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DISSOLUTION SHELF LIFE OF PREDNISONE THERAPEUTIC DOSAGE FORM TABLET

by

Matthew S. Thomas

A Thesis

Submitted to
Michigan State University
In partial fulfillment of the requirements
For the degree of

MASTER OF SCIENCE

School of Packaging 2000

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Abstract

DISSOLUTION SHELF LIFE OF PREDNISONE THERAPEUTIC DOSAGE FORM TABLET by Matthew S. Thomas

Uncoated 5 mg Prednisone tablets were stored (open dish) in humidity buckets, which included nominal relative humidities (RH) of 12%, 33%, 50%, 65%, 75%, 80% and 90% at three ICH temperatures (25C, 30C and 40C). Moisture sorption isotherms, initial and critical moisture contents were determined for the product and used in a dissolution shelf life model.

Critical moisture content data was generated using a dissolution procedure according to United States Pharmacopoeia (USP) section <711>.

Prednisone tablets were stored at conditions mentioned above and dissolution testing was performed in triplicate at each storage condition every three days for approximately two months. Dissolution failures were identified at storage conditions corresponding to RH of 75% and higher for each temperature.

The dissolution shelf life model was used to suggest packaging materials, which minimize material costs while providing sufficient protection over a desired shelf life. This study shows that PVC blister materials (low moisture barrier) may not provide enough protection from moisture. So, a higher moisture barrier material, such as 0.6 mil Aclar (more expensive than PVC), may be required.

Acknowledgments

First of all, my love and appreciation goes out to my family for all of their support throughout the years. Thanks to Mom and Dad for always being there, no matter what the issue. Thanks to my brothers and sisters for being such a big part of my life. Thanks to my wife for being so supportive and patient through the years. I could not have done any of this without you.

I would also like to thank my colleagues and the faculty at the School of Packaging for making my second college adventure so memorable. It is this group of people who truly makes the School of Packaging a special place.

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My Acknowledgment would not be complete without sending an added thank you to Dr. Lockhart for his dedication to his profession. Thank you for your guidance and support. I appreciate everything you have done for me.

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Introduction

Stability testing is required by federal Food and Drug Administration (FDA) regulations. It is taken as a laboratory verification that the drug in its package will continue to meet USP monograph requirements during its expiration dating period (shelf life).

The pharmaceutical industry relies on efficient and timely drug development plans, which are often described as "speed to market". The objective is to get the drug product to market as quickly as possible. The primary responsibility of each participating group in a drug development plan is not to delay the drug development timeline. Every day wasted in the timeline can mean the loss of millions of dollars.

Package development groups rely on experience to dictate which packaging materials will be used for product stability testing. Stability testing can be very expensive, so the number of package alternatives should be limited and chosen very carefully. For example, three blister materials may be used to package a product for initial stability testing. Usually these three blisters will incorporate high, medium and low barriers to moisture. If the high barrier material does not protect the product adequately, the stability process must start over. This is the worst case scenario, and should be avoided at all costs. A low barrier material offers the opportunity to save money if the product passes

stability requirements. Therefore, such a barrier should be included in stability testing.

Prior to putting a package scenario together for a product entering initial stability, any package/product information a packaging engineer can find will be useful. Upon final product formulation, characterization testing of the drug product is performed to provide sensitivity information about that product. These tests take the form of open dish studies at designated ICH (International Conference on Harmonisation) temperatures and relative humidities (RH). If a product formulation is extremely sensitive to moisture or light, for example, the package selections for stability will take this into account.

Dissolution shelf life (DSL) can be used for moisture sensitive products to provide additional information before package materials are chosen for stability testing. Since moisture is often the major concern for product sensitivity, the DSL model can prove to be very powerful. The study objectives listed below highlight key areas of this project.

Standardize the dissolution testing procedure for recording dissolution data.
 USP standards were used to develop a calibration curve, which determined the percent dissolution values from absorbance units (AU). These AU were the direct readings from an ultra violet/visible spectrophotometer (UV-Vis).
 USP dissolution calibrator tablets were used to calibrate the performance of the dissolution apparatus.

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- 2. Determine the initial moisture content of the Prednisone tablets using a Karl Fisher autotitration method.
- 3. Develop moisture sorption isotherms using a gravimetric method for product stored in open dish at various ICH RH and temperatures.
- 4. Perform dissolution testing of the product being stored at various ICH temperatures and RH. Determine the critical moisture content of the product from respective dissolution failures, which were used in the shelf life model. The critical moisture content is defined as the moisture content at which the product fails dissolution, or at which there is a significant change in dissolution behavior.
- 5. Use the critical moisture content in the shelf life model to determine package selection options for stability testing of the drug product.

Pharmaceutical companies will conduct many analytical tests during the product characterization phase. These tests can be expensive and time consuming, but they provide essential testing data. Since chemical testing resources were limited at the School of Packaging, one test method (dissolution) was chosen to indicate critical conditions. Dissolution is a physical test based on physical properties. The following quotes verify that dissolution testing is an excellent choice, especially for a moisture sensitive pharmaceutical product.

"Dissolution analysis of pharmaceutical solid dosage forms has emerged as the single most important test that, when carried out appropriately, will ensure the quality of the product" (Banaker, 1992).

"The importance of dissolution rate on clinical performance of drugs and drug delivery systems has long been recognized. It is the overwhelmingly important property of dosage forms that contributes to the rate and extent of drug availability to the body and, as such, is deserving of the effort that has been put forth to develop dissolution systems that provide fundamental information on the dissolution process of many drugs and chemicals as well as meaningful in vitro dissolution system models that can be correlated with some index of in vivo performance" (Banaker, 1992).

"Dissolution testing, of course, is a regular quality control procedure in good manufacturing practice. Whether or not its numbers have been correlated with biological effectiveness, the standard dissolution test is a simple and inexpensive indicator of a product's physical consistency" (Hanson, 1991).

This thesis is the sixth in a series of theses reporting the development at the School of Packaging of a method for calculating the moisture barrier requirements for drug products. The two previous theses (Adams, Yoon) are listed in the bibliography. The work done involved method development and application of the method to hard gelatin capsules, coated tablets and two variations of uncoated tablets.

Literature Review

Many sources have indicated that dissolution is one of the most important tests to verify the efficacy of pharmaceutical products. In fact, over 100 years ago, scientists recognized dissolution as an important prerequisite for drug absorption. Other theses (Adams, Yoon) published at the School of Packaging, based on shelf life modeling, have detailed literature reviews, which highlight the history and importance of dissolution in measuring drug product efficacy.

Many studies have correlated drug bioavailability (in-vivo) and drug dissolution (in-vitro). The following schematic illustrates the dissolution process of solid dosage forms (Banakar, 1992).

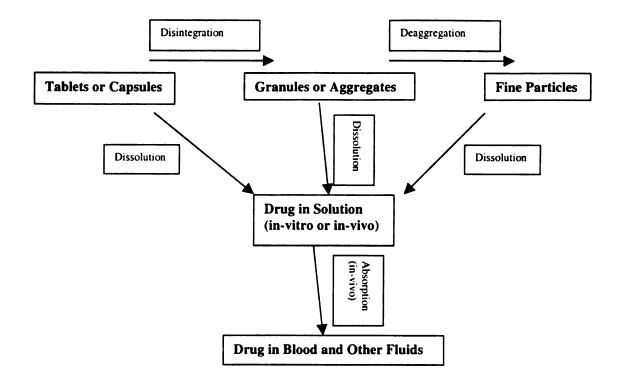
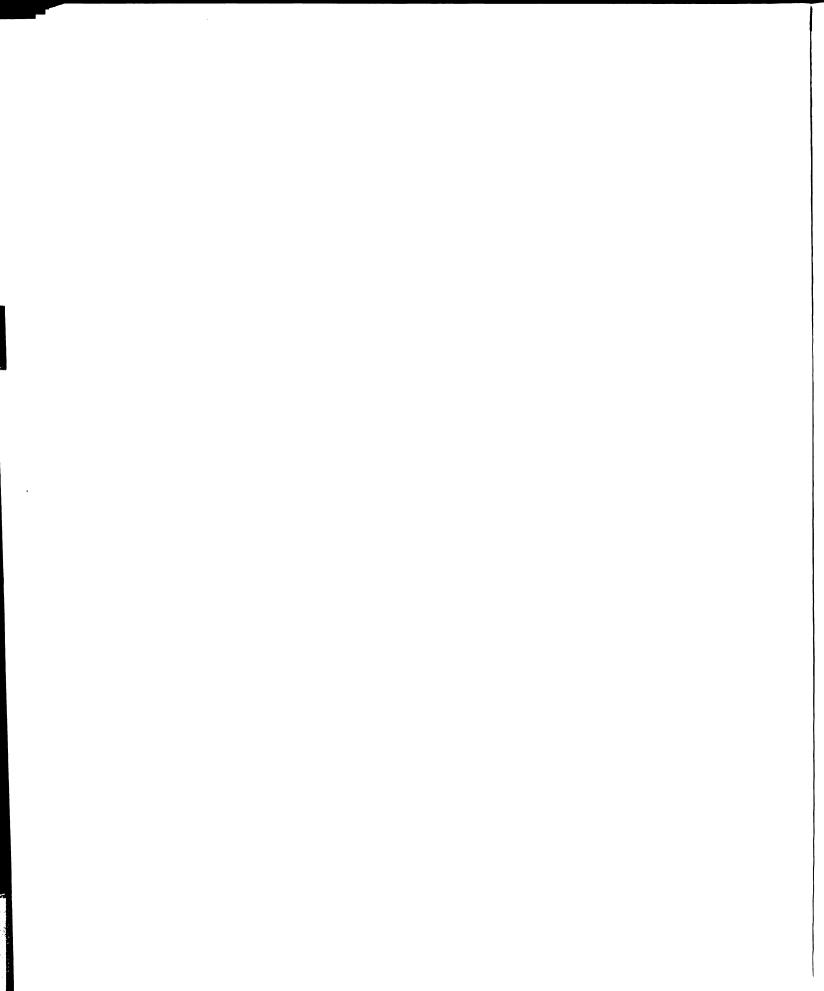


Figure 1. Dissolution process of solid dosage forms



In Figure 1, the rate of drug dissolution can be the rate-limiting step before the drug appears in the blood. This establishes the important link between dissolution and bioavailability. Various dosage forms can have different dissolution rates, which correspond to different bioavailabilities. Figure 2 shows the order of dissolution rates and thus absorption rates for various dosage forms (Banakar, 1992).

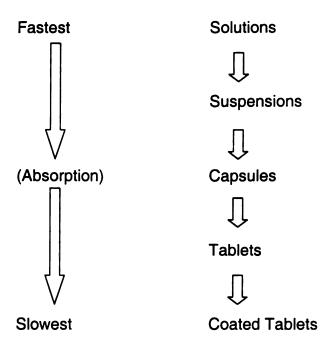


Figure 2. Dissolution rates for various dosage forms

Looking back on the long history of dissolution, an important milestone was the development of the USP paddle method in 1978. This is the method used in this study for dissolution testing. This method contains specific

requirements for the positioning of the paddles, shaft rotation, medium temperature, etc. Figure 3 illustrates the forced-convection nonsink dissolution testing method of the USP paddle apparatus (Banakar, 1992).

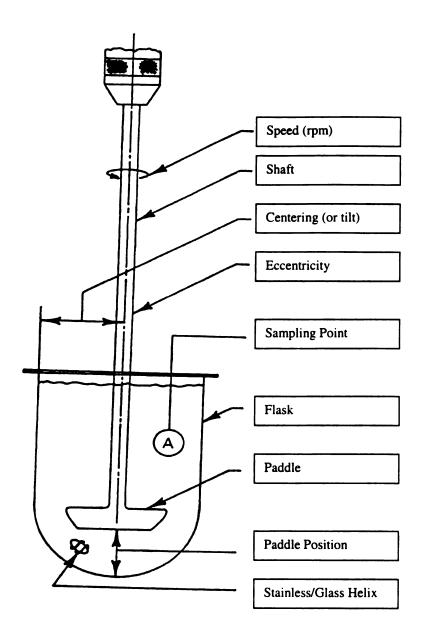


Figure 3. USP dissolution method (paddle)

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When a dissolution test is initiated, especially when a new dissolution test is being developed, it is important to recognize all the variables. In the case of this study, specific protocols are followed, such as the procedure developed by the UpJohn Company for Prednisone 5 mg therapeutic tablets. Following a specific procedure will keep dissolution variables to a minimum.

"The dissolution-rate data can be meaningful only if the results of successive tests on the same dosage form are consistent within reason. The dissolution test should yield reproducible results even when it is performed in different laboratories or with different personnel" (Banakar, 1992).

Looking at the specific parameters involved in dissolution testing, it is very important to minimize the variables within the testing protocol. For example, the preparation of the dissolution medium is a critical step. The USP dissolution section <711> specifically notes, "Dissolved gases can cause bubbles to form, which may change the results of the test. In such cases, dissolved gases should be removed prior to testing." (USP 23, 1995)

When analytical development creates a dissolution procedure for a new drug, many variables are taken into account. Banaker (1992) wrote "The various factors affecting the dissolution rate of a drug from a dosage form fall in six main classes:

1. Factors related to the physicochemical properties of the drug

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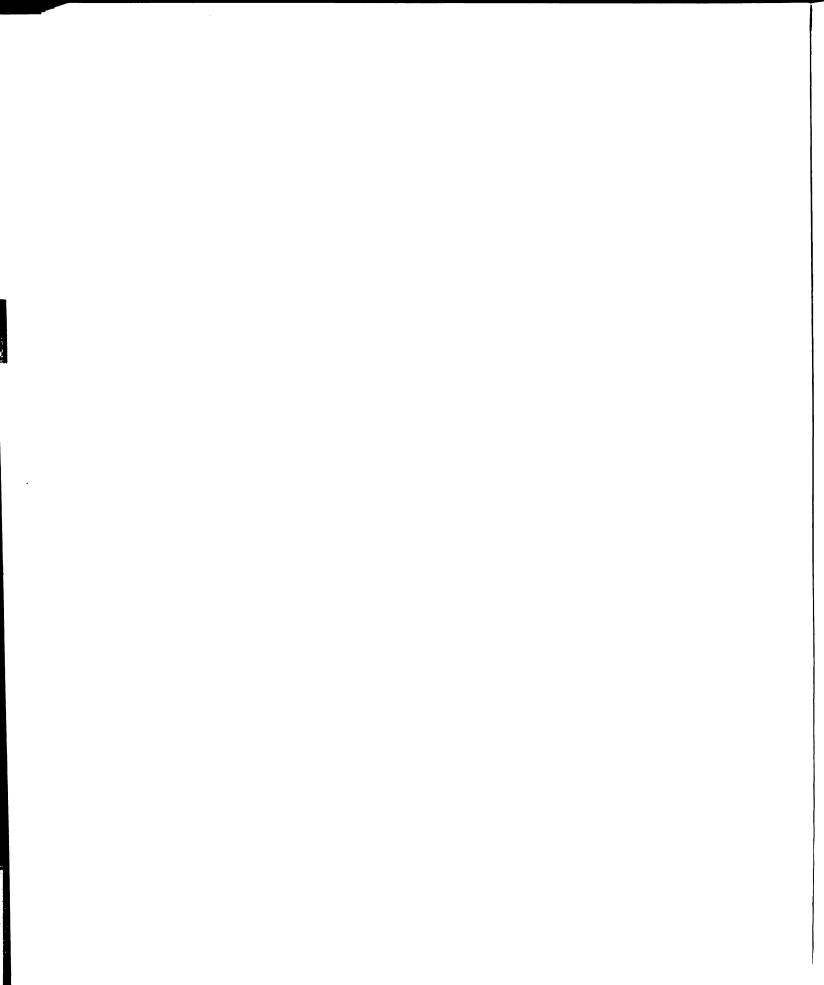
potentia

- 2. Factors related to drug product formulation
- 3. Factors related to dosage form
- 4. Factors related to dissolution testing device
- 5. Factors related to dissolution test parameters
- 6. Miscellaneous factors

It must be stated at the outset that this classification is oversimplified for the purpose of understanding their influence on the dissolution process".

The factors listed above, when related to dosage form, can significantly influence dissolution. Depending on the form of the product (coated tablet, uncoated tablet, gelatin capsule), several intermediate steps will be involved, which influence the dissolution process.

"The process of dissolution of an active ingredient from solid pharmaceutical dosage forms involves several intermediate physicochemical steps such as wetting, swelling, capillarity, solubility, and diffusion" (Banakar, 1992). For example, wetting is one of the first steps in the dissolution process, in which the outside surface of the product is initially penetrated by the liquid dissolution medium. Development chemists must understand complex variables such as this when new formulations are developed. Minor changes within the formulation can create significant changes in dissolution, which indicates potential problems with bioavailability.



The dissolution procedures used in this research were developed with reference to the Dissolution general chapter <711> (USP 23, 1995). As stated earlier, the USP paddle method (Figure 3, Page 7) is the preferred dissolution setup for this product. The assembly is similar to the USP basket method except for a blade, which replaces a basket. To verify that the system is working correctly, a suitability test can be performed using USP Dissolution Calibrator Tablets. These tablets will deliver a specific amount of active ingredient (Prednisone) if the apparatus is functioning correctly. This dissolution chapter (USP<711>) continues to discuss parameters within the test, such as dissolution medium and time. The official monograph for Prednisone tablets can be referenced within the USP for specific dissolution information. A pharmaceutical testing laboratory would implement an in-house procedure, which includes these testing parameters and references the USP's official monograph.

Taborsky used dissolution testing to show that Prednisone is a moisture sensitive product. "This study demonstrates a direct correlation between an important performance feature of the pharmaceutical product and the moisture barrier of its packaging" (Taborsky-Urdinola, 1981). Taking this study one step further, the dissolution tests can determine a critical storage condition, while moisture isotherms and initial moisture content data can be used to generate shelf life information. Shelf life programs can be utilized to take a product's moisture sensitivity into account, and determine the proper amount of protection needed to package a pharmaceutical product for a defined shelf life.

The shelf life program used in this study was developed at the School of Packaging by Seung-Yil Yoon (Yoon, 2000). The program uses product moisture contents and isotherms and package permeability and dimensional information to determine a shelf life for a specific package selection. The program can also be used to determine the type of package needed for a desired shelf life. For example, the desired shelf life can be entered into the program along with the product information. The program will then calculate the required package permeance to create a given shelf life for a specific product. At this point, the desired package can be selected based on the permeance alone.

The program calculates shelf life by either a linear method or the G.A.B. method. Both methods use mathematical expressions to represent a product's moisture isotherm. The linear method simply uses a linear model, while the G.A.B. model uses a complex non-linear regression. For example, Figure 4 shows a typical moisture isotherm for a dry pharmaceutical product (Adams, 1998).

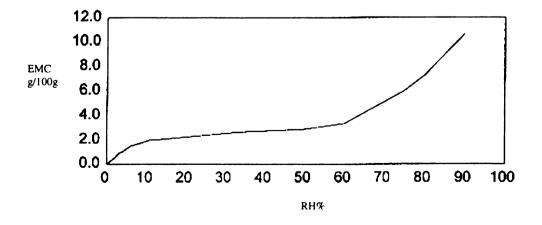


Figure 4. Moisture sorption isotherm (example)

A linear model does not represent the entire curve. However, if the portion of the isotherm, which represents all of the testing conditions, is linear, then that linear equation can be used in the shelf life calculations.

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Chapter 3: Materials and Methods

3.1 Standardizing the Dissolution Procedure

Purpose

The dissolution procedure must be calibrated to validate the generated dissolution data. Dissolution samples were analyzed by a UV-visible spectrophotometer, which generates absorbance units (AU). These AU are relative numbers, which correspond to specific dissolution values. USP Prednisone standards were used to correlate AU to specific dissolution values (percent dissolution).

Materials

- VanKel VK6010 Dissolution Apparatus (paddle)
- > USP Prednisone Reference Standard
- UV-Vis Spectrophotometer (Perkin-Elmer, Lambda 20)
- > USP Calibrator Tablets

Methods

A specific amount of reference standard was added to the dissolution medium to represent dissolution percentages of 100%, 75%, 50% and 25% for Prednisone tablets. The corresponding absorbance values were plotted versus the dissolution percentages. The resulting linear regression of these points was used as the calibration curve. USP calibrator tablets were then tested in the dissolution apparatus. The dissolution percentage for these tablets was determined by using the calibration curve. Standardization of the dissolution

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apparatus was verified by comparing the calibrator tablet's experimental dissolution percentage to the actual dissolution percentage, which was listed on the calibrator tablet's label.

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3.2 Moisture Sorption Isotherms

Purpose

Determine moisture sorption isotherms of the 5 mg Prednisone tablets at three ICH temperatures (25C, 30C, and 40C) by gravimetric methods.

Materials

- > Temperature Chambers for 25C, 30C and 40C
- > Five-Gallon Plastic Buckets (RH Buckets)
- > Product Racks and Recrystallization Dishes
- "Hygrodynamics" RH Monitoring Equipment
- > Saturated Salt Solutions (Table 3, Page 26)
- > 5 mg Prednisone Tablets
- ➤ Mettler Analytical Balance (+/- 0.05 mg)

Methods

Each temperature chamber contained seven RH buckets corresponding to nominal RH of 12%, 33%, 50%, 65%, 75%, 80% and 90%. The RH of each bucket was achieved by preparing the appropriate salt solution (Table 3, Page 26) in a Pyrex recrystallization dish. After this dish was placed in the corresponding bucket, the bucket was sealed and allowed to equilibrate before the RH was monitored and product was placed inside.

Each bucket contained a product rack, which was placed over the top of the recrystallization dish. This rack allowed an open dish of product to safely rest inside the bucket while being exposed to the RH within the bucket. Each bucket contained 15 Prednisone tablets, which were carefully placed in an aluminum weighing dish (open dish).

As the RH buckets equilibrated over a period of at least 24 hours, the RH inside each bucket was measured and recorded (Table 4, Page 27) at various intervals during the test procedure. Once the desired RH was measured for each bucket, fifteen Prednisone tablets were placed in aluminum weighing dishes for each bucket. The weight of the weighing dishes was initially recorded along with the weight of the dish containing fifteen tablets. After approximately two days, all of these dishes (with tablets) were weighed. To verify that the tablets reached an equilibrium moisture content (EMC), periodic weighings continued (Tables 5, 6 and 7; Pages 28, 28 and 29).

To construct an isotherm for the Prednisone tablets, the tablet EMC (g*Water/100g Dry Product) for each temperature was plotted versus the corresponding RH (Figure 11, Page 31).

Calculations

Equilibrium Moisture Content
$$(EMC) = [(Pf(1+IMC)/Pi)-1]*100$$
 (1)

Pf = Weight of dry product

Pi = Initial weight of product

IMC = Initial Moisture Content (g*Water/100g Dry Product)

Water Activity
$$(Aw) = %RH / 100$$
 (2)

%RH = Percent Relative Humidity

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3.3 Initial Moisture Content

Purpose

The initial moisture content (IMC) data represents the average amount of moisture contained in a five mg Prednisone tablet, when the tablet's original container was first opened. The IMC was used in the computer shelf life model.

Materials

- > Brinkmann Karl Fisher Autotitrator
- > Hydranal Composite 5 Titrant
- Deionized Water
- > HPLC Grade Methanol
- Mettler Analytical Balance (+/- 0.05 mg)
- Prednisone 5 mg Tablets

Methods

Prednisone 5 mg tablets were received from the Pharmacia and UpJohn Company in high density polyethylene bottles (approximately 170mLs) containing 1000 tablets. Five tablets were taken out of a new bottle and tested individually on the Brinkmann autotitrator. The autotitrator was set up to calculate MC on a wet weight basis. This MC was converted to a MC on a dry weight basis (Table 9, Page 33).

A standardization check was performed to ensure the autotitrator was properly calibrated. Injecting a specific amount of water into the titrator should theoretically yield a value of 100%. Results in triplicate between 98% and 102% were required to confirm the unit was calibrated properly.

Calculations

Initial Moisture Content (IMC) = [(Wi - Wf) / Wf]*100 "dry basis" (3)

IMC = Initial Moisture Content

Wi = Weight of product containing initial moisture

Wf = Weight of dry product

Initial Moisture Content (IMC) = [(Wi - Wf) / Wi]*100 "wet basis" (4)

IMC = Initial Moisture Content

Wi = Weight of product containing initial moisture

Wf = Weight of dry product

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3.4 Dissolution Testing

Purpose

Dissolution testing data was used to identify critical conditions

(temperature and RH) and corresponding critical moisture contents, which
represented the Prednisone tablets failing, or beginning to fail, USP dissolution
limits.

Materials

- > Temperature Chambers for 25C, 30C and 40C
- > Five-Gallon Plastic Buckets (RH Buckets)
- Product Racks and Recrystallization Dishes
- "Hygrodynamics" RH Monitoring Equipment
- Saturated Salt Solutions (Table 3, Page 26)
- > 5 mg Prednisone Tablets
- VanKel VK6010 Dissolution Apparatus (paddle)
- > UV/Vis Spectrophotometer (Perkin Elmer, Lambda 20)

Methods

Five-gallon buckets containing equilibrated saturated-salt solutions, corresponding to specific RH (12%, 33%, 50%, 65%, 75%, 80%, 90%), were placed in three separate chambers set to ICH temperatures (25C, 30C, 40C). Prednisone tablets were placed in these buckets corresponding to the specific RH and temperatures mentioned above. These tablets were tested for dissolution every three days for nearly two months. In addition, tablets were tested at time zero to establish a dissolution profile. For the dissolution profile,

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dissolution data was generated at 10, 20, 30, 40, 50 and 60 minutes. To determine critical conditions for the Prednisone tablets at the various temperatures and RH, dissolution data was generated at 30 minutes according to the USP dissolution monograph. Per the monograph, less than 80% dissolution was determined to be a failure.

Calculations

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3.5 Shelf Life Determination

Purpose

The shelf life computer model recommends the use of specific packaging materials for the Prednisone tablets being studied. The goal is to minimize material costs by choosing the least expensive packaging materials, which provide sufficient protection from moisture over a desired shelf life.

Materials

 School of Packaging Shelf Life Computer Model (Windows based program for IBM Compatible Computers)

Methods

The shelf life computer model performs shelf life calculations using data generated for a specific moisture sensitive product. For this study, the initial moisture content, moisture sorption isotherm data, critical moisture contents, and a desired shelf life value, are entered into the shelf life computer model. From this data, a permeance value is generated. This permeance value is used to suggest a packaging material, which minimizes costs and provides sufficient moisture protection for a desired shelf life. For example, looking at permeance values for various blister materials, a specific material's permeance value must be lower than the permeance value specified by the shelf life computer model. Since higher moisture barrier materials tend to be more expensive, choosing a material which has a permeance value closest to the permeance value generated by the shelf life computer program will minimize material costs.

Calculations

The calculation for the linear model is:

$$t = (I * W * B / A * P * p_s) * In [(RH_e - RH_i) / (RH_e - RH_c)]$$
 (6)

t = Desired Product Shelf Life

I = Material Thickness

W = Product Weight

B = Slope of "EMC (g*Water/100g Dry Product) versus Aw" Graph (Unitless)

A = Area of Material

P = Permeance (Unknown)

p_s = Partial Pressure

RH_e = Relative Humidity of Storage Condition (External)

RH_i = Relative Humidity Corresponding to Initial Moisture Content of Product

RH_c = Relative Humidity Corresponding to Critical Moisture Content of Product

Chapter 4: Data and Results

4.1 Standardizing the Dissolution Procedure

Looking at the three calibration curves (Figures 5, 6, and 7; Page 24, Page 24 and Page 25), the average of the three slopes will be used to determine dissolution percentages (ex: Table 11, Page 35) throughout this paper. The specification for calibrator tablet lot "L" shows the dissolution percentages to be between 38% and 44%. Table 2 (Page 25) obviously shows values within this range, so the dissolution apparatus can be considered calibrated and standardized.

Table 1. Dissolution Calibration Data

| Conc (mg/mL) | Dilution | | Absorbanc | е |
|--------------|----------|--------|-----------|---------|
| | _ | 1/5/99 | 1/6/99 | 1/10/99 |
| 0.100 | 100% | 0.457 | 0.460 | 0.458 |
| 0.075 | 75% | 0.346 | 0.342 | 0.336 |
| 0.050 | 50% | 0.227 | 0.228 | 0.224 |
| 0.025 | 25% | 0.116 | 0.115 | 0.115 |

^{*100%} Dilution represents 100% Dissolution of 5 mg Prednisone tablets

Figure 5. Dissolution Calibration Curve (1/5/99)

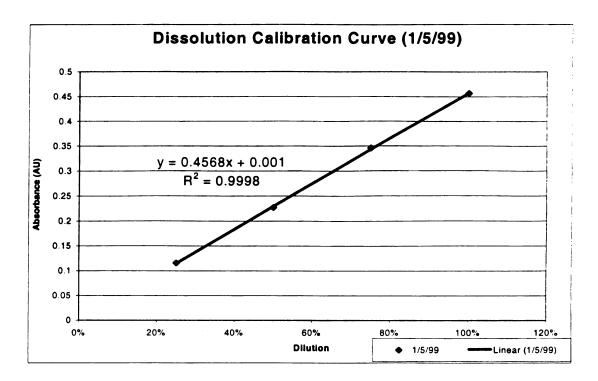
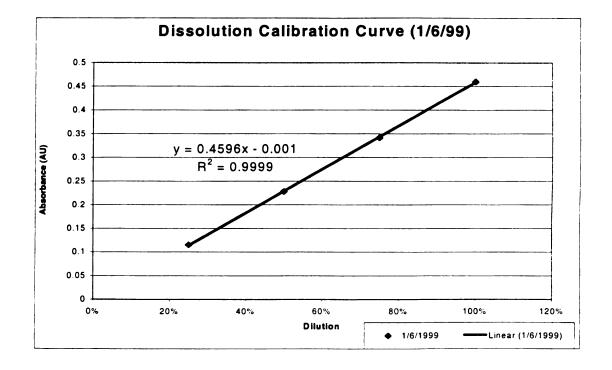


Figure 6. Dissolution Calibration Curve (1/6/99)





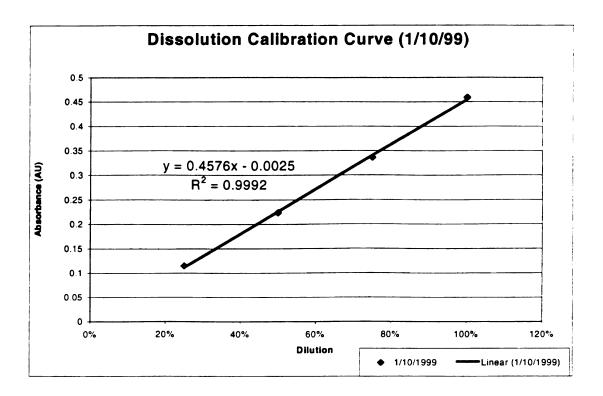


Table 2. USP Calibrator Tablet Dissolution Results

| Tablet # | Absorbance (AU) | % Dissolution |
|----------|-----------------|---------------|
| 1 | 0.177 | 39.2 |
| 2 | 0.181 | 40.1 |
| 3 | 0.192 | 42.5 |
| 4 | 0.182 | 40.3 |
| 5 | 0.185 | 41.0 |
| 6 | 0.174 | 38.6 |

^{*}Figure 7 calibration curve was used to determine % dissolution
**USP lot "L" calibrator tablets should be between 38% and 44% dissolution

4.2 Moisture Sorption Isotherms

Looking at Figure 11 (Page 31), we can see that the isotherm data for all three temperatures follow similar patterns. The data points between 30% RH and 80% RH are well represented by a linear regression (Figure 12, Page 32). Therefore, a linear equation will be used in the shelf life computer model to represent specific moisture sorption isotherms. The isotherms in Figure 11 could not be represented using the GAB model.

Since the product will not be exposed to a RH above 80% in our shelf life model, this linear region will be sufficient to represent the product's sorption isotherms. For example, the product fails dissolution at a storage condition which corresponds to 75% RH. Therefore, concerning the shelf life calculation, the highest RH is 75%.

The isotherms were obtained using tablets stored in five-gallon buckets over salt solutions as shown in Table 3. The humidities achieved at 25C, 30C and 40C are shown in Table 4 (Page 27).

Table 3. Salt Solution RH at Three Temperatures

| Salt Solution | Formula | %RH at Stated Temperature | | | | |
|--------------------|---|---------------------------|------|------|--|--|
| | | 20C | 25C | 30C | | |
| Lithium Chloride | LiCl - H₂O | 12.4 | 12 | 11.8 | | |
| Magnesium Chloride | MgCl₂ - 6H₂O | 33.6 | 33.2 | 32.8 | | |
| Magnesium Nitrate | Mg(NO ₃) ₂ - 6H ₂ O | 54.9 | 53.4 | 52 | | |
| Sodium Nitrite | NaNO₂ | 65.3 | 64.3 | 63.3 | | |
| Sodium Chloride | NaCl | 75.5 | 75.8 | 75.6 | | |
| Ammonium Sulfate | (NH₄)₂SO₄ | 80.6 | 80.3 | 80 | | |
| Potassium Nitrate | KNO₄ | 93.2 | 92 | 90.7 | | |
| | | | | | | |

Table 4. Bucket RH Readings for Isotherms

| Chamber #4: 25 degrees Celsius (3/16/99 11:35a) | | | | | | | |
|---|----------------|--------------------------|--|--|--|--|--|
| Mercury Thermometer | Chart Recorder | Digital Chamber Recorder | | | | | |
| 25C | 25C | 24.7 | | | | | |
| 200 | Hygrometer | - | | | | | |
| RH "nominal" Bucket | Dial Reading | %RH | | | | | |
| 12% | 94 | 22.2* | | | | | |
| 33% | 46 | 32.75 | | | | | |
| 50% | 75 | 51 | | | | | |
| 65% | 85 | 69.25 | | | | | |
| 75% | 54 | 77.25 | | | | | |
| 80% | 75 | 80.5 | | | | | |
| 90% | 63 | 90.75 | | | | | |
| Chamber #3: 30 de | | | | | | | |
| Mercury Thermometer | Chart Recorder | Digital Chamber Recorder | | | | | |
| 32C | 33C | 31.0C | | | | | |
| | Hygrometer | | | | | | |
| RH "nominal" Bucket | Dial Reading | %RH | | | | | |
| 12% | 20 | 11.8 | | | | | |
| 33% | 59 | 32.75 | | | | | |
| 50% | 77 | 49.75 | | | | | |
| 65% | 78 | 65.5 | | | | | |
| 75% | 67 | 77.75 | | | | | |
| 80% | 83 | 81.25 | | | | | |
| 90% | 67 | 90.25 | | | | | |
| Chamber #1: 40 deg | • | | | | | | |
| Mercury Thermometer | Chart Recorder | Digital Chamber Recorder | | | | | |
| 40C | 41C | 40.1C | | | | | |
| | Hygrometer | | | | | | |
| RH "nominal" Bucket | Dial Reading | %RH | | | | | |
| 12% | 53 | 13 | | | | | |
| 33% | 72 | 32.25 | | | | | |
| 50% | 80 | 47.5 | | | | | |
| 65% | 82 | 63 | | | | | |
| 75% | 77 | 77.25 | | | | | |
| 80% | 88 | 80 | | | | | |
| 90% | 64 | 88.25 | | | | | |

^{*}The reading for this bucket was abnormally high because the seal was faulty.

Table 5. Moisture Gain for Prednisone Tablets at 25C

| Chamber #4: 25 degrees Celsius | | | | | | | | | |
|--------------------------------|-------------|-----------|-----------|-----------|-----------|-----------|-----------|--|--|
| | | 3/16/99 | 3/18/99 | 3/20/99 | 3/22/99 | 3/29/99 | 4/5/99 | | |
| | | 1:18p | 2:15p | 12:55p | 2:40p | 3:15p | 10:25p | | |
| Bucket/Dish | Dish Wt (g) | Dish +Smp | | |
| | | (g) | (g) | (g) | (g) | (g) | (g) | | |
| 12%/1 | 1.2783 | 2.7764 | 2.7771 | 2.777 | 2.7774 | 2.7767 | 2.7769 | | |
| 33%/2 | 1.2854 | 2.7882 | 2.7905 | 2.7905 | 2.7912 | 2.7901 | 2.7901 | | |
| 50%/3 | 1.2763 | 2.7785 | 2.7847 | 2.7839 | 2.7845 | 2.784 | 2.7835 | | |
| 60%/4 | 1.2801 | 2.7755 | 2.785 | 2.7846 | 2.7843 | 2.7842 | 2.784 | | |
| 75%/5 | 1.2716 | 2.772 | 2.7849 | 2.784 | 2.7834 | 2.7834 | 2.7827 | | |
| 80%/6 | 1.2778 | 2.782 | 2.7965 | 2.7956 | 2.7951 | 2.795 | 2.7945 | | |
| 90%/7 | 1.2813 | 2.7798 | 2.8089 | 2.8093 | 2.8092 | 2.8092 | 2.8116 | | |

Table 6. Moisture Gain for Prednisone Tablets at 30C

| Bucket/Dish | Dish Wt (g) | 3/16/99 8:00p Dish +Smp (g) | 3/18/99 9:15p Dish +Smp (g) | 3/20/99 11:00p Dish +Smp (g) | 3/23/99 12:10a Dish +Smp (g) | 3/29/99 10:50p Dish +Smp (g) | 4/6/99 8:05p Dish +Smp (g) |
|-------------|-------------|--------------------------------------|--------------------------------------|---------------------------------------|---------------------------------------|---------------------------------------|-------------------------------------|
| 12%/1 | 1.2811 | 2.7806 | 2.779 | 2.7788 | 2.7783 | 2.7789 | 2.7785 |
| 33%/2 | 1.2701 | 2.7629 | 2.7633 | 2.7631 | 2.7631 | 2.7633 | 2.7636 |
| 50%/3 | 1.2653 | 2.7657 | 2.7712 | 2.7697 | 2.7694 | 2.7695 | 2.7695 |
| 60%/4 | 1.2687 | 2.7742 | 2.7819 | 2.7809 | 2.7805 | 2.7805 | 2.7804 |
| 75%/5 | 1.277 | 2.7743 | 2.7853 | 2.7845 | 2.7839 | 2.7838 | 2.7833 |
| 80%/6 | 1.2694 | 2.7625 | 2.7744 | 2.7741 | 2.7731 | 2.7731 | 2.7726 |
| 90%/7 | 1.2738 | 2.7728 | 2.7963 | 2.796 | 2.7953 | 2.7964 | 2.7966 |

Table 7. Moisture Gain for Prednisone Tablets at 40C

| | | 3/16/99 | 3/19/99 | 3/21/99 | 3/23/99 | 3/30/99 | 4/7/99 |
|-------------|-------------|-----------|-----------|-----------|-----------|-----------|-----------|
| | | | | | | | |
| | | 11:55p | 12:35a | 12:00a | 1:30a | 1:00a | 9:00p |
| Bucket/Dish | Dish Wt (g) | Dish +Smp |
| _ | | (g) | (g) | (g) | (g) | (g) | (g) |
| 12%/1 | 1.2779 | 2.7762 | 2.773 | 2.7741 | 2.7736 | 2.7738 | 2.7736 |
| 33%/2 | 1.2781 | 2.7818 | 2.7823 | 2.7827 | 2.7824 | 2.7824 | 2.7822 |
| 50%/3 | 1.2768 | 2.7753 | 2.778 | 2.7773 | 2.7773 | 2.7774 | 2.7768 |
| 60%/4 | 1.2829 | 2.7828 | 2.7876 | 2.7879 | 2.7873 | 2.7874 | 2.7873 |
| 75%/5 | 1.2857 | 2.7922 | 2.8016 | 2.8009 | 2.8 | 2.8 | 2.7998 |
| 80%/6 | 1.2736 | 2.781 | 2.791 | 2.7906 | 2.7897 | 2.7898 | 2.7891 |
| 90%/7 | 1.2694 | 2.7696 | 2.7888 | 2.788 | 2.788 | 2.7877 | 2.7883 |

Figure 8. Moisture Gain for Prednisone Tablets at 25C

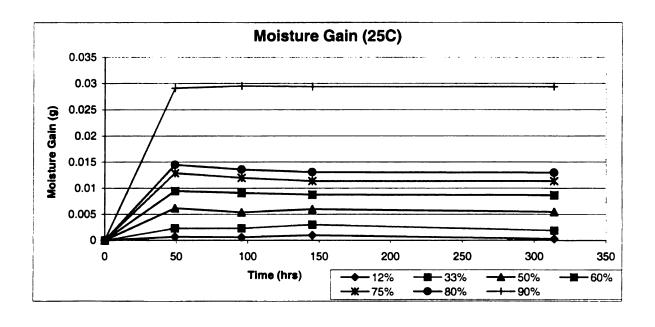


Figure 9. Moisture Gain for Prednisone Tablets at 30C

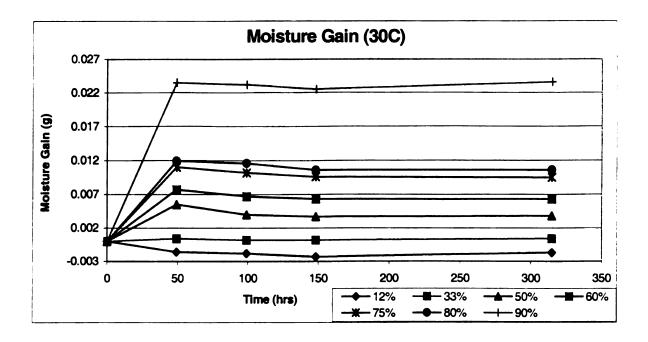


Figure 10. Moisture Gain for Prednisone Tablets at 40C

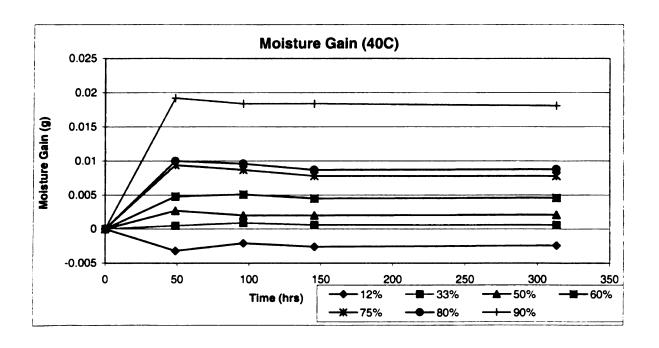


Table 8. Moisture Sorption Isotherm Data

| MSU Isotherm (25C) | Aw | MSU Isotherm (30C) | Aw | MSU Isotherm (40C) | Aw |
|----------------------------------|-------|----------------------------------|-------|----------------------------------|-------|
| EMC (gWater/100g Dry Product) | | EMC (gWater/100g Dry Product) | | EMC (gWater/100g Dry Product) | |
| 0 | 0 | 0 | 0 | 0 | 0 |
| 4.9613 | .2220 | 4.8858 | .1180 | 4.8593 | .1300 |
| 5.0215 | .3275 | 4.9652 | .3275 | 4.9726 | .3225 |
| 5.1577 | .5100 | 5.0942 | .4975 | 5.0294 | .4750 |
| 5.2790 | .6925 | 5.1883 | .6550 | 5.1235 | .6300 |
| 5.3816 | .7725 | 5.3094 | .7775 | 5.2432 | .7725 |
| 5.4404 | .8050 | 5.3527 | .8125 | 5.2821 | .8000 |
| 6.0600 | .9075 | 5.8433 | .9025 | 5.6359 | .8825 |

Figure 11. Moisture Sorption Isotherms

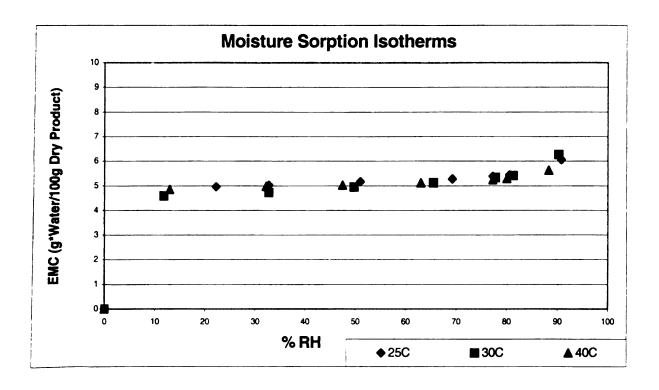
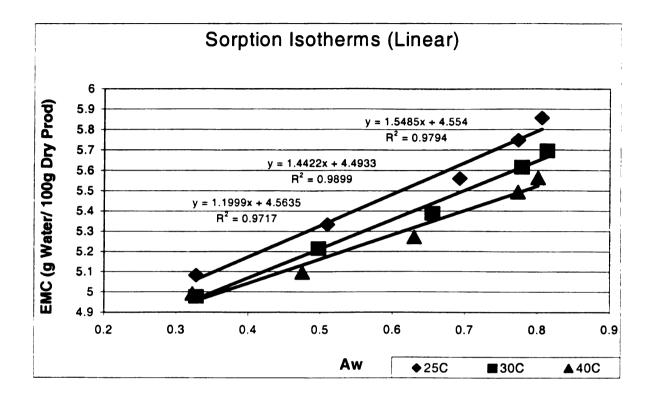


Figure 12. Linear Regression of Moisture Sorption Isotherms



4.3 Initial Moisture Content

The average of the "dry weight" IMC values, based on 100 grams of dry product, was used in the shelf life calculations.

Table 9. Initial Moisture Content of Prednisone 5 mg Tablets

| IMC | | | | | | | |
|-----------------------|---|---|--|--|--|--|--|
| Standardization Check | 99.31%, 98.91%, 100.09% | | | | | | |
| Sample Wt (g) "wet" | IMC (g*Water/100g Product) "wet weight" | IMC (g*Water/100g Product) "dry weight" | | | | | |
| 0.099 | 4.740 | 4.976 | | | | | |
| 0.0999 | 4.700 | 4.932 | | | | | |
| 0.1005 | 4.670 | 4.899 | | | | | |
| 0.0993 | 4.730 | 4.965 | | | | | |
| 0.1001 | 4.730 | 4.965 | | | | | |
| | | Average = 4.947 | | | | | |

4.4 Dissolution Testing

Dissolution data was gathered for Prednisone tablets at various RH to determine critical conditions at each ICH temperature (25C, 30C, 40C). Looking at Table 12 (Page 36), dissolution failures only occurred at RH of 75% or higher for each temperature. So, the critical RH used in shelf life calculations for each ICH temperature was 65%.

65% RH was used as the critical RH, instead of 75%, because the tablets were failing dissolution at a condition somewhere between 65% and 75%. This is one example of conservatism, which is built into the system.

Table 12 (Page 36) is a summary table, which reports the average dissolution values. The average dissolution values displayed in the table represent triplicate dissolution testing. So, if one of the average dissolution values in Table 12 (Page 36) is identified as a failure, this means that at least one of the three tablets failed dissolution according to the USP Prednisone monograph, which specifies that dissolution values below 80% are considered failures. These failures within Table 12 (Page 36) are indicated by a dark outline.

Table 10. Absorbances of Dissolution Profile

Absorbances (AU)

| Amp # | 0 min | 10 min | 20 min | 30 min | 40 min | 50 min | 60 min |
|-------|-------|--------|--------|--------|--------|--------|--------|
| 1 | 0 | 0.279 | 0.422 | 0.456 | 0.464 | 0.467 | 0.469 |
| 2 | 0 | 0.263 | 0.415 | 0.455 | 0.463 | 0.467 | 0.469 |
| 3 | 0 | 0.326 | 0.438 | 0.457 | 0.462 | 0.465 | 0.466 |
| 4 | 0 | 0.31 | 0.441 | 0.459 | 0.463 | 0.465 | 0.468 |
| 5 | 0 | 0.277 | 0.426 | 0.454 | 0.46 | 0.467 | 0.466 |
| 6 | 0 | 0.261 | 0.424 | 0.456 | 0.465 | 0.468 | 0.469 |

Table 11. % Dissolution of Dissolution Profile

% Dissolution

| Samp # | 0 min | 10 min | 20 min | 30 min | 40 min | 50 min | 60 min |
|--------|-------|--------|--------|--------|--------|--------|--------|
| 1 | 0 | 61.5 | 92.7 | 100.1 | 101.9 | 102.5 | 102.9 |
| 2 | 0 | 58.0 | 91.2 | 99.9 | 101.6 | 102.5 | 102.9 |
| 3 | 0 | 71.7 | 96.2 | 100.3 | 101.4 | 102.1 | 102.3 |
| 4 | 0 | 68.2 | 96.8 | 100.8 | 101.6 | 102.1 | 102.7 |
| 5 | 0 | 61.0 | 93.6 | 99.7 | 101.0 | 102.5 | 102.3 |
| 6 | 0 | 57.5 | 93.1 | 100.1 | 102.1 | 102.7 | 102.9 |

Figure 13. Prednisone Tablet Dissolution Profile

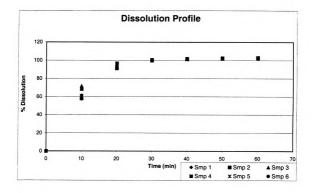


Table 12. Summary of Dissolution Data (Averages)

| OFO Assessed 8/ Discolation Values | | | | | | | | | | | | | |
|------------------------------------|------------|---------------------------------------|--|--|----------------|----------------|----------------|-------------|----------------|---------------|----------------|-------|----------------|
| 25C Average %Dissolution Values | | | | | | | | | | | | | |
| %RH | 0 | Day Day 3 6 9 12 15 18 21 24 37 44 51 | | | | | | | | | | | 58 |
| | | | | | | | | | <u> </u> | | | | |
| 50 65 | 100 100 | 96.98 98.58 | 97.2 90.14 | 97.49 95.52 | 95.82 97.34 | 99.82 96.69 | 97.93 96.54 | | 97.64 95.02 | 96.03 97.2 | 97.49 96.03 | 94.72 | 96.83 95.52 |
| | | | | | | | | | | | | | |
| 75 | 100 | 94.8 | 91.96 | 88.03 | | 91.89 | 94.29 | | 89.92 | | 86.14 | 85.77 | 86.86 |
| 80 | 100 | 92.69 | | 88.9 | 88.03 | 83.37 | 87.52 | 81.91 | 81.26 | 81.55 | 70.12 | 81.84 | 84.39 |
| 90 | 100 | 22.74 | | | | | | | | | 6.95 | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| 30C Average %Dissolution Values | | | | | | | | | | | | | |
| Day | | | | | | | | | | | | | |
| %RH | 0 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 27 | 33 | 40 | 47 | 54 |
| 33 | 100 | 93.27 | 95.52 | 93.78 | 95.52 | X | X | 98 | X | 95.82 | 96.98 | X | 98.58 |
| 50 | 100 | 97.64 | 96.69 | 101.3 | 97.64 | 94.51 | 98.95 | | 96.76 | 94.94 | 94.36 | 96.03 | 96.47 |
| 65 | 100 | 95.74 | 96.11 | 101.3 | 94.65 | 94.65 | 96.25 | 94.43 | 94.29 | 93.27 | 95.09 | 90.58 | 96.47 |
| 75 | 100 | 95.74 | 95.6 | 89.56 | 88.32 | 94.36 | 91.96 | 91.16 | 89.19 | 92.39 | 86.28 | 93.41 | 88.83 |
| 80 | 100 | 87.59 | 80.68 | 84.39 | 87.23 | 82.93 | 84.03 | 79.66 | 86.06 | 73.62 | 76.24 | 82.72 | 83.37 |
| 90 | 100 | 28.28 | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| 40C Average %Dissolution Values | | | | | | | | | | | | | |
| | | | | | | ay | | | | | | | |
| %RH | 0 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 27 | 33 | 40 | 47 | 54 |
| 12 | 100 | 97.93 | 92.03 | 97.05 | 96.11 | Х | 96.76 | Х | Х | 96.83 | X | X | Х |
| 33 | 100 | 96.33 | 97.56 | 96.83 | 96.03 | X | 97.78 | X | X | 96.18 | X | X | X |
| 50 | 100 | 93.92 | | 96.11 | 94.72 | 95.74 | 97.56 | 95.74 | 93.71 | 95.89 | 93.63 | 92.1 | 95.09 |
| 65 | 100 | 96.03 | 97.93 | 98 | 96.91 | 96.33 | 95.23 | 96.03 | 94.51 | 96.4 | 91.08 | 91.45 | 94.14 |
| 75 | 100 | 96.03 | 84.03 | 89.19 | 90.14 | 86.06 | 84.61 | 88.83 | 84.68 | 83.88 | 82.72 | 80.82 | 85.26 |
| 80 | 100 | 91.89 | 78.2 | 80.17 | 81.11 | 74.2 | 62.05 | 65.1 | 75.22 | 71.87 | 73.69 | 52.95 | 72.82 |
| 90 | 100 | 41.52 | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | = Failure (at least 1 of 3) X = not tested | | | | | | | | | | |
| | | | | T | | | | | | | | | |
| | | | | ــــــــــــــــــــــــــــــــــــــ | | | | | | | l | | |

^{*}Appendix A contains all of the raw dissolution data.

^{**}Each value in this table is an average of three dissolution tests. A failure is defined by the USP official monograph for Prednisone tablets as not less than 80% dissolved in 30 minutes.

4.5 Statistical Analysis

Each sampling point was tested in triplicate nearly every three days for approximately two months. Appendix A contains raw dissolution data and statistical analysis for every testing point.

First of all, as the raw dissolution data is reviewed for each storage temperature, dissolution failures (< 80% dissolution) only occur at RH of 75% or higher. This means that we are reaching our critical condition somewhere between 65% and 75% RH. The conservative approach is to conclude 65% to be the critical RH. The critical moisture content is then determined by using the corresponding isotherm (Figure 12, Page 32).

To reinforce this conclusion, the variability of the individual dissolution testing points can be analyzed. Table 14 (Page 46) lists the standard deviations for the dissolution testing at each test interval. Looking at the average of the standard deviations for each RH, a significant increase in variation occurs at 75%. This corresponds to the dissolution failures previously mentioned.

As the testing conditions become more severe (higher RH and temperatures), the Prednisone tablets are less likely to readily disintegrate in the dissolution medium. In fact, for most of the dissolution failures (Appendix A, Page 48), especially for samples stored at 90% RH, large chunks of tablet were found in the bottom of the dissolution vessel when samples were taken at 30 minutes. These dissolution failures were accompanied by high variability between dissolution values taken at the same testing intervals.

Table 13. Summary of Dissolution Data (Standard Deviations)

| | 25C Dissolution Testing: Standard Deviations from Triplicate Testing | | | | | | | | | | | | |
|-----|--|--------|----------|----------|-----------|---------|----------|----------|-----------|--------|-------|-------|-------|
| Day | | | | | | | | | | | | 1 | |
| %RH | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 24 | 37 | 44 | 51 | 58 | Ave |
| 50 | 1.957 | 0.504 | 0.655 | 2.531 | 1.668 | 1.135 | 0.550 | 1.032 | 2.605 | 6.839 | 4.314 | 3.033 | 2.235 |
| 65 | 4.008 | 7.745 | 0.218 | 0.504 | 3.859 | 1.857 | 1.120 | 1.077 | 1.580 | 3.106 | 1.316 | 0.756 | 2.262 |
| 75 | 1.334 | 2.241 | 11.722 | 2.461 | 3.720 | 1.668 | 6.150 | 2.395 | 1.120 | 10.122 | 8.211 | 6.602 | 4.812 |
| 80 | 1.364 | 5.282 | 2.559 | 5.456 | 6.685 | 6.850 | 5.057 | 11.630 | 11.446 | 3.938 | 4.869 | 3.431 | 5.714 |
| | | | | | | | | | | | | | |
| | 30C Dissolution Testing: Standard Deviations from Triplicate Testing | | | | | | | | | | | | |
| Day | | | | | | | | | | | |] | |
| %RH | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 27 | 33 | 40 | 47 | 54 | Ave |
| 50 | 0.549 | 1.486 | 5.412 | 0.630 | 3.241 | 0.882 | 1.941 | 1.778 | 1.639 | 3.385 | 2.435 | 0.882 | 2.022 |
| 65 | 1.155 | 2.405 | 0.334 | 3.725 | 5.575 | 2.314 | 2.150 | 0.909 | 4.476 | 0.952 | 5.460 | 1.765 | 2.602 |
| 75 | 1.513 | 2.531 | 10.374 | 8.132 | 2.605 | 0.767 | 3.712 | 5.677 | 0.882 | 3.314 | 0.882 | 2.355 | 3.562 |
| 80 | 2.605 | 11.347 | 3.297 | 4.560 | 6.537 | 5.929 | 8.816 | 4.685 | 9.009 | 3.363 | 1.696 | 2.782 | 5.386 |
| | | | | | | | | _ | | | | | |
| | | 40C | Dissolut | on Testi | ing: Stan | dard De | viations | from Tri | plicate T | esting | | | |
| | | | | | | D | ay | | | | | | |
| %RH | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 27 | 33 | 40 | 47 | 54 | Ave |
| 50 | 4.745 | 2.335 | 2.899 | 2.355 | 1.216 | 1.099 | 5.689 | 1.077 | 0.985 | 1.120 | 2.531 | 1.891 | 2.329 |
| 65 | 3.636 | 1.513 | 2.605 | 1.279 | 1.404 | 1.981 | 2.559 | 4.087 | 1.216 | 1.421 | 1.203 | 0.549 | 1.954 |
| 75 | 3.285 | 9.911 | 5.571 | 3.278 | 8.147 | 9.919 | 3.550 | 7.269 | 4.369 | 8.953 | 4.269 | 5.614 | 6.178 |
| 80 | 1.316 | 4.582 | 1.580 | 8.893 | 15.362 | 8.083 | 10.420 | 9.965 | 7.029 | 6.626 | 6.078 | 3.172 | 6.926 |
| | | | | | | | | | | | | | |

Chapter 5: Conclusions

The calculations below were accomplished using the shelf life equation (Eq 6) described on page 22. Using the data within the sections of Chapter 4, permeance values (P) were calculated given a desired shelf life (t). The permeance values were then used to determine package options. Blister calculations are listed first.

25C / 75% RH Testing (Blisters)

t = 730 days (2 years) [desired shelf life]

I = 1 mil (Use a value of 1 for blisters)

W = 0.1 g per tablet

B = 1.5485 (unitless) (Reference Figure 11, Page 31)

 $A = 1 \text{ m}^2$ (Use a value of 1 for blisters)

P = Permeance (Unknown)

 $p_s = 23.756 \text{ mm Hg}$

 $RH_e = 75\%$ (RH of storage conditions)

RH_i = 25.4% (RH generated by shelf life computer model using the IMC)

 $RH_c = 65\%$ (Same RH for all three temperatures)

730 days = $(1mil^*0.1g^*1.5485/1m^2*P^*23.756mmHg)^*ln[(.75-.254)/(.75-.65)]$

 $P = 1.43 * 10^{-5} g/day*cavity*mmHg$

30C / 75% RH Testing (Blisters)

t = 365 days (1 year) [desired shelf life]

I = 1 mil (Use a value of 1 for blisters)

W = 0.1 g per tablet

B = 1.4422 (unitless) (Reference Figure 11, Page 31)

 $A = 1 \text{ m}^2$ (Use a value of 1 for blisters)

P = Permeance (Unknown)

 $p_s = 31.824 \text{ mm Hg}$

 $RH_e = 75\%$ (RH of storage conditions)

RH_i = 31.5% (RH generated by shelf life computer model using the IMC)

 $RH_c = 65\%$ (Same RH for all three temperatures)

 $365 \text{ days} = (1 \text{mil}^{+} 0.1 \text{g}^{+} 1.4422 / 1 \text{m}^{2} + \text{P}^{+} 31.824 \text{mmHg})^{+} \ln[(.75 - .315) / (.75 - .65)]$

P = 1.83 * 10⁻⁵ g/day*cavity*mmHg

40C / 75% RH Testing (Blisters)

t = 180 days (6 months) [desired shelf life]

I = 1 mil (Use a value of 1 for blisters)

W = 0.1 g per tablet

B = 1.2000 (unitless) (Reference Figure 11, Page 31)

 $A = 1 \text{ m}^2$ (Use a value of 1 for blisters)

P = Permeance (Unknown)

 $p_s = 55.324 \text{ mm Hg}$

 $RH_e = 75\%$ (RH of storage conditions)

RH_i = 32.2% (RH generated by shelf life computer model using the IMC)

 $RH_c = 65\%$ (Same RH for all three temperatures)

 $180 \text{ days} = (1 \text{mil}^{*} 0.1 \text{g}^{*} 1.2000 / 1 \text{m}^{2} \text{P}^{*} 55.324 \text{mmHg})^{*} \ln[(.75 - .322) / (.75 - .65)]$

 $P = 1.75 * 10^{-5} g/day*cavity*mmHg$

Looking at the 25C (room temperature) shelf life calculation for blisters, 730 days (two years) was used as the desired shelf life. For marketed products, this is a typical shelf life to use during the initial stages of development for room temperature or real-time stability. For the 30C (accelerated) blister calculation, 365 days (one year) was used as the desired shelf life. As a rule of thumb, if packaged product passes analytical testing after one year at 30C, the packaged product can be assumed to pass two years at 25C. For similar reasons, the 40C (accelerated) calculations use 180 days (six months) as the desired shelf life. If

the packaged product passes analytical testing after six months at 40C, the packaged product can be assumed to pass two years at 25C.

Using the 40C permeation result as an example, blister materials which have a permeance value below 1.75 * 10-5 g/day*cavity*mmHg (tested at 40C / 75%RH) will be packaging options for this Prednisone product. The calculated permeance value identifies a specific level of moisture, which will initiate product failure within a package. For example, PVC is a relatively inexpensive material, which has a high permeance to moisture. Using PVC blisters for a developmental product is an excellent way to reduce material costs once the product is packaged at high volumes for market. A typical permeance value for PVC blisters at 40C / 75% RH is 4.57 * 10⁻⁵ g/day*cavity*mmHg (Eli Lilly and Company, 2000). Since this value is higher than the calculated permeance value for blisters at 40C, PVC may not be an option, and a more expensive, higher barrier material will be recommended. Aclar is a popular high barrier blister used in the pharmaceutical industry. A typical permeance value for 0.6mil Aclar blisters at 40C / 75% RH is 3.88 * 10⁻⁶ g/day*cavity*mmHg (Eli Lilly and Company, 2000). Reviewing the calculated permeance value for blisters at 40C, the level of moisture protection received from 0.6mil Aclar is sufficient.

Pharmaceutical companies typically use high density polyethylene (HDPE) containers when a solid oral product requires a bottle for packaging. The Prednisone tablets being used for this study were supplied in HDPE bottles.

These bottles contained 1000 tablets and were approximately 170cc in volume.

The permeance calculations at three conditions for the bottles described above are as follows.

25C / 75% RH Testing (Bottles)

t = 730 days (2 years) [desired shelf life]

l = 34 mil

W = 100 g (0.1 g per tablet, 1000 tablets per bottle)

B = 1.5485 (unitless) (Reference Figure 11, Page 31)

 $A = 0.03m^2$ (Area of bottle walls)

P = Permeance (Unknown)

 $p_s = 23.756 \text{ mm Hg}$

 $RH_e = 75\%$ (RH of storage conditions)

 $RH_i = 25.4\%$ (RH generated by shelf life computer model using the IMC)

 $RH_c = 65\%$ (Same RH for all three temperatures)

730 days = $(34mil*100g*1.5485/0.03m^2*P*23.756mmHg)*In[(.75-.254)/(.75-.65)]$

P = 16.2 g/day*bottle*mmHg

30C / 75% RH Testing (Bottles)

t = 365 days (1 year) [desired shelf life]

l = 34 mil

W = 100 g (0.1 g per tablet, 1000 tablets per bottle)

B = 1.4422 (unitless) (Reference Figure 11, Page 31)

 $A = 0.03 \text{ m}^2$ (Area of bottle walls)

P = Permeance (Unknown)

 $p_s = 31.824 \text{ mm Hg}$

 $RH_e = 75\%$ (RH of storage conditions)

RH_i = 31.5% (RH generated by shelf life computer model using the IMC)

 $RH_c = 65\%$ (Same RH for all three temperatures)

 $365 \text{ days} = (34\text{mil}*100\text{g}*1.4422/0.03\text{m}^2*\text{P}*31.824\text{mmHg})*\text{ln}[(.75-.315)/(.75-.65)]$

P = 20.7 g/day*bottle*mmHg

40C / 75% RH Testing (Bottles)

t = 180 days (6 months) [desired shelf life]

l = 34 mil

W = 100 g (0.1 g per tablet, 1000 tablets per bottle)

B = 1.2000 (unitless) (Reference Figure 11, Page 31)

 $A = 0.03 \text{ m}^2$ (Area of bottle walls)

P = Permeance (Unknown)

 $p_s = 55.324 \text{ mm Hg}$

 $RH_e = 75\%$ (RH of storage conditions)

RH_i = 32.2% (RH generated by shelf life computer model using the IMC)

 $RH_c = 65\%$ (Same RH for all three temperatures)

 $180 \text{ days} = (34\text{mil}*100\text{g}*1.2000/0.03\text{m}^2*\text{P}*55.324\text{mmHg})*\ln[(.75-.322)/(.75-.65)]$

P = 19.9 g/day*bottle*mmHg

A typical HDPE bottle (34mil thickness and area equal to 0.03m²) at 170cc will have a permeance value of approximately 0.04 g/day*bottle*mmHg at 40C / 75% RH (Eli Lilly and Company, 2000). Comparing this value to the bottle permeation results for 40C, 0.04 is much lower than 19.9. The level of protection for this product in a 1000 count HDPE bottle with minimal head space is very high. However, as the bottle count decreases, the permeation value in the shelf life calculation will decrease. So, a lower count in the same bottle will ultimately be less protected because there are fewer tablets to share the moisture permeating into the bottle.

The shelf life calculations have provided packaging options for this

Prednisone product for blisters and bottles. Concerning blisters, this product
may not meet stability requirements in PVC blisters, but should be protected
sufficiently in 0.6 mil Aclar. For bottles, higher count bottle presentations (bulk) in
typical HDPE bottles should provide sufficient protection. However, as the
product count significantly decreases for a specific bottle presentation,
permeation values should be reviewed closely.

Table 14. Summary of Calculated Permeance Values

| Condition | Package | Permeance (g/day*package*mmHg) | Desired Shelf Life |
|-----------|---------|--------------------------------|--------------------|
| 25C/75%RH | Blister | 1.43 * 10 ⁻⁵ | 2 years |
| 30C/75%RH | Blister | 1.83 * 10 ⁻⁵ | 1 year |
| 40C/75%RH | Blister | 1.75 * 10 ⁻⁵ | 6 months |
| 25C/75%RH | Bottle | 16.2 | 2 years |
| 30C/75%RH | Bottle | 20.7 | 1 year |
| 40C/75%RH | Bottle | 19.9 | 6 months |

These packaging calculations are not meant to replace any type of product/package stability test. However, the information gathered and calculations made in such a study, especially for early development products, can identify packaging options for early phase stability studies. For example, instead of using four or five blister materials in initial product/package stability testing, shelf life modeling can narrow the choices down to two or three options, which can significantly reduce development costs.

Chapter 6: Recommendations for Future Work

My recommendation for future work is to expand the existing shelf life model at the School of Packaging to include other packaging components. For example, isotherms can be developed for desiccant packages and bottle fillers (ex: cotton), which compete with the product to absorb moisture. The moisture contents of these components can be accounted for within the model, similar to the product moisture content. Packaging components such as fillers and desiccant are popular materials in the pharmaceutical industry. Modeling a complex system such as a bottle containing product, cotton and desiccant, is a realistic packaging option used in industry.

Appendix A

25C Dissolution Values (Raw Data and Statistics)

%Dissolution Determination (25C)

| | | ABS | S(AU) | | . 9 | | | |
|-----|--------|-------|-------|---------|--------|--------|--------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.437 | 0.452 | 0.436 | | 95.96 | 99.24 | 95.74 | |
| | Mean = | 0.442 | STD = | 0.00896 | Mean = | 96.980 | STD = | 1.95696 |
| 65 | 0.428 | 0.457 | 0.462 | | 94.00 | 100.33 | 101.42 | |
| | Mean = | 0.449 | STD = | 0.0184 | Mean = | 98.581 | STD = | 4.00820 |
| 75 | 0.437 | 0.433 | 0.425 | i | 95.96 | 95.09 | 93.34 | |
| | Mean = | 0.432 | STD = | 0.0061 | Mean = | 94.796 | STD = | 1.33408 |
| 80 | 0.415 | 0.427 | 0.424 | | 91.16 | 93.78 | 93.12 | |
| | Mean = | 0.422 | STD = | 0.0062 | Mean = | 92.686 | STD = | 1.36354 |
| 90 | 0.113 | 0.097 | 0.095 | | 25.22 | 21.72 | 21.29 | |
| | Mean = | 0.102 | STD = | 0.0099 | Mean = | 22.744 | STD = | 2.15410 |

Time(days)= 3

Calibration Curve: "y=0.458 x - 0.0025"

Table 15. 25C Raw Dissolution Data and Statistics (Day3)

%Dissolution Determination (25C)

| | | ABS | (AU) | | o, | %Dissolution | | |
|-----|--------|-------|-------|---------|---------------|--------------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.44 | 0.444 | 0.444 | | 96.62 | 97.49 | 97.49 | |
| | Mean = | 0.443 | STD = | 0.00231 | Mean = | 97.198 | STD = | 0.50424 |
| 65 | 0.442 | 0.417 | 0.372 | | 97.05 | 91.59 | 81.77 | |
| | Mean = | 0.410 | STD = | 0.0355 | Mean = | 90.138 | STD = | 7.74520 |
| 75 | 0.416 | 0.43 | 0.41 | | 91.38 | 94.43 | 90.07 | |
| | Mean = | 0.419 | STD = | 0.0103 | Mean = | 91.958 | STD = | 2.24087 |
| 80 | 0.389 | 0.353 | 0.399 | | 85. 48 | 77.62 | 87.66 | |
| | Mean = | 0.380 | STD = | 0.0242 | Mean = | 83.588 | STD = | 5.28246 |

Time(days)=

Calibration Curve: "y=0.458 x - 0.0025"

Table 16. 25C Raw Dissolution Data and Statistics (Day6)

| | | ABS | S(AU) | | 9 | | | |
|-----|--------|-------|-------|---------|--------|--------|-------|----------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.444 | 0.447 | 0.441 | | 97.49 | 98.14 | 96.83 | |
| | Mean = | 0.444 | STD = | 0.00300 | Mean = | 97.489 | STD = | 0.65502 |
| 65 | 0.436 | 0.434 | 0.435 | | 95.74 | 95.31 | 95.52 | |
| | Mean = | 0.435 | STD = | 0.0010 | Mean = | 95.524 | STD = | 0.21834 |
| 75 | 0.426 | 0.437 | 0.339 | | 93.56 | 95.96 | 74.56 | |
| | Mean = | 0.401 | STD = | 0.0537 | Mean = | 88.028 | STD = | 11.72213 |
| 80 | 0.396 | 0.4 | 0.418 | | 87.01 | 87.88 | 91.81 | |
| | Mean = | 0.405 | STD = | 0.0117 | Mean = | 88.901 | STD = | 2.55872 |

Time(days)= 9 Calibration Curve: "y=0.458 x - 0.0025"

Table 17. 25C Raw Dissolution Data and Statistics (Day9)

%Dissolution Determination (25C)

| | | ABS | S(AU) | | ٩ | | | |
|-----|--------|-------|-------|---------|--------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.424 | 0.447 | 0.438 | | 93.12 | 98.14 | 96.18 | |
| | Mean = | 0.436 | STD = | 0.01159 | Mean = | 95.815 | STD = | 2.53062 |
| 65 | 0.442 | 0.442 | 0.446 | | 97.05 | 97.05 | 97.93 | |
| | Mean = | 0.443 | STD = | 0.0023 | Mean = | 97.344 | STD = | 0.50424 |
| 75 | 0.415 | 0.435 | 0.434 | | 91.16 | 95.52 | 95.31 | |
| | Mean = | 0.428 | STD = | 0.0113 | Mean = | 93.996 | STD = | 2.46057 |
| 80 | 0.379 | 0.428 | 0.395 | | 83.30 | 94.00 | 86.79 | |
| | Mean = | 0.401 | STD = | 0.0250 | Mean = | 88.028 | STD = | 5.45560 |

Time(days)= 12 Calibration Curve: "y=0.458 x - 0.0025"

Table 18. 25C Raw Dissolution Data and Statistics (Day12)

| | | ABS | S(AU) %Dissolution | | | | #1 #2 #3 101.64 99.45 98.36 Mean = 99.818 STD = 98.58 99.24 92.25 | | | | |
|-----|--------|-------|--------------------|---------|--------|--------|--|---------|--|--|--|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | | | | |
| 50 | 0.463 | 0.453 | 0.448 | | 101.64 | 99.45 | 98.36 | | | | |
| | Mean = | 0.455 | STD = | 0.00764 | Mean = | 99.818 | STD = | 1.66760 | | | |
| 65 | 0.449 | 0.452 | 0.42 | | 98.58 | 99.24 | 92.25 | | | | |
| | Mean = | 0.440 | STD = | 0.0177 | Mean = | 96.689 | STD = | 3.85872 | | | |
| 75 | 0.402 | 0.417 | 0.436 | | 88.32 | 91.59 | 95.74 | | | | |
| | Mean = | 0.418 | STD = | 0.0170 | Mean = | 91.885 | STD = | 3.72034 | | | |
| 80 | 0.344 | 0.396 | 0.398 | | 75.66 | 87.01 | 87.45 | | | | |
| | Mean = | 0.379 | STD = | 0.0306 | Mean = | 83.370 | STD = | 6.68469 | | | |

Time(days)= 15 Calibration Curve: "y=0.458 x - 0.0025"

Table 19. 25C Raw Dissolution Data and Statistics (Day15)

%Dissolution Determination (25C)

| | ABS | S(AU) | | 9 | | | |
|--------|--|--------------|---------|-----------------|--------------------|-----------------------|--------------------------|
| #1 | #2 | #3 | | #1 | #2 | #3 | |
| 0.452 | 0.443 | 0.443 | | 99.24 | 97.27 | 97.27 | |
| Mean = | 0.446 | STD = | 0.00520 | Mean = | 97.926 | STD = | 1.13453 |
| 0.431 | 0.448 | 0.44 | | 94.65 | 98.36 | 96.62 | |
| Mean = | 0.440 | STD = | 0.0085 | Mean = | 96.543 | STD = | 1.85697 |
| 0.421 | 0.431 | 0.436 | | 92.47 | 94.65 | 95.74 | |
| Mean = | 0.429 | STD = | 0.0076 | Mean = | 94.287 | STD = | 1.66760 |
| 0.375 | 0.434 | 0.386 | | 82.42 | 95.31 | 84.83 | |
| Mean = | 0.398 | STD = | 0.0314 | Mean = | 87.518 | STD = | 6.85024 |
| | 0.452 Mean = 0.431 Mean = 0.421 Mean = 0.375 | #1 #2 0.452 | 0.452 | #1 #2 #3 0.452 | #1 #2 #3 #1 0.452 | #1 #2 #3 #1 #2 0.452 | #1 #2 #3 #1 #2 #3 0.452 |

Time(days)= 18 Calibration Curve: "y=0.458 x - 0.0025"

Table 20. 25C Raw Dissolution Data and Statistics (Day18)

| | | ABS | S(AU) | | 9 | %Dissolution | | |
|-----|--------|-------|-------|---------|--------|--------------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.442 | 0.44 | 0.445 | | 97.05 | 96.62 | 97.71 | |
| | Mean = | 0.442 | STD = | 0.00252 | Mean = | 97.125 | STD = | 0.54948 |
| 65 | 0.431 | 0.441 | 0.438 | | 94.65 | 96.83 | 96.18 | |
| | Mean = | 0.437 | STD = | 0.0051 | Mean = | 95.888 | STD = | 1.12044 |
| 70 | 0.363 | 0.419 | 0.396 | | 79.80 | 92.03 | 87.01 | |
| | Mean = | 0.393 | STD = | 0.0281 | Mean = | 86.281 | STD = | 6.14594 |
| 80 | 0.392 | 0.379 | 0.347 | | 86.14 | 83.30 | 76.31 | |
| | Mean = | 0.373 | STD = | 0.0232 | Mean = | 81.914 | STD = | 5.05652 |

Time(days)= 21 Calibration Curve: "y=0.458 x - 0.0025"

Table 21. 25C Raw Dissolution Data and Statistics (Day21)

%Dissolution Determination (25C)

| | | ABS | S(AU) | | 9 | %Dissolution | | |
|-----|--------|-------|-------|---------|--------|--------------|-------|----------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.441 | 0.45 | 0.443 | | 96.83 | 98.80 | 97.27 | |
| | Mean = | 0.445 | STD = | 0.00473 | Mean = | 97.635 | STD = | 1.03184 |
| 65 | 0.435 | 0.436 | 0.427 | | 95.52 | 95.74 | 93.78 | |
| | Mean = | 0.433 | STD = | 0.0049 | Mean = | 95.015 | STD = | 1.07705 |
| 70 | 0.397 | 0.413 | 0.418 | | 87.23 | 90.72 | 91.81 | |
| | Mean = | 0.409 | STD = | 0.0110 | Mean = | 89.920 | STD = | 2.39512 |
| 80 | 0.383 | 0.415 | 0.311 | | 84.17 | 91.16 | 68.45 | |
| | Mean = | 0.370 | STD = | 0.0533 | Mean = | 81.259 | STD = | 11.63027 |

Time(days)= 24 Calibration Curve: "y=0.458 x - 0.0025"

Table 22. 25C Raw Dissolution Data and Statistics (Day24)

| | | ABS | S(AU) | | 9 | %Dissolution | | |
|-----|--------|-------|-------|---------|--------|--------------|-------|----------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.432 | 0.429 | 0.451 | | 94.87 | 94.21 | 99.02 | |
| | Mean = | 0.437 | STD = | 0.01193 | Mean = | 96.033 | STD = | 2.60488 |
| 65 | 0.439 | 0.451 | 0.438 | | 96.40 | 99.02 | 96.18 | |
| | Mean = | 0.443 | STD = | 0.0072 | Mean = | 97.198 | STD = | 1.57951 |
| 75 | 0.429 | 0.419 | 0.422 | | 94.21 | 92.03 | 92.69 | |
| | Mean = | 0.423 | STD = | 0.0051 | Mean = | 92.977 | STD = | 1.12044 |
| 80 | 0.313 | 0.415 | 0.385 | | 68.89 | 91.16 | 84.61 | |
| | Mean = | 0.371 | STD = | 0.0524 | Mean = | 81.550 | STD = | 11.44571 |

Time(days)= 37 Calibration Curve: "y=0.458 x - 0.0025"

Table 23. 25C Raw Dissolution Data and Statistics (Day37)

%Dissolution Determination (25C)

| | | ABS(AU) %Dissolution | | | | | | |
|-----|--------|----------------------|-------|---------|--------|--------|--------|----------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.408 | 0.465 | 0.459 | | 89.63 | 102.07 | 100.76 | |
| | Mean = | 0.444 | STD = | 0.03132 | Mean = | 97.489 | STD = | 6.83863 |
| 65 | 0.444 | 0.421 | 0.447 | | 97.49 | 92.47 | 98.14 | |
| | Mean = | 0.437 | STD = | 0.0142 | Mean = | 96.033 | STD = | 3.10576 |
| 75 | 0.339 | 0.412 | 0.425 | | 74.56 | 90.50 | 93.34 | |
| | Mean = | 0.392 | STD = | 0.0464 | Mean = | 86.135 | STD = | 10.12168 |
| 80 | 0.336 | 0.32 | 0.3 | | 73.91 | 70.41 | 66.05 | |
| | Mean = | 0.319 | STD = | 0.0180 | Mean = | 70.124 | STD = | 3.93821 |
| 90 | 0.028 | 0.028 | 0.032 | | 6.66 | 6.66 | 7.53 | |
| | Mean = | 0.029 | STD = | 0.0023 | Mean = | 6.951 | STD = | 0.50424 |

Time(days)= 44 Calibration Curve: "y=0.458 x - 0.0025"

Table 24. 25C Raw Dissolution Data and Statistics (Day44)

| | | | ABS | S(AU) | | Ģ | %Dissolution | | |
|---|-----|--------|-------|-------|---------|--------|--------------|-------|---------|
| | %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| • | 50 | 0.435 | 0.41 | 0.449 | | 95.52 | 90.07 | 98.58 | |
| | | Mean = | 0.431 | STD = | 0.01976 | Mean = | 94.723 | STD = | 4.31372 |
| | 65 | 0.446 | 0.441 | 0.434 | | 97.93 | 96.83 | 95.31 | |
| | | Mean = | 0.440 | STD = | 0.0060 | Mean = | 96.689 | STD = | 1.31609 |
| | 75 | 0.376 | 0.362 | 0.433 | | 82.64 | 79.59 | 95.09 | |
| | | Mean = | 0.390 | STD = | 0.0376 | Mean = | 85.771 | STD = | 8.21127 |
| | 80 | 0.347 | 0.389 | 0.381 | | 76.31 | 85.48 | 83.73 | |
| | | Mean = | 0.372 | STD = | 0.0223 | Mean = | 81.841 | STD = | 4.86921 |
| | | | | | | | | | |

Time(days)= 51 Calibration Curve: "y=0.458 x - 0.0025"

Table 25. 25C Raw Dissolution Data and Statistics (Day51)

%Dissolution Determination (25C)

| | | ABS(AU) | | | q | %Dissolution | | |
|-----|--------|---------|-------|---------|----------|--------------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.437 | 0.448 | 0.448 | | 95.96 | 98.36 | 98.36 | |
| | Mean = | 0.444 | STD = | 0.00635 | Mean = | 97.562 | STD = | 1.38665 |
| 33 | 0.446 | 0.452 | 0.448 | | 97.93 | 99.24 | 98.36 | |
| | Mean = | 0.449 | STD = | 0.0031 | Mean = | 98.508 | STD = | 0.66704 |
| 50 | 0.425 | 0.448 | 0.45 | | 93.34 | 98.36 | 98.80 | |
| | Mean = | 0.441 | STD = | 0.0139 | Mean = | 96.834 | STD = | 3.03328 |
| 65 | 0.433 | 0.433 | 0.439 | | 95.09 | 95.09 | 96.40 | |
| | Mean = | 0.435 | STD = | 0.0035 | Mean = | 95.524 | STD = | 0.75635 |
| 75 | 0.407 | 0.361 | 0.418 | | 89.41 | 79.37 | 91.81 | |
| | Mean = | 0.395 | STD = | 0.0302 | Mean = | 86.863 | STD = | 6.60217 |
| 80 | 0.401 | 0.381 | 0.37 | | 88.10 | 83.73 | 81.33 | |
| | Mean = | 0.384 | STD = | 0.0157 | Mean = | 84.389 | STD = | 3.43149 |

Time(days)= 58 Calibration Curve: "y=0.458 x - 0.0025"

Table 26. 25C Raw Dissolution Data and Statistics (Day58)

30C Dissolution Values (Raw Data and Statistics)

%Dissolution Determination (30C)

| | | ABS | S(AU) | | ę | | | |
|-----|--------|-------|-------|---------|--------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 33 | 0.443 | 0.402 | 0.429 | | 97.27 | 88.32 | 94.21 | |
| | Mean = | 0.425 | STD = | 0.02084 | Mean = | 93.268 | STD = | 4.55036 |
| 50 | 0.442 | 0.445 | 0.447 | | 97.05 | 97.71 | 98.14 | |
| | Mean = | 0.445 | STD = | 0.0025 | Mean = | 97.635 | STD = | 0.54948 |
| 65 | 0.432 | 0.442 | 0.434 | | 94.87 | 97.05 | 95.31 | |
| | Mean = | 0.436 | STD = | 0.0053 | Mean = | 95.742 | STD = | 1.15535 |
| 75 | 0.432 | 0.444 | 0.432 | | 94.87 | 97.49 | 94.87 | |
| | Mean = | 0.436 | STD = | 0.0069 | Mean = | 95.742 | STD = | 1.51271 |
| 80 | 0.407 | 0.404 | 0.385 | | 89.41 | 88.76 | 84.61 | |
| | Mean = | 0.399 | STD = | 0.0119 | Mean = | 87.591 | STD = | 2.60488 |
| 90 | 0.146 | 0.087 | 0.148 | | 32.42 | 19.54 | 32.86 | |
| | Mean = | 0.127 | STD = | 0.0347 | Mean = | 28.275 | STD = | 7.56669 |

Time(days)= 3 Calibration Curve: "y=0.458 x - 0.0025"

Table 27. 30C Raw Dissolution Data and Statistics (Day3)

%Dissolution Determination (30C)

| | | ABS(AU) | | | 9 | 6Dissolution | | |
|-----|--------|---------|-------|---------|--------|--------------|-------|----------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.442 | 0.408 | 0.454 | | 97.05 | 89.63 | 99.67 | |
| | Mean = | 0.435 | STD = | 0.02386 | Mean = | 95.451 | STD = | 5.20976 |
| 33 | 0.417 | 0.456 | 0.432 | | 91.59 | 100.11 | 94.87 | |
| | Mean = | 0.435 | STD = | 0.0197 | Mean = | 95.524 | STD = | 4.29527 |
| 50 | 0.438 | 0.448 | 0.435 | | 96.18 | 98.36 | 95.52 | |
| | Mean = | 0.440 | STD = | 0.0068 | Mean = | 96.689 | STD = | 1.48621 |
| 65 | 0.437 | 0.449 | 0.427 | | 95.96 | 98.58 | 93.78 | |
| | Mean = | 0.438 | STD = | 0.0110 | Mean = | 96.106 | STD = | 2.40505 |
| 75 | 0.423 | 0.437 | 0.446 | | 92.90 | 95.96 | 97.93 | |
| | Mean = | 0.435 | STD = | 0.0116 | Mean = | 95.597 | STD = | 2.53062 |
| 80 | 0.406 | 0.308 | 0.387 | | 89.19 | 67.79 | 85.04 | |
| | Mean = | 0.367 | STD = | 0.0520 | Mean = | 80.677 | STD = | 11.34741 |

Time(days)= 6 Calibration Curve: "y=0.458 x - 0.0025"

Table 28. 30C Raw Dissolution Data and Statistics (Day6)

| | | ABS(AU) | | | • | | | |
|-----|--------|---------|-------|---------|--------|---------|--------|----------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.45 | 0.441 | 0.437 | | 98.80 | 96.83 | 95.96 | |
| | Mean = | 0.443 | STD = | 0.00666 | Mean = | 97.198 | STD = | 1.45378 |
| 33 | 0.423 | 0.429 | 0.429 | | 92.90 | 94.21 | 94.21 | |
| | Mean = | 0.427 | STD = | 0.0035 | Mean = | 93.777 | STD = | 0.75635 |
| 50 | 0.433 | 0.479 | 0.472 | | 95.09 | 105.13 | 103.60 | |
| | Mean = | 0.461 | STD = | 0.0248 | Mean = | 101.274 | STD = | 5.41174 |
| 65 | 0.461 | 0.463 | 0.46 | | 101.20 | 101.64 | 100.98 | |
| | Mean = | 0.461 | STD = | 0.0015 | Mean = | 101.274 | STD = | 0.33352 |
| 75 | 0.353 | 0.439 | 0.431 | | 77.62 | 96.40 | 94.65 | |
| | Mean = | 0.408 | STD = | 0.0475 | Mean = | 89.556 | STD = | 10.37367 |
| 80 | 0.382 | 0.4 | 0.37 | | 83.95 | 87.88 | 81.33 | |
| | Mean = | 0.384 | STD = | 0.0151 | Mean = | 84.389 | STD = | 3.29687 |

Time(days)= 9 Calibration Curve: "y=0.458 x - 0.0025"

Table 29. 30C Raw Dissolution Data and Statistics (Day9)

%Dissolution Determination (30C)

| | | ABS(AU) | | | | %Dissolution | 1 | |
|-----|--------|---------|-------|---------|--------|--------------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.439 | 0.45 | 0.431 | | 96.40 | 98.80 | 94.65 | |
| | Mean = | 0.440 | STD = | 0.00954 | Mean = | 96.616 | STD = | 2.08284 |
| 33 | 0.436 | 0.43 | 0.439 | | 95.74 | 94.43 | 96.40 | |
| | Mean = | 0.435 | STD = | 0.0046 | Mean = | 95.524 | STD = | 1.00056 |
| 50 | 0.443 | 0.448 | 0.443 | | 97.27 | 98.36 | 97.27 | |
| | Mean = | 0.445 | STD = | 0.0029 | Mean = | 97.635 | STD = | 0.63030 |
| 65 | 0.417 | 0.426 | 0.45 | | 91.59 | 93.56 | 98.80 | |
| | Mean = | 0.431 | STD = | 0.0171 | Mean = | 94.651 | STD = | 3.72461 |
| 75 | 0.359 | 0.423 | 0.424 | | 78.93 | 92.90 | 93.12 | |
| | Mean = | 0.402 | STD = | 0.0372 | Mean = | 88.319 | STD = | 8.13154 |
| 80 | 0.387 | 0.421 | 0.383 | | 85.04 | 92.47 | 84.17 | |
| | Mean = | 0.397 | STD = | 0.0209 | Mean = | 87.227 | STD = | 4.55909 |

Time(days)= 12 Calibration Curve: "y=0.458 x - 0.0025"

Table 30. 30C Raw Dissolution Data and Statistics (Day12)

| | | ABS | (AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.434 | 0.414 | 0.443 | | 95.31 | 90.94 | 97.27 | |
| | Mean = | 0.430 | STD = | 0.01484 | Mean = | 94.505 | STD = | 3.24097 |
| 65 | 0.437 | 0.453 | 0.403 | | 95.96 | 99.45 | 88.54 | |
| | Mean = | 0.431 | STD = | 0.0255 | Mean = | 94.651 | STD = | 5.57517 |
| 75 | 0.426 | 0.42 | 0.443 | | 93.56 | 92.25 | 97.27 | |
| | Mean = | 0.430 | STD = | 0.0119 | Mean = | 94.360 | STD = | 2.60488 |
| 80 | 0.398 | 0.343 | 0.391 | | 87.45 | 75.44 | 85.92 | |
| | Mean = | 0.377 | STD = | 0.0299 | Mean = | 82.933 | STD = | 6.53686 |

Time(days)= 15 Calibration Curve: "y=0.458 x - 0.0025"

Table 31. 30C Raw Dissolution Data and Statistics (Day15)

%Dissolution Determination (30C)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.447 | 0.45 | 0.455 | | 98.14 | 98.80 | 99.89 | |
| | Mean = | 0.451 | STD = | 0.00404 | Mean = | 98.945 | STD = | 0.88241 |
| 65 | 0.427 | 0.448 | 0.44 | | 93.78 | 98.36 | 96.62 | |
| | Mean = | 0.438 | STD = | 0.0106 | Mean = | 96.252 | STD = | 2.31414 |
| 75 | 0.419 | 0.422 | 0.415 | | 92.03 | 92.69 | 91.16 | |
| | Mean = | 0.419 | STD = | 0.0035 | Mean = | 91.958 | STD = | 0.76679 |
| 80 | 0.351 | 0.397 | 0.399 | | 77.18 | 87.23 | 87.66 | |
| | Mean = | 0.382 | STD = | 0.0272 | Mean = | 84.025 | STD = | 5.92880 |

Time(days)= 18 Calibration Curve: "y=0.458 x - 0.0025"

Table 32. 30C Raw Dissolution Data and Statistics (Day18)

| | | ABS | S(AU) | | 9 | | | |
|-----|--------|-------|-------|---------|--------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.45 | 0.455 | 0.437 | | 98.80 | 99.89 | 95.96 | |
| | Mean = | 0.447 | STD = | 0.00929 | Mean = | 98.217 | STD = | 2.02873 |
| 33 | 0.437 | 0.453 | 0.449 | | 95.96 | 99.45 | 98.58 | |
| | Mean = | 0.446 | STD = | 0.0083 | Mean = | 97.999 | STD = | 1.81805 |
| 50 | 0.437 | 0.441 | 0.424 | | 95.96 | 96.83 | 93.12 | |
| | Mean = | 0.434 | STD = | 0.0089 | Mean = | 95.306 | STD = | 1.94065 |
| 65 | 0.427 | 0.441 | 0.422 | | 93.78 | 96.83 | 92.69 | |
| | Mean = | 0.430 | STD = | 0.0098 | Mean = | 94.432 | STD = | 2.15041 |
| 75 | 0.415 | 0.398 | 0.432 | | 91.16 | 87.45 | 94.87 | |
| | Mean = | 0.415 | STD = | 0.0170 | Mean = | 91.157 | STD = | 3.71179 |
| 80 | 0.39 | 0.381 | 0.316 | | 85.70 | 83.73 | 69.54 | |
| | Mean = | 0.362 | STD = | 0.0404 | Mean = | 79.658 | STD = | 8.81602 |

Time(days)= 21 Calibration Curve: "y=0.458 x - 0.0025"

Table 33. 30C Raw Dissolution Data and Statistics (Day21)

%Dissolution Determination (30C)

| | | ABS | S(AU) | | 9 | | | |
|-----|--------|-------|-------|---------|--------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.435 | 0.437 | 0.45 | | 95.52 | 95.96 | 98.80 | |
| | Mean = | 0.441 | STD = | 0.00814 | Mean = | 96.761 | STD = | 1.77828 |
| 65 | 0.426 | 0.434 | 0.428 | | 93.56 | 95.31 | 94.00 | |
| | Mean = | 0.429 | STD = | 0.0042 | Mean = | 94.287 | STD = | 0.90902 |
| 75 | 0.406 | 0.38 | 0.432 | | 89.19 | 83.52 | 94.87 | |
| | Mean = | 0.406 | STD = | 0.0260 | Mean = | 89.192 | STD = | 5.67686 |
| 80 | 0.367 | 0.406 | 0.402 | | 80.68 | 89.19 | 88.32 | |
| | Mean = | 0.392 | STD = | 0.0215 | Mean = | 86.063 | STD = | 4.68458 |

Time(days)= 27 Calibration Curve: "y=0.458 x - 0.0025"

Table 34. 30C Raw Dissolution Data and Statistics (Day27)

| | | ABS(AU) | | | %Dissolution | | | |
|-----|--------|---------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.401 | 0.435 | 0.432 | | 88.10 | 95.52 | 94.87 | |
| | Mean = | 0.423 | STD = | 0.01882 | Mean = | 92.831 | STD = | 4.10999 |
| 33 | 0.446 | 0.459 | 0.404 | | 97.93 | 100.76 | 88.76 | |
| | Mean = | 0.436 | STD = | 0.0287 | Mean = | 95.815 | STD = | 6.27642 |
| 50 | 0.432 | 0.425 | 0.44 | | 94.87 | 93.34 | 96.62 | |
| | Mean = | 0.432 | STD = | 0.0075 | Mean = | 94.942 | STD = | 1.63877 |
| 65 | 0.436 | 0.437 | 0.401 | | 95.74 | 95.96 | 88.10 | |
| | Mean = | 0.425 | STD = | 0.0205 | Mean = | 93.268 | STD = | 4.47643 |
| 75 | 0.417 | 0.42 | 0.425 | | 91.59 | 92.25 | 93.34 | |
| | Mean = | 0.421 | STD = | 0.0040 | Mean = | 92.394 | STD = | 0.88241 |
| 80 | 0.373 | 0.34 | 0.291 | | 81.99 | 74.78 | 64.08 | |
| | Mean = | 0.335 | STD = | 0.0413 | Mean = | 73.617 | STD = | 9.00859 |

Time(days)= 33 Calibration Curve: "y=0.458 x - 0.0025"

Table 35. 30C Raw Dissolution Data and Statistics (Day33)

%Dissolution Determination (30C)

| | | ABS(AU) | | | | %Dissolution | | |
|-----|--------|---------|-------|---------|--------|--------------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.45 | 0.439 | 0.448 | | 98.80 | 96.40 | 98.36 | |
| | Mean = | 0.446 | STD = | 0.00586 | Mean = | 97.853 | STD = | 1.27936 |
| 33 | 0.439 | 0.443 | 0.443 | | 96.40 | 97.27 | 97.27 | |
| | Mean = | 0.442 | STD = | 0.0023 | Mean = | 96.980 | STD = | 0.50424 |
| 50 | 0.412 | 0.436 | 0.441 | | 90.50 | 95.74 | 96.83 | |
| | Mean = | 0.430 | STD = | 0.0155 | Mean = | 94.360 | STD = | 3.38487 |
| 65 | 0.428 | 0.436 | 0.435 | | 94.00 | 95.74 | 95.52 | |
| | Mean = | 0.433 | STD = | 0.0044 | Mean = | 95.087 | STD = | 0.95172 |
| 75 | 0.39 | 0.409 | 0.379 | | 85.70 | 89.85 | 83.30 | |
| | Mean = | 0.393 | STD = | 0.0152 | Mean = | 86.281 | STD = | 3.31370 |
| 80 | 0.316 | 0.35 | 0.374 | | 69.54 | 76.97 | 82.21 | |
| | Mean = | 0.347 | STD = | 0.0291 | Mean = | 76.237 | STD = | 6.36317 |

Time(days)= 40 Calibration Curve: "y=0.458 x - 0.0025"

Table 36. 30C Raw Dissolution Data and Statistics (Day40)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.429 | 0.45 | 0.433 | | 94.21 | 98.80 | 95.09 | |
| | Mean = | 0.437 | STD = | 0.01115 | Mean = | 96.033 | STD = | 2.43460 |
| 65 | 0.395 | 0.441 | 0.401 | | 86.79 | 96.83 | 88.10 | |
| | Mean = | 0.412 | STD = | 0.0250 | Mean = | 90.575 | STD = | 5.45997 |
| 75 | 0.421 | 0.429 | 0.426 | | 92.47 | 94.21 | 93.56 | |
| | Mean = | 0.425 | STD = | 0.0040 | Mean = | 93.413 | STD = | 0.88241 |
| 80 | 0.37 | 0.374 | 0.385 | | 81.33 | 82.21 | 84.61 | |
| | Mean = | 0.376 | STD = | 0.0078 | Mean = | 82.715 | STD = | 1.69595 |

Time(days)= 47 Calibration Curve: "y=0.458 x - 0.0025"

Table 37. 30C Raw Dissolution Data and Statistics (Day47)

%Dissolution Determination (30C)

| , ,,,, | S(AU) | | %Dissolution | | | |
|--------|---|--|--------------|-----------------|--------------------|-----------------------|
| #2 | #3 | | #1 | #2 | #3 | |
| 0.432 | 0.448 | | 95.96 | 94.87 | 98.36 | |
| 0.439 | STD = | 0.00819 | Mean = | 96.397 | STD = | 1.78719 |
| 0.447 | 0.448 | | 99.24 | 98.14 | 98.36 | |
| 0.449 | STD = | 0.0026 | Mean = | 98.581 | STD = | 0.57767 |
| 0.435 | 0.44 | | 97.27 | 95.52 | 96.62 | |
| 0.439 | STD = | 0.0040 | Mean = | 96.470 | STD = | 0.88241 |
| 0.444 | 0.444 | | 94.43 | 97.49 | 97.49 | |
| 0.439 | STD = | 0.0081 | Mean = | 96.470 | STD = | 1.76483 |
| 0.412 | 0.409 | 3 | 86.14 | 90.50 | 89.85 | |
| 0.404 | STD = | 0.0108 | Mean = | 88.828 | STD = | 2.35498 |
| 0.373 | 0.394 | | 81.55 | 81.99 | 86.57 | |
| 0.379 | STD = | 0.0127 | Mean = | 83.370 | STD = | 2.78188 |
| | #2 0.432 0.439 0.447 0.449 0.435 0.439 0.444 0.439 0.412 0.404 0.373 | #2 #3 0.432 0.448 0.439 STD = 0.447 0.448 0.449 STD = 0.435 0.44 0.439 STD = 0.444 0.439 STD = 0.412 0.409 0.404 STD = 0.373 0.394 | #2 #3 0.432 | #2 #3 #1 0.432 | #2 #3 #1 #2 0.432 | #2 #3 #1 #2 #3 0.432 |

Time(days)= 54 Calibration Curve: "y=0.458 x - 0.0025"

Table 38. 30C Raw Dissolution Data and Statistics (Day54)

40C Dissolution Values (Raw Data and Statistics)

%Dissolution Determination (40C)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.438 | 0.45 | 0.45 | | 96.18 | 98.80 | 98.80 | |
| | Mean = | 0.446 | STD = | 0.00693 | Mean = | 97.926 | STD = | 1.51271 |
| 33 | 0.432 | 0.45 | 0.434 | | 94.87 | 98.80 | 95.31 | |
| | Mean = | 0.439 | STD = | 0.0099 | Mean = | 96.325 | STD = | 2.15410 |
| 50 | 0.444 | 0.403 | 0.436 | | 97.49 | 88.54 | 95.74 | |
| | Mean = | 0.428 | STD = | 0.0217 | Mean = | 93.923 | STD = | 4.74525 |
| 65 | 0.424 | 0.456 | 0.432 | | 93.12 | 100.11 | 94.87 | |
| | Mean = | 0.437 | STD = | 0.0167 | Mean = | 96.033 | STD = | 3.63610 |
| 75 | 0.445 | 0.447 | 0.42 | | 97.71 | 98.14 | 92.25 | |
| | Mean = | 0.437 | STD = | 0.0150 | Mean = | 96.033 | STD = | 3.28480 |
| 80 | 0.424 | 0.419 | 0.412 | | 93.12 | 92.03 | 90.50 | |
| | Mean = | 0.418 | STD = | 0.0060 | Mean = | 91.885 | STD = | 1.31609 |
| 90 | 0.206 | 0.169 | 0.188 | | 45.52 | 37.45 | 41.59 | |
| | Mean = | 0.188 | STD = | 0.0185 | Mean = | 41.521 | STD = | 4.03979 |

Time(days)= 3 Calibration Curve: "y=0.458 x - 0.0025"

Table 39. 40C Raw Dissolution Data and Statistics (Day3)

%Dissolution Determination (40C)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.388 | 0.429 | 0.44 | | 85.26 | 94.21 | 96.62 | |
| | Mean = | 0.419 | STD = | 0.02740 | Mean = | 92.031 | STD = | 5.98349 |
| 33 | 0.437 | 0.461 | 0.435 | | 95.96 | 101.20 | 95.52 | |
| | Mean = | 0.444 | STD = | 0.0145 | Mean = | 97.562 | STD = | 3.15903 |
| 50 | 0.426 | 0.44 | 0.447 | | 93.56 | 96.62 | 98.14 | |
| | Mean = | 0.438 | STD = | 0.0107 | Mean = | 96.106 | STD = | 2.33465 |
| 65 | 0.438 | 0.45 | 0.45 | | 96.18 | 98.80 | 98.80 | |
| | Mean = | 0.446 | STD = | 0.0069 | Mean = | 97.926 | STD = | 1.51271 |
| 75 | 0.33 | 0.406 | 0.411 | | 72.60 | 89.19 | 90.28 | |
| | Mean = | 0.382 | STD = | 0.0454 | Mean = | 84.025 | STD = | 9.91068 |
| 80 | 0.332 | 0.372 | 0.363 | | 73.03 | 81.77 | 79.80 | |
| | Mean = | 0.356 | STD = | 0.0210 | Mean = | 78.202 | STD = | 4.58169 |

Time(days)= 6 Calibration Curve: "y=0.458 x - 0.0025"

Table 40. 40C Raw Dissolution Data and Statistics (Day6)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|--------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.45 | 0.439 | 0.437 | | 98.80 | 96.40 | 95.96 | |
| | Mean = | 0.442 | STD = | 0.00700 | Mean = | 97.052 | STD = | 1.52838 |
| 33 | 0.44 | 0.444 | 0.439 | | 96.62 | 97.49 | 96.40 | |
| | Mean = | 0.441 | STD = | 0.0026 | Mean = | 96.834 | STD = | 0.57767 |
| 50 | 0.43 | 0.43 | 0.453 | | 94.43 | 94.43 | 99.45 | |
| | Mean = | 0.438 | STD = | 0.0133 | Mean = | 96.106 | STD = | 2.89936 |
| 65 | 0.433 | 0.45 | 0.456 | | 95.09 | 98.80 | 100.11 | |
| | Mean = | 0.446 | STD = | 0.0119 | Mean = | 97.999 | STD = | 2.60488 |
| 75 | 0.377 | 0.425 | 0.416 | | 82.86 | 93.34 | 91.38 | |
| | Mean = | 0.406 | STD = | 0.0255 | Mean = | 89.192 | STD = | 5.57090 |
| 80 | 0.373 | 0.361 | 0.36 | | 81.99 | 79.37 | 79.15 | |
| | Mean = | 0.365 | STD = | 0.0072 | Mean = | 80.167 | STD = | 1.57951 |

Time(days)= 9 Calibration Curve: "y=0.458 x - 0.0025"

Table 41. 40C Raw Dissolution Data and Statistics (Day9)

%Dissolution Determination (40C)

| | | ABS | S(AU) | | Ģ | %Dissolution | | |
|-----|--------|-------|-------|---------|--------|--------------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.435 | 0.431 | 0.447 | | 95.52 | 94.65 | 98.14 | |
| | Mean = | 0.438 | STD = | 0.00833 | Mean = | 96.106 | STD = | 1.81805 |
| 33 | 0.441 | 0.444 | 0.427 | | 96.83 | 97.49 | 93.78 | |
| | Mean = | 0.437 | STD = | 0.0091 | Mean = | 96.033 | STD = | 1.98117 |
| 50 | 0.436 | 0.439 | 0.419 | | 95.74 | 96.40 | 92.03 | |
| | Mean = | 0.431 | STD = | 0.0108 | Mean = | 94.723 | STD = | 2.35498 |
| 65 | 0.439 | 0.448 | 0.437 | | 96.40 | 98.36 | 95.96 | |
| | Mean = | 0.441 | STD = | 0.0059 | Mean = | 96.907 | STD = | 1.27936 |
| 75 | 0.395 | 0.411 | 0.425 | | 86.79 | 90.28 | 93.34 | |
| | Mean = | 0.410 | STD = | 0.0150 | Mean = | 90.138 | STD = | 3.27753 |
| 80 | 0.322 | 0.394 | 0.391 | | 70.85 | 86.57 | 85.92 | |
| | Mean = | 0.369 | STD = | 0.0407 | Mean = | 81.114 | STD = | 8.89319 |

Time(days)= 12 Calibration Curve: "y=0.458 x - 0.0025"

Table 42. 40C Raw Dissolution Data and Statistics (Day12)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|----------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.431 | 0.435 | 0.442 | | 94.65 | 95.52 | 97.05 | |
| | Mean = | 0.436 | STD = | 0.00557 | Mean = | 95.742 | STD = | 1.21567 |
| 65 | 0.434 | 0.436 | 0.446 | | 95.31 | 95.74 | 97.93 | |
| | Mean = | 0.439 | STD = | 0.0064 | Mean = | 96.325 | STD = | 1.40373 |
| 75 | 0.35 | 0.403 | 0.422 | | 76.97 | 88.54 | 92.69 | |
| | Mean = | 0.392 | STD = | 0.0373 | Mean = | 86.063 | STD = | 8.14716 |
| 80 | 0.367 | 0.388 | 0.257 | | 80.68 | 85.26 | 56.66 | |
| | Mean = | 0.337 | STD = | 0.0704 | Mean = | 74.199 | STD = | 15.36214 |

Time(days)= 15 Calibration Curve: "y=0.458 x - 0.0025"

Table 43. 40C Raw Dissolution Data and Statistics (Day15)

%Dissolution Determination (40C)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 12 | 0.445 | 0.445 | 0.432 | | 97.71 | 97.71 | 94.87 | |
| | Mean = | 0.441 | STD = | 0.00751 | Mean = | 96.761 | STD = | 1.63877 |
| 33 | 0.444 | 0.442 | 0.45 | | 97.49 | 97.05 | 98.80 | |
| | Mean = | 0.445 | STD = | 0.0042 | Mean = | 97.780 | STD = | 0.90902 |
| 50 | 0.439 | 0.445 | 0.449 | | 96.40 | 97.71 | 98.58 | |
| | Mean = | 0.444 | STD = | 0.0050 | Mean = | 97.562 | STD = | 1.09896 |
| 65 | 0.435 | 0.442 | 0.424 | | 95.52 | 97.05 | 93.12 | |
| | Mean = | 0.434 | STD = | 0.0091 | Mean = | 95.233 | STD = | 1.98117 |
| 75 | 0.333 | 0.417 | 0.405 | | 73.25 | 91.59 | 88.97 | |
| | Mean = | 0.385 | STD = | 0.0454 | Mean = | 84.607 | STD = | 9.91949 |
| 80 | 0.244 | 0.318 | 0.283 | | 53.82 | 69.98 | 62.34 | |
| | Mean = | 0.282 | STD = | 0.0370 | Mean = | 62.045 | STD = | 8.08254 |

Time(days)= 18 Calibration Curve: "y=0.458 x - 0.0025"

Table 44. 40C Raw Dissolution Data and Statistics (Day18)

| | | ABS | (AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|----------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.406 | 0.449 | 0.453 | | 89.19 | 98.58 | 99.45 | |
| | Mean = | 0.436 | STD = | 0.02606 | Mean = | 95.742 | STD = | 5.68944 |
| 65 | 0.442 | 0.446 | 0.424 | | 97.05 | 97.93 | 93.12 | |
| | Mean = | 0.437 | STD = | 0.0117 | Mean = | 96.033 | STD = | 2.55872 |
| 75 | 0.41 | 0.386 | 0.417 | | 90.07 | 84.83 | 91.59 | |
| | Mean = | 0.404 | STD = | 0.0163 | Mean = | 88.828 | STD = | 3.54985 |
| 80 | 0.257 | 0.349 | 0.281 | | 56.66 | 76.75 | 61.90 | |
| | Mean = | 0.296 | STD = | 0.0477 | Mean = | 65.102 | STD = | 10.41952 |

Time(days)= 21 Calibration Curve: "y=0.458 x - 0.0025"

Table 45. 40C Raw Dissolution Data and Statistics (Day21)

%Dissolution Determination (40C)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.43 | 0.429 | 0.421 | | 94.43 | 94.21 | 92.47 | |
| | Mean = | 0.427 | STD = | 0.00493 | Mean = | 93.705 | STD = | 1.07705 |
| 65 | 0.438 | 0.444 | 0.409 | | 96.18 | 97.49 | 89.85 | |
| | Mean = | 0.430 | STD = | 0.0187 | Mean = | 94.505 | STD = | 4.08672 |
| 75 | 0.402 | 0.407 | 0.347 | | 88.32 | 89.41 | 76.31 | |
| | Mean = | 0.385 | STD = | 0.0333 | Mean = | 84.680 | STD = | 7.26892 |
| 80 | 0.356 | 0.379 | 0.291 | | 78.28 | 83.30 | 64.08 | |
| | Mean = | 0.342 | STD = | 0.0456 | Mean = | 75.218 | STD = | 9.96504 |

Time(days)= 27 Calibration Curve: "y=0.458 x - 0.0025"

Table 46. 40C Raw Dissolution Data and Statistics (Day27)

| | | | ABS | S(AU) | | 9 | | | |
|---|-----|--------|-------|-------|---------|--------|--------|-------|---------|
| | %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| - | 12 | 0.44 | 0.441 | 0.442 | | 96.62 | 96.83 | 97.05 | |
| | | Mean = | 0.441 | STD = | 0.00100 | Mean = | 96.834 | STD = | 0.21834 |
| | 33 | 0.43 | 0.445 | 0.439 | | 94.43 | 97.71 | 96.40 | |
| | | Mean = | 0.438 | STD = | 0.0075 | Mean = | 96.179 | STD = | 1.64844 |
| | 50 | 0.432 | 0.441 | 0.437 | | 94.87 | 96.83 | 95.96 | |
| | | Mean = | 0.437 | STD = | 0.0045 | Mean = | 95.888 | STD = | 0.98455 |
| | 65 | 0.434 | 0.438 | 0.445 | | 95.31 | 96.18 | 97.71 | |
| | | Mean = | 0.439 | STD = | 0.0056 | Mean = | 96.397 | STD = | 1.21567 |
| | 75 | 0.381 | 0.362 | 0.402 | | 83.73 | 79.59 | 88.32 | |
| | | Mean ≃ | 0.382 | STD = | 0.0200 | Mean = | 83.879 | STD = | 4.36863 |
| | 80 | 0.319 | 0.299 | 0.362 | | 70.20 | 65.83 | 79.59 | |
| | | Mean = | 0.327 | STD = | 0.0322 | Mean = | 71.870 | STD = | 7.02885 |
| | | | | | | | | | |

Time(days)= 33 Calibration Curve: "y=0.458 x - 0.0025"

Table 47. 40C Raw Dissolution Data and Statistics (Day33)

%Dissolution Determination (40C)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.425 | 0.432 | 0.422 | . , , | 93.34 | 94.87 | 92.69 | |
| | Mean = | 0.426 | STD = | 0.00513 | Mean = | 93.632 | STD = | 1.12044 |
| 65 | 0.408 | 0.415 | 0.421 | | 89.63 | 91.16 | 92.47 | |
| | Mean = | 0.415 | STD = | 0.0065 | Mean = | 91.084 | STD = | 1.42061 |
| 75 | 0.329 | 0.401 | 0.399 | | 72.38 | 88.10 | 87.66 | |
| | Mean = | 0.376 | STD = | 0.0410 | Mean = | 82.715 | STD = | 8.95285 |
| 80 | 0.3 | 0.351 | 0.354 | | 66.05 | 77.18 | 77.84 | |
| | Mean = | 0.335 | STD = | 0.0303 | Mean = | 73.690 | STD = | 6.62620 |

Time(days)= 40 Calibration Curve: "y=0.458 x - 0.0025"

Table 48. 40C Raw Dissolution Data and Statistics (Day40)

| | | ABS | S(AU) | | %Dissolution | | | |
|-----|--------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.406 | 0.427 | 0.425 | | 89.19 | 93.78 | 93.34 | |
| | Mean = | 0.419 | STD = | 0.01159 | Mean = | 92.103 | STD = | 2.53062 |
| 65 | 0.42 | 0.419 | 0.41 | | 92.25 | 92.03 | 90.07 | |
| | Mean = | 0.416 | STD = | 0.0055 | Mean = | 91.448 | STD = | 1.20253 |
| 75 | 0.384 | 0.373 | 0.346 | | 84.39 | 81.99 | 76.09 | |
| | Mean = | 0.368 | STD = | 0.0196 | Mean = | 80.822 | STD = | 4.26929 |
| 80 | 0.245 | 0.265 | 0.21 | | 54.04 | 58.41 | 46.40 | |
| | Mean = | 0.240 | STD = | 0.0278 | Mean = | 52.948 | STD = | 6.07835 |

Time(days)= 47 Calibration Curve: "y=0.458 x - 0.0025"

Table 49. 40C Raw Dissolution Data and Statistics (Day47)

%Dissolution Determination (40C)

| | ABS(AU) | | | | %Dissolution | | | |
|-----|---------|-------|-------|---------|--------------|--------|-------|---------|
| %RH | #1 | #2 | #3 | | #1 | #2 | #3 | |
| 50 | 0.438 | 0.423 | 0.438 | | 96.18 | 92.90 | 96.18 | |
| | Mean = | 0.433 | STD = | 0.00866 | Mean = | 95.087 | STD = | 1.89089 |
| 65 | 0.426 | 0.431 | 0.429 | | 93.56 | 94.65 | 94.21 | |
| | Mean = | 0.429 | STD = | 0.0025 | Mean = | 94.141 | STD = | 0.54948 |
| 75 | 0.397 | 0.359 | 0.408 | | 87.23 | 78.93 | 89.63 | |
| | Mean = | 0.388 | STD = | 0.0257 | Mean = | 85.262 | STD = | 5.61352 |
| 80 | 0.332 | 0.345 | 0.316 | | 73.03 | 75.87 | 69.54 | |
| | Mean = | 0.331 | STD = | 0.0145 | Mean = | 72.817 | STD = | 3.17158 |

Time(days)= 54 Calibration Curve: "y=0.458 x - 0.0025"

Table 50. 40C Raw Dissolution Data and Statistics (Day54)

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