1) TO CHANGE AND (2) TO INSERT.'
    READ(1,*,ERR=2266) ICHAINS
    CALL IONETWO(ICHAINS)
    IF(ICHAINS.EQ.1) THEN
2267 CONTINUE
        WRITE(1,*)
        WRITE(1,*) 'PLEASE ENTER THE INDEX NUMBER J'
        READ(1,*,ERR=2267) JI
        IF(JI.LE.0.OR.JI.GE.I+1) THEN
            CALL INCORRES
            GO TO 2267
        ENDIF
        WRITE(1,*)
        WRITE(1,*) 'PLEASE ENTER THE NEW VALUES FOR '
        WRITE(1,*) 'TIME(J) AND RADIUS(J). '

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2270      READ(1,*,ERR=2270) TMA(JI), RA(JI)
        GO TO 2261
ELSE IF(ICHAINS.EQ.2) THEN
2272      CONTINUE
        WRITE(1,*)
        WRITE(1,*)'ENTER THE INDEX NUMBER J YOU WISH TO '
        WRITE(1,*)'CHANGE, (OR PUSH DOWN).'

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        GO TO 2261
    ENDIF
    IBACK = 0
    RINIT = RA(1)
ELSE IF(IRELPSE.EQ.2) THEN
    IF(IRUNAG.GE.1.OR.IMISTAK.EQ.'Y') GO TO 2319
    WRITE(1,*)
    WRITE(1,*)'SINCE YOU HAVE CHOSEN THE PSEUDO-EXPERIMENTAL'
    WRITE(1,*)'OPTION, THE FOLLOWING PARAMETERS MUST ALSO'
    WRITE(1,*)'BE ENTERED.'
    WRITE(1,*)
2300    CONTINUE
    WRITE(1,*)'THE PERMEABILITY VALUE WITH WHICH THE PROGRAM'
    WRITE(1,*)'GENERATES PSEUDO-EXPERIMENTAL DATA, PTRU, '
    WRITE(1,*)'(MICRONS/SEC.).'
    READ(1,*,ERR=2300) PTRU
2303    CONTINUE
    WRITE(1,*)
    WRITE(1,*)'DO YOU WISH TO ENTER THE INITIAL RADIUS USING UNITS'
    WRITE(1,*)'OF (1) MICRONS OR (2) CENTIMETERS, (ENTER 1 OR 2)?'
    READ(1,*,ERR=2303) IMICCEN
    CALL IONETWO(IMICCEN)
2305    CONTINUE
    WRITE(1,*)
    WRITE(1,*)'PLEASE ENTER THE INITIAL RADIUS OF THE CELL, RINIT,'
    IF(IMICCEN.EQ.1) WRITE(1,*)'(MICRONS).'
    IF(IMICCEN.EQ.2) WRITE(1,*)'(CENTIMETERS).'
    READ(1,*,ERR=2305) RINIT
2310    CONTINUE
    WRITE(1,*)
    WRITE(1,*)'SINCE THIS IS A SIMULATION THE DATA POINTS '
    WRITE(1,*)'GENERATED WILL HAVE A RADIUS HISTORY THAT WILL'
    WRITE(1,*)'LOOK EXACTLY LIKE THAT OF THEORY, THEREFORE'
    WRITE(1,*)'THE PROGRAM ALLOWS THE USER TO IMPOSE A PSEUDO-'
    WRITE(1,*)'RANDOMNESS FACTOR, DR, ON THE DATA. DR CAN BE'
    WRITE(1,*)'THOUGHT OF AS THE MAGNITUDE OF THE VARIATION'
    WRITE(1,*)'IN MEASURING THE RADIUS OF THE CELL.'
    WRITE(1,*)'PLEASE ENTER DR NOW.'
    IF(IMICCEN.EQ.1) WRITE(1,*)'(MICRONS).'
    IF(IMICCEN.EQ.2) WRITE(1,*)'(CENTIMETERS).'
    READ(1,*,ERR=2310) DR
    WRITE(1,*)
    WRITE(1,*)'WHEN USING THIS OPTION THE USER CAN CHANGE'
    WRITE(1,*)'THE TIME STEP IN TWO REGIONS TO STUDY THE '
    WRITE(1,*)'EFFECT OF DATA SPACING OF PARAMETER ESTIMATION.'
    WRITE(1,*)'DO YOU WISH TO DO THIS, (Y/N)? '
    READ(1, '(A1)') IMORE
    CALL IYESNO(IMORE)
    IF(IMORE.EQ.'N') THEN
        TM01 = TM1
        DT1 = DT
        DT2 = DT

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ELSE IF(IMORE.EQ.'Y') THEN
2311   CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE FIRST TIME STEP, DT1, (SEC.). '
      READ(1,*,ERR=2311) DT1
2312   CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE SECOND TIME STEP, DT2, (SEC.) '
      READ(1,*,ERR=2312) DT2
2313   CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE INTERMEDIATE TIME LIMIT, TM01, '
      WRITE(1,*)'(SEC.) FOR THE FIRST TIME INTERVAL. (TM01 '
      WRITE(1,*)'TO TM1 IS ASSUMED TO BE THE SECOND TIME '
      WRITE(1,*)'INTERVAL.)'
      READ(1,*,ERR=2313) TM01
ENDIF
C
2319   CONTINUE
      IF(IMICCEN.EQ.1) XMICCEN = 'MICRONS'
      IF(IMICCEN.EQ.2) XMICCEN = 'CENTIMETERS'
      WRITE(1,*)
      WRITE(1,2320) PTRU,RINIT,XMICCEN,DR,XMICCEN,DT1,DT2,TM01
2320   FORMAT(1X,'THE VALUES ENTERED FOR THE PSEUDO-EXPERIMENTAL'
      , ' OPTION ARE:',/,
      . 1X,'1) PSEUDO-PERMEABILITY = ',F8.1,' MICRONS/SEC.',/,
      . 1X,'2) INITIAL CELL RADIUS = ',E11.3,1X,A11,/,
      . 1X,'3) RADIUS RANDOMNESS = ',E11.4,1X,A11,/,
      . 1X,'4) FIRST TIME STEP = ',F7.2,' SEC.',/,
      . 1X,'5) SECOND TIME STEP = ',F7.2,' SEC.',/,
      . 1X,'6) INTERMEDIATE TIME LIMIT = ',F8.1,' SEC.',/)
      WRITE(1,*)'DO YOU WISH TO CHANGE ANY OF THEM, (Y/N)?'
      READ(1,'(A1)') ICHANG
      CALL IYESNO(ICHANG)
      IF(ICHANG.EQ.'Y') THEN
2330   CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE NUMBER BESIDE THE PARAMETER'
      WRITE(1,*)'YOU WISH TO CHANGE, (1-5). '
      READ(1,*,ERR=2330) NCHANG
2340   CONTINUE
      WRITE(1,*)
      WRITE(1,*)'PLEASE ENTER THE NEW VALUE. '
      IF(NCHANG.EQ.1) THEN
          READ(1,*,ERR=2340) PTRU
      ELSE IF(NCHANG.EQ.2) THEN
          READ(1,*,ERR=2340) RINIT
      ELSE IF(NCHANG.EQ.3) THEN
          READ(1,*,ERR=2340) DR
      ELSE IF(NCHANG.EQ.4) THEN
          READ(1,*,ERR=2340) DT1
      ELSE IF(NCHANG.EQ.5) THEN

```

```

        READ(1,*,ERR=2340) DT2
    ELSE IF(NCHANG.EQ.6) THEN
        READ(1,*,ERR=2340) TM01
    ELSE IF(NCHANG.LE.0.OR.NCHANG.GE.7) THEN
        CALL INCORRES
        GO TO 2330
    ENDIF
    GO TO 2319
ENDIF
ENDIF
C
2341 CONTINUE
    IF(IRUNAG.EQ.0) THEN
        IF1 = 0
        IF2 = 0
        IF3 = 0
        IF4 = 0
        CAB0 = 0.0
        CAB1 = 5.0
        SEN0 = -0.1
        SEN1 = 0.0
        SUM0 = 0.0
        SUM1 = 100.0
    ELSE IF(IRUNAG.GT.0) THEN
        WRITE(1,*)
        WRITE(1,*)'DO YOU WISH TO CHANGE ANY OF THE LIMITS OF THE'
        WRITE(1,*)'GRAPHICAL OPTIONS YOU HAVE CHOOSSEN AND/OR '
        WRITE(1,*)'WOULD YOU LIKE TO CHOOSE ANOTHER OPTION, (Y/N)?'
        READ(1,'(A1)') ICHANG
        CALL IYESNO(ICHANG)
        IF(ICHANG.EQ.'N') GO TO 3999
        IF(ICHANG.EQ.'Y') THEN
            WRITE(1,*)
            WRITE(1,*)'THE PROGRAM WILL NOW ALLOW TO CHANGE OR '
            WRITE(1,*)'CHOOSE ANOTHER OPTION BY SELECTING ONE'
            WRITE(1,*)'OF THE FOLLOWING OPTIONS.'
            GO TO 2345
        ENDIF
    ENDIF
    WRITE(1,*)'DO YOU WISH TO VIEW THE OUTPUT IN GRAPHICAL '
    WRITE(1,*)'FORM, (Y/N)?'
    READ(1,'(A1)') IGRAPH
    CALL IYESNO(IGRAPH)
    IF(IGRAPH.EQ.'Y') THEN
2345 CONTINUE
        WRITE(1,*)
        WRITE(1,*)'THE OUTPUT CAN BE VIEWED IN THE FOLLOWING WAYS:'
        WRITE(1,*)
        WRITE(1,*)'1) CONCENTRATION V.S. DIMENSIONLESS TIME'
        WRITE(1,*)'2) SENSITIVITY COEFFICIENT V.S. TIME'
        WRITE(1,*)'3) NORMALIZED VOLUME V.S. TIME'
        WRITE(1,*)'4) SUM OF ERRORS OF SQUARES V.S. PERMEABILITY'
    
```

```

WRITE(1,*)
IF(IRUNAG.EQ.0) THEN
    WRITE(1,*)'WHICH GRAPHICAL OPTION WOULD YOU LIKE (1-4),'
ELSE IF(IRUNAG.GT.0) THEN
    WRITE(1,*)'WHICH GRAPHICAL OPTION WOULD YOU LIKE TO'
    WRITE(1,*)'SELECT OR CHANGE LIMITS ON, (1-4)'
ENDIF
WRITE(1,*)'(PLEASE CHOOSE ONE GRAPH AT A TIME).'

```



```

        WRITE(1,*)
        WRITE(1,*)'DO YOU WISH TO CHOOSE ANOTHER GRAPH, (Y/N)? '
        READ(1,'(A1)') IANOTH
        CALL IYESNO(IANOTH)
        IF(IANOTH.EQ.'Y') GO TO 2345
    ENDIF
2400  CONTINUE
        WRITE(1,*)'HAVE YOU MADE ANY MISTAKES THAT YOU WOULD LIKE '
        WRITE(1,*)'ANOTHER CRACK AT ENTERING/CHANGING THE PARAMETERS '
        WRITE(1,*)'OR DATA AGAIN, (Y/N)?'
        READ(1,'(A1)') IMISTAK
        CALL IYESNO(IMISTAK)
        IF(IMISTAK.EQ.'Y') GO TO 2180
        WRITE(1,*)
        WRITE(1,*)'OKAY, THE PROGRAM IS NOW CRUNCHING.'
        GO TO 3999
C-----
C      OPTION ITERINP = 2: ENTERING THE INPUT FILE
C-----
2999  CONTINUE
        OPEN(11,FILE=ISENS)
        READ(11,'(A11)') PROBLEM
        READ(11,3100) RL1,RL2,LIP
3100  FORMAT(///,1X,F11.6,F11.6,I2)
        READ(11,3110) D1,D2,H
3110  FORMAT(//,1X,E11.2,E11.2,E11.2)
        READ(11,3120) CINIT, CINF
3120  FORMAT(//,1X,F11.6,F11.6)
        READ(11,3125) VINA,RMAG
3125  FORMAT(//,1X,E11.6,E11.6)
        READ(11,3130) DT,TM0,TM1,DELAY
3130  FORMAT(//,1X,F11.6,F11.6,F11.6,F11.6)
        READ(11,3140) DP,PSEN
3140  FORMAT(//,1X,F11.6,F11.6)
        READ(11,3145) RINIT
3145  FORMAT(//,1X,F11.6)
        READ(11,3150) PTRU,DR,TM01,DT1,DT2
3150  FORMAT(///,1X,F11.6,F11.6,F11.6,F11.6,F10.6)
        READ(11,3160) IRELPSE,IMICCEN
3160  FORMAT(///,1X,I9,I9)
        READ(11,3170) IF1,IF2,IF3,IF4,IPRINT
3170  FORMAT(///,1X,I11,I11,I11,I11,I2,/)
        READ(11,3180) CAB0,CAB1
3180  FORMAT(//,1X,F11.6,F11.6)
        READ(11,3180) SEN0,SEN1
        READ(11,3180) VOLO,VOL1
        READ(11,3190) P0,P1,SUM0,SUM1
3190  FORMAT(//,1X,F11.6,F11.6,F11.6,F11.6,///)
C
        IF(IMICCEN.EQ.1) XMICCEN='MICRONS'
        IF(IMICCEN.EQ.2) XMICCEN='CENTIMETERS'
C

```

```

C-----
C   WRITING THE INPUT DATA TO THE OUTPUT FILE O_SENS.DAT'
C-----
      WRITE(1,3195) ISENS
3195  FORMAT(/,' THE INPUT FILE ',A10,' HAS BEEN ENTERED.')
```

```

3999  CONTINUE
      OPEN(10,FILE='O_SENS.DAT')
      WRITE(10,4000) ISENS
4000  FORMAT(1X,'***** THE INPUT FILE ',A10,
.      '*****',/)
      WRITE(10,4005)
4005  FORMAT(/,'RL1,RL2,LIP ARE',/)
      WRITE(10,*) RL1,RL2,LIP
      WRITE(10,4010)
4010  FORMAT(/,'D1,D2,H ARE',/)
      WRITE(10,*) D1, D2, H
      WRITE(10,4020)
4020  FORMAT(/,'CINIT,CINF, ARE:',/)
      WRITE(10,*) CINIT,CINF
      WRITE(10,4030)
4030  FORMAT(/,'VINA,RMAG ARE:',/)
      WRITE(10,*) VINA,RMAG
      WRITE(10,4040)
4040  FORMAT(/,'DT,TM0,TM1,DELAY ARE:',/)
      WRITE(10,*) DT,TM0,TM1,DELAY
      WRITE(10,4050)
4050  FORMAT(/,'DP,PSEN ARE:',/)
      WRITE(10,*) DP, PSEN
      WRITE(10,4060)
4060  FORMAT(/,'RINIT IS:',/)
      WRITE(10,*) RINIT
      WRITE(10,4070)
4070  FORMAT(/,'PTRU,DR,TM01,DT1,DT2 ARE:',/)
      WRITE(10,*) PTRU,DR,TM01,DT1,DT2
      WRITE(10,4080)
4080  FORMAT(/,'IRELPSE,IMICCEN ARE:',/)
      WRITE(10,*) IRELPSE, IMICCEN
      WRITE(10,4090)
4090  FORMAT(/,'IF1,IF2,IF3,IF4,IPRINT ARE:',/)
      WRITE(10,*) IF1,IF2,IF3,IF4,IPRINT
      WRITE(10,4100)
4100  FORMAT(/,'CAB0,CAB1 ARE:',/)
      WRITE(10,*) CAB0, CAB1
      WRITE(10,4110)
4110  FORMAT(/,'SEN0,SEN1 ARE:',/)
      WRITE(10,*) SEN0,SEN1
      WRITE(10,4120)
4120  FORMAT(/,'VOLO,VOL1 ARE:',/)
      WRITE(10,*) VOLO,VOL1
      WRITE(10,4130)
4130  FORMAT(/,'P0,P1,SUM0,SUM1 ARE:',/)
      WRITE(10,*) P0,P1,SUM0,SUM1

```

```

C
C-----
C      USING SUBROUTINE MBCON TO PREDICT THE CONCENTRATION CHANGE
C      INSIDE THE CELL CHAMBER
C-----
C      CALL MBCON(IOPNAG)
C-----
C      INITIALIZATION OF THE TIME VARIABLES AND RINIT
C-----
C      IT=INT((TM1-TM0)/DT)+1
C      DO 100 I=1, IT
C          TMS(I)=TM0+(I-1)*DT
C          TMB(I)=TMS(I)
100    CONTINUE
C      IF(IMICCEN.EQ.1) THEN
C          RINIT = RINIT/RMAG
C      ELSE IF(IMICCEN.EQ.2) THEN
C          RINIT = RINIT*10000./RMAG
C      ENDIF
C-----
C      CALCULATE R(TM,P) AND R(TM,P+DP)
C-----
C      CALL RGKT(TMS,RS,IT,DT,RINIT,PSEN)
C      CALL RGKT(TMB,RB,IT,DT,RINIT,PSEN+EPI*PSEN)
C-----
C      CALCULATE SENSITIVITY COEFF. (SEN)
C-----
C      WRITE(10,4175)
4175  FORMAT(/,1X,'***** DIMENSIONLESS SENSIVITY ',
.      'COEFFICIENT VERSUS TIME *****')
C      WRITE(10,4180)
4180  FORMAT(/,6X,'TIME(I)',7X,'SEN(I)',/)
C      DO 4190 J=1, IT
C          SEN(J)=(RB(J)-RS(J))*PSEN/RINIT/(EPI*PSEN)
C          WRITE(10,*)TMS(J),SEN(J)
4190  CONTINUE
C-----
C      PLOTTING SENSITIVITY VERSUS TIME (IF2=0 STOP THE OUTPUT)
C-----
C      IF(IF2.EQ.0)GO TO 4230
C      CALL NEWPAG
C      CALL PLOT(TM0,TM1,10,SEN0,SEN1,10,TMS,SEN,IT,FCT0,5,2)
C      CALL ANMODE
C      CALL HOME
C      WRITE(1,*)
C      WRITE(1,*)'PRESS [RETURN] TO CONTINUE.'
C      READ(1,'(A1)') IMORE
4230  CONTINUE
C      WRITE(10,*)
C      WRITE(10,4235)
4235  FORMAT(1X,'***** RADIUS VERSUS TIME',
.      '*****')

```

```

C-----
C   READING THE EXPERIMENTAL DATA AND CONVERTING TO MICRONS
C-----
      IF (IRELPSE.EQ.1.AND.ITERINP.EQ.2) THEN
        I=0
        WRITE(10,4240)
4240      FORMAT(/,6X,'TM(I)',10X,'R(I)',/)
4250      I=I+1
        READ(11,*)TMA(I),RA(I)
        RSAVE(I) = RA(I)
        IF(RA(I).GT.0.) TMA(I) = TMA(I)-DELAY
        WRITE(10,4253)TMA(I),RA(I)
        IF(IMICCEN.EQ.1) THEN
          RA(I) = RA(I)/RMAG
        ELSE IF(IMICCEN.EQ.2) THEN
          RA(I) = RA(I)*10000./RMAG
        ENDIF
        IF(I.EQ.1) RAMAX = RA(I)
        IF(I.GE.2) THEN
          IF(RA(I).GT.RAMAX) RAMAX = RA(I)
        ENDIF
        IF ((TMA(I).GT.0.).OR.(RA(I).GT.0.)) GO TO 4250
        ICOUNT=I-1
        IF (TM1.LE.TMA(ICOUNT)) THEN
          WRITE(1,*)
          WRITE(1,*)'PLEASE MAKE SURE TM1 IS LARGER THAN THE TIME'
          WRITE(1,*)'OF THE LAST DATA POINT, AND RUN IT AGAIN.'
          GO TO 6000
        END IF
      ELSE IF(IRELPSE.EQ.1.AND.ITERINP.EQ.1) THEN
        WRITE(10,4240)
        DO 4255 K=1,ICOUNT+1
          RSAVE(K) = RA(K)
          WRITE(10,4253) TMA(K),RA(K)
4253      FORMAT(5X,F7.2,5X,E11.4)
4255      CONTINUE
        IF(IMICCEN.EQ.1)THEN
          DO 4260 K=1,ICOUNT
            RA(K) = RA(K)/RMAG
4260      CONTINUE
            RAMAX = RAMAX/RMAG
          ELSE IF(IMICCEN.EQ.2) THEN
            DO 4270 K=1,ICOUNT
              RA(K) = RA(K)*10000./RMAG
4270      CONTINUE
              RAMAX = RAMAX*10000./RMAG
            ENDIF
          C-----
          C   GENERATING THE SIMULATED (PSEUDO) EXPERIMENTAL DATA

```

C-----

```

      ELSE IF(IRELPSE.EQ.2) THEN
        ICOUNT = ((TM01-TM0)/DT1+(TM1-TM01)/DT2+1)
        CALL RGKT(TMS,RB,IT,DT,RINIT,PTRU)
        DO 4280 J=1,IT
          TMA(J) = TMS(J)
          RC(J) = RB(J)
4280      CONTINUE
          TMA(1)=TM0
          DO 4290 J=2,ICOUNT
            IF (TMA(J-1).LT.TM01) THEN
              TMA(J)=TMA(J-1)+DT1
            ELSE IF (TMA(J-1).GE.TM01) THEN
              TMA(J)=TMA(J-1)+DT2
            END IF
4290      CONTINUE
            IF(IMICCEN.EQ.1) THEN
              DR = DR/RMAG
            ELSE IF(IMICCEN.EQ.2) THEN
              DR = DR*10000./RMAG
            ENDIF
            RAMAXC = RC(1)
            DO 4292 J=2,IT
              IF(RC(J).GT.RAMAXC) RAMAXC = RC(J)
4292      CONTINUE
              RAMAX = RB(1)
              DO 4300 J=1,ICOUNT
                ITM=INT(TMA(J)/DT)+1
                IF (ITM.GE.IT) THEN
                  RA(J)=RB(ITM)+DR*RANND()
                ELSE
                  DRA=(RB(ITM+1)-RB(ITM))*(TMA(J)-(ITM-1)*DT)/DT
                  RA(J)=RB(ITM)+DRA+DR*RANND()
                END IF
                IF(RA(J).GT.RAMAX) RAMAX = RA(J)
4300      CONTINUE
                WRITE(10,*)
                WRITE(10,4301)
4301      FORMAT(/,1X,'***** SIMULATED RADIUS VERSUS TIME ',
                  '*****',/)
                DO 4302 J=1,ICOUNT+1
                  IF(IMICCEN.EQ.1) RSAVE(J)=RA(J)*RMAG
                  IF(IMICCEN.EQ.2) RSAVE(J)=RA(J)*RMAG/10000.
4302      CONTINUE
                  DO 4305 J=1,ICOUNT
                    WRITE(10,4253) TMA(J),RA(J)
4305      CONTINUE
                  END IF
C-----
C      CALCULATING THE NORMALIZED VOLUME
C-----
      DO 4315 I=1,ICOUNT

```

```

      VOLA(I)=(RA(I)/RAMAX)**3
4315  CONTINUE
      IF(IRELPSE.EQ.2) THEN
        DO 4316 J=1,IT
          VOLC(J) =(RC(J)/RAMAXC)**3
4316  CONTINUE
      ENDIF
C-----
C    CALCULATE SUM OF ERROR OF SQUARE FOR P VALUES FROM
C    P0 TO P1
C-----
      IP=(P1-P0)/DP+1
      DO 4330 I=1,IP
        P(I)=P0+(I-1)*DP
        CALL RGKT(TMB,RB,IT,DT,RINIT,P(I))
        SUM(I)=0.
        DO 4320 J=1,ICOUNT
          ITM=INT(TMA(J)/DT)+1
          IF (ITM.GE.IT) THEN
            RN=RB(ITM)
          ELSE
            DRN=(RB(ITM+1)-RB(ITM))*(TMA(J)-(ITM-1)*DT)/DT
            RN=RB(ITM)+DRN
          END IF
          SUM(I)=SUM(I)+(RN-RA(J))**2
4320  CONTINUE
4330  CONTINUE
C----
C
C----
      WRITE(10,4332)
4332  FORMAT(///,1X,'***** SUM OF SQUARES OF ERRORS ',
             'VERSUS PERMEABILITY *****')
      WRITE(10,4335)
4335  FORMAT(/,'      P(J)          SUM(J)',/)
      DO 4338 J=1,IP
        WRITE(10,4336) P(J),SUM(J)
4336  FORMAT(1X,F8.2,6X,E10.4)
4338  CONTINUE
C
      SUMIN=SUM(1)
      PEST = P(1)
      DO 4340 I=2,IP
        IF (SUMIN.GT.SUM(I)) THEN
          SUMIN=SUM(I)
          PEST=P(I)
        END IF
4340  CONTINUE
      CALL RGKT(TMB,RC,IT,DT,RINIT,PEST)
      CALL RGKT(TMB,RB,IT,DT,RINIT,PEST+EP1*PEST)
      DO 4350 J=1,IT
        SEN(J)=(RB(J)-RC(J))/(EP1*PEST)

```

```

4350  CONTINUE
      DO 4360 J=1, ICOUNT
        ITM=INT(TMA(J)/DT)+1
        IF (ITM.GE.IT) THEN
          SEN(J)=SEN(ITM)
        ELSE
          DSEN=(SEN(ITM+1)-SEN(ITM))*(TMA(J)-(ITM-1)*DT)/DT
          SEN(J)=SEN(ITM)+DSEN
        END IF
      DO 4360 CONTINUE
      SENSUM=0.
      DO 4365 I=1, ICOUNT
        SENSUM=SENSUM+SEN(I)**2
      4365  CONTINUE
      C----
      C  DUMPING SUMMARY INPUT PARAMETERS, INPUT DATA AND RESULTING
      C  PEST, SDP, SUMIN TO 'O_SMRY.DAT'
      C----
        OPEN(14,FILE='O_SMRY.DAT')
        WRITE(14,*)
        WRITE(14,4366)
      4366  FORMAT(/, '***** THIS IS FILE O_SMRY.DAT'
        .    ' *****', //)
        WRITE(14,4367)
      4367  FORMAT(/, 'THE INPUT PARAMETERS AND DATA WERE:', //)
        WRITE(14,2190)RL1,RL2,LIP,D2,D1,H,CINIT,CINF,VINA,RMAG
        WRITE(14,*)
        WRITE(14,2240)DT,TM0,TM1,DP,PO,P1,PSEN
        IF(IRELPS.EQ.1) THEN
          WRITE(14,*)
          WRITE(14,*)'THE DATA POINTS ENTERED WERE:'
          WRITE(14,2259) DELAY
          WRITE(14,*)
          WRITE(14,*)'  J          TIME(J)          RADIUS(J)'
          IF(IMICCEN.EQ.1) THEN
            WRITE(14,*)'              (SEC.)          (MICRONS)'
          ELSEIF(IMICCEN.EQ.2) THEN
            WRITE(14,*)'              (SEC.)          (CENTIMETERS)'
          ENDIF
          DO 4368 J=1, ICOUNT+1
            WRITE(14,2263) J,TMA(J),RA(J)
          4368  CONTINUE
        ELSE IF(IRELPS.EQ.2) THEN
          WRITE(14,*)
          WRITE(14,2320)PTRU,RINIT,XMICCEN,DR,XMICCEN,DT1,DT2,TM01
        ENDIF
      C
      C----
      C  THE ESTIMATED PERMEABILITY
      C----
        WRITE(10,4375)
        WRITE(14,4375)

```

```

4375  FORMAT(///,'***** THE RESULTING '
      'PERMEABILITY *****',/)
      SDP=SQRT(SUMIN/(ICOUNT-1)/SENSUM)
      WRITE(10,4380)PEST
      WRITE(14,4380)PEST
4380  FORMAT(/,'THE LOCAL MINIMUN OCCURS AT P =',F8.3,' MICRONS/SEC.')
      WRITE(10,4390)SDP
      WRITE(14,4390)SDP
4390  FORMAT(/,'THE STANDARD DEVIATION OF ESTIMATED P IS ',E8.3)
      WRITE(10,4395)SUMIN
      WRITE(14,4395)SUMIN
4395  FORMAT(/,'THE MINIMUM VALUE OF SUM IS',F8.3)
C
      CLOSE(14)
C
      IF(IRELPE.EQ.1) THEN
          DO 4396 J=1,IT
              IF(J.EQ.1) RAMAXC = RC(1)
              IF(J.GE.2.AND.RC(J).GT.RAMAXC) RAMAXC=RC(J)
4396      CONTINUE
          DO 4397 J=1,IT
              VOLC(J) = (RC(J)/RAMAXC)**3
4397      CONTINUE
      ENDIF
C
      IF(IF3.EQ.0) GO TO 4398
C-----
C      PLOTTING NORMALIZED VOLUME CHART (IF3=0 STOP THE OUTPUT)
C-----
      CALL NEWPAG
      CALL PLOT(TM0,TM1,10,VOL0,VOL1,10,TMA,VOLA,ICOUNT,FCT0,1,3)
      CALL PLOT(TM0,TM1,10,VOL0,VOL1,10,TMS,VOLC,IT,FCT0,5,3)
      CALL ANMODE
      CALL HOME
      WRITE(1,*)
      WRITE(1,*)'PRESS [RETURN] TO CONTINUE.'
      READ(1,'(A1)') IMORE
C
4398  CONTINUE
C
      IF(IF4.EQ.0)GO TO 6000
C-----
C      PLOTTING SUM OF SQUARE OF ERRORS (IF4=0 STOP THE OUTPUT)
C-----
      CALL NEWPAG
      CALL PLOT(P0,P1,10,SUM0,SUM1,10,P,SUM,IP,FCT0,5,4)
      CALL ANMODE
      CALL HOME
      WRITE(1,*)
      WRITE(1,*)'PRESS [RETURN] TO CONTINUE.'
      READ(1,'(A1)') IMORE
6000  CONTINUE

```



```

        WRITE(1,6100) PEST,SDP,SUMIN
6100  FORMAT(' ESTIMATED PERMEABILITY = ',F8.3,
        .      ' STANDARD DEVIATION = ',E8.3,
        .      ' MINIMUM SUM SQUARES = ',F8.3)
        WRITE(1,*)
        WRITE(1,*)'PRESS [RETURN] TO CONTINUE'
        READ(1,'(A1)') IMORE
C-----
C      RESETTING THE RA(I) = RSAVE(I) AND RINIT, RAMAX TO ORIGINAL VALUESS
C-----
        IF(IMICCEN.EQ.1) THEN
            RINIT = RINIT * RMAG
            RAMAX = RAMAX * RMAG
            IF(IRELPSE.EQ.2) DR = DR *RMAG
            DO 280 K = 1, ICOUNT+1
                RA(K) = RSAVE(K)
280      CONTINUE
        ELSE IF(IMICCEN.EQ.2) THEN
            RINIT = RINIT *RMAG/10000.
            RAMAX = RAMAX *RMAG/10000.
            IF(IRELPSE.EQ.2) DR = DR*RMAG/10000.
            DO 290 K=1,ICOUNT+1
                RA(K) = RSAVE(K)
290      CONTINUE
        ENDIF
C-----
C      OPTION TO SAVE INPUT FILE
C-----
        DELAY = 0.0
        WRITE(1,*)
        WRITE(1,*)'DO YOU WISH TO SAVE THE INPUT DATA IN A FILE,'
        WRITE(1,*)'(Y/N)?'
        READ(1,'(A1)') ISAVE
        CALL IYESNO(ISAVE)
        IF(ISAVE.EQ.'Y') THEN
320      CONTINUE
            WRITE(1,*)
            WRITE(1,*)'WHAT WOULD YOU LIKE TO NAME THIS FILE,'
            WRITE(1,*)'(ENTER NO MORE THAN 10 CHARATERS)?'
            READ(1,'(A10)',ERR=320) NAMFIL
            OPEN(12,FILE=NAMFIL)
            WRITE(12,325)
325      FORMAT(1X,'THIS IS THE FILE YOU HAD SAVED.  YOU CAN '
            .      'USE THIS FILE AS',/, ' AN INPUT FILE IF YOU DESIRE BY'
            .      ' ACCESSING THIS FILE',/, ' WHEN YOU ARE PROMPTED FOR'
            .      ' THE NAME OF AN INPUT FILE.')
331      CONTINUE
            WRITE(12,*)'RL1          RL2          LIP'
            WRITE(12,332) RL1,RL2,LIP
332      FORMAT(1X,F5.2,6X,F7.2,4X,I2,/)
            WRITE(12,*)'D1          D2          H'
            WRITE(12,333) D1,D2,H

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333     FORMAT(1X,E9.3,2X,E9.3,2X,E9.3,/)
      WRITE(12,*) 'CINIT      CINF'
      WRITE(12,334) CINIT,CINF
334     FORMAT(1X,F8.3,3X,F8.3,/)
      WRITE(12,*) 'VINA      RMAG'
      WRITE(12,335) VINA,RMAG
335     FORMAT(1X,F5.2,6X,F9.2,/)
      WRITE(12,*) 'DT      TMO      TM1      DELAY'
      WRITE(12,336) DT,TMO,TM1,DELAY
336     FORMAT(1X,F6.3,5X,F7.2,4X,F7.2,4X,F7.2,/)
      WRITE(12,*) 'DP      PSEN'
      WRITE(12,337) DP,PSEN
337     FORMAT(1X,F5.2,6X,F6.2,/)
      WRITE(12,*) 'RINIT'
      WRITE(12,338) RINIT
338     FORMAT(1X,E10.4,/)
      WRITE(12,339)
339     FORMAT(1X,'THE PARAMETERS FOR THE LINE BELOW ARE FOR ',
      . 'SIMULATION OPTION:')
      WRITE(12,*) 'PTRU      DR      TM01      DT1      DT2'
      WRITE(12,340) PTRU,DR,TM01,DT1,DT2
340     FORMAT(1X,F6.2,5X,F7.3,4X,F7.2,4X,F6.3,5X,F6.3,/)
      WRITE(12,341)
341     FORMAT(1X,'THESE PARAMETERS BELOW ARE FOR DATA INPUT ',
      . 'CONTROL:')
      WRITE(12,*) 'IRELPSE      IMICCEN'
      WRITE(12,342) IRELPSE, IMICCEN
342     FORMAT(2X,I1,9X,I1,/)
      WRITE(12,*) 'THESE PARAMETERS ARE FOR DATA OUTPUT CONTROL:'
      WRITE(12,*) 'IF1      IF2      IF3      IF4      IPRINT'
      WRITE(12,345) IF1,IF2,IF3,IF4,IPRINT
345     FORMAT(1X,I1,10X,I1,10X,I1,10X,I1,10X,I2,/)
      WRITE(12,346)
346     FORMAT(1X,'THESE PARAMETERS ARE FOR GRAPHICAL OUTPUT ',
      . 'CONTROL:')
      WRITE(12,*) 'CAB0      CAB1'
      WRITE(12,347) CAB0,CAB1
347     FORMAT(1X,F5.2,6X,F7.2,/)
      WRITE(12,*) 'SENO      SEN1'
      WRITE(12,347) SEN0, SEN1
      WRITE(12,*) 'VOLO      VOL1'
      WRITE(12,347) VOLO,VOL1
      WRITE(12,*) 'P0      P1      SUM0      SUM1'
      WRITE(12,348) P0,P1,SUM0,SUM1
348     FORMAT(1X,F6.2,5X,F6.2,5X,F5.2,6X,F6.2,5X,/)
      WRITE(12,349)
349     FORMAT(1X,'THE LAST GROUP BELOW IS THE DATA POINTS:')
      WRITE(12,*) ' TMA(I)      RA(I)'
      DO 360 I =1,ICOUNT
          WRITE(12,350) TMA(I), RA(I)
350         FORMAT(1X,F9.4,5X,F7.2)
360     CONTINUE

```

```

        WRITE(12,*)'  0.0          0.0'
        CLOSE(12)
        IF(IQUIT.EQ.'Y') GO TO 600
        WRITE(1,362) NAMFIL
362      FORMAT('OKAY, THE FILE ',A10,' HAS BEEN SAVED.')
        ENDIF
        CLOSE(11)
C-----
C      OPTION TO RUN THE PROGRAM AGAIN
C-----
        WRITE(1,*)
        WRITE(1,*)'DO YOU WISH TO RUN THE PROGRAM AGAIN, (Y/N)?'
        READ(1,'(A1)') IAGAIN
        CALL IYESNO(IAGAIN)
        IOPNAG = IOPNAG + 1
        IF(IAGAIN.EQ.'Y') THEN
500      CONTINUE
C-----
C      OPTION TO ENTER NEW DATA OR REVIEW OLD DATA
C-----
        WRITE(1,*)
        WRITE(1,*)'DO YOU WISH TO (1) ENTER ALL NEW DATA OR '
        WRITE(1,*)'(2) USE AND REVIEW THE DATA ALREADY ENTERED,'
        WRITE(1,*)'(ENTER 1 OR 2)?'
        READ(1,*,ERR=500) INEWREV
        CALL IONETWO(INEWREV)
        DELAY = 0.0
        IBACK = 0
        IF(INEWREV.EQ.1) THEN
            IRUNAG = 0
            GO TO 2000
        ELSE IF(INEWREV.EQ.2) THEN
            ITERINP = 1
            IRUNAG = IRUNAG + 1
            GO TO 2180
        ENDIF
    ENDIF
ENDIF
C-----
C      STOPPING THE PROGRAM
C-----
600      WRITE(1,*)
        WRITE(1,*)'OKAY, PROGRAM DONE.'
        CALL CLOSTK(I)
        CLOSE(10)
        CALL EXIT
    END
C-----
C      SUBROUTINE RGKT(X,Y,N,DX,Y0,P)
C
C      USE RUNGE-KUTTA METHOD TO SOLVE ORDINARY DIFFERENTIAL
C      EQUATION
C

```

```

C      X: INDEPENDENT VARIABLE
C
C      Y: DEPENDENT VARIABLE
C
C      N: DIMENSION OF X(N) AND Y(N)
C
C      DX: INCREMENT OF X
C
C      YO: INITIAL CONDITION OF Y
C
C      P: PARAMETER
C
C      F: THE SUPPLIED FUNCTION. (DY/DX=F(X,Y))
C-----
      SUBROUTINE RGKT(X,Y,N,DX,YO,P)
      DIMENSION X(N),Y(N)
      Y(1)=YO
      DO 1 I=1,N-1
        RK1=DX*F(X(I),Y(I),P)
        RK2=DX*F(X(I)+DX/2.,Y(I)+RK1/2.,P)
        RK3=DX*F(X(I)+DX/2.,Y(I)+RK2/2.,P)
        RK4=DX*F(X(I)+DX,Y(I)+RK3,P)
        Y(I+1)=Y(I)+(RK1+2*RK2+2*RK3+RK4)/6.
1      CONTINUE
      RETURN
      END
C-----
C      FUNCTION F(X,Y,Z)
C
C      X: INDEPENDENT VARIABLE
C
C      Y: DEPENDENT VARIABLE
C
C      Z: PARAMETER
C-----
      FUNCTION F(X,Y,Z)
      PARAMETER N4=301,PI=3.14159
      COMMON /C2/RINIT,VINA,DT,TM1,COUT(N4)
      COMMON /C3/RL1,RL2,LIP,D1,D2,CINIT,CINF,H
      V=0.018
      I=INT(X/DT)+1
      CO=COUT(I)+(COUT(I+1)-COUT(I))*(X-(I-1)*DT)/DT
      VO=4.*PI*RINIT**3/3.
      VIN=VINA*VO/100.
      F=-Z*V*(CO-CINIT*(VO-VIN))/(4.*PI*Y**3/3.-VIN)
      RETURN
      END
C-----
C      FUNCTION RANND()
C
C      RANDOM VARIABLE GENERATOR
C      NORMAL DISTRIBUTION WITH STANDARD DEVIATION EQUAL TO 1.

```

C-----

```

      FUNCTION RANND()
      DOUBLE PRECISION RANDOM
      R=RANDOM()
      A0=2.30753
      A1=0.27061
      B1=0.99299
      B2=0.04481
      IF (R-0.5) 10,10,20
10    AK=1.
      GO TO 30
20    AK=-1.
      R=R-0.5
30    T=SQRT(ALOG(1./(R*R)))
      E=T-(A0+A1*T)/(1.+B1*T+B2*T*T)
      RANND=AK*E
      RETURN
      END

```

C

```

      SUBROUTINE IONETWO(ITEST)
10    CONTINUE
      IF(ITEST.LE.0.OR.ITEST.GE.3) THEN
          WRITE(1,*)
          WRITE(1,*) '** INCORRECT RESPONSE **'
          WRITE(1,*) 'PLEASE ENTER 1 OR 2'
          WRITE(1,*)
          READ(1,*) ITEST
          GO TO 10
      ENDIF
      RETURN
      END

```

C

```

      SUBROUTINE IYESNO(ITEST)
      CHARACTER *1 ITEST
10    CONTINUE
      IF(ITEST.NE.'Y'.AND.ITEST.NE.'N') THEN
          WRITE(1,*)
          WRITE(1,*) '** INCORRECT RESPONSE **'
          WRITE(1,*) 'PLEASE ENTER "Y" OR "N"'
          WRITE(1,*)
          READ(1,'(A1)') ITEST
          GO TO 10
      ENDIF
      RETURN
      END

```

C

```

      SUBROUTINE CHANLIM(Z0,Z1)
      CHARACTER *1 ICHANGE
10    CONTINUE
      WRITE(1,*)
      WRITE(1,*) 'THE VALUES ENTERED ARE: '
      WRITE(1,*)

```

```

WRITE(1,*) Z0, Z1
WRITE(1,*)
WRITE(1,*)' DO YOU WISH TO CHANGE THEM,(Y/N)? '
READ(1,'(A1)') ICHANG
CALL IYESNO(ICHANG)
IF(ICHANG.EQ.'Y') THEN
  WRITE(1,*)
20  CONTINUE
  WRITE(1,*)'PLEASE ENTER THE NEW VALUES. '
  WRITE(1,*)
  READ(1,*,ERR=20) Z0,Z1
  GO TO 10
ENDIF
RETURN
END
SUBROUTINE INCORRES
WRITE(1,*)
WRITE(1,*)'**  INCORRECT RESPONSE  **'
RETURN
END
C
SUBROUTINE CHANNAM(FILNAM)
CHARACTER*1 ICHANG
CHARACTER*10 FILNAM
33  CONTINUE
  WRITE(1,*)
  WRITE(1,35) FILNAM
35  FORMAT(1X,'THE FILE NAME ENTERED IS ',A10)
  WRITE(1,*)
  WRITE(1,*)'DO YOU WISH TO CHANGE IT, (Y/N)?'
  READ(1,'(A1)') ICHANG
  CALL IYESNO(ICHANG)
  IF(ICHANG.EQ.'Y') THEN
    WRITE(1,*)
36  CONTINUE
    WRITE(1,*)'PLEASE ENTER THE NEW NAME. '
    WRITE(1,*)
    READ(1,'(A10)',ERR=36) FILNAM
    GO TO 33
  ENDIF
RETURN
END

```

```

      SUBROUTINE MBCON(IOPNAG)
C-----
C      JOB: 1. PREDICT THE CONCENTRATION CHANGE INSIDE THE CELL
C            CHAMBER
C            2. PLOTTING CONCENTRATION VERSUS TIME CHART
C-----
      PARAMETER (N1=4,N2=6,II=2,N4=301)
      REAL L1,L2,M
      CHARACTER*1 ICONT
      DIMENSION CN(N1+N2+1),CO(N1+N2+1),CE(N1+N2+1,N1+N2+1),
&              W(N1+N2+2,N1+N2+2),CONC(N1+N2+1),CA(25),CB(25),
&              DC(25),TM(25),X(II,II),Y1(II),Y2(II),W1(II+1,II+1)
      COMMON /C1/IPRINT,IF1,A1(II),A2(II),CAB0,CAB1
      COMMON /C2/RINIT,VINA,DT,TM1,COUT(N4)
      COMMON /C3/RL1,RL2,LIP,D1,D2,CINIT,CINF,H
      EXTERNAL FCT1,FCT2
C-----
C      INITIALIZATION
C-----
      L1=RL1*1.0E-6
      L2=RL2*1.0E-6
      TMAX=TM1
      DX1=L1/N1
      DX2=L2/N2
      RX=DX2/DX1
      P1=DT*D1/DX1/DX1
      P2=DT*D2/DX2/DX2
      B1=H*DX1/D1
      M=2./(1+RX)
      DO 1 I=1,N1+N2+1
        CN(I)=0.
        CO(I)=0.
        DO 1 J=1,N1+N2+1
          CE(I,J)=0.
1      CONTINUE
      ICOUNT=0
C-----
C      USING THE BACKWARD DIFFERENCE METHOD TO CALCULATE THE
C      CONCENTRATION INSIDE THE CELL CHAMBER
C-----
      WRITE(10,151)
151  FORMAT(///,1X,'***** THE CONCENTRATION',
.      ' HISTORY *****')
C-----
C      INPUT VALUES TO THE COEFFICIENT MATRIX
C-----
      CE(1,1)=1+2*P1+2*P1*B1
      CE(1,2)=-2*P1
      DO 2 I=2,N1
        CE(I,I-1)=-P1
        CE(I,I)=1+2*P1
        CE(I,I+1)=-P1

```

```

2      CONTINUE
      CE(N1+1,N1)--P1*M
      CE(N1+1,N1+1)=1+P1*M+P1*M*(D2/D1)/RX
      CE(N1+1,N1+2)--P1*M*(D2/D1)/RX
      DO 3 I=N1+2,N1+N2
          CE(I,I-1)--P2
          CE(I,I)=1+2*P2
          CE(I,I+1)--P2
3      CONTINUE
      CE(N1+N2+1,N1+N2)--2*P2
      CE(N1+N2+1,N1+N2+1)=1+2*P2
6      CO(1)=CO(1)+2*B1*P1
C-----
C      CALCULATE THE COEFFICIENT MATRIX
C-----
      CALL LINEQ(CN,CO,CE,W,N1+N2+1,N1+N2+2,I)
C-----
C      PUT CN INTO CO FOR NEXT CALCULATION
C-----
      ICOUNT=ICOUNT+1
      DO 4 I=1,N1+N2+1
          CO(I)=CN(I)
4      CONTINUE
      COUT(ICOUNT)=CN(LIP)*(CINF-CINIT)+CINIT
C      COUT(ICOUNT)=CINF+(CINIT-CINF)*EXP(-(ICOUNT-1)*DT/19.6)
C-----
C      CHECK TO SEE WHETHER IT IS TIME TO OUTPUT THE DATA
C-----
      IF (ICOUNT/IPRINT*IPRINT.EQ.ICOUNT) THEN
101      WRITE(10,101)ICOUNT*DT
          FORMAT(/,'CONCENTRATION DIST. AT TIME-',F10.4,'SEC. IS',/)
          DO 5 I=1,N1+N2+1
              CONC(I)=CN(I)*(CINF-CINIT)+CINIT
5      CONTINUE
      WRITE(10,*)
      WRITE(10,*)'      DIALYSIS MEMBRANE          CELL CHAMBER'
      WRITE(10,*)'|          |          |          |'
      WRITE(10,*)'|B          |          |          |'
      WRITE(10,*)'|U          |          |          |'
      WRITE(10,*)'|L          |          |          |'
      WRITE(10,*)'|K          |          |          |'
      WRITE(10,*)'|          |          |          |'
      WRITE(10,*)'| 1          3          5          7          9          11'
201      WRITE(10,201) CONC(1),CONC(3),CONC(5),CONC(7),CONC(9),CONC(11)
          FORMAT(1X,E9.3,1X,E9.3,1X,E9.3,1X,E9.3,1X,E9.3,1X,E9.3)
      WRITE(10,*)'|          |          |          |'
      WRITE(10,*)'| 2          4          | 6          8          10 |'
202      WRITE(10,202) CONC(2),CONC(4),CONC(6),CONC(8),CONC(10)
          FORMAT(3X,E9.3,2X,E9.3,1X,E9.3,1X,E9.3,1X,E9.3)
      WRITE(10,*)'|F          |          |          |'
      WRITE(10,*)'|L          |          |          |'
      WRITE(10,*)'|O          |          |          |'

```



```

WRITE(10,*) 'W |
WRITE(10,*)
WRITE(10,*)
      IP=ICOUNT/IPRINT
      IF (CN(N1+1).GE.1.) CN(N1+1)=1.-1.E-6
      IF (CN(N1+N2+1).GE.1.) CN(N1+N2+1)=1.-1.E-6
      CA(IP)=-LOG(1-CN(N1+1))
      CB(IP)=-LOG(1-CN(N1+N2+1))
      DC(IP)=CONC(N1+1)-CONC(N1+N2+1)
      TM(IP)=ICOUNT*DT/TMAX
END IF
C-----
C      CHECK TO SEE WHETHER IT IS TIME TO STOP THE EXECUTION
C-----
      IF (ICOUNT*DT.LT.TMAX+DT) GO TO 6
C-----
C      FINDING THE BEST LINEAR FIT FOR THE CONCENTRATION VERSUS
C      TIME POINTS
C-----
      DO 10 I=1,2
        X(I,2)=0.
        Y1(I)=0.
        Y2(I)=0.
10    CONTINUE
      DO 11 I=1,IP
        X(1,2)=X(1,2)+TM(I)
        X(2,2)=X(2,2)+TM(I)**2
        Y1(1)=Y1(1)+CA(I)
        Y1(2)=Y1(2)+CA(I)*TM(I)
        Y2(1)=Y2(1)+CB(I)
        Y2(2)=Y2(2)+CB(I)*TM(I)
11    CONTINUE
      X(2,1)=X(1,2)
      X(1,1)=IP
      CALL LINEQ(A1,Y1,X,W1,2,3,I)
      CALL LINEQ(A2,Y2,X,W1,2,3,I)
      WRITE(10,103)A1(1),A1(2)
103  FORMAT(/,' THE EQUATION FOR THE LINEAR BEST FIT FOR THE',/,
.      ' CONCENTRATION VERSUS TIME IS',/,
.      ' Y = ',F6.3,' + ',F6.3,' *X',/)
      WRITE(10,103)A2(1),A2(2)
      IF(IOPNAG.EQ.0) CALL PLOTINIT
      IF (IF1.EQ.0) GO TO 12
C-----
C      PLOTTING THE CONCENTRATION VERSUS TIME CHART
C      (IF1=0 STOP THE OUTPUT)
C-----
      CALL PLOT(0.,1.,10,CAB0,CAB1,10,TM,CA,IP,FCT1,1,1)
      CALL PLOT(0.,1.,10,CAB0,CAB1,10,TM,CB,IP,FCT2,2,0)
      CALL ANMODE
      CALL HOME
      WRITE(1,*)

```

```

        WRITE(1,*)'PRESS [RETURN] TO CONTINUE.'
        READ(1,'(A1)') ICONT
12      RETURN
        END
C-----
C      FUNCTIONS FOR THE INPUT OF THE SUBROUTINE 'PLOT'
C-----
        FUNCTION FCT1(X)
        PARAMETER II=2
        COMMON /C1/IPRINT,IF1,A1(II),A2(II),CAB0,CAB1
        FCT1=A1(1)+A1(2)*X
        RETURN
        END
        FUNCTION FCT2(X)
        PARAMETER II=2
        COMMON /C1/IPRINT,IF1,A1(II),A2(II),CAB0,CAB1
        FCT2=A2(1)+A2(2)*X
        RETURN
        END

```

```

C-----
C   OPEN THE GRAPHIC FILE
C-----
C   SUBROUTINE PLOTINIT
C   CALL INITT(480)
C   CALL OPENTK('G_PLOT',I)
C   RETURN
C   END
C-----
C   SUBROUTINE PLOT(X0,X1,NX,Y0,Y1,NY,X,Y,N,FCT,IMARK,IFX)
C
C   THIS SUBROUTINE PLOT THE GRAPH WITH WINDOW X0,X1,Y0,Y1.
C
C   X0, X1: RANGE ON X-AXIS
C
C   Y0, Y1: RANGE ON Y-AXIS
C
C   NX: NUMBER OF SCALE MARK ON X-AXIS
C
C   NY: NUMBER OF SCALE MARK ON Y-AXIS
C
C   X, Y: THE SUPPLIED DATA POINTS TO BE PLOTTED ON THE GRAPH
C
C   N: TOTAL NUMBER OF DATA POINTS
C
C   FCT: SUPPLIED FUNCTION TO COMPARE WITH THE DATA POINTS
C        (MIGHT BE THE EXACT SOLUTION CURVE)
C
C   IMARK: SELECT THE KIND OF SYMBOL TO MARK THE DATA POINTS.
C
C           1. SQUARE
C           2. TRIANGLE (POINTS UPWARD)
C           3. TRIANGLE (POINTS DOWNWARD)
C           4. DIAMAND SHAPE
C           5. CONTINUOUS CURVE
C
C   IFX: GRAPH TO BE PLOTTED.
C
C           1. CONCENTRATION V.S. DIMENSIONLESS TIME
C           2. SENSITIVITY COEFFICIENT V.S. TIME
C           3. NORMALIZED VOLUME V.S. TIME
C           4. SUM OF THE SQUARES OF THE ERRORS V.S. PERMEABILITY
C
C-----
C   SUBROUTINE PLOT(X0,X1,NX,Y0,Y1,NY,X,Y,N,FCT,IMARK,IFX)
C   PARAMETER IN=1,EP1=1E-15
C   DIMENSION X(N),Y(N)
C   CHARACTER*10 LABEL(2,21)
C   CHARACTER*24 YTITLE
C   CHARACTER*1 A
C   RNX=NX
C   RNY=NY

```

```

      RGX=X1-X0
      RGY=Y1-Y0
      IF (ABS(RGX).LT.EP1.OR.ABS(RGY).LT.EP1) THEN
        WRITE(1,102)
102      FORMAT(/,'THE SIZE OF THE WINDOW IS ZERO',/)
        GO TO 11
      END IF
      CALL DWINDO(0.5*(X1+X0)-RGX,0.5*(X1+X0)+RGX,0.5*(Y1+Y0)
      &-RGY,0.5*(Y1+Y0)+RGY)
C-----
C      DRAW HORIZONTAL AND VERTICAL GRID TICKS
C
C      NOTICE TYPE CONVERSION IN THE STATEMENTS INVOLVING
C      RNX AND RNY
C-----
      CALL MOVEA(X0,Y0)
      CALL DRAWA(X1,Y0)
      DO 1 I=2,NX+1
        P=(I-1.)*RGX/RNX+X0
        CALL MOVEA(P,Y0)
        CALL DRAWA(P,Y0+RGY/20)
1      CONTINUE
      CALL MOVEA(X0,Y0)
      CALL DRAWA(X0,Y1)
      DO 2 I=2,NY+1
        Q=(I-1.)*RGY/RNY+Y0
        CALL MOVEA(X0,Q)
        CALL DRAWA(X0+RGX/20,Q)
2      CONTINUE
C-----
C      WRITING CHARACTERS
C-----
      DO 3 I=1,NX+1,2
        P=(I-1.)*RGX/RNX+X0-RGX/15.
        Q=(I-1.)*RGX/RNX+X0
        CALL MOVEA(P,Y0-RGY/9.)
        WRITE(LABEL(1,I),101) Q
        CALL CHARTK(LABEL(1,I),0.7)
3      CONTINUE
      DO 4 I=1,NY+1,2
        P=(I-1.)*RGY/RNY+Y0
        CALL MOVEA(X0-RGX/6.,P)
        WRITE(LABEL(2,I),101) P
101     FORMAT(E8.2)
        CALL CHARTK(LABEL(2,I),0.7)
4      CONTINUE
C
C-----
C      LABELLING THE AXES
C-----
      CALL MOVEA(X0+(RGX*0.25),Y0-3.*(RGY/10.))
      IF(IFX.EQ.1) THEN

```

```

        CALL CHARTK('DIMENSIONLESS TIME',0.85)
    ELSE IF(IFX.EQ.2.OR.IFX.EQ.3) THEN
        CALL CHARTK('TIME (SEC.)',0.85)
    ELSE IF(IFX.EQ.4) THEN
        CALL CHARTK('PERMEABILITY (UM/SEC.)',0.85)
    ENDIF
    IF(IFX.EQ.1) THEN
        YTITLE = 'CONCENTRATION'
        NCHAR = 13
    ELSE IF(IFX.EQ.2) THEN
        YTITLE = 'SENSITIVITY COEFFICIENT'
        NCHAR = 23
    ELSE IF(IFX.EQ.3) THEN
        YTITLE = 'NORMALIZED VOLUME'
        NCHAR = 17
    ELSE IF(IFX.EQ.4) THEN
        YTITLE = 'SUM OF SQUARES OF ERRORS'
        NCHAR = 24
    ENDIF
C
    IF(IFX.EQ.1.OR.IFX.EQ.2.OR.IFX.EQ.3.OR.IFX.EQ.4) THEN
        DO 200 I=1,NCHAR
            AINDEX = I-1
            YYY = (Y0+RGY)-(AINDEX*RGY*0.0533)
            CALL MOVEA((X0-0.3*RGX),YYY)
            A = YTITLE(I:I)
            CALL CHARTK(A,0.85)
200        CONTINUE
    ENDIF
C-----
C    PLOTTING THE CURVES
C-----
    CALL MOVEA(X0,FCT(X0))
    DO 5 I=1,IN*N
        XF=X0+I*RGX/IN/N
        CALL DRAWA(XF,FCT(XF))
5    CONTINUE
    IF (IMARK.EQ.1) THEN
        DO 6 I=1,N
            CALL SQUARE(X(I),Y(I),RGX/60,RGY/60)
6    CONTINUE
    ELSE IF (IMARK.EQ.2) THEN
        DO 7 I=1,N
            CALL TRI(X(I),Y(I),RGX/60,RGY/60)
7    CONTINUE
    ELSE IF (IMARK.EQ.3) THEN
        DO 8 I=1,N
            CALL TRI2(X(I),Y(I),RGX/60,RGY/60)
8    CONTINUE
    ELSE IF (IMARK.EQ.4) THEN
        DO 9 I=1,N
            CALL DIAMAND(X(I),Y(I),RGX/60,RGY/60)

```

```

9      CONTINUE
      ELSE IF (IMARK.EQ.5) THEN
          CALL MOVEA(X0,Y0)
          DO 10 I=1,N
              CALL DRAWA(X(I),Y(I))
10      CONTINUE
      END IF
C
      CALL MOVEA(X0,0.5*(Y1+Y0)+RGY)
      CALL DRAWA(X0+0.0000000001,0.5*(Y1+Y0)+RGY)
C
11     RETURN
      END
C-----
C      SUBROUTINE SQUARE(X,Y,DX,DY)
C
C      X, Y: POSITION TO PLACE THIS MARK
C
C      DX, DY: SIZE OF THIS MARK
C-----
C      SUBROUTINE SQUARE(X,Y,DX,DY)
C      CALL MOVEA(X-DX/2,Y-DY/2)
C      CALL DRAWA(X-DX/2,Y+DY/2)
C      CALL DRAWA(X+DX/2,Y+DY/2)
C      CALL DRAWA(X+DX/2,Y-DY/2)
C      CALL DRAWA(X-DX/2,Y-DY/2)
C      RETURN
C      END
C-----
C      SUBROUTINE TRI(X,Y,DX,DY)
C-----
C      SUBROUTINE TRI(X,Y,DX,DY)
C      CALL MOVEA(X-DX/2,Y-DY/2)
C      CALL DRAWA(X,Y+DY/2)
C      CALL DRAWA(X+DX/2,Y-DY/2)
C      CALL DRAWA(X-DX/2,Y-DY/2)
C      RETURN
C      END
C-----
C      SUBROUTINE TRI2(X,Y,DX,DY)
C-----
C      SUBROUTINE TRI2(X,Y,DX,DY)
C      CALL MOVEA(X-DX/2,Y+DY/2)
C      CALL DRAWA(X,Y-DY/2)
C      CALL DRAWA(X+DX/2,Y+DY/2)
C      CALL DRAWA(X-DX/2,Y+DY/2)
C      RETURN
C      END
C-----
C      SUBROUTINE DIANAMD(X,Y,DX,DY)
C-----
C      SUBROUTINE DIAMAND(X,Y,DX,DY)

```

```

CALL MOVEA(X,Y+DY/2)
CALL DRAWA(X-DX/2,Y)
CALL DRAWA(X,Y-DY/2)
CALL DRAWA(X+DX/2,Y)
CALL DRAWA(X,Y+DY/2)
RETURN
END

```

C-----

C FUNCTION FCTO(X)

C

C TRIVIAL CURVE, IT PLOTS A STRAIGHT LINE AT Y=0.

C-----

```

FUNCTION FCTO(X)
FCTO=0.
RETURN
END

```

APPENDIX E

SENS - The IBM PC Version Fortran Source Code

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```

1      PROGRAM SENS
2 C$DEBUG
3 C-----
4 C      THIS PROGRAM INCLUDES THE COMPUTER MODEL FOR THE
5 C      DIFFUSION CHAMBER AND THE PARAMETER ESTIMATION FOR FINDING
6 C      PERMEABILITY OF A CELL INSIDE THE CELL CHAMBER OF THE
7 C      DIFFUSION CHAMBER.
8 C
9 C      THIS PROGRAM CONSISTS OF 1 MAIN PROGRAM, 5 SUBROUTINES
10 C     AND 2 FUNCTIONS.  THEY ALL ARE INSIDE THE FILES 'SENS.FOR',
11 C     'MBCON.FOR'.
12 C
13 C     THE INPUT DATA CAN BE ENTERED ONE OF TWO WAYS, VIA THE
14 C     TERMINAL/KEYBOARD OR BY USING A PRE-EXISTING INPUT FILE SET
15 C     UP BY THE USER; FOR EXAMPLE 'I_SENS.DAT'.
16 C
17 C     THE OUTPUT CAN BE VIEWED BY (1) LOOKING AT THE TABLES GENERATED,
18 C     WHICH RESIDE IN FILE 'O_SENS.DAT' AND 'O_SMRY.DAT', AND/OR (2)
19 C     HAVING THE PROGRAM GENERATE FILES TO BE USED IN CONJUNCTION WITH
20 C     PLOTIT TO VIEW THE OUTPUT GRAPHICALLY.
21 C
22 C     THE INPUT DATA REQUIRED IS AS FOLLOWS:
23 C
24 C     RL1: THICKNESS OF DIALYSIS MEMBRANE (M)
25 C
26 C     RL2: THICKNESS OF CELL CHAMBER (M)
27 C
28 C     LIP: APPROXIMATE LOCATION OF THE LIPOSOME (FROM 5 TO 11)
29 C
30 C     D1: DIFFUSIVITY OF SOLUTE INSIDE DIALYSIS MEMBRANE (M*M/SEC)
31 C
32 C     D2: DIFFUSIVITY OF SOLUTE INSIDE CELL CHAMBER (M*M/SEC)
33 C
34 C     CINIT: INITIAL CONCENTRATION (OSM)
35 C
36 C     CINF: FINAL CONCENTRATION (OSM)
37 C
38 C     H: MASS TRANSFER COEFF. (APPROXIMATELY 10000*D2)
39 C
40 C     IPRINT: NUMERICAL DATA OUTPUT FREQUENCY. (EVERY IPRINT*DT
41 C             SEC. PRINTS THE CONC. DIST. ON OUTPUT FILE)
42 C
43 C     IRELPSE: OPTION FOR EXPERIMENTAL DATA INPUT 1-REAL-EXPERIMENT
44 C                                                     2-PSUESO-EXPERIMENT
45 C
46 C     IMICCEN: OPTION FOR ENTERING DATA IN 1-MICRONS  2-CENTIMETERS
47 C

```

48 C TM0, TM1: SETTING THE TIME RANGE ON THE PLOTS (SEC.)
 49 C
 50 C DT: TIME STEP FOR PROCEEDING THE CALCULATION (SEC.)
 51 C (NOTE: IF DT IS SET TOO LARGE, THE RESULT WILL FLUCTUATE.
 52 C IN THIS CASE, REDUCE THE SIZE OF DT AND TRY AGAIN.
 53 C THIS IS DUE TO THE UNSTABLE OF THE NUMERICAL METHOD.)
 54 C
 55 C DELAY: TIME DELAY SUBTRACTED FROM TIME ARRAY TM(I).
 56 C

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57 C PSEN: THE PERMEABILITY VALUE AT WHICH WE INVESTIGATE THE
 58 C SENSITIVITY COEFF. (P'S EFFECT ON R'S CHANGE)
 59 C
 60 C PTRU: THE PERMEABILITY VALUE WITH WHICH THE PROGRAM GENERATES
 61 C PSUDO-EXPERIMENTAL DATA (R(TM,PTRU)).
 62 C
 63 C DT1: THE TIME STEP FOR THE PSUDO-EXPT'L DATA DURING TM0 TO
 64 C TM01. (SEC.)
 65 C
 66 C TM01: THE PARTITION BETWEEN TWO DIFFERENT TIME STEPS RANGE.
 67 C (YOU CAN ASK THE PROGRAM TO GENERATES PSUDO-EXPT'L DATA
 68 C WITH TWO DIFFERENT INCREMENT IN TIME FOR TWO TIME
 69 C RANGE.)
 70 C
 71 C DT2: THE TIME STEP FOR THE PSUDO-EXPT'L DATA DURING TM01
 72 C TO TM1. (SEC.)
 73 C
 74 C
 75 C RINIT: INITIAL RADIUS (MICRONS OR CM)
 76 C
 77 C VINA: INACTIVE VOLUME (%)
 78 C
 79 C RMAG: THE MAGNIFICATION OF THE MICROSCOPE
 80 C
 81 C DR: MAGNITUDE FOR THE PSEUDO-RANDOMNESS IMPOSED ON THE
 82 C PREDICTED RADIUS RESPONSE (MICRONS OR CM)
 83 C
 84 C P0, P1: PERMEABILITY RANGE UNDER INVESTIGATION (MICRONS/SEC.)
 85 C
 86 C DP: INCREMENT OF PERMEABILITY IN CALCULATING SUM OF ERROR OF
 87 C SQUARE FOR EACH P VALUE
 88 C
 89 C CON1: NAME OF THE FILE CONTAINING CA V.S.
 90 C DIMENSIONLESS TIME
 91 C
 92 C CON2: NAME OF THE FILE CONTAINING CB V.S.
 93 C DIMENSEIONLESS TIME
 94 C


```

142 C          (4) SUM OF SQUARE OF ERRORS V.S. PERMEABILITY
143 C
144 C-----
145 C    INITIALIZATION AND DECLARATIONS
146 C-----
147 $INCLUDE: 'IMSL'
148 1 $LARGE: DMY327
149 2    DIMENSION DMY327(1)
150 3    PARAMETER (N3=301,II=2,N1=301,N4=301,EP1=0.01,N5=25)
151 4    DIMENSION TMA(N3),TMB(N3),RA(N3),RB(N3),SEN(N3),SUM(N1),P(N1)
152 5    DIMENSION VOLC(N3),VOLA(N3),TMS(N3),RS(N3),RC(N3),RSAVE(N3)
153 6    DIMENSION CA(N5),CB(N5)
154 7    CHARACTER*1 ICHANG, IGRAPH, IMORE, IAGAIN, IANOTH, ISAVE
155 8    CHARACTER*1 IMISTAK, IFIRST, IQUIT, IDEL
156 9    CHARACTER*11 XMICCEN, PROBLEM
157 10   CHARACTER*10 NAMFIL, CON1, SENC, VOL1, SUMR, CON2, VOL2, ISENS
158 11   COMMON /C1/IPRINT, IF1, A1(II), A2(II)
159 12   COMMON /C2/RINIT, VINA, DT, TM1, COUT(N4)
160 13   COMMON /C3/RL1, RL2, LIP, D1, D2, CINIT, CINF, H
161 14   EXTERNAL F
162 15   XSEED =566387.0
163 16   ISC = 0
164 17   IBACK = 0
165 18   IRUNAG=0
166 19   IOPNAG=0
167 20   IMISTAK = 'N'
168 C-----

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167 C    EXPLANATION TO THE USER WHAT THE PROGRAM DOES.
168 C-----
169 2000 CONTINUE
170      WRITE(*,*)
171      WRITE(*,*)'WOULD YOU LIKE AN EXPLANATION OF THIS PROGRAM, '
172      WRITE(*,*)'(SENS), (Y/N)?'
173      READ(*,'(A1)') IFIRST
174      IF(IFIRST.EQ.'N') GO TO 1200
175      WRITE(*,*)
176      WRITE(*,*)'  WELCOME TO THE PROGRAM SENS.  THIS PROGRAM WILL '
177      WRITE(*,*)'ALLOW THE USER TO (1) ANALYZE THE DATA OBTAINED USING '
178      WRITE(*,*)'THE MICROSCOPE DIFFUSION CHAMBER I.E. PARAMETER '
179      WRITE(*,*)'ESTIMATION OF THE PERMEABILITY OF A CELL OR (2) RUN '
180      WRITE(*,*)'A SIMULATION (PSEUDO) EXPERIMENT TO SEE WHAT MIGHT '
181      WRITE(*,*)'TO A CELL UNDER SPECIFIED CONDITIONS.'
182 C-----
183 C    OPTION TO HAVE A LIST OF THE NECESSARY PARAMETERS SENT TO
184 C    'I_DATA.LST'
185 C-----
186      WRITE(*,*)'  IF THIS IS THE FIRST TIME YOU HAVE USED THIS '

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187 WRITE(*,*)'PROGRAM AND YOU WANT TO ENTER DATA FROM A REAL '
188 WRITE(*,*)'EXPERIMENT YOU MAY WANT TO OBTAIN A LIST OF THE '
189 WRITE(*,*)'PARAMETERS AND DATA NECESSARY TO RUN THE PROGRAM.'
190 WRITE(*,*)
191 WRITE(*,*)'WOULD YOU LIKE TO DO THIS, (Y/N)?'
192 READ(*,'(A1)') IFIRST
193 CALL IYESNO(IFIRST)
194 IF(IFIRST.EQ.'Y') THEN
195     OPEN(13,FILE='I_DATA.LST',STATUS='NEW')
196     WRITE(*,*)
197     WRITE(*,*)'THE LIST OF THE NECESSARY INPUT TO RUN THE PROGRAM'
198     WRITE(*,*)'WILL BE IN FILE "I_DATA.LST". THE PROGRAM WILL'
199     WRITE(*,*)'STOP NOW. HAVE I_DATA.LST PRINT AT THE PRINTER.'
200     WRITE(13,*)
201     WRITE(13,*)'THE PARAMETES AND DATA NEEDED TO RUN THE PROGRAM'
202     WRITE(13,*)'ARE:'
203     WRITE(13,*)
204     WRITE(13,*)'1) DIALYSIS MEMBRANE THICKNESS (RL1), MICRONS.'
205     WRITE(13,*)'2) CELL CHAMBER THICKNESS (RL2), MICRONS.'
206     WRITE(13,*)'3) CELL POSITION IN THE CELL CHAMBER (5-11).'
207     WRITE(13,*)'4) DIFUSSIVITY OF SOLUTE IN MEMBRANE (D1), '
208     WRITE(13,*)' - METERS*METERS/SEC.'
209     WRITE(13,*)'5) DIFUSSIVITY OF SOLUTE IN FREE SOLUTION (D2), '
210     WRITE(13,*)' - METERS*METERS/SEC.'
211     WRITE(13,*)'6) MASS TRANSFER COEFFICIENT (H).'
212     WRITE(13,*)' - METERS/SEC.'
213     WRITE(13,*)'7) INITIAL CONCENTRATION (CINIT), OSMOLALITY.'
214     WRITE(13,*)'8) FINAL CONCENTRATION (CINF), OSMOLALITY.'
215     WRITE(13,*)'9) INACTIVE VOLUME (VINA), %'
216     WRITE(13,*)'10) MAGNIFICATION FACTOR (RMAG).'
217     WRITE(13,*)'11) TIME STEP (DT), SEC.'
218     WRITE(13,*)'12) STARTING TIME (TMO), SEC.'
219     WRITE(13,*)'13) ENDING TIME (TM1), SEC.'
220     WRITE(13,*)'14) TIME DELAY (DELAY), SEC., (0.0 IF NO DELAY)'
221     WRITE(13,*)'15) PERMEABILITY STEP (DP), MICRONS/SEC.'
222     WRITE(13,*)'16) THE LIMITS OF THE PERMEABILITY RANGE UNDER , '

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223 WRITE(13,*)' INVESTIGATION (PO TO P1), MICRONS/SEC.'
224 WRITE(13,*)'17) PERMEABILITY AT WHICH INVESTIGATE THE '
225 WRITE(13,*)' SENSITIVITY COEFFICIENTS (PSEN), MICRONS/SEC.'
226 WRITE(13,*)'18) THE DATA POINTS: TIME (TMA(I)), SEC. AND '
227 WRITE(13,*)' RADIUS (RA(I)), MICRONS OR '
228 WRITE(13,*)' CENTIMETERS.'
229 WRITE(13,*)
230 WRITE(13,*)' (NOTE: YOU ONLY NEED THE DATA POINTS IF YOU'
231 WRITE(13,*)' ARE USEING THE PARAMETER ESTIMATION OPTION,'
232 WRITE(13,*)' I.E. A REAL EXPERIMENT.)'
233 CLOSE(13,STATUS='KEEP')

```

```

234          GO TO 600
235      ENDIF
236 C-----
237 C      EXPLAINING THE OPTION TO ENTER DATA USING KEYBOARD OR AN INPUT
238 C      FILE (WHICH IS SPECIFIED BY THE USER).
239 C-----
240      WRITE(*,*)
241      WRITE(*,*)'  THIS PROGRAM WILL ALLOW YOU TO ENTER THE DATA'
242      WRITE(*,*)'USING THE TERMINAL/KEYBOARD OR A PRE-EXISTING INPUT'
243      WRITE(*,*)'FILE SET UP BY THE USER.  AN EXAMPLE OF AN INPUT FILE'
244      WRITE(*,*)'CAN BE SEEN BY QUITTING THIS PROGRAM AND PRINTING '
245      WRITE(*,*)'I_SENS.EXP AT THE PRINTER.  DO YOU WISH TO QUIT AND '
246      WRITE(*,*)'PRINT THE EXAMPLE, (Y/N)?'
247      READ(*, '(A1)') IQUIT
248      CALL IYESNO(IQUIT)
249 C-----
250 C      IF IQUIT IT YES THE PROGRAM WILL GENERATE I_SENS.EXP AND QUIT.
251 C-----
252      IEXP = 0
253      IF (IQUIT.EQ.'Y') THEN
254          OPEN(12, FILE='I_SENS.EXP', STATUS='NEW')
255          WRITE(12, *) 'THIS IS THE EXAMPLE INPUT FILE I_SENS.EXP FOR THE '
256          WRITE(12, *) 'PROGRAM SENS.FOR.  THE PROGRAM WILL READ THE DATA'
257          WRITE(12, *) 'ALINING THE VALUE UNDER THE LEFT MOST CHARACTER.'
258          RL1=16.
259          RL2 = 100.
260          LIP = 9
261          D1 = 5.21E-11
262          D2 = 5.21E-10
263          H = 5.21E-6
264          CINIT = 0.02
265          CINF = 0.04
266          VINA = 6.
267          RMAG = 5080.
268          DT = 5.0
269          TMO = 0.
270          TM1 = 500.
271          DELAY = 0.0
272          DP = 2.
273          PO = 0.
274          P1 = 100.
275          PSEN = 40.
276          RINIT = 7.7
277          PTRU = 40.
278          DR = 0.01

```

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```

279          TM01 = 500.
280          DT1 = 5.0

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281         DT2 = 5.0
282         IRELPSE = 1
283         IMICCEN = 2
284         IF1 = 1
285         IF2 = 1
286         IF3 = 1
287         IF4 = 1
288         IPRINT = 10
289         CON1 = 'O_CON1.DAT'
290         CON2 = 'O_CON2.DAT'
291         SENC = 'O_SENC.DAT'
292         VOL1 = 'O_VOL1.DAT'
293         VOL2 = 'O_VOL2.DAT'
294         SUMR = 'O_SUMR.DAT'
295         ICOUNT = 40
296         RA(1) = 7.7
297         TMA(1) = 0.0
298         DO 1100 I = 2,40
1 299             TMA(I) = TMA(I-1) + 10.
1 300             RA(I) = RA(I-1) - 0.05
1 301 1100     CONTINUE
302             IEXP = 1
303             ISAVE = 'Y'
304             GO TO 319
305         ENDIF
306 C-----
307 C     EXPLAINING THE INPUT AND OUTPUT OPTIONS
308 C-----
309         WRITE(*,*)
310         WRITE(*,*)'    THE PROGRAM WILL ALSO ALLOW THE USER TO VIEW THE'
311         WRITE(*,*)'RESULTS BY 1) TABLES AND/OR 2) HAVING FILES CREATED'
312         WRITE(*,*)'WHICH THE USER USES "PLOTIT" TO GENERATE GRAPHICAL'
313         WRITE(*,*)'OUTPUT.  THE TABLES GENERATED CAN BE FOUND IN A FILE'
314         WRITE(*,*)'CALLED "O_SENS.DAT".  A SUMMARY OF THE INPUT '
315         WRITE(*,*)'PARAMETERS, INPUT DATA AND RESULTING PERMEABILITY'
316         WRITE(*,*)'CAN BE FOUND IN "O_SMRY.DAT".'
317         WRITE(*,*)'THE FILES THAT CAN BE CREATED FOR PLOTIT ARE'
318         WRITE(*,*)'FOR THE FOLLOWING DATA SETS.'
319         WRITE(*,*)
320         WRITE(*,*)'1) CONCENTRATION V.S. DIMENSIONLESS TIME'
321         WRITE(*,*)'2) SENSITIVITY COEFFICIENTS V.S. TIME'
322         WRITE(*,*)'3) NORMALIZED VOLUME V.S. TIME'
323         WRITE(*,*)'4) SUM OF THE SQUARE OF THE ERRORS V.S. PERMEABILITY'
324         WRITE(*,*)
325         WRITE(*,*)'THE PROGRAM WILL PROMPT THE USER TO ENTER A FILE'
326         WRITE(*,*)'NAME FOR EACH OF THE DESIRED DATA SETS TO BE PLOTTED.'
327         WRITE(*,*)
328         WRITE(*,*)'YOU ARE NOW READY TO START THE PROGRAM.'
329 1200     CONTINUE
330         WRITE(*,*)
331         WRITE(*,*)'DO YOU WISH TO ENTER THE DATA USING (1) THE TERMINAL'
332         WRITE(*,*)'OR (2) A PRE-EXISTING INPUT FILE, (ENTER 1 OR 2)?'

```



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333      WRITE(*,*)
334      READ(*,*,ERR=1200) ITERINP
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335      CALL IONETWO(ITERINP)
336      IF(ITERINP.EQ.2) THEN
337          WRITE(*,*)
338          WRITE(*,*)'PLEASE ENTER THE NAME OF THE INPUT FILE TO BE USED,'
339          WRITE(*,*)'(ENTER NO MORE THAN 10 CHARACTERS).'
340          READ(*, '(A10)') ISENS
341          CALL CHANNAM(ISENS)
342          WRITE(*,*)
343          WRITE(*,*)'OKAY, THE PROGRAM IS CRUNCHING.'
344          GO TO 2999
345      ENDIF
346 C
347      IPRINT = 10
348 C-----
349 C      PROMPTING THE USER TO ENTER THE REQUIRED DATA AND PARAMETERS
350 C      NEEDED TO RUN THE PROGRAM.
351 C-----
352 2005 CONTINUE
353      WRITE(*,*)
354      WRITE(*,*)'DO YOU WISH TO (1) ENTER DATA FROM A REAL EXPERIMENT'
355      WRITE(*,*)'OR (2) USE THE PROGRAM FOR A SIMULATION (PSEUDO-'
356      WRITE(*,*)'EXPERIMENT), (ENTER 1 OR 2)?'
357      WRITE(*,*)
358      READ(*,*,ERR=2005) IRELPSE
359      CALL IONETWO(IRELPSE)
360 2100 CONTINUE
361      WRITE(*,*)'ENTERING THE PHYSICAL PARAMETERS OF THE SYSTEM:'
362      WRITE(*,*)
363      WRITE(*,*)'PLEASE ENTER THICKNESS OF THE DIALYSIS MEMBRANE, '
364      WRITE(*,*)'(MICRONS).'
365      WRITE(*,*)
366      READ(*,*,ERR=2100) RL1
367      WRITE(*,*)
368 2105 CONTINUE
369      WRITE(*,*)'PLEASE ENTER THE THICKNESS OF THE CELL CHAMBER,'
370      WRITE(*,*)'(MICRONS).'
371      WRITE(*,*)
372      READ(*,*,ERR=2105) RL2
373      WRITE(*,*)
374 2106 CONTINUE
375      WRITE(*,*)'PLEASE ENTER THE CELL POSITION, (5-11).'
376      WRITE(*,*)'(SEE THE DIAGRAM BELOW FOR BETTER UNDERSTANDING.)'
377      WRITE(*,*)
378      WRITE(*,*)'      DIALYSIS MEMBRANE      CELL CHAMBER'
379      WRITE(*,*)'      |                      |                      |'

```

```

380      WRITE(*,*)'B |
381      WRITE(*,*)'U |
382      WRITE(*,*)'L |
383      WRITE(*,*)'K |
384      WRITE(*,*)' 1 2 3 4 5 6 7 8 9 10 11'
385      WRITE(*,*)'F |
386      WRITE(*,*)'L |
387      WRITE(*,*)'O |
388      WRITE(*,*)'W |
389      WRITE(*,*)' |
390      WRITE(*,*)

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```

391      READ(*,*,ERR=2106) LIP
392      WRITE(*,*)
393 2110  CONTINUE
394      WRITE(*,*)'PLEASE ENTER THE DIFFUSIVITY OF THE SOLUTE INSIDE'
395      WRITE(*,*)'THE CELL CHAMBER, (METERS*METERS/SEC.), D2.'
396      WRITE(*,*)
397      READ(*,*,ERR=2110) D2
398      WRITE(*,*)
399 2120  CONTINUE
400      WRITE(*,*)'DO YOU WISH TO ENTER (1) SEPARATE VALUES FOR THE'
401      WRITE(*,*)'DIFFUSIVITY OF THE SOLUTE INSIDE THE DIALYSIS'
402      WRITE(*,*)'MEMBRANE (METERS*METERS/SEC.), D1, AND THE MASS'
403      WRITE(*,*)'TRANSFER COEFFICIENT, H, OR (2) USE PRESET'
404      WRITE(*,*)'VALUES OF D1=D2/10 AND H=10000*D2?'
405      WRITE(*,*)
406      READ(*,*,ERR=2120) ISEPPRE
407      CALL IONETWO(ISEPPRE)
408      IF(ISEPPRE.EQ.1) THEN
409 2130  CONTINUE
410          WRITE(*,*)'PLEASE ENTER D1 (METERS*METERS/SEC.).'
411          WRITE(*,*)
412          READ(*,*,ERR=2130) D1
413          WRITE(*,*)
414 2140  CONTINUE
415          WRITE(*,*)'PLEASE ENTER H, (METERS/SEC.)'
416          WRITE(*,*)
417          READ(*,*,ERR=2140) H
418      ELSE IF (ISEPPRE.EQ.2) THEN
419          D1 = D2/10.0
420          H = 10000.*D2
421      ENDIF
422 2150  CONTINUE
423      WRITE(*,*)
424      WRITE(*,*)'PLEASE ENTER THE INITIAL AND FINAL CONCENTRATION, '
425      WRITE(*,*)'CINIT CINF, (OSMOLALITY). (ENTER BOTH VALUES AND'
426      WRITE(*,*)'SEPARATE WITH A SPACE.)'

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427      WRITE(*,*)
428      READ(*,*,ERR=2150) CINIT, CINF
429 2160  CONTINUE
430      WRITE(*,*)
431      WRITE(*,*)'PLEASE ENTER THE INACTIVE VOLUME (%).'
432      WRITE(*,*)
433      READ(*,*,ERR=2160) VINA
434      WRITE(*,*)
435 2170  CONTINUE
436      WRITE(*,*)
437      WRITE(*,*)'PLEASE ENTER THE MAGNIFICATION FACTOR. (USE 5080.0 '
438      WRITE(*,*)'FOR BTP MEASUREMENTS. IF YOU ARE ENTERING THE'
439      WRITE(*,*)'EXACT CELL SIZE ENTER 1.0.)'
440      WRITE(*,*)
441      READ(*,*,ERR=2170) RMAG
442      WRITE(*,*)
443 2180  CONTINUE
444      WRITE(*,*)
445      WRITE(*,2190) RL1,RL2,LIP,D2,D1,H,CINIT,CINF,VINA,RMAG
446 2190  FORMAT(1X,'THE VALUES ENTERED SO FAR ARE:',/,

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
447      . 1X,'1) DIALYSIS MEMBRANE THICKNESS = ',E11.3,' MICRONS',/,
448      . 1X,'2) CELL CHAMBER THICKNESS = ',E11.3,' MICRONS',/,
449      . 1X,'3) LIPOSOME POSITION (5-11) = ',I2,/,
450      . 1X,'4) DIFFUSIVITY IN CELL CHAMBER = ',E11.3,' M*M/SEC.',/,
451      . 1X,'5) DIFFUSIVITY IN DIALYSIS MEMBRANE = ',E11.3,' M*M/SEC.',/,
452      . 1X,'6) MASS TRANSFER COEFFICIENT = ',E11.3,' M/SEC ',/,
453      . 1X,'7) INITIAL CONCENTRATION = ',F7.3,' OSMOLALITY',/,
454      . 1X,'8) FINAL CONCENTRATION = ',F7.3,' OSMOLALITY',/,
455      . 1X,'9) INACTIVE VOLUME % = ',F5.2,/,
456      . 1X,'10) MAGNIFICATION FACTOR = ',F7.1,/)
457      WRITE(*,*)'DO YOU WISH TO CHANGE ANY OF THEM, (Y/N)?'
458      READ(*, '(A1)') ICHANG
459      CALL IYESNO(ICHANG)
460      IF(ICHANG.EQ.'Y') THEN
461 2210  CONTINUE
462      WRITE(*,*)
463      WRITE(*,*)'PLEASE ENTER THE NUMBER BESIDE THE PARAMETER'
464      WRITE(*,*)'YOU WISH TO CHANGE, (1-10). '
465      READ(*,*,ERR=2210) NCHANG
466 2215  CONTINUE
467      WRITE(*,*)
468      WRITE(*,*)'PLEASE ENTER THE NEW VALUE.'
469      IF(NCHANG.EQ.1) THEN
470          READ(*,*,ERR=2215) RL1
471      ELSE IF(NCHANG.EQ.2) THEN
472          READ(*,*,ERR=2215) RL2
473      ELSE IF(NCHANG.EQ.3) THEN

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474      READ(*,*,ERR=2215) LIP
475      ELSE IF(NCHANG.EQ.4) THEN
476          READ(*,*,ERR=2215) D2
477      ELSE IF(NCHANG.EQ.5) THEN
478          READ(*,*,ERR=2215) D1
479      ELSE IF(NCHANG.EQ.6) THEN
480          READ(*,*,ERR=2215) H
481      ELSE IF(NCHANG.EQ.7) THEN
482          READ(*,*,ERR=2215) CINIT
483      ELSE IF(NCHANG.EQ.8) THEN
484          READ(*,*,ERR=2215) CINF
485      ELSE IF(NCHANG.EQ.9) THEN
486          READ(*,*,ERR=2215) VINA
487      ELSE IF(NCHANG.EQ.10) THEN
488          READ(*,*,ERR=2215) RMAG
489      ELSE IF(NCHANG.LE.0.OR.NCHANG.GE.11) THEN
490          CALL INCORRES
491          GO TO 2210
492      ENDIF
493      GO TO 2180
494  ENDIF
495  IF(IRUNAG.GE.1.OR.IMISTAK.EQ.'Y') GO TO 2235
496  WRITE(*,*)
497  WRITE(*,*)'IN ORDER FOR THE PROGRAM TO RUN THE USER'
498  WRITE(*,*)'MUST ALSO ENTER THE FOLLOWING DATA:'
499 2220 CONTINUE
500  WRITE(*,*)
501  WRITE(*,*)'THE TIME RANGE OF THE EXPERIMENT, TMO  TM1, (SEC.),'
502  WRITE(*,*)'(NOTE:  PLEASE MAKE SURE TM1 IS GREATER THAN THE '
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503  WRITE(*,*)'TIME OF THE LAST DATA POINT TO BE ENTERED AND ENTER '
504  WRITE(*,*)'BOTH VALUES WITH A SPACE BETWEEN THEM.)'
505  READ(*,*,ERR=2220) TMO, TM1
506 2223 CONTINUE
507  WRITE(*,*)
508  WRITE(*,*)'THE TIME STEP, DT, (SEC.). (NOTE:  THIS TIME STEP IS'
509  WRITE(*,*)'USED FOR NUMERICAL INTEGRATION - CHOOSE DT SUCH THAT'
510  WRITE(*,*)'DT .GE. (TM1-TMO)/301  TO PREVENT ARRAY OVERFLOW.)'
511  READ(*,*,ERR=2223) DT
512 2225 CONTINUE
513  WRITE(*,*)
514  WRITE(*,*)'THE PERMEABILITY RANGE WHICH YOU ARE INVESTIGATING, '
515  WRITE(*,*)'PO  P1, (MICRONS/SEC.). (ENTER BOTH VALUES WITH '
516  WRITE(*,*)'A SPACE BETWEEN THEM.)'
517  READ(*,*,ERR=2225) PO, P1
518 2226 CONTINUE
519  WRITE(*,*)
520  WRITE(*,*)'THE PERMEABILITY STEP, DP, (MICRONS/SEC.) (NOTE: '

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521      WRITE(*,*)'CHOOSE DP SUCH THAT DP .GE. (P1-P0)/301  TO '
522      WRITE(*,*)'PREVENT ARRAY OVERFLOW.)'
523      READ(*,*,ERR=2226) DP
524 2230  CONTINUE
525      WRITE(*,*)
526      WRITE(*,*)'THE PERMEABILITY VALUE AT WHICH THE SENSITIVITY'
527      WRITE(*,*)'COEFFICIENT WILL BE EVALUATED, PSEN, (MICRONS/SEC.) '
528      READ(*,*,ERR=2230) PSEN
529 2235  CONTINUE
530      WRITE(*,*)
531      WRITE(*,2240) DT,TM0,TM1,DP,P0,P1,PSEN
532 2240  FORMAT(1X,'THE VALUES ENTERED ARE:',/,
533      . 1X,'1) TIME STEP = ',F7.2,' SEC.',/,
534      . 1X,'2) TIME RANGE = ',F8.1,' SEC.', ' TO ',F8.1,' SEC.',/,
535      . 1X,'3) PERMEABILITY STEP = ',F7.2,' MICRONS/SEC.',/,
536      . 1X,'4) PERMEABILITY RANGE = ',F7.2,' MICRONS/SEC. TO',/,
537      . 1X,' ',F7.2,' MICRONS/SEC.',/,
538      . 1X,'5) INVESTIGATING PERMEABILITY = ',F7.2,' MICRONS/SEC.',/)
539      WRITE(*,*)'DO YOU WISH TO CHANGE ANY OF THEM, (Y/N)?'
540      READ(*,'(A1)') ICHANG
541      CALL IYESNO(ICHANG)
542      IF(ICHANG.EQ.'Y')THEN
543 2245  CONTINUE
544      WRITE(*,*)
545      WRITE(*,*)'PLEASE ENTER THE NUMBER BESIDE THE PARAMETER'
546      WRITE(*,*)'YOU WISH TO CHANGE, (1-5). '
547      READ(*,*,ERR=2245) NCHANG
548 2246  CONTINUE
549      WRITE(*,*)
550      WRITE(*,*)'PLEASE ENTER THE NEW VALUE(S). '
551      IF(NCHANG.EQ.1) THEN
552          READ(*,*,ERR=2246) DT
553      ELSE IF(NCHANG.EQ.2) THEN
554          WRITE(*,*)'(BOTH TM0 AND TM1 - SEPARATE WITH A SPACE)'
555          READ (*,*,ERR=2246) TM0, TM1
556      ELSE IF(NCHANG.EQ.3) THEN
557          READ(*,*,ERR=2246) DP
558      ELSE IF(NCHANG.EQ.4) THEN

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559      WRITE(*,*)'(BOTH P0 AND P1 - SEPARATE WITH A SPACE)'
560      READ(*,*,ERR=2246) P0,P1
561      ELSE IF(NCHANG.EQ.5) THEN
562          READ(*,*,ERR=2246) PSEN
563      ELSE IF(NCHANG.LE.0.OR.NCHANG.GE.6) THEN
564          CALL INCORRES
565          GO TO 2246
566      ENDIF
567      GO TO 2235

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568      ENDIF
569 C
570      IF(IRELPS.EQ.1) THEN
571          IF(IRUNAG.GE.1.OR.IMISTAK.EQ.'Y') THEN
572 2248      CONTINUE
573          WRITE(*,*)
574          WRITE(*,*)'DO YOU WISH TO (1) ENTER ALL NEW DATA POINTS'
575          WRITE(*,*)'OR (2) REVIEW THE PREVIOUS DATA POINTS, (Y/N)?'
576          READ(*,*,ERR=2248) INR
577          CALL IONETWO(INR)
578          IF(INR.EQ.2)GO TO 2261
579          IF(INR.EQ.1) THEN
580              I=0
581              WRITE(*,*)
582              GO TO 2250
583          ENDIF
584      ENDIF
585      I = 0
586      WRITE(*,*)
587      WRITE(*,*)'SINCE YOU HAVE CHOSEN THE REAL-EXPERIMENTAL'
588      WRITE(*,*)'OPTION THE DATA POINTS MUST BE ENTERED. BUT'
589 2250      CONTINUE
590      WRITE(*,*)'BEFORE ENTERING THE DATA, IS THERE A TIME'
591      WRITE(*,*)'DELAY THAT YOU WOULD LIKE TO HAVE SUBTRACTED'
592      WRITE(*,*)'FROM THE TIME ARRAY YOU WILL BE ENTERING,'
593      WRITE(*,*)'(Y/N)?'
594      READ(*, '(A1)')IDEL
595      CALL IYESNO(IDEL)
596      IF(IDEL.EQ.'N') THEN
597          DELAY = 0.0
598      ELSE IF(IDEL.EQ.'Y') THEN
599 2251      CONTINUE
600          WRITE(*,*)
601          WRITE(*,*)'PLEASE ENTER THE TIME DELAY TO BE SUBTRACTED,'
602          WRITE(*,*)'(SEC.).'
603          READ(*,*,ERR=2251) DELAY
604          WRITE(*,2252) DELAY
605 2252      FORMAT(/,' THE TIME DELAY THAT WILL BE SUBTRACTED IS ',
606              F7.4,' SEC.',/,/,', DO YOU WISH TO CHANGE IT, (Y/N)?')
607          READ(*, '(A1)') ICHANG
608          CALL IYESNO(ICHANG)
609          IF(ICHANG.EQ.'Y') GO TO 2251
610      ENDIF
611      WRITE(*,*)
612      WRITE(*,*)'DO YOU WISH TO ENTER THE RADIUS USING UNITS'
613      WRITE(*,*)'OF (1) MICRONS OR (2) CENTIMETERS?'
614 2253      READ(*,*,ERR=2253) IMICCEN

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615      CALL IONETWO(IMICCEN)
616      WRITE(*,*)
617      WRITE(*,*)'PLEASE ENTER THE DATA POINTS,'
618      IF(IMICCEN.EQ.1)THEN
619          WRITE(*,*)'TIME(I) (SEC.)  RADIUS(I) (MICRONS)'
620      ELSE IF(IMICCEN.EQ.2) THEN
621          WRITE(*,*)'TIME(I) (SEC.)  RADIUS(I) (CENTIMETERS)'
622      ENDIF
623      WRITE(*,*)'(ENTER BOTH VALUES AND SEPARATE WITH A SPACE.)'
624      WRITE(*,*)'(NOTE:  ENTER 0.0 0.0 FOR THE LAST DATA POINT.) '
625      WRITE(*,*)
626 2255      I = I+1
627      WRITE(*,2256) I
628 2256      FORMAT(1X,'ENTER POINT ',I3)
629 2257      READ(*,*,ERR=2257) TMA(I), RA(I)
630          IF((TMA(I).GT.0.).AND.(RA(I).GT.0.)) TMA(I) = TMA(I) - DELAY
631      IF(I.EQ.1) RAMAX = RA(I)
632      IF(I.GE.2.AND.RA(I).GT.RAMAX) RAMAX = RA(I)
633      IF((TMA(I).GT.0.).OR.(RA(I).GT.0.)) GO TO 2255
634      ICOUNT = I-1
635      IF(TM1.LE.TMA(ICOUNT)) THEN
636          WRITE(*,*)
637          WRITE(*,*)'PLEASE MAKE SURE THE TIME LIMIT, TM1, IS'
638          WRITE(*,*)'LARGER THAN THE TIME OF THE LAST DATA POINT.'
639      WRITE(*,*)'IF YOU DO NOT CHANGE THIS THE PROGRAM WILL STOP.'
640          WRITE(*,*)'(RELAX YOU WILL HAVE A CHANCE TO CHANGE IT.)'
641          WRITE(*,*)
642      ENDIF
643 2260      CONTINUE
644      WRITE(*,*)'THE NEXT TABLE WILL SHOW YOU THE POINTS YOU HAVE'
645      WRITE(*,*)'JUST ENTERED.  IF YOU HAVE ENTERED MORE THAN 20'
646      WRITE(*,*)'POINTS THE TABLE WILL STOP SPOOLING EVERY 20 POINTS'
647      WRITE(*,*)'TO ALLOW YOU TO REVIEW THE POINTS ENTERED.  MAKE'
648      WRITE(*,*)'A NOTE OF WHICH POINT YOU WISH TO CHANGE OR'
649      WRITE(*,*)'INSERT AND PRESS [RETURN] TO CONTINUE NOTE, YOU'
650      WRITE(*,*)'YOU WILL ONLY BE ABLE TO CHANGE OR INSERT ONE '
651      WRITE(*,*)'POINT AT A TIME.'
652      WRITE(*,*)'(NOW PRESS [RETURN] TO CONTINUE.)'
653      READ(*, '(A1)') ICHANG
654 2261      CONTINUE
655      WRITE(*,*)
656      WRITE(*,*)'THE DATA POINTS YOU HAVE ENTERED ARE: '
657      WRITE(*,2262) DELAY
658 2262      FORMAT(' (INCLUDING THE TIME DELAY OF ',F8.4,' SEC.)')
659      WRITE(*,*)
660      WRITE(*,*)'  J          TIME(J)          RADIUS(J)'
661      IF(IMICCEN.EQ.1) THEN
662          WRITE(*,*)'          (SEC.)          (MICRONS)'
663      ELSE IF(IMICCEN.EQ.2) THEN
664          WRITE(*,*)'          (SEC.)          (CENTIMETERS)'
665      ENDIF
666      DO 2265 J=1,ICOUNT+1

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1 667          WRITE(*,2263) J, TMA(J), RA(J)
1 668 2263      FORMAT(1X,I3,5X,F8.2,5X,F8.2)
1 669          IF((J/20)*20.EQ.J) THEN
1 670              WRITE(*,*)

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1 671          WRITE(*,*)'PRESS [RETURN] TO CONTINUE.'
1 672          READ(*, '(A1)') IMORE
1 673          ENDIF
1 674 2265      CONTINUE
675          IF(IBACK.EQ.1) GO TO 2281
676          WRITE(*,*)
677          WRITE(*,*)'DO YOU WISH TO CHANGE OR INSERT ANY OF THE POINTS,'
678          WRITE(*,*)'(Y/N)?'
679          READ(*, '(A1)') ICHANG
680          CALL IYESNO(ICHANG)
681          IF(ICHANG.EQ.'Y') THEN
682 2266          CONTINUE
683              WRITE(*,*)
684              WRITE(*,*)'ENTER (1) TO CHANGE AND (2) TO INSERT.'
685              READ(*,*,ERR=2266) ICHAINS
686              CALL IONETWO(ICHAINS)
687              IF(ICHAINS.EQ.1) THEN
688 2267          CONTINUE
689              WRITE(*,*)
690              WRITE(*,*)'PLEASE ENTER THE INDEX NUMBER J'
691              READ(*,*,ERR=2267) JI
692              IF(JI.LE.0.OR.JI.GE.I+1) THEN
693                  CALL INCORRES
694                  GO TO 2267
695              ENDIF
696              WRITE(*,*)
697              WRITE(*,*)'PLEASE ENTER THE NEW VALUES FOR '
698              WRITE(*,*)'TIME(J) AND RADIUS(J). '
699 2270          READ(*,*,ERR=2270) TMA(JI), RA(JI)
700              GO TO 2260
701          ELSE IF(ICHAINS.EQ.2) THEN
702 2272          CONTINUE
703              WRITE(*,*)
704              WRITE(*,*)'ENTER THE INDEX NUMBER J YOU WISH TO '
705              WRITE(*,*)'CHANGE, (OR PUSH DOWN).'
706              READ(*,*,ERR=2272) JI
707              IF(JI.LE.0.OR.JI.GE.I+1) THEN
708                  CALL INCORRES
709                  GO TO 2272
710              ENDIF
711              I = I+1
712              DO 2278 J=JI,I-1
1 713              TMA( I+JI-J ) = TMA( (I-1)+JI-J )

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1  714          RA( I+JI-J ) = RA( (I-1)+JI-J )
1  715 2278      CONTINUE
      716          WRITE(*,*)
      717          WRITE(*,*)'PLEASE ENTER THE NEW VALUES FOR'
      718          WRITE(*,*)'TIME(J) AND RADIUS(J).'

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      727          WRITE(*,*)'FROM THE DATA POINTS, (Y/N)?'
      728          READ(*, '(A1)') IDEL
      729          CALL IYESNO(IDEL)
      730          IF(IDEL.EQ.'Y') THEN
      731 2282          CONTINUE
      732              WRITE(*,*)
      733              WRITE(*,*)'PLEASE ENTER THE DELAY TO BE SUBTRACTED.'
      734              READ(*,*,ERR=2282) DELAY
      735              WRITE(*,*)
      736              WRITE(*,2283) DELAY
      737 2283          FORMAT(' THE DELAY ENTERED IS ',F10.4,' (SEC.)',/,
      738              ' DO YOU WISH TO CHANGE IT, (Y/N)?')
      739              READ(*, '(A1)') ICHANG
      740              IF(ICHANG.EQ.'Y') GO TO 2282
      741          ELSE IF(IDEL.EQ.'N') THEN
      742              DELAY = 0.0
      743              GO TO 2341
      744          ENDIF
      745          DO 2284 J = 1, ICOUNT
1  746              TMA(J) = TMA(J) - DELAY
1  747 2284          CONTINUE
      748          IBACK = 1
      749          GO TO 2261
      750      ENDIF
      751          IBACK = 0
      752          RINIT = RA(1)
      753      ELSE IF(IRELPSE.EQ.2) THEN
      754          IF(IRUNAG.GE.1.OR.IMISTAK.EQ.'Y') GO TO 2319
      755          WRITE(*,*)
      756          WRITE(*,*)'SINCE YOU HAVE CHOSEN THE PSEUDO-EXPERIMENTAL'
      757          WRITE(*,*)'OPTION, THE FOLLOWING PARAMETERS MUST ALSO'
      758          WRITE(*,*)'BE ENTERED.'
      759          WRITE(*,*)
      760 2300          CONTINUE

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761      WRITE(*,*)'THE PERMEABILITY VALUE WITH WHICH THE PROGRAM'
762      WRITE(*,*)'GENERATES PSEUDO-EXPERIMENTAL DATA, PTRU, '
763      WRITE(*,*)'(MICRONS/SEC.).'
764      READ(*,*,ERR=2300) PTRU
765 2303  CONTINUE
766      WRITE(*,*)
767      WRITE(*,*)'DO YOU WISH TO ENTER THE INITIAL RADIUS USING UNITS'
768      WRITE(*,*)'OF (1) MICRONS OR (2) CENTIMETERS, (ENTER 1 OR 2)?'
769      READ(*,*,ERR=2303) IMICCEN
770      CALL IONETWO(IMICCEN)
771 2305  CONTINUE
772      WRITE(*,*)
773      WRITE(*,*)'PLEASE ENTER THE INITIAL RADIUS OF THE CELL, RINIT,'
774      IF(IMICCEN.EQ.1) WRITE(*,*)'(MICRONS).'
775      IF(IMICCEN.EQ.2) WRITE(*,*)'(CENTIMETERS).'
776      READ(*,*,ERR=2305) RINIT
777 2310  CONTINUE
778      WRITE(*,*)
779      WRITE(*,*)'SINCE THIS IS A SIMULATION THE DATA POINTS '
780      WRITE(*,*)'GENERATED WILL HAVE A RADIUS HISTORY THAT WILL'
781      WRITE(*,*)'LOOK EXACTLY LIKE THAT OF THEORY, THEREFORE'
782      WRITE(*,*)'THE PROGRAM ALLOWS THE USER TO IMPOSE A PSEUDO-'

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783      WRITE(*,*)'RANDOMNESS FACTOR, DR, ON THE DATA. DR CAN BE'
784      WRITE(*,*)'THOUGHT OF AS THE MAGNITUDE OF THE VARIATION'
785      WRITE(*,*)'IN MEASURING THE RADIUS OF THE CELL.'
786      WRITE(*,*)'PLEASE ENTER DR NOW.'
787      IF(IMICCEN.EQ.1) WRITE(*,*)'(MICRONS).'
788      IF(IMICCEN.EQ.2) WRITE(*,*)'(CENTIMETERS).'
789      READ(*,*,ERR=2310) DR
790      WRITE(*,*)
791      WRITE(*,*)'WHEN USING THIS OPTION THE USER CAN CHANGE'
792      WRITE(*,*)'THE TIME STEP IN TWO REGIONS TO STUDY THE '
793      WRITE(*,*)'EFFECT OF DATA SPACING OF PARAMETER ESTIMATION.'
794      WRITE(*,*)'DO YOU WISH TO DO THIS, (Y/N)? '
795      READ(*, '(A1)') IMORE
796      CALL IYESNO(IMORE)
797      IF(IMORE.EQ.'N') THEN
798          TM01 = TM1
799          DT1 = DT
800          DT2 = DT
801      ELSE IF(IMORE.EQ.'Y') THEN
802 2311  CONTINUE
803          WRITE(*,*)
804          WRITE(*,*)'PLEASE ENTER THE FIRST TIME STEP, DT1, (SEC.). '
805          READ(*,*,ERR=2311) DT1
806 2312  CONTINUE
807          WRITE(*,*)

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808      WRITE(*,*)'PLEASE ENTER THE SECOND TIME STEP, DT2, (SEC.) '
809      READ(*,*,ERR=2312) DT2
810 2313      CONTINUE
811      WRITE(*,*)
812      WRITE(*,*)'PLEASE ENTER THE INTERMEDIATE TIME LIMIT, TM01,'
813      WRITE(*,*)'(SEC.) FOR THE FIRST TIME INTERVAL. (TM01 '
814      WRITE(*,*)'TO TM1 IS ASSUMED TO BE THE SECOND TIME '
815      WRITE(*,*)'INTERVAL.)'
816      READ(*,*,ERR=2313) TM01
817      ENDIF
818 C
819 2319      CONTINUE
820      IF(IMICCEN.EQ.1) XMICCEN ='MICRONS'
821      IF(IMICCEN.EQ.2) XMICCEN ='CENTIMETERS'
822      WRITE(*,*)
823      WRITE(*,2320) PTRU,RINIT,XMICCEN,DR,XMICCEN,DT1,DT2,TM01
824 2320      FORMAT(1X,'THE VALUES ENTERED FOR THE PSEUDO-EXPERIMENTAL'
825      , ' OPTION ARE:',/,
826      . 1X,'1) PSEUDO-PERMEABILITY - ',F8.1,' MICRONS/SEC.',/,
827      . 1X,'2) INITIAL CELL RADIUS - ',E11.3,1X,A11,/,
828      . 1X,'3) RADIUS RANDOMNESS - ',E11.4,1X,A11,/,
829      . 1X,'4) FIRST TIME STEP - ',F7.2,' SEC.',/,
830      . 1X,'5) SECOND TIME STEP - ',F7.2,' SEC.',/,
831      . 1X,'6) INTERMEDIATE TIME LIMIT - ',F8.1,' SEC.',/)
832      WRITE(*,*)'DO YOU WISH TO CHANGE ANY OF THEM, (Y/N)?'
833      READ(*,'(A1)') ICHANG
834      CALL IYESNO(ICHANG)
835      IF(ICHANG.EQ.'Y') THEN
836 2330      CONTINUE
837      WRITE(*,*)
838      WRITE(*,*)'PLEASE ENTER THE NUMBER BESIDE THE PARAMETER'

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839      WRITE(*,*)'YOU WISH TO CHANGE, (1-5). '
840      READ(*,*,ERR=2330) NCHANG
841 2340      CONTINUE
842      WRITE(*,*)
843      WRITE(*,*)'PLEASE ENTER THE NEW VALUE. '
844      IF(NCHANG.EQ.1) THEN
845          READ(*,*,ERR=2340) PTRU
846      ELSE IF(NCHANG.EQ.2) THEN
847          READ(*,*,ERR=2340) RINIT
848      ELSE IF(NCHANG.EQ.3) THEN
849          READ(*,*,ERR=2340) DR
850      ELSE IF(NCHANG.EQ.4) THEN
851          READ(*,*,ERR=2340) DT1
852      ELSE IF(NCHANG.EQ.5) THEN
853          READ(*,*,ERR=2340) DT2
854      ELSE IF(NCHANG.EQ.6) THEN

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855             READ(*,*,ERR=2340) TM01
856             ELSE IF(NCHANG.LE.0.OR.NCHANG.GE.7) THEN
857                 CALL INCORRES
858                 GO TO 2330
859             ENDIF
860             GO TO 2319
861         ENDIF
862     ENDIF
863 C
864 2341 CONTINUE
865     IF1 = 0
866     IF2 = 0
867     IF3 = 0
868     IF4 = 0
869     CON1 = 'O_CON1.DAT'
870     CON2 = 'O_CON2.DAT'
871     SENC = 'O_SENC.DAT'
872     VOL1 = 'O_VOL1.DAT'
873     VOL2 = 'O_VOL2.DAT'
874     SUMR = 'O_SUMR.DAT'
875     WRITE(*,*) 'DO YOU WISH TO HAVE FILES CREATED SO THAT YOU CAN'
876     WRITE(*,*) 'USE PLOTIT TO GENERATE GRAPHICAL OUTPUT, (Y/N)?'
877     READ(*, '(A1)') IGRAPH
878     CALL IYESNO(IGRAPH)
879     IF(IGRAPH.EQ.'Y') THEN
880 2342         CONTINUE
881             WRITE(*,*)
882             WRITE(*,*) 'THE OUTPUT CAN BE VIEWED IN THE FOLLOWING WAYS:'
883             WRITE(*,*)
884             WRITE(*,*) '1) CONCENTRATION V.S. DIMENSIONLESS TIME'
885             WRITE(*,*) '2) SENSITIVITY COEFFICIENT V.S. TIME'
886             WRITE(*,*) '3) NORMALIZED VOLUME V.S. TIME'
887             WRITE(*,*) '4) SUM OF SQUARE OF ERRORS V.S. PERMEABILITY'
888             WRITE(*,*)
889             WRITE(*,*) 'WHICH GRAPHICAL OPTION WOULD YOU LIKE (1-4), -'
890             WRITE(*,*) '(PLEASE CHOOSE ONE GRAPH AT A TIME).'
891 2343         CONTINUE
892             READ(*,*,ERR=2343) IOPTGR
893             IF(IOPTGR.LE.0.OR.IOPTGR.GE.5) THEN
894                 CALL INCORRES

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895             GO TO 2342
896         ENDIF
897         WRITE(*,*)
898         WRITE(*,*) '(NOTE: WHEN ENTERING THE FILE NAME USE 10'
899         WRITE(*,*) ' CHARACTERS OR LESS.)'
900         IF(IOPTGR.EQ.1) THEN
901             IF1 = 1

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902 2344      CONTINUE
903          WRITE(*,*)'THE DATA GENERATED FOR THE GRAPH CONCENTRATION'
904          WRITE(*,*)'V.S. DIMENSIONLESS TIME REQUIRES THE USER TO '
905          WRITE(*,*)'CHOOSE TWO FILE NAMES.'
906          WRITE(*,*)
907          WRITE(*,*)'PLEASE ENTER THE NAME FOR THE FIRST DATA SET,'
908          WRITE(*,*)'(CA(I) V.S. TIME(I)/TMAX).'
909          READ(*,'(A10)',ERR=2344) CON1
910          CALL CHANNAM(CON1)
911 2345      CONTINUE
912          WRITE(*,*)
913          WRITE(*,*)'PLEASE ENTER THE NAME FOR THE SECOND DATA SET,'
914          WRITE(*,*)'(CB(I) V.S. TIME(I)/TMAX).'
915          READ(*,'(A10)',ERR=2345) CON2
916          CALL CHANNAM(CON2)
917      ELSE IF(IOPTGR.EQ.2) THEN
918          IF2 = 1
919 2346      CONTINUE
920          WRITE(*,*)'PLEASE ENTER THE FILE NAME YOU DESIRE FOR THE'
921          WRITE(*,*)'GRAPH - SENSITIVITY COEFFICIENT V.S. TIME.'
922          WRITE(*,*)'(SEN(I) V.S. TIME(I)).'
923          READ(*,'(A10)',ERR=2346) SENC
924          CALL CHANNAM(SENC)
925      ELSE IF(IOPTGR.EQ.3) THEN
926          IF3 = 1
927 2347      CONTINUE
928          WRITE(*,*)'THE DATA GENERATED FOR THE GRAPH OF NORMALIZED'
929          WRITE(*,*)'VOLUME V.S. TIME REQUIRES THE USER TO CHOOSE'
930          WRITE(*,*)'TWO FILE NAMES. THE FIRST FILE WILL CONTAIN'
931          IF(IRELPS.EQ.1) THEN
932              WRITE(*,*)'THE ACTUAL DATA POINTS ENTERED (WHICH ARE'
933              WRITE(*,*)'CONVERTED TO NORMALIZED VOLUME). THE '
934              WRITE(*,*)'SECOND FILE WILL CONTAIN THE DATA FOR THE'
935              WRITE(*,*)'BEST FIT CURVE BASED OF THE PERMEABILITY'
936              WRITE(*,*)'ESTIMATED FROM THE DATA ENTERED.'
937          ELSE IF(IRELPS.EQ.2) THEN
938              WRITE(*,*)'THE SIMULATED DATA POINTS, WITH AN IMPOSED'
939              WRITE(*,*)'RANDOMNESS TO THE DATA, BASED ON THE TRUE'
940              WRITE(*,*)'PERMEABILITY ENTERED. THE SECOND FILE WILL'
941              WRITE(*,*)'CONTAIN THE DATA FOR THE BEST FIT CURVE'
942              WRITE(*,*)'BASED ON THE TRUE PERMEABILITY ENTERED ALSO.'
943          ENDIF
944          WRITE(*,*)
945          WRITE(*,*)'PLEASE ENTER THE NAME FOR THE FIRST DATA SET,'
946          WRITE(*,*)'(VOLA(I) V.S. TIME(I)).'
947          READ(*,'(A10)',ERR=2347) VOL1
948          CALL CHANNAM(VOL1)
949 2348      CONTINUE
950          WRITE(*,*)

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951      WRITE(*,*)'PLEASE ENTER THE NAME FOR THE SECOND DATA SET,'
952      WRITE(*,*)'(VOLC(I) V.S. TIME(I)).'
953      READ(*, '(A10)',ERR=2348) VOL2
954      CALL CHANNAM(VOL2)
955      ELSE IF(IOPTGR.EQ.4) THEN
956          IF4 = 1
957 2349      CONTINUE
958          WRITE(*,*)'PLEASE ENTER THE FILE NAME YOU DESIRE FOR THE'
959      WRITE(*,*)'GRAPH - SUM OF SQUARE OF ERRORS V.S. PERMEABILITY,'
960          WRITE(*,*)'(SUM(I) V.S. P(I)).'
961          READ(*, '(A10)',ERR=2349) SUMR
962          CALL CHANNAM(SUMR)
963      ENDIF
964      WRITE(*,*)
965      WRITE(*,*)'DO YOU WISH TO CHOOSE ANOTHER FILE NAME FOR'
966      WRITE(*,*)'ANOTHER DATA SET, (Y/N)?'
967      READ(*, '(A1)') IANOTH
968      CALL IYESNO(IANOTH)
969      IF(IANOTH.EQ.'Y') GO TO 2342
970  ENDIF
971      WRITE(*,*)
972      WRITE(*,*)'HAVE YOU MADE ANY MISTAKES THAT YOU WOULD LIKE '
973      WRITE(*,*)'ANOTHER CRACK AT ENTERING/CHANGING THE PARAMETERS '
974      WRITE(*,*)'OR DATA AGAIN, (Y/N)?'
975      READ(*, '(A1)') IMISTAK
976      CALL IYESNO(IMISTAK)
977      IF(IMISTAK.EQ.'Y') GO TO 2180
978      WRITE(*,*)
979      WRITE(*,*)'OKAY, THE PROGRAM IS NOW CRUNCHING.'
980      GO TO 3999
981 C-----
982 C      OPTION ITERINP = 2:  ENTERING THE INPUT FILE
983 C-----
984 2999  CONTINUE
985      OPEN(11,FILE=ISENS,STATUS='OLD')
986      READ(11,'(A11)') PROBLEM
987      READ(11,3100) RL1,RL2,LIP
988 3100  FORMAT(///,1X,F11.6,F11.6,I2)
989      READ(11,3110) D1,D2,H
990 3110  FORMAT(//,1X,E9.3,2X,E9.3,2X,E9.3)
991      READ(11,3120) CINIT, CINF
992 3120  FORMAT(//,1X,F11.6,F11.6)
993      READ(11,3125) VINA,RMAG
994 3125  FORMAT(//,1X,F11.6,F11.6)
995      READ(11,3130) DT,TM0,TM1,DELAY
996 3130  FORMAT(//,1X,F11.6,F11.6,F11.6,F11.6)
997      READ(11,3140) DP,P0,P1,PSEN
998 3140  FORMAT(//,1X,F11.6,F11.6,F11.6,F11.6)
999      READ(11,3145) RINIT
1000 3145  FORMAT(//,1X,F11.6)

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1001      READ(11,3150) PTRU,DR,TM01,DT1,DT2
1002 3150  FORMAT(///,1X,F11.6,F11.6,F11.6,F11.6,F10.6)
1003      READ(11,3160) IRELPS,IMICCEN
1004 3160  FORMAT(///,1X,I1,10X,I1)
1005      READ(11,3170) IF1,IF2,IF3,IF4,IPRINT
1006 3170  FORMAT(///,1X,I1,10X,I1,10X,I1,10X,I1,10X,I2,/)

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1007      READ(11,3175) CON1,CON2,SENC,VOL1,VOL2,SUMR
1008 3175  FORMAT(/,1X,A10,1X,A10,/,1X,A10,/,1X,A10,1X,A10,/,1X,A10,///)
1009 C
1010      IF(IMICCEN.EQ.1) XMICCEN='MICRONS'
1011      IF(IMICCEN.EQ.2) XMICCEN='CENTIMETERS'
1012 C
1013 C-----
1014 C      WRITING THE INPUT DATA TO THE OUTPUT FILE O_SENS.DAT
1015 C-----
1016      WRITE(*,3180) ISENS
1017 3180  FORMAT(/,' THE INPUT FILE ',A10,' HAS BEEN ENTERED. ')
1018 3999  CONTINUE
1019      IF(IOPNAG.EQ.0) THEN
1020          OPEN(10,FILE='O_SENS.DAT',STATUS='NEW')
1021          OPEN(20,FILE='O_SMRY.DAT',STATUS='NEW')
1022      ENDIF
1023      WRITE(10,4000) ISENS
1024 4000  FORMAT(1X,'***** THE INPUT FILE ',A10,
1025          .   ' *****',/)
1026      WRITE(10,4005)
1027 4005  FORMAT(/,'RL1,RL2,LIP ARE',/)
1028      WRITE(10,*)RL1,RL2,LIP
1029      WRITE(10,4010)
1030 4010  FORMAT(/,'D1,D2,H ARE:',/)
1031      WRITE(10,*) D1,D2,H
1032      WRITE(10,4020)
1033 4020  FORMAT(/,'CINIT,CINF ARE:',/)
1034      WRITE(10,*) CINIT,CINF
1035      WRITE(10,4030)
1036 4030  FORMAT(/,'VINA,RMAG ARE:',/)
1037      WRITE(10,*) VINA,RMAG
1038      WRITE(10,4040)
1039 4040  FORMAT(/,'DT,TM0,TM1,DELAY ARE:',/)
1040      WRITE(10,*) DT,TM0,TM1,DELAY
1041      WRITE(10,4050)
1042 4050  FORMAT(/,'DP,P0,P1,PSEN ARE:',/)
1043      WRITE(10,*) DP,P0,P1,PSEN
1044      WRITE(10,4060)
1045 4060  FORMAT(/,'RINIT IS:',/)
1046      WRITE(10,*) RINIT
1047      WRITE(10,4070)

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1048 4070  FORMAT(/,'PTRU,DR,TM01,DT1,DT2 ARE:',/)
1049      WRITE(10,*) PTRU,DR,TM01,DT1,DT2
1050      WRITE(10,4080)
1051 4080  FORMAT(/,'IRELPSE,IMICCEN ARE:',/)
1052      WRITE(10,*) IRELPSE, IMICCEN
1053      WRITE(10,4090)
1054 4090  FORMAT(/,'IF1,IF2,IF3,IF4,IPRINT ARE:',/)
1055      WRITE(10,*) IF1,IF2,IF3,IF4,IPRINT
1056      WRITE(10,4100)
1057 4100  FORMAT(/,'CON1,CON2,SENC,VOL1,VOL2,SUMR ARE:'
1058      ,/)
1059      WRITE(10,4110) CON1,CON2,SENC,VOL1,VOL2,SUMR
1060 4110  FORMAT(A10,5X,A10,/,A10,/,A10,5X,A10,/,A10)
1061 C
1062 C-----

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1063 C      USING SUBROUTINE MBCON TO PREDICT THE CONCENTRATION
1064 C      CHANGE INSIDE THE CELL CHAMBER
1065 C-----
1066      WRITE(*,*)
1067      WRITE(*,*)'ENTERING SUBROUTINE MBCON.'
1068      CALL MBCON(TMS,CA,CB,IP)
1069      WRITE(*,*)
1070      WRITE(*,*)'LEAVING MBCON.'
1071 C-----
1072 C      IF IF1=1 (YES), WRITE DATA TO CON1 AND CON2
1073 C-----
1074      IF(IF1.EQ.0) GO TO 4150
1075      OPEN(14,FILE=CON1,STATUS='NEW')
1076      OPEN(15,FILE=CON2,STATUS='NEW')
1077      DO 4140 I=1,IP
1 1078          WRITE(14,4135) TMS(I),CA(I)
1 1079          WRITE(15,4135) TMS(I),CB(I)
1 1080 4135      FORMAT(1X,F6.4,1X,',',1X,E9.3)
1 1081 4140      CONTINUE
1082      WRITE(*,*)
1083      WRITE(*,*)'THE DATA FOR THE GRAPH CONCETRATION V.S. '
1084      WRITE(*,*)'DIMENSIONLESS TIME HAS BEEN SENT TO FILES -'
1085      WRITE(*,4142) CON1, CON2
1086 4142      FORMAT(1X,A10,' AND ',A10)
1087      CLOSE(14,STATUS='KEEP')
1088      CLOSE(15,STATUS='KEEP')
1089 4150  CONTINUE
1090 C-----
1091 C      INITIALIZATION OF THE TIME VARIABLES AND RINIT
1092 C-----
1093      IT=INT((TM1-TM0)/DT)+1
1094      DO 4170 I=1,IT

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1 1095      TMS(I)=TMO+(I-1)*DT
1 1096      TMB(I)=TMS(I)
1 1097 4170  CONTINUE
1098      IF(IMICCEN.EQ.1) THEN
1099          RINIT = RINIT/RMAG
1100      ELSE IF(IMICCEN.EQ.2) THEN
1101          RINIT = RINIT*10000./RMAG
1102      ENDIF
1103 C-----
1104 C      CALCULATE R(TM,P) AND R(TM,P+DP)
1105 C-----
1106      WRITE(*,*)
1107      WRITE(*,*)'CALCULATING R(TM,P). '
1108      CALL RGKT(TMS,RS,IT,DT,RINIT,PSEN)
1109      WRITE(*,*)
1110      WRITE(*,*)'CALCULATING R(TM,P+DP). '
1111      CALL RGKT(TMB,RB,IT,DT,RINIT,PSEN+EP1*PSEN)
1112 C-----
1113 C      CALCULATE SENSITIVITY COEFF. (SEN)
1114 C-----
1115      WRITE(10,4175)
1116 4175  FORMAT(/,1X,'***** DIMENSIONLESS SENSIVITY ',
1117      .      'COEFFICIENT VERSUS TIME *****')
1118      WRITE(*,*)

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1119      WRITE(*,*)'CALCULATING SENSITIVITY COEFFICIENT, SEN.'
1120      WRITE(10,4180)
1121 4180  FORMAT(/,6X,'TIME(I)',7X,'SEN(I)',/)
1122      DO 4190 J=1,IT
1 1123          SEN(J)=(RB(J)-RS(J))*PSEN/RINIT/(EP1*PSEN)
1 1124          WRITE(10,4185)TMS(J),SEN(J)
1 1125 4185  FORMAT(5X,F7.2,5X,E10.3)
1 1126 4190  CONTINUE
1127 C-----
1128 C      IF IF2 = 1 (YES), WRITE DATA TO SENC
1129 C-----
1130      IF(IF2.EQ.0)GO TO 4230
1131 C-----
1132      OPEN(16,FILE=SENC,STATUS='NEW')
1133      DO 4220 I=1,IT
1 1134          WRITE(16,4210) TMS(I),SEN(I)
1 1135 4210  FORMAT(1X,F8.2,1X,',',1X,E9.3)
1 1136 4220  CONTINUE
1137      WRITE(*,*)
1138      WRITE(*,*)'THE DATA FOR THE GRAPH OF THE SENSITIVITY '
1139      WRITE(*,*)'COEFFICIENTS V.S. TIME HAS BEEN SENT TO FILE -'
1140      WRITE(*, '(1X,A10)') SENC
1141      CLOSE(16,STATUS='KEEP')

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1142 4230  CONTINUE
1143      WRITE(10,*)
1144 4235  FORMAT(1X,'*****' , 'RADIUS VERSUS TIME',
1145      .      '*****')
1146 C-----
1147 C      READING THE EXPERIMENTAL DATA AND CONVERTING TO MICRONS
1148 C-----
1149      IF (IRELPSE.EQ.1.AND.ITERINP.EQ.2) THEN
1150          WRITE(10,4235)
1151          I=0
1152          WRITE(10,4240)
1153 4240      FORMAT(/,6X,'TM(I)',10X,'R(I)',/)
1154 4250      I=I+1
1155          READ(11,*)TMA(I),RA(I)
1156          RSAVE(I) = RA(I)
1157          IF(RA(I).GT.0.) TMA(I) =TMA(I)-DELAY
1158          WRITE(10,4253) TMA(I), RA(I)
1159          IF(IMICCEN.EQ.1) THEN
1160              RA(I) = RA(I)/RMAG
1161          ELSE IF(IMICCEN.EQ.2) THEN
1162              RA(I) = RA(I)*10000./RMAG
1163          ENDIF
1164          IF(I.EQ.1) RAMAX = RA(I)
1165          IF(I.GE.2) THEN
1166              IF(RA(I).GT.RAMAX) RAMAX = RA(I)
1167          ENDIF
1168          IF ((TMA(I).GT.0.).OR.(RA(I).GT.0.)) GO TO 4250
1169          ICOUNT=I-1
1170          IF (TM1.LE.TMA(ICOUNT)) THEN
1171              WRITE(*,*)
1172              WRITE(*,*)'PLEASE MAKE SURE TM1 IS LARGER THAN THE TIME'
1173              WRITE(*,*)'OF THE LAST DATA POINT, AND RUN IT AGAIN.'
1174              GO TO 6000

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1175      END IF
1176 C-----
1177 C      CONVERTING INPUT DATA, ENTERED BY THE TERMINAL, TO MICRONS
1178 C-----
1179      ELSE IF(IRELPSE.EQ.1.AND.ITERINP.EQ.1) THEN
1180          WRITE(10,4235)
1181          WRITE(10,4240)
1182          DO 4255 K=1,ICOUNT+1
1 1183      RSAVE(K) = RA(K)
1 1184      WRITE(10,4253) TMA(K),RA(K)
1 1185 4253      FORMAT(5X,F7.2,5X,E11.5)
1 1186 4255      CONTINUE
1187          IF(IMICCEN.EQ.1)THEN
1188              DO 4260 K=1,ICOUNT

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1 1189          RA(K) = RA(K)/RMAG
1 1190 4260      CONTINUE
1191          RAMAX = RAMAX/RMAG
1192      ELSE IF(IMICCEN.EQ.2) THEN
1193          DO 4270 K=1,ICOUNT
1 1194              RA(K) = RA(K)*10000./RMAG
1 1195 4270      CONTINUE
1196          RAMAX = RAMAX*10000./RMAG
1197      ENDIF
1198 C-----
1199 C      GENERATING THE SIMULATED (PSEUDO) EXPERIMENTAL DATA
1200 C-----
1201      ELSE IF(IRELPS.EQ.2) THEN
1202          ICOUNT = ((TM01-TM0)/DT1+(TM1-TM01)/DT2+1)
1203          CALL RGKT(TMS,RB,IT,DT,RINIT,PTRU)
1204          DO 4280 J=1,IT
1 1205              TMA(J) = TMS(J)
1 1206              RC(J) = RB(J)
1 1207 4280      CONTINUE
1208          TMA(1) = TM0
1209          DO 4290 J=2,ICOUNT
1 1210              IF (TMA(J-1).LT.TM01) THEN
1 1211                  TMA(J)=TMA(J-1)+DT1
1 1212              ELSE IF (TMA(J-1).GE.TM01) THEN
1 1213                  TMA(J)=TMA(J-1)+DT2
1 1214              END IF
1 1215 4290      CONTINUE
1216          IF(IMICCEN.EQ.1) THEN
1217              DR = DR/RMAG
1218          ELSE IF(IMICCEN.EQ.2) THEN
1219              DR = DR*10000./RMAG
1220          ENDIF
1221          RAMAXC = RC(1)
1222          DO 4292 J=2,IT
1 1223              IF(RC(J).GT.RAMAXC) RAMAXC = RC(J)
1 1224 4292      CONTINUE
1225          RAMAX = RB(1)
1226          RA(1) = RB(1)
1227          DO 4300 J=2,ICOUNT
1 1228              ITM=INT(TMA(J)/DT)+1
1 1229              IF (ITM.GE.IT) THEN
1 1230                  RA(J)=RB(ITM)+DR*RANND(XSEED,ISC)

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1 1231      ELSE
1 1232          DRA=(RB(ITM+1)-RB(ITM))*(TMA(J)-(ITM-1)*DT)/DT
1 1233          RA(J)=RB(ITM)+DRA+DR*RANND(XSEED,ISC)
1 1234      END IF
1 1235      IF(RA(J).GT.RAMAX) RAMAX = RA(J)

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1 1236 4300      CONTINUE
      1237      WRITE(10,*)
      1238      WRITE(10,4302)
      1239 4302  FORMAT(1X,'***** SIMULATED RADIUS VERSUS TIME'
      1240      ' *****')
      1241      WRITE(10,*)
      1242      DO 4305 J=1,ICOUNT+1
1 1243          IF(IMICCEN.EQ.1) THEN
1 1244              RSAVE(J) = RA(J)*RMAG
1 1245          ELSE IF(IMICCEN.EQ.2) THEN
1 1246              RSAVE(J) = RA(J)*RMAG/10000.
1 1247          ENDIF
1 1248 4305      CONTINUE
      1249      WRITE(10,4240)
      1250      DO 4310 J = 1,ICOUNT
1 1251          WRITE(10,4253) TMA(J), RSAVE(J)
1 1252 4310      CONTINUE
      1253      ENDIF
      1254 C-----
      1255 C      CALCULATING THE NORMALIZED VOLUME
      1256 C-----
      1257      DO 4315 I=1,ICOUNT
1 1258          VOLA(I)=(RA(I)/RAMAX)**3
1 1259          IF(IRELPSE.EQ.2) VOLC(I) =(RC(I)/RAMAXC)**3
1 1260 4315      CONTINUE
      1261 C-----
      1262 C      CALCULATE SUM OF ERROR OF SQUARE FOR P VALUES FROM
      1263 C      P0 TO P1
      1264 C-----
      1265      WRITE(*,*)
      1266      WRITE(*,*)'CALCULATING SUM OF SQUARE OF ERRORS FROM P0 TO P1.'
      1267      IP=(P1-P0)/DP+1
      1268      DO 4330 I=1,IP
1 1269          P(I)=P0+(I-1)*DP
1 1270          CALL RGKT(TMB,RB,IT,DT,RINIT,P(I))
1 1271          SUM(I)=0.
1 1272          DO 4320 J=1,ICOUNT
2 1273              ITM=INT(TMA(J)/DT)+1
2 1274              IF (ITM.GE.IT) THEN
2 1275                  RN=RB(ITM)
2 1276              ELSE
2 1277                  DRN=(RB(ITM+1)-RB(ITM))*(TMA(J)-(ITM-1)*DT)/DT
2 1278                  RN=RB(ITM)+DRN
2 1279              END IF
2 1280              SUM(I)=SUM(I)+(RN-RA(J))**2
2 1281 4320          CONTINUE
1 1282 4330      CONTINUE
      1283 C-----
      1284 C
      1285 C-----
      1286      WRITE(10,4332)

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1287 4332  FORMAT(///,1X,'*****      SUM OF SQUARES OF ERRORS ',
1288      .      'VERSUS PERMEABILITY *****')
1289      WRITE(10,4335)
1290 4335  FORMAT(/,'      P(J)      SUM(J)',/)
1291      DO 4338 J=1,IP
1 1292      WRITE(10,4460) P(J),SUM(J)
1 1293 4338  CONTINUE
1294 C
1295      SUMIN=SUM(1)
1296      PEST = P(1)
1297      DO 4340 I=2,IP
1 1298      IF (SUMIN.GT.SUM(I)) THEN
1 1299      SUMIN=SUM(I)
1 1300      PEST=P(I)
1 1301      END IF
1 1302 4340  CONTINUE
1303      CALL RGKT(TMB,RC,IT,DT,RINIT,PEST)
1304      CALL RGKT(TMB,RB,IT,DT,RINIT,PEST+EP1*PEST)
1305      DO 4350 J=1,IT
1 1306      SEN(J) = (RB(J)-RC(J))/(EP1*PEST)
1 1307 4350  CONTINUE
1308      DO 4360 J=1,ICOUNT
1 1309      ITM=INT(TMA(J)/DT)+1
1 1310      IF (ITM.GE.IT) THEN
1 1311      SEN(J)=SEN(ITM)
1 1312      ELSE
1 1313      DSEN=(SEN(ITM+1)-SEN(ITM))*(TMA(J)-(ITM-1)*DT)/DT
1 1314      SEN(J)=SEN(ITM)+DSEN
1 1315      END IF
1 1316 4360  CONTINUE
1317      SENSUM=0.
1318      DO 4365 I=1,ICOUNT
1 1319      SENSUM=SENSUM+SEN(I)**2
1 1320 4365  CONTINUE
1321 C----
1322 C      DUMPING SUMMARY INPUT PARAMETERS, INPUT DATA AND RESULTING
1323 C      PEST, SDP, SUMIN TO 'O_SMRY.DAT'
1324 C----
1325      WRITE(20,*)
1326      WRITE(20,4366)
1327 4366  FORMAT(//,'*****      THIS IS FILE',
1328      .      ' O_SMRY.DAT *****',/)
1329      WRITE(20,4367)
1330 4367  FORMAT(/,'THE INPUT PARAMETERS AND DATA WERE:',/)
1331      WRITE(20,2190) RL1,RL2,LIP,D2,D1,H,CINIT,CINF,VINA,RMAG
1332      WRITE(20,*)
1333      WRITE(20,2240) DT,TMO,TM1,DP,PO,P1,PSEN
1334      IF(IRELPSE.EQ.1) THEN

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1335      WRITE(20,*)
1336      WRITE(20,*)'THE DATA POINTS ENTERED WERE:'
1337      WRITE(20,2262) DELAY
1338      WRITE(20,*)
1339      WRITE(20,*)'  J          TIME(J)          RADIUS(J) '
1340      IF(IMICCEN.EQ.1) THEN
1341      WRITE(20,*)'          (SEC.)          (MICRONS) '
1342      ELSEIF(IMICCEN.EQ.2) THEN

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1343      WRITE(20,*)'          (SEC.)          (CENTIMETERS) '
1344      ENDIF
1345      DO 4368 J=1,ICOUNT+1
1 1346          WRITE(20,2263) J,TMA(J),RA(J)
1 1347 4368      CONTINUE
1348      ELSEIF(IRELSPE.EQ.2) THEN
1349      WRITE(20,*)
1350      WRITE(20,2320) PTRU,RINIT,XMICCEN,DR,XMICCEN,DT1,DT2,TM01
1351      ENDIF
1352 C----
1353 C      THE ESITMATED PERMEABILITY
1354 C----
1355      WRITE(10,4375)
1356      WRITE(20,4375)
1357 4375      FORMAT(///,'***** THE RESULTING '
1358      .      'PERMEABILITY *****',/)
1359      SDP=SQRT(SUMIN/(ICOUNT-1)/SENSUM)
1360      WRITE(10,4380)PEST
1361      WRITE(20,4380)PEST
1362 4380      FORMAT(/,'THE LOCAL MINIMUM OCCURS AT P =',F8.3,
1363      .      ' MICRONS/SEC.')
1364      WRITE(10,4385)SDP
1365      WRITE(20,4385)SDP
1366 4385      FORMAT(/,'THE STANDARD DEVIATION OF ESTIMATED P IS ',E8.3)
1367      WRITE(10,4390)SUMIN
1368      WRITE(20,4390)SUMIN
1369 4390      FORMAT(/,'THE MINIMUM VALUE OF SUM IS',F8.3)
1370 C
1371 C
1372      IF(IRELPSE.EQ.1) THEN
1373      DO 4400 J=1,IT
1 1374          IF(J.EQ.1) RAMAXC = RC(1)
1 1375          IF(J.GE.2.AND.RC(J).GT.RAMAXC) RAMAXC = RC(J)
1 1376 4400      CONTINUE
1377      DO 4410 J=1,IT
1 1378          VOLC(J) = (RC(J)/RAMAXC)**3
1 1379 4410      CONTINUE
1380      ENDIF
1381 C-----

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1382 C      IF IF3 = 1 (YES), WRITE THE DATA TO VOL1 AND VOL2
1383 C-----
1384      IF(IF3.EQ.0) GO TO 4450
1385      OPEN(17,FILE=VOL1,STATUS='NEW')
1386      OPEN(18,FILE=VOL2,STATUS='NEW')
1387      DO 4430 J=1,ICOUNT
1 1388          WRITE(17,4420) TMA(J),VOLA(J)
1 1389 4420      FORMAT(1X,F7.2,1X,',',1X,F7.5)
1 1390 4430      CONTINUE
1391      DO 4431 J=1,IT
1 1392          WRITE(18,4420) TMS(J), VOLC(J)
1 1393 4431      CONTINUE
1394      WRITE(*,*)
1395      WRITE(*,*)'THE DATA FOR THE GRAPH NORMALIZED VOLUME V.S.'
1396      WRITE(*,*)'TIME HAS BEEN SENT TO FILES - '
1397      WRITE(*,4432) VOL1, VOL2
1398 4432      FORMAT(1X,A10,' AND ',A10)

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1399      CLOSE(17,STATUS='KEEP')
1400      CLOSE(18,STATUS='KEEP')
1401 C
1402 4450 CONTINUE
1403 C-----
1404 C      IF IF4 = 1 (YES), WRITE THE DATA TO SUMR
1405 C-----
1406      IF(IF4.EQ.0) GO TO 6000
1407      OPEN(19,FILE=SUMR,STATUS='NEW')
1408      DO 4470 J=1,IP
1 1409          WRITE(19,4460) P(J),SUM(J)
1 1410 4460      FORMAT(1X,F8.2,1X,',',1X,E9.2)
1 1411 4470      CONTINUE
1412      WRITE(*,*)
1413      WRITE(*,*)'THE DATA FOR THE GRAPH OF THE SUM OF SQUARE OF'
1414      WRITE(*,*)'ERRORS V.S. PERMEABILITY HAS BEEN SENT TO FILE - '
1415      WRITE(*,'(1X,A10)') SUMR
1416      CLOSE(19,STATUS='KEEP')
1417 6000 CONTINUE
1418      WRITE(*,*)
1419      WRITE(*,6100) PEST,SDP,SUMIN
1420 6100 FORMAT(' THE ESTIMATED PERMEABILITY IS ',F8.3,' MICRONS/SEC.',//,
1421      ' THE STANDARD DEVIATION IS ',E9.3,' MICRONS/SEC.',//,
1422      ' THE MINIMUM SUM OF THE SQUARE OF THE ERRORS IS ',E9.3)
1423 C-----
1424 C      RESETTNG THE RA(I) = RSAVE(I) AND RINIT, RAMAX TO ORIGNAL VALUES
1425 C-----
1426      IF(IMICCEN.EQ.1) THEN
1427          RINIT = RINIT * RMAG
1428          RAMAX = RAMAX * RMAG

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1429          IF(IRELPS.EQ.2) DR = DR * RMAG
1430          DO 280 K = 1, ICOUNT+1
1 1431             RA(K) = RSAVE(K)
1 1432 280      CONTINUE
1433          ELSE IF(IMICCEN.EQ.2) THEN
1434             RINIT = RINIT *RMAG/10000.
1435             RAMAX = RAMAX *RMAG/10000.
1436             IF(IRELPS.EQ.2) DR = DR *RMAG/10000.
1437             DO 290 K = 1, ICOUNT+1
1 1438                RA(K) = RSAVE(K)
1 1439 290      CONTINUE
1440          ENDIF
1441 C-----
1442 C      OPTION TO SAVE THE INPUT FILE
1443 C-----
1444          WRITE(*,*)
1445          WRITE(*,*)'DO YOU WISH TO SAVE THE INPUT DATA IN A FILE,'
1446          WRITE(*,*)'(Y/N)?'
1447          READ(*, '(A1)') ISAVE
1448          CALL IYESNO(ISAVE)
1449 319      CONTINUE
1450          IF(ISAVE.EQ.'Y') THEN
1451             IF(IEXP.EQ.1) GO TO 331
1452 320      CONTINUE
1453          WRITE(*,*)
1454          WRITE(*,*)'WHAT WOULD YOU LIKE TO NAME THIS FILE,'

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```

D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1455          WRITE(*,*)'(ENTER NO MORE THAN 10 CHARATERS)?'
1456          READ(*, '(A10)',ERR=320) NAMFIL
1457          OPEN(12,FILE=NAMFIL,STATUS='NEW')
1458          WRITE(12,325)
1459 325      FORMAT(1X,'THIS IS THE FILE YOU HAD SAVED.  YOU CAN '
1460          .      , 'USE THIS FILE AS',/, ' AN INPUT FILE IF YOU DESIRE BY'
1461          .      , ' ACCESSING THIS FILE ',/, ' WHEN YOU ARE PROMPTED FOR'
1462          .      , ' THE NAME OF AN INPUT FILE.')
1463 331      CONTINUE
1464          WRITE(12,*)'RL1          RL2          LIP'
1465          WRITE(12,332)RL1,RL2,LIP
1466 332      FORMAT(1X,F5.2,6X,F7.2,4X,I2,/)
1467          WRITE(12,*)'D1          D2          H'
1468          WRITE(12,333) D1,D2,H
1469 333      FORMAT(1X,E9.3,2X,E9.3,2X,E9.3,/)
1470          WRITE(12,*)'CINIT          CINF'
1471          WRITE(12,334) CINIT,CINF
1472 334      FORMAT(1X,F8.3,3X,F8.3,/)
1473          WRITE(12,*)'VINA          RMAG'
1474          WRITE(12,335) VINA,RMAG
1475 335      FORMAT(1X,F5.2,6X,F7.2,/)

```

```

1476      WRITE(12,*)'DT          TMO          TM1          DELAY'
1477      WRITE(12,336) DT,TMO,TM1,DELAY
1478 336    FORMAT(1X,F6.3,5X,F7.2,4X,F7.2,4X,F7.2,/)
1479      WRITE(12,*)'DP          PO          P1          PSEN'
1480      WRITE(12,337) DP,PO,P1,PSEN
1481 337    FORMAT(1X,F5.2,5X,F6.2,6X,F6.2,5X,F6.2,5X,/)
1482      WRITE(12,*)'RINIT'
1483      WRITE(12,338) RINIT
1484 338    FORMAT(1X,E9.3,/)
1485      WRITE(12,339)
1486 339    FORMAT(1X,'THE PARAMETERS FOR THE LINE BELOW ARE FOR ',
1487      .    'SIMULATION OPTION:')
1488      WRITE(12,*)'PTRU          DR          TMO1          DT1          DT2'
1489      WRITE(12,340) PTRU,DR,TMO1,DT1,DT2
1490 340    FORMAT(1X,F6.2,5X,F7.3,4X,F7.2,4X,F6.3,5X,F6.3,/)
1491      WRITE(12,341)
1492 341    FORMAT(1X,'THESE PARAMETERS BELOW ARE FOR DATA INPUT '
1493      .    ', 'CONTROL:')
1494      WRITE(12,*)'IRELPSE  IMICCEN'
1495      WRITE(12,342) IRELPSE, IMICCEN
1496 342    FORMAT(1X,I1,10X,I1,/)
1497      WRITE(12,*)'THESE PARAMETERS ARE FOR DATA OUTPUT CONTROL:'
1498      WRITE(12,*)'IF1          IF2          IF3          IF4          IPRINT'
1499      WRITE(12,345) IF1,IF2,IF3,IF4,IPRINT
1500 345    FORMAT(1X,I1,10X,I1,10X,I1,10X,I1,10X,I2,/)
1501      WRITE(12,346)
1502 346    FORMAT(1X,'THESE ARE THE FILE NAMES FOR THE GRAPHICAL ',
1503      .    'OUTPUT:')
1504      WRITE(12,347) CON1,CON2,SENC,VOL1,VOL2,SUMR
1505 347    FORMAT(/,1X,A10,1X,A10,/1X,A10,/1X,A10,1X,A10,/1X,A10,/)
1506      WRITE(12,349)
1507 349    FORMAT(1X,'THE LAST GROUP BELOW ARE THE DATA POINTS:')
1508      WRITE(12,*)'      TMA(I)          RA(I)'
1509      DO 360 I =1,ICOUNT
1 1510      WRITE(12,350) TMA(I), RA(I)

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```

D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1 1511 350      FORMAT(1X,F9.4,5X,F9.4)
1 1512 360      CONTINUE
1513      WRITE(12,*)' 0.0          0.0'
1514      CLOSE(12,STATUS='KEEP')
1515      IF(IQUIT.EQ.'Y') GO TO 600
1516      WRITE(*,*)
1517      WRITE(*,362) NAMFIL
1518 362      FORMAT(' OKAY, THE FILE ',A10,' HAS BEEN SAVED.')
1519      ENDIF
1520      CLOSE(11,STATUS='KEEP')
1521 C-----
1522 C      OPTION TO RUN THE PROGRAM AGAIN

```

```

1523 C-----
1524     WRITE(*,*)
1525     WRITE(*,*)'DO YOU WISH TO RUN THE PROGRAM AGAIN, (Y/N)?'
1526     READ(*, '(A1)') IAGAIN
1527     CALL IYESNO(IAGAIN)
1528     IOPNAG = IOPNAG + 1
1529     IF(IAGAIN.EQ.'Y') THEN
1530 500      CONTINUE
1531 C-----
1532 C      OPTION TO ENTER NEW DATA OR REVIEW OLD DATA
1533 C-----
1534     WRITE(*,*)
1535     WRITE(*,*)'DO YOU WISH TO (1) ENTER ALL NEW DATA OR '
1536     WRITE(*,*)'(2) USE AND REVIEW THE DATA ALREADY ENTERED,'
1537     WRITE(*,*)'(ENTER 1 OR 2)?'
1538     READ(*,*,ERR=500) INEWREV
1539     CALL IONETWO(INEWREV)
1540     DELAY = 0.0
1541     IBACK = 0
1542     IF(INEWREV.EQ.1) THEN
1543         IRUNAG = 0
1544         GO TO 2000
1545     ELSE IF(INEWREV.EQ.2) THEN
1546         ITERINP = 1
1547         IRUNAG = IRUNAG + 1
1548         GO TO 2180
1549     ENDIF
1550 ENDIF
1551 C-----
1552 C      STOPPING THE PROGRAM.
1553 C-----
1554 600  WRITE(*,*)
1555     WRITE(*,*)'OKAY, PROGRAM DONE.'
1556     CLOSE(10,STATUS='KEEP')
1557     CLOSE(20,STATUS='KEEP')
1558     END

```

Name	Type	Offset	P	Class
A1	REAL	8	/C1	/
A2	REAL	16	/C1	/
CA	REAL	15668		
CB	REAL	15768		
CINF	REAL	24	/C3	/
^H				
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D Line# 1	7			
CINIT	REAL	20	/C3	/
CON1	CHAR*10	15964		
CON2	CHAR*10	15974		

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COUT	REAL	16	/C2	/
D1	REAL	12	/C3	/
D2	REAL	16	/C3	/
DELAY	REAL	15904		
DMY327	REAL	0	LARGE	
DP	REAL	15908		
DR	REAL	15928		
DRA	REAL	19444		
DRN	REAL	19560		
DSEN	REAL	19732		
DT	REAL	8	/C2	/
DT1	REAL	15936		
DT2	REAL	15940		
EP1	REAL		PARAMETER	
F			EXTERNAL	
H	REAL	28	/C3	/
I	INTEGER*4	16028		
IAGAIN	CHAR*1	21420		
IANOTH	CHAR*1	18080		
IBACK	INTEGER*4	15876		
ICHAIN	INTEGER*4	17444		
ICHANG	CHAR*1	16748		
ICOUNT	INTEGER*4	16024		
IDEL	CHAR*1	17212		
IEXP	INTEGER*4	15892		
IF1	INTEGER*4	4	/C1	/
IF2	INTEGER*4	15952		
IF3	INTEGER*4	15956		
IF4	INTEGER*4	15960		
IFIRST	CHAR*1	15889		
IGRAPH	CHAR*1	18074		
II	INTEGER*4		PARAMETER	
IMICCE	INTEGER*4	15948		
IMISTA	CHAR*1	15888		
IMORE	CHAR*1	17442		
INewRE	INTEGER*4	21422		
INR	INTEGER*4	17208		
INT			INTRINSIC	
IOPNAG	INTEGER*4	15884		
IOPTGR	INTEGER*4	18076		
IP	INTEGER*4	18972		
IPRINT	INTEGER*4	0	/C1	/
IQUIT	CHAR*1	15890		
IRELPS	INTEGER*4	15944		
IRELSP	INTEGER*4	19904		
IRUNAG	INTEGER*4	15880		
ISAVE	CHAR*1	16032		
ISC	INTEGER*4	15872		
ISENS	CHAR*10	16038		
ISEPPR	INTEGER*4	16048		
IT	INTEGER*4	19024		
ITERIN	INTEGER*4	16034		

ITM INTEGER*4 19440
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D Line# 1	7		
J	INTEGER*4	17410	
JI	INTEGER*4	17448	
K	INTEGER*4	19384	
LIP	INTEGER*4	8	/C3 /
N1	INTEGER*4		PARAMETER
N3	INTEGER*4		PARAMETER
N4	INTEGER*4		PARAMETER
N5	INTEGER*4		PARAMETER
NAMFIL	CHAR*10	20516	
NCHANG	INTEGER*4	16750	
O	REAL	18472	
P	REAL	14464	
P0	REAL	15912	
P1	REAL	15916	
PEST	REAL	19716	
PROBLE	CHAR*11	18081	
PSEN	REAL	15920	
PTRU	REAL	15924	
RA	REAL	6036	
RAMAX	REAL	17358	
RAMAXC	REAL	19428	
RANND	REAL		FUNCTION
RB	REAL	7240	
RC	REAL	13260	
RINIT	REAL	0	/C2 /
RL1	REAL	0	/C3 /
RL2	REAL	4	/C3 /
RMAG	REAL	15896	
RN	REAL	19556	
RS	REAL	10852	
RSAVE	REAL	12056	
SDP	REAL	20024	
SEN	REAL	8444	
SENC	CHAR*10	15984	
SENSUM	REAL	19736	
SQRT			INTRINSIC
SUM	REAL	9648	
SUMIN	REAL	19712	
SUMR	CHAR*10	16014	
TM0	REAL	15900	
TM01	REAL	15932	
TM1	REAL	12	/C2 /
TMA	REAL	16	
TMB	REAL	1220	
TMS	REAL	4832	
VINA	REAL	4	/C2 /

```

VOL1  CHAR*10      15994
VOL2  CHAR*10      16004
VOLA  REAL          3628
VOLC  REAL          2424
XMICCE CHAR*11      17558
XSEED  REAL          15868

```

```

1559 C-----
1560 C      SUBROUTINE RGKT(X,Y,N,DX,YO,P)
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```

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D Line# 1 7 Microsoft FORTRAN77 V3.31 August 1985

```

1561 C
1562 C      USE RUNGE-KUTTA METHOD TO SOLVE ORDINARY DIFFERENTIAL
1563 C      EQUATION
1564 C
1565 C      X: INDEPENDENT VARIABLE
1566 C
1567 C      Y: DEPENDENT VARIABLE
1568 C
1569 C      N: DIMENSION OF X(N) AND Y(N)
1570 C
1571 C      DX: INCREMENT OF X
1572 C
1573 C      YO: INITIAL CONDITION OF Y
1574 C
1575 C      P: PARAMETER
1576 C
1577 C      F: THE SUPPLIED FUNCTION. (DY/DX=F(X,Y))
1578 C-----
1579      SUBROUTINE RGKT(X,Y,N,DX,YO,P)
1580      DIMENSION X(N),Y(N)
1581      Y(1)=YO
1582      DO 1 I=1,N-1
1 1583          RK1=DX*F(X(I),Y(I),P)
1 1584          RK2=DX*F(X(I)+DX/2.,Y(I)+RK1/2.,P)
1 1585          RK3=DX*F(X(I)+DX/2.,Y(I)+RK2/2.,P)
1 1586          RK4=DX*F(X(I)+DX,Y(I)+RK3,P)
1 1587          Y(I+1)=Y(I)+(RK1+2*RK2+2*RK3+RK4)/6.
1 1588 1      CONTINUE
1589      RETURN
1590      END

```

Name	Type	Offset	P	Class
DX	REAL	12	*	
F	REAL			FUNCTION
I	INTEGER*4	21426		
N	INTEGER*4	8	*	

```

P      REAL          20 *
RK1    REAL          21434
RK2    REAL          21438
RK3    REAL          21442
RK4    REAL          21446
X      REAL          0 *
Y      REAL          4 *
Y0     REAL          16 *

```

```

1591 C-----
1592 C      FUNCTION F(X,Y,Z)
1593 C
1594 C      X: INDEPENDENT VARIABLE
1595 C
1596 C      Y: DEPENDENT VARIABLE
1597 C
1598 C      Z: PARAMETER
1599 C-----

```

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D Line# 1 7 Microsoft FORTRAN77 V3.31 August 1985

```

1600 FUNCTION F(X,Y,Z)
1601 PARAMETER (N4=301,PI=3.14159)
1602 COMMON /C2/RINIT,VINA,DT,TM1,COU(N4)
1603 COMMON /C3/RL1,RL2,LIP,D1,D2,CINIT,CINF,H
1604 V=0.018
1605 I=INT(X/DT)+1
1606 CO=COU(I)+(COU(I+1)-COU(I))*(X-(I-1)*DT)/DT
1607 V0=(4.*PI*(RINIT**3))/3.
1608 VIN=VINA*V0/100.
1609 F=-Z*V*(CO-CINIT*(V0-VIN))/(4.*PI*Y**3/3.-VIN))
1610 RETURN
1611 END

```

Name	Type	Offset	P	Class
CO	REAL	21458		
CINF	REAL	24	/C3	/
CINIT	REAL	20	/C3	/
COU	REAL	16	/C2	/
D1	REAL	12	/C3	/
D2	REAL	16	/C3	/
DT	REAL	8	/C2	/
H	REAL	28	/C3	/
I	INTEGER*4	21454		
INT			INTRINSIC	
LIP	INTEGER*4	8	/C3	/
N4	INTEGER*4		PARAMETER	
PI	REAL		PARAMETER	

RINIT	REAL	0	/C2	/
RL1	REAL	0	/C3	/
RL2	REAL	4	/C3	/
TM1	REAL	12	/C2	/
V	REAL	21450		
VO	REAL	21462		
VIN	REAL	21466		
VINA	REAL	4	/C2	/
X	REAL	0	*	
Y	REAL	4	*	
Z	REAL	8	*	

```

1612 C-----
1613 C      FUNCTION RANND(XSEED,ISC)
1614 C
1615 C      RANDOM VARIABLE GENERATOR
1616 C      NORMAL DISTRIBUTION WITH STANDARD DEVIATION EQUAL TO 1.
1617 C-----
1618 C      FUNCTION RANND(XSEED,ISC)
1619 C      DOUBLE PRECISION RANDOM
1620 C
1621 C      GENERATING A UNIFORM RANDOM NUMBER
1622 C
1623 C      INTEGER A,X
1624 C      IF(ISC.EQ.0) X = XSEED
1625 C
1626 C      A = 2**10 + 3

```

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```

D Line# 1      7
1627      M = 2**20
1628      FM = M
1629      X = MOD(A*X, M)
1630      FX = X
1631      XSEED = X
1632      Z = FX/FM
1633 C
1634 C      CONVERTING THE RANDOM NUMBER WITH A UNIFORM DISTRIBUTION TO A
1635 C      RANDOM NUMBER HAVING A NORMAL DISTRIBUTION
1636 C
1637 C      R = RANDOM()
1638 C      R = Z
1639 C      A0=2.30753
1640 C      A1=0.27061
1641 C      B1=0.99299
1642 C      B2=0.04481
1643 C      IF (R-0.5) 10,10,20
1644 10      AK=1.
1645      GO TO 30

```

```

1646 20      AK=-1.
1647          R=R-0.5
1648 30      T=SQRT(ALOG(1./(R*R)))
1649          E=T-(A0+A1*T)/(1.+B1*T+B2*T*T)
1650          RANND=AK*E
1651          ISC = ISC + 1
1652          RETURN
1653          END

```

Name	Type	Offset	P	Class
A	INTEGER*4	21474		
A0	REAL	21498		
A1	REAL	21502		
AK	REAL	21514		
ALOG				INTRINSIC
B1	REAL	21506		
B2	REAL	21510		
E	REAL	21522		
FM	REAL	21482		
FX	REAL	21486		
ISC	INTEGER*4		4 *	
M	INTEGER*4	21478		
MOD				INTRINSIC
R	REAL	21494		
SQRT				INTRINSIC
T	REAL	21518		
X	INTEGER*4	21470		
XSEED	REAL		0 *	
Z	REAL	21490		

```

1654 C
1655      SUBROUTINE IONETWO(ITEST)
1656 31      CONTINUE
1657          IF(ITEST.LE.0.OR.ITEST.GE.3) THEN
1658              WRITE(*,*)

```

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```

D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1659          WRITE(*,*) '** INCORRECT RESPONSE **'
1660          WRITE(*,*) 'PLEASE ENTER 1 OR 2'
1661          WRITE(*,*)
1662          READ(*,*) ITEST
1663          GO TO 31
1664      ENDIF
1665      RETURN
1666      END

```

Name	Type	Offset	P	Class
------	------	--------	---	-------

ITEST INTEGER*4 0 *

```

1667 C
1668     SUBROUTINE IYESNO(ITEST)
1669     CHARACTER *1 ITEST
1670 32    CONTINUE
1671     IF(ITEST.NE.'Y'.AND.ITEST.NE.'N') THEN
1672         WRITE(*,*)
1673         WRITE(*,*)'** INCORRECT RESPONSE **'
1674         WRITE(*,*)'PLEASE ENTER  "Y"  OR  "N"'
1675         WRITE(*,*)
1676         READ(*,'(A1)') ITEST
1677         GO TO 32
1678     ENDIF
1679     RETURN
1680     END

```

Name	Type	Offset	P	Class
------	------	--------	---	-------

ITEST	CHAR*1	0	*	
-------	--------	---	---	--

```

1681 C
1682     SUBROUTINE CHANNAM(FILNAM)
1683     CHARACTER *1 ICHANG
1684     CHARACTER *10 FILNAM
1685 33    CONTINUE
1686     WRITE(*,*)
1687     WRITE(*,35) FILNAM
1688 35    FORMAT(1X,'THE FILE NAME ENTERED IS ',A10)
1689     WRITE(*,*)
1690     WRITE(*,*)' DO YOU WISH TO CHANGE IT,(Y/N)? '
1691     READ(*,'(A1)') ICHANG
1692     CALL IYESNO(ICHANG)
1693     IF(ICHANG.EQ.'Y') THEN
1694         WRITE(*,*)
1695 36    CONTINUE
1696         WRITE(*,*)'PLEASE ENTER THE NEW NAME. '
1697         WRITE(*,*)
1698         READ(*,'(A10)',ERR=36) FILNAM
1699         GO TO 33
1700     ENDIF
1701     RETURN
1702     END

```

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D Line# 1 7

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Name	Type	Offset	P	Class
------	------	--------	---	-------

FILNAM	CHAR*10	0	*	
ICHANG	CHAR*1	21562		

1703	SUBROUTINE INCORRES
1704	WRITE(*,*)
1705	WRITE(*,*)'*** INCORRECT RESPONSE **'
1706	RETURN
1707	END

Name	Type	Offset	P	Class
------	------	--------	---	-------

Name	Type	Size	Class
C1		24	COMMON
C2		1220	COMMON
C3		32	COMMON
CHANNA			SUBROUTINE
F	REAL		FUNCTION
INCORR			SUBROUTINE
IONETW			SUBROUTINE
IYESNO			SUBROUTINE
MBCON			SUBROUTINE
RANND	REAL		FUNCTION
RGKT			SUBROUTINE
SENS			PROGRAM

Pass One No Errors Detected
 1707 Source Lines

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D Line# 1 7 Microsoft FORTRAN77 V3.31 August 1985

```

1      SUBROUTINE MBCON(TM,CA,CB,IP)
2 C$DEBUG
3 $INCLUDE: 'IMSL'
1 $LARGE: DMY327
2      DIMENSION DMY327(1)
4 C-----
5 C      JOB: 1. PREDICT THE CONCENTRATION CHANGE INSIDE THE CELL
6 C          CHAMBER
7 C          2. PLOTTING CONCENTRATION VERSUS TIME CHART
8 C-----
9      PARAMETER (II=2,III=3,N4=301)
10     REAL L1,L2,M
11     DIMENSION CN(11),CO(11),CE(11,11),
12     &          WK1(154),CONC(11),CA(25),CB(25),
13     &          DC(25),TM(25),X(II,II),Y1(II),Y2(II),WK2(10)
14     COMMON /C1/IPRINT,IF1,A1(II),A2(II)
15     COMMON /C2/RINIT,VINA,DT,TM1,COUT(N4)
16     COMMON /C3/RL1,RL2,LIP,D1,D2,CINIT,CINF,H
17 C-----
18 C      INITIALIZATION
19 C-----
20     N1 = 4
21     N2 =6
22     L1=RL1*1.0E-6
23     L2=RL2*1.0E-6
24     TMAX=TM1
25     DX1=L1/N1
26     DX2=L2/N2
27     RX=DX2/DX1
28     P1=DT*D1/DX1/DX1
29     P2=DT*D2/DX2/DX2
30     B1=H*DX1/D1
31     M=2./(1+RX)
32     DO 1 I=1,N1+N2+1
1 33         CN(I)=0.
1 34         CO(I)=0.
1 35         DO 1 J=1,N1+N2+1
2 36             CE(I,J)=0.
2 37 1      CONTINUE
38         ICOUNT=0
39 C-----
40 C      USING THE BACKWARD DIFFERENCE METHOD TO CALCULATE THE
41 C          CONCENTRATION INSIDE THE CELL CHAMBER
42 C-----
43         WRITE(10,151)
44 151     FORMAT(///,1X,'***** THE CONCENTRATION',
45         ,          ' HISTORY *****')
```

```

46 C-----
47 C          INPUT VALUES TO THE COEFFICIENT MATRIX
48 C-----
49          CE(1,1)=-1+2*P1+2*P1*B1
50          CE(1,2)=-2*P1
51          DO 2 I=2,N1
1 52          CE(I,I-1)=-P1
1 53          CE(I,I)=-1+2*P1
1 54          CE(I,I+1)=-P1

```

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```

D Line# 1      7
1 55 2      CONTINUE
56          CE(N1+1,N1)=-P1*M
57          CE(N1+1,N1+1)=-1+P1*M+P1*M*(D2/D1)/RX
58          CE(N1+1,N1+2)=-P1*M*(D2/D1)/RX
59          DO 3 I=N1+2,N1+N2
1 60          CE(I,I-1)=-P2
1 61          CE(I,I)=-1+2*P2
1 62          CE(I,I+1)=-P2
1 63 3      CONTINUE
64          CE(N1+N2+1,N1+N2)=-2*P2
65          CE(N1+N2+1,N1+N2+1)=-1+2*P2
66          WRITE(*,*)
67          WRITE(*,*)'CALCULATING THE COEFFICIENT MATRIX -'
68          WRITE(*,*)'ENTERING LEQT2F (1)'
69 6      CO(1)=CO(1)+2*B1*P1
70 C-----
71 C          CALCULATE THE COEFFICIENT MATRIX
72 C-----
73          NX1 = N1+N2+1
74          MX = 1
75          IDGT1 = 3
76          CALL LEQT2F(CE,MX,NX1,NX1,CO,IDGT1,WK1,IER1)
77          IX =1
78          IF(IER1.NE.0) THEN
79              WRITE(*,*)
80              WRITE(*,110) IX,IER1,ICOUNT
81 110      FORMAT(' IER',I1,' = ',I5,5X,'ICOUNT='I4)
82          ENDIF
83 C-----
84 C          PUT CO INTO CN FOR NEXT CALCULATION
85 C-----
86          ICOUNT=ICOUNT+1
87          DO 4 I=1,N1+N2+1
1 88          CN(I)=CO(I)
1 89 4      CONTINUE
90          COUT(ICOUNT)=CN(LIP)*(CINF-CINIT)+CINIT
91 C          COUT(ICOUNT)=CINF+(CINIT-CINF)*EXP(-(ICOUNT-1)*DT/19.6)
92 C-----

```

```

93 C      CHECK TO SEE WHETHER IT IS TIME TO OUTPUT THE DATA
94 C-----
95      IF (ICOUNT/IPRINT*IPRINT.EQ.ICOUNT) THEN
96          WRITE(10,101)ICOUNT*DT
97 101      FORMAT(/,'CONCENTRATION DISTRIBUTION AT TIME-',
98          F8.2,'SEC. IS',)
99      DO 5 I=1,N1+N2+1
1 100          CONC(I)=CN(I)*(CINF-CINIT)+CINIT
1 101 5      CONTINUE
102      WRITE(10,*)
103      WRITE(10,*)'      DIALYSIS MEMBRANE      CELL CHAMBER'
104      WRITE(10,*)'|      |      |      |'
105      WRITE(10,*)'|B      |      |      |'
106      WRITE(10,*)'|U      |      |      |'
107      WRITE(10,*)'|L      |      |      |'
108      WRITE(10,*)'|K      |      |      |'
109      WRITE(10,*)'|      |      |      |'
110      WRITE(10,*)'| 1      3      5      7      9      11'
^H
3

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
111      WRITE(10,201) CONC(1),CONC(3),CONC(5),CONC(7),CONC(9),CONC(11)
112 201      FORMAT(1X,E9.3,1X,E9.3,1X,E9.3,1X,E9.3,1X,E9.3,1X,E9.3)
113      WRITE(10,*)'|      |      |      |'
114      WRITE(10,*)'| 2      4      | 6      8      10      |'
115      WRITE(10,202) CONC(2),CONC(4),CONC(6),CONC(8),CONC(10)
116 202      FORMAT(3X,E9.3,2X,E9.3,1X,E9.3,1X,E9.3,1X,E9.3)
117      WRITE(10,*)'|      |      |      |'
118      WRITE(10,*)'|F      |      |      |'
119      WRITE(10,*)'|L      |      |      |'
120      WRITE(10,*)'|O      |      |      |'
121      WRITE(10,*)'|W      |      |      |'
122      WRITE(10,*)'|      |      |      |'
123      WRITE(10,*)
124      WRITE(10,*)
125          IP=ICOUNT/IPRINT
126          IF (CN(N1+1).GE.1.) CN(N1+1)=1.-1.E-6
127          IF (CN(N1+N2+1).GE.1.) CN(N1+N2+1)=1.-1.E-6
128          CA(IP)=-LOG(1-CN(N1+1))
129          CB(IP)=-LOG(1-CN(N1+N2+1))
130          DC(IP)=CONC(N1+1)-CONC(N1+N2+1)
131          TM(IP)=ICOUNT*DT/TMAX
132      END IF
133 C-----
134 C      CHECK TO SEE WHETHER IT IS TIME TO STOP THE EXECUTION
135 C-----
136      IF (ICOUNT*DT.LT.TMAX+DT) GO TO 6
137      WRITE(*,*)
138      WRITE(*,*)'LEAVING LEQT2F (1)'
139 C-----

```

```

140 C      FINDING THE BEST LINEAR FIT FOR THE CONCENTRATION VERSUS
141 C      TIME POINTS
142 C-----
143      DO 10 I=1,2
1 144          X(I,2)=0.
1 145          Y1(I)=0.
1 146          Y2(I)=0.
1 147 10      CONTINUE
148      DO 11 I=1,IP
1 149          X(1,2)=X(1,2)+TM(I)
1 150          X(2,2)=X(2,2)+TM(I)**2
1 151          Y1(1)=Y1(1)+CA(I)
1 152          Y1(2)=Y1(2)+CA(I)*TM(I)
1 153          Y2(1)=Y2(1)+CB(I)
1 154          Y2(2)=Y2(2)+CB(I)*TM(I)
1 155 11      CONTINUE
156          X(2,1)=X(1,2)
157          X(1,1)=IP
158          NX2 = 2
159          IDGT2 = 3
160          IDGT3 = 3
161          WRITE(*,*)
162          WRITE(*,*)'FINDING BEST LINEAR FIT FOR CONCENTRATION V.S. TIME - '
163          WRITE(*,*)
164          WRITE(*,*)'ENTERING LEQT2F (2)'
165          CALL LEQT2F(X,MX,NX2,NX2,Y1,IDGT2,WK2,IER2)
166          WRITE(*,*)

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
167      WRITE(*,*)'LEAVING LEQT2F (2)'
168      IX = 2
169      IF(IER2.NE.0) THEN
170          WRITE(*,*)
171          WRITE(*,120) IX, IER2
172 120      FORMAT(' IER',I1,' - ',I3)
173      ENDIF
174      DO 200 K = 1,2
1 175          A1(K) = Y1(K)
1 176 200      CONTINUE
177          WRITE(*,*)
178          WRITE(*,*)'ENTERING LEQT2F (3)'
179          CALL LEQT2F(X,MX,NX2,NX2,Y2,IDGT3,WK2,IER3)
180          WRITE(*,*)
181          WRITE(*,*)'LEAVING LEQT2F (3)'
182          IX = 3
183          IF(IER3.NE.0) THEN
184              WRITE(*,*)
185              WRITE(*,120) IX, IER2
186          ENDIF

```



```

187      DO 210 K =1,2
1 188          A2(K) = Y2(K)
1 189 210      CONTINUE
190          WRITE(10,103)A1(1),A1(2)
191 103      FORMAT(/,' THE EQUATION FOR THE LINEAR BEST FIT FOR THE',/,
192          .      ' CONCENTRATION VERSUS TIME IS,',/,
193          .      ' Y = ',F6.3,' + ',F6.3,' *X',/ )
194          WRITE(10,103)A2(1),A2(2)
195          RETURN
196          END

```

Name	Type	Offset	P	Class
A1	REAL	8	/C1	/
A2	REAL	16	/C1	/
B1	REAL	1460		
CA	REAL	4	*	
CB	REAL	8	*	
CE	REAL	936		
CINF	REAL	24	/C3	/
CINIT	REAL	20	/C3	/
CN	REAL	704		
CO	REAL	748		
CONC	REAL	792		
COUT	REAL	16	/C2	/
D1	REAL	12	/C3	/
D2	REAL	16	/C3	/
DC	REAL	836		
DMY327	REAL	0	LARGE	
DT	REAL	8	/C2	/
DX1	REAL	1440		
DX2	REAL	1444		
H	REAL	28	/C3	/
I	INTEGER*4	1468		
ICOUNT	INTEGER*4	1484		
IDGT1	INTEGER*4	1632		
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D Line#	1	7
IDGT2	INTEGER*4	1876
IDGT3	INTEGER*4	1880
IER1	INTEGER*4	1636
IER2	INTEGER*4	1884
IER3	INTEGER*4	1912
IF1	INTEGER*4	4
II	INTEGER*4	
III	INTEGER*4	
IP	INTEGER*4	12 *
IPRINT	INTEGER*4	0
IX	INTEGER*4	1640

J	INTEGER*4	1476		
K	INTEGER*4	1908		
L1	REAL	1428		
L2	REAL	1432		
LIP	INTEGER*4	8	/C3	/
LOG			INTRINSIC	
M	REAL	1464		
MX	INTEGER*4	1628		
N1	INTEGER*4	1420		
N2	INTEGER*4	1424		
N4	INTEGER*4		PARAMETER	
NX1	INTEGER*4	1624		
NX2	INTEGER*4	1872		
P1	REAL	1452		
P2	REAL	1456		
RINIT	REAL	0	/C2	/
RL1	REAL	0	/C3	/
RL2	REAL	4	/C3	/
RX	REAL	1448		
TM	REAL	0	*	
TM1	REAL	12	/C2	/
TMAX	REAL	1436		
VINA	REAL	4	/C2	/
WK1	REAL	16		
WK2	REAL	664		
X	REAL	632		
Y1	REAL	648		
Y2	REAL	656		

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198
199

Name	Type	Size	Class
C1		24	COMMON
C2		1220	COMMON
C3		32	COMMON
LEQT2F			SUBROUTINE
MBCON			SUBROUTINE

Pass One No Errors Detected
199 Source Lines

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