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SIMULATION OF WINTER ENVIRONMENTAL  
AND PRODUCTION FOR LAYING HENS

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Ph.D. degree in Agricultural  
Engineering

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SIMULATION OF WINTER ENVIRONMENT

AND PRODUCTION FOR LAYING HENS

By

Dhia Ahmed Al-Chalabi

A DISSERTATION

Submitted to  
Michigan State University  
in partial fulfillment of the requirements  
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ABSTRACT

SIMULATION OF WINTER ENVIRONMENT  
AND PRODUCTION FOR LAYING HENS

By

Dhia Ahmed Al-Chalabi

A chicken will eat to meet its energy needs. Temperature directly and significantly influences its energy need and feed intake. A ambient temperature goes beyond the thermal neutral zone (the range at which chicken's performance is at its best), the bird makes adjustments to keep its body temperature normal. Feed consumption and required nutrient decrease as the ambient temperature increases, while energy needs may be met, intake of other essential nutrients may be inadequate. In turn, growth and egg production are decreased. Therefore, it is important that chickens be housed and cared for so as to provide an environment that enables them to maintain their thermal balance and allows them to convert feed to product (eggs and body growth) more efficiently..

This study was undertaken to provide an analytical tool that would help evaluate environmental conditions under different management strategies and climatic

conditions. The tool was a simulation model designed to predict hourly temperature, average daily temperature for inside, and management information, including feed consumption, feed costs, metabolizable energy, egg production, electricity cost, bodyweight, mortality rate using lower ventilation rate to evaluate poultry house. The simulation model was based on psychrometric and biological relationships for laying hens.

The basis of the simulation model and the test facilities for model verification was a commercial-type laying house near East Lansing, Michigan. The laying house has a capacity of 4,100 birds in each room. The system was managed as a small commercial unit at Michigan State University Poultry Science Research and Training Center.

Verification data were collected on five winter days and compared satisfactorily with simulated data. The carbon dioxide ventilation rate control was used as minimum ventilation rate in cool days to replace the moisture control ventilation rate commonly used in poultry houses. Carbon dioxide and ammonia levels were well under control with a ventilation rate of  $0.2 \text{ m}^3/\text{hr}/\text{bird}$ .

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## TABLE OF CONTENTS

	Page
LIST OF TABLES . . . . .	v
LIST OF FIGURES . . . . .	vii
 Chapter	
I. INTRODUCTION . . . . .	1
1.1 Objectives . . . . .	5
1.2 Literature Review . . . . .	5
II. METHODOLOGY . . . . .	20
2.1 Model Development . . . . .	20
2.2 Weather Model . . . . .	25
2.3 Sensible Heat Balance . . . . .	28
2.3.1 Sensible Heat Production of Animals . . . . .	34
2.3.2 Heat From Mechanical Lighting System . . . . .	35
2.3.3 Conductive Heat Loss Through the Building Shell . . . . .	36
2.4 Moisture Balance . . . . .	39
2.4.1 Moisture from Animals . . . . .	41
2.4.2 Moisture from Manure and Spilled Water . . . . .	43
2.5 Carbon Dioxide Balance . . . . .	47
2.6 Bodyweight . . . . .	49
2.7 Feed Consumption . . . . .	50
2.8 Egg Production . . . . .	54
2.9 Cost Calculations . . . . .	58
2.9.1 Fuel Cost . . . . .	58
2.10 Electricity Cost . . . . .	59
2.11 Feed Cost . . . . .	61
2.12 Egg Revenue . . . . .	61
2.13 Outline of Computer Program . . . . .	62
2.14 Model Calibration and Verification . . . . .	94
2.15 Experimental Facilities and Equipment . . . . .	95
2.16 Data Collection and Analysis . . . . .	102

Chapter	Page
III. VERIFICATION . . . . .	108
3.1 Simulation Model Evaluation . . . . .	108
3.2 Results and Discussion . . . . .	109
IV. RESULTS FROM MODEL USE . . . . .	129
V. SUMMARY AND CONCLUSIONS . . . . .	142
5.1 Summary . . . . .	142
5.2 Conclusions . . . . .	143
5.3 Recommendations for Further Research . . . . .	144
APPENDICES . . . . .	144
REFERENCES . . . . .	195



## LIST OF TABLES

Table	Page
2.1 Heat Production from Chickens . . . . .	35
2.2 Latent Heat from Chickens . . . . .	42
2.3 Values of Factor $f_1$ , which Adjusts Feed Intake for Age . . . . .	52
2.4 Values of the Factor $f_2$ , which Adjusts Feed Intake for Wastage using Various Feeding Operations . . . . .	53
2.5 Values of Age Factor A, which Adjusts Egg Output . . . . .	57
3.1 Output Values Simulated and Measured on February 13, 1986 . . . . .	114
3.2 Output Values Simulated and Measured on February 16, 1986 . . . . .	115
3.3 Output Values Simulated and Measured on February 27, 1986 . . . . .	116
3.4 Output Values Simulated and Measured on March 3, 1986 . . . . .	117
3.5 Average Daily Inside Temperatures Measured and Simulated from February 13 to March 3, 1986 . . . . .	118
4.1 Output Values for Decision Analysis for Expected Values (E V) . . . . .	132
4.2 Weather Information Used in Decision Analysis 1889-1980 (83 Years) . . . . .	137
4.3 Output Values from the Model Used in Decision Analysis . . . . .	141
A.1 Carbon Dioxide and Ammonia Concentration Measured on February 11, 1986 . . . . .	148

Table		Page
A.2	Carbon Dioxide and Ammonia Concentration Measured on February 21, 1986 . . . . .	149
A.3	Carbon Dioxide and Ammonia Concentration Measured on February 18, 1986 (All fans off)	150
A.4	Management Factors, Design, and Input Values as Used for Verifying the Model on February 13, 1986 . . . . .	151
A.5	Management Factors, Design, and Input Values as Used for Verifying the Model on February 16, 1986 . . . . .	152
A.6	Management Factors, Design, and Input Values as Used for Verifying the Model on February 27, 1986 . . . . .	153
A.7	Management Factors, Design, and Input Values as Used for Verifying the Model on March 3, 1986 . . . . .	154

## LIST OF FIGURES

Figure	Page
2.1 Shallow and deep cage systems labeled by line from House Seven green room . . . .	21
2.2 General layout of House Seven . . . . .	23
2.3 Main program . . . . .	63
2.4 Subroutine Number 1--Heat Loss Through Building . . . . .	66
2.5 Subroutine Number 2--Body weight of chickens . . . . .	67
2.6 Subroutine Number 3--Sensible heat from chickens . . . . .	68
2.7 Subroutine Number 4--Latent heat from chickens . . . . .	69
2.8 Subroutine Number 5--Water evaporation from manure . . . . .	70
2.9 Subroutine Number 6--Outside hourly ambient temperature and relative humidity . . . .	71
2.10 Subroutine 8: Julian Day (calendar) . . .	72
2.11 Subroutine Number 9--Day and Night . . .	73
2.12 Subroutine Number 10--Gain in Weight . .	74
2.13 Subroutine Number 11--Electricity Cost . .	75
2.14 Subroutine Number 12: Supplemental Heat Needed . . . . .	76
2.15 Subroutine Number 13: Graphics Presen- tation . . . . .	77
2.16 Subroutine Number 14: Estimate of age and feed system factors . . . . .	78

Figure		Page
2.17	Subroutine Number 15: Feed intake and egg production . . . . .	79
2.18	Subroutine Number 16: Ventilation rate . .	80
2.19	Subroutine Number 18: Control inside temperature . . . . .	81
2.20	Subroutine Number 19: Summing the values .	82
2.21	Subroutine Number 21: Design hourly output page . . . . .	83
2.22	Subroutine Number 22: Hourly report . . .	84
2.23	Subroutine Number 23: Input program . . .	85
2.24	Subroutine Number 24: Wall temperature . .	86
2.25	Subroutine Number 25: Daily report . . .	87
2.26	Subroutine Number 26: Costs . . . . .	88
2.27	Typical hourly report output . . . . .	92
2.28	Typical daily report output . . . . .	93
2.29	Floor plan of the commercial-type poultry house used as base for the simulation . .	96
2.30	Psychrometric fan control circuit . . . .	98
2.31	Current (I) sensor circuit . . . . .	99
2.32	Current (I) to CR-21 interface diagram . .	100
2.33	Carbon dioxide sampling locations . . . .	103
2.34	Carbon dioxide sampling instrumentation . .	104
3.1	Simulated vs. measured temperature, and relative humidity February 13, 1986 . . .	110
3.2	Simulated vs. measured temperature, and relative humidity February 16, 1986 . . .	111
3.3	Simulated vs. measured temperature, and relative humidity February 27, 1986 . . .	112

Figure		Page
3.4	Simulated vs. measured temperature, and relative humidity March 3, 1986 . . . .	113
3.5	Carbon dioxied concentration vs. time February 11, 1986 . . . . .	126
3.6	Carbon dioxide concentration vs. time February 21, 1986 . . . . .	127
3.7	Carbon dioxide concentration vs. time February 18, 1986 . . . . .	128
4.1	Decision Analysis Inputs, Revenue Margins and Probabilities . . . . .	133
4.2	Decision Analysis Expected Values . . . .	134

## CHAPTER I

### INTRODUCTION

In the broad sense, environment may be interpreted as all external conditions that might affect animals. The concept of "environment" can be divided into social, physical, chemical, and biological components. The social factors pertain to animal behavior, such as crowding and the social or "pecking" order. The physical factors pertain to all of the surroundings, such as lighting, sound, cages, floor, and other equipment. The thermal factors pertain to air temperature, humidity, and movement.

Chemical factors pertain to all gases, such as oxygen, carbon dioxide, carbon monoxide, ammonia, and other gases, and also to water and feed. Some are necessary for life, while others are toxic and irritating.

In this study there will be emphasis on physical and chemical environment factors.

From a manager's and engineer's point of view, it is necessary to know both the optimal temperatures, and

CO<sub>2</sub> and NH<sub>3</sub> concentrations to be able to provide optimal management. To do so, the manager should know about the poultry environment and its effect on production and feed consumption. Chickens, being warm blooded, have the ability to maintain a rather uniform temperature of their internal organs. However, the mechanism (homeostasis) is efficient only when the ambient temperature is within certain limits. The thermoneutral zone is the range at which chickens' performance is at their best (21-25 C). Inside temperature below this range will increase the feed intake.

A chicken will eat to meet its energy needs. Ambient temperatures directly and significantly influences its energy needs and feed intake. As temperature go beyond the thermal neutral zone, the bird must make more effort to make adjustments to keep its body temperature normal. Feed consumption decreases as the ambient temperature increases. While energy needs may be met, intake of other essential nutrients may be inadequate. In turn, growth and egg production are decreased. As an approximate guide within the range of 15 C to 31 C, when the ambient temperature goes up 1 C, the energy requirement goes down approximately 2 Kcal/kg of body weight and feed consumption goes down about 0.7 g/bird/day (North, 1979). As the temperature goes down,



the reverse is true. Therefore, it is important that chickens be housed and cared for so as to provide an environment that enables them to maintain their thermal balance, and allows them to convert feed to product (eggs and body growth) most efficiently.

Not only is thermal environment important, but there are other factors which effect egg production, such as the chemical environment. Concentration of carbon dioxide and ammonia could also effect egg production, and it may cause a high mortality rate.

Winter ventilation rates commonly used is set to control moisture. Sometimes this ventilation rate is too high to maintain inside temperature in the optimal range. Without using supplemental heat, this means a drop in inside temperature, which also means an increase in feed consumption and may effect egg production (Ariel, 1980).

Using ventilation rates below that commonly used for moisture control could help solve the problem of maintaining inside temperature in the optimal range. Moisture level could increase to the level that water condensation may occur inside the house on the walls or equipment. If this situation occurs for a short duration and infrequently, corrosion of cages and other equipment or any health problems may not be a problem.

The relative humidity may sometimes exceed 85% in this situation, but according to Hellickson et al. (1983), an increase in humidity will decrease production only at higher air temperature. Therefore, in general, humidity changes would not effect the response of nearly mature animals, such as laying hens for environmental temperatures below 24 C.

For pullets just starting production, maintaining the temperature below the thermal neutral zone could mean a delay in egg laying, which could mean a serious cash flow problem.

There was more than one alternative to be tested or used in egg production. For example, to keep the inside temperature in the optimal range, producers may think about adding more insulation to the interior of the building, or using supplemental heat in cool days, or using lower ventilation rates below the commonly used moisture venntilation rate.

Because the trade off between these alternatives, fuel input, increase in feed intake insulating the building, and short-time below the ideal environment are not clear or unknown. Therefore, there is a need to construct a simulation model to evaluate these alternatives.

### 1.1 Objectives

The objectives of this study are:

Objective 1: To develop a simulation model that will predict inside air temperature, relative humidity, ventilation rate and  $\text{CO}_2$  concentration on an hourly and a daily basis within a laying house and the influence of these environmental conditions upon daily feed consumption, energy use, egg production, as well as feed and energy costs and income from egg sales.

Objective 2: To demonstrate the use of this model in providing input for a decision analysis to evaluate various cost control strategies.

### 1.2 Literature Review

Growers and scientists have tried to find optimal conditions to grow chickens for both meat and egg production. The first reported investigation of critical temperature of the chickens appears to be that of Regnault and Reiset (1850).

Mitchell and Haines (1927) studied the critical temperature of chickens in 36 experiments with 12 Rhode Island hens, which involved 137 determinations of carbon dioxide production during fasting and quiescence at

different temperatures. It was found that the average lower critical temperature was 16.7 C. This value applied to winter-feathered birds in an environment of low humidity with an air flow of 3 liters per minute. Some of the individual birds appeared to exhibit distinct differences in their reaction to change in environmental temperature.

Results from Barott and Prince (1941) were quite different from those by Mitchell and Haines (1927). Mitchell and Haines (1972) found a lower critical temperature (the temperature at which the metabolism is at minimum) at 16.7 C. Barott and Prince's analysis gives a very different temperature for the minimum metabolism. They studied the metabolic rate during the experimental period, as measured by both heat and CO<sub>2</sub> elimination and oxygen consumption over the temperature range of 10 to 35 C on the metabolic rate during each 24 hour period. It showed that the typical diurnal rhythm in the metabolism of the hen had a maximum value in the morning (8 a.m.) and minimum value in the evening (8 p.m.). The minimum metabolism of the hen occurred at 25.6 C. The maximum metabolism occurred at 16.1 C. The rate at 16.1 C is approximately 8% higher than at 25.6 C.

Helback and Casterline (1963) studied the effect of high CO<sub>2</sub> atmosphere on the laying hens. Four Hy-Line

laying hens were kept in an enclosed 6.5 ft<sup>3</sup> plastic-covered chamber to which a 5% CO<sub>2</sub> and 95% gas mixture was metered at 4 liters per minute for a 19-hour period. The temperature was 21 C ± 2 C. Excess moisture was removed with sulfuric acid. The chamber resembled a closed system. Results indicated that during exposure to high CO<sub>2</sub>, the shell thickness rose above pretreatment levels. However, there was no drop in egg size following the exposure.

Anderson et al. (1964) found 5,000 to 6,000 ppm of CO<sub>2</sub> in a commercial poultry house. In studies reported by Longhouse (1967), CO<sub>2</sub> was as high as 10,000 ppm. Hiestand et al. (1941) reported that chickens (no age and breed given) would withstand up to 6% (60,000 ppm) CO<sub>2</sub> concentration with slight inhibition of breathing, while at a 10% level, there was increased amplitude, but not an increased rate of breathing.

Kotula et al. (1957) reported that concentrations, as high as 20%, failed to immobilize birds in 75 seconds in a slaughtering study. Longhouse et al. (1968) published information for growing and studying broilers. Some experimental data on levels of NH<sub>3</sub>, and CO gas levels were:

CO <sub>2</sub>	860	to	10,000 ppm
CO	0	to	62 ppm
NH <sub>3</sub>	0	to	50 ppm

They stated that exposure to variable concentrations of CO, in the presence of CO<sub>2</sub> may have a serious physiological effect on growing broilers in winter.

Charles and Payne (1965) reported the effects of ammonia on the performance of White Leghorn hens housed in various environments of defined temperature and humidity. At 18 C and 67% relative humidity, the use of atmospheres containing 105 ppm of ammonia by volume significantly reduced egg production after a 10-week exposure. No effects in egg quality were observed. However, voluntary feed intake was reduced in ammoniated atmospheres and live weight gain was lower. No recovery in production occurred when the treated groups were maintained for a further 12 weeks in an atmosphere free of ammonia.

When White Leghorn hens were housed at an environmental temperature of 28 C and various ammonia concentrations, a decrease in body weight occurred. The decrease in live weight was greatest at ammonia concentration of 102 ppm, and was significant after only one week of exposure to ammonia. Feed intake of controls was approximately 25% lower at 28 C than at 18 C. The

presence of 100 ppm of ammonia further reduced feed intake by more than 10%. In one experiment at 28 C, egg production was significantly reduced after 7 weeks' exposure to ammonia.

Deaton et al. (1981) studied the effect of temperature cycles on egg shell quality and layer performance. Laying hens exposed to 24 hour linear temperature cycle ranging from 16.7 C to 35 C had significantly poorer egg shell breaking strength, and significantly greater body weight change than hens exposed to temperature cycles of 21 to 35 C and 15.6 to 35 C. No significant difference in performance existed in hens exposed to 24 hour linear temperature cycles of 21 to 35 C and 15.6 to 35 C. Egg shell quality deteriorated when the laying hen was exposed to high environmental temperatures.

Bray and Gesell (1961) studied the environmental temperature as a factor affecting performance of pullets fed diets suboptimal (11.5, 12.0, and 14.0% protein levels. White Leghorn pullets 29 to 31 weeks were used. Diets contained a mixture of corn and soybean oil meal, in which corn provided 45% of the protein. Chambers were maintained at 5.6 C and 24.4 C in one experiment and at 24.4 C and 30 C in a second experiment for a 8-week period.



Temperature extremes of 5.6 C and 30 C altered feed intake, but did not appear to affect rate of lay, with the protein provided. Intake remained above a minimum throughout the period. The rate of decline in egg production of pullets fed a given suboptimal protein diet was greater at higher temperatures. An inverse relationship existed between temperature and egg production at suboptimal protein levels.

Arad et al. (1981) studied the effect for 7 months of daily exposures to increasing ambient temperature on egg production for different breeds, including the White Leghorn.

Egg weight of Leghorns was stable up to 40 C, but decreased at higher temperatures. The laying rate decreased consistently from 35 C to 44 C. They concluded that the White Leghorn breed is highly tolerant of heat compared with other conventional breeds, shown by its long survival time, its moderate increase in metabolic rate, body temperature, and its accelerated evaporation.

DeShazer et al. (1970) reported on the effect of acclimation on partitioning of heat loss by the laying hen (White Leghorn). Hens acclimated to a 35 C environment reduced their total metabolic rate which included decreasing body weight by 15% and decreasing egg production by approximately 30%.

Weiss et al. (1963) also observed that the body weight of hens acclimated to a 32.2 C environment was significantly lower than the controls at 22.8 C. They also showed that the shell conductance of the hens acclimated to 23.9 C temperature environment decrease significantly when exposed to a 35 C environment as compared to a 25 C and 30.6 C.

Cowan and Michie (1980) studied the effect of increasing the environmental temperature late in lay and the performance of the hens. Their hens, ranging in age from 333 to 500 days, were fed on a conventional diet (161 g crude protein). Those kept at 27 C had a significantly lower egg output than at 21 C. Birds fed on the higher protein diet (192 g cp) kept at 27 C had a significantly lower egg output than those kept at 21 C. They also clearly noticed that for birds fed on a conventional diet (161 g cp) and an increased environmental temperature (27 C) at an age of 333 days still resulted in a depressed rate of egg output compared with hens maintained at 21 C.

Vohra et al. (1979) studied egg production, feed consumption, and maintenance energy requirements of Leghorn hens as influenced by energy content at 15.6 C and 26.7 C. They reported that the hens reduced their feed intake significantly at both ambient temperatures as

the energy content of the diet increased from 1,980 to 2,830 Kcal/kg. Also the intake of low and high diets was significantly less at 26.7 C than at 15.6 C. The decrease in feed consumption was about 13% and 15.3% at ambient temperature of 15.6 and 26.7 C as the median of the diets increased from 1,980 to 2,830 Kcal/kg, respectively. Within this temperature range the feed intake decreased by 1.2% and 1.41% per 1 C rise in ambient temperature for the low and high diets, respectively.

Neither egg production nor shell thickness was influenced by the treatments, but egg weight was significantly depressed at 26.7 C as compared to those at 15.6 C.

The maintenance energy requirements were significantly lower at the two ambient temperatures when hens were fed the low diet as compared with the high diet. The energetic efficiency was increased for the conversion of maintenance energy intake to egg energy either by increasing the ambient temperature or by lowering the dietary maintenance energy.

Valencia et al. (1980) studied the energy utilization in laying hens and the effect of dietary protein level at 21 C and 32 C. They investigated White Leghorn housed at either 21 or 32 C and the effects of

dietary protein level on energy utilization. Protein levels 12, 14, 16, 18 and 20% were used in this study for 21 days. They reported that maintenance metabolizable energy (was estimated at 134 and 121 kcal/kg physiological body weight ( $BW^{0.75}$ ) was 21% higher at the lower temperature (89 vs. 70 kcal). Estimates of energetic efficiencies at 21 C varied from 60.9% for the 12% protein diet to 72.4% for the 18% protein diets.

Egg weights were significantly higher at lower environmental temperature, and at each temperature they were increased with feeding the higher protein diets. The average feed efficiency (g of egg/ g of feed) was significantly higher at higher environmental temperature (.46 vs. .53).

Henken et al. (1982) studied the effect of environmental temperature on some aspects of energy and protein metabolism of 3 to 6 week old pullets, at low temperatures. Feed conversion (g feed/g growth) was higher at lower temperature ( $p < .25$ ) and 10.5% (at 10 to 20 C) compared to intake at 25 C. Growth rate and protein gains were not significantly affected by low temperatures.

Higher temperatures reduced ( $p < .05$ ) feed intake 15.9% at 35 C and 14.9% at 30 to 40 C and growth rate 12.3% at 35 C and 12.5% at 30 to 40 C compared to 25 C.

Protein gains and feed conversion were not significantly affected by high temperatures.

Prince et al. (1965) studied the response of chickens to temperature and relative humidity environments. White Plymouth Rock male chicks 4 to 8 weeks old were subjected to environment temperatures of 12 C and 23.8 C and supplied with relative humidity 52,70 and 90%. They found that the feed consumption was significantly higher in the 12.6 C than in the 23.8 C.

Difference in feed consumption, due to relative humidity, were not significant. The difference in weight gains due to temperature was significant. Weight gain in the 12.6 C was 53 grams/bird greater than in the 23.8 C. No differences in weight gain were observed which would be attributable to relative humidity. The feed efficiency in 12.6 C was significantly lower than in 23.8 C.

Hellickson et al. (1983) in their book Ventilation of Agricultural Structures summarized the literature about the effects of humidity on heat loss for domestic animals. White Leghorn chickens at high air temperature of 30 C and 35 C an increased relative humidity from approximately 40 to 90% resulted in an overall decline of 77% in the respiratory evaporative heat loss. This lowered the ability of the hen to

dissipate its total heat dissipation by 15% at environmental temperature 35 C and by 7% in a 30 C environment. At 20 C an increase in relative humidity from 55 to 88% caused a 3% increase in the total heat production and a 25% decrease in the respiratory evaporative heat loss.

Increases in humidity decreased production only at high air temperature. In general, humidity changes did not affect the responses of growing laying animals for environmental temperatures below 24 C.

North (1979) reported that the most important factor which had the greatest affect on layer feed intake was the ambient temperature. At extremes, daily feed consumption varied up to 50%. Layers ate more feed as ambient temperature decreased, and ate less as it increased. Variations in feed intake were not uniform. With 11.7 kg of feed consumed per 100 layers at 5 C as the base, they ate 46% less at 38 C. If 6.312 kg/100 layers per day at 38 C is used as the base, the flock ate 85.7% more at 5 C.

He concluded that birds adjust their energy intake to compensated for fluctuations in ambient temperature. At higher temperatures, the birds still consumed enough feed to meet their energy needs, but the

diet becomes inadequate because of inadequate intake of other dietary constituents.

Greninger et al. (1982) developed a simulation model for poultry energetics for developing environmental recommendations. The model was based on the general relationship that the total metabolizable energy intake required by the hen is equal to the summation of maintenance energy, used in production of an egg, and the energy used for body weight gain. The actual metabolizable energy intake was assumed to be equal to the required feed intake. The necessary amount of protein in the diet was assumed to be provided for required maintenance of the hen, egg content, and egg development.

Mueller (1961; 1967) developed a method to estimate egg weight and production for an energy laying cycle.

Greninger et al. concluded that based on feed efficiency for egg output, the environmental temperature in layer house should be between 21 C to 25 C. However, economic parameters dictated that the temperature should be controlled at higher or lower temperatures, depending on protein cost, energy cost, fuel cost, insulation cost, and marketing situations.



Phillips and Esmay (1973) applied the systems approach to the analysis of summer environment for laying hens and developed a simulation model to be used in studying parameters affecting the environment. A mathematical model was developed to predict system temperature and humidity as a function of heat and mass transfer rates across system boundaries at discreet points of time at half-hour intervals throughout the day.

They studied six different constant ventilation rates in 1 cfm increments ranging from 2.5 to 7.5 cfm per 4.5 lb bird. Housing density was .7 ft<sup>2</sup> per bird and artificial day was from 6 a.m. to 8 p.m. The conclusion was that higher ventilation rates were not effective in reducing system temperatures during night hours when outside temperatures were lower. Density effects were most noticeable during the 11 a.m. to 6 p.m. period when outside temperatures were in the maximal area of the diurnal cycle. Summer ventilation rates in excess of 1.0 cfm per pound of body weight did not significantly reduce maximum system temperature.

Dixon and Esmay (1979) studied the feasibility of maximizing poultry excreta dehydration with ventilation air using a simulation model. The study was undertaken to provide an analytical tool that would help evaluate the feasibility of drying poultry excreta. The

simulation model was designed to estimate the drying potential of excreta using mechanical ventilation systems commonly provided for commercial egg production houses. The simulation model was based on psychrometric calculations in combination with constant rate drying theory.

The critical factors for maximizing in-house manure drying were the drying surface area and the manure drying rate. The larger the surface are, the greater the drying. The variables which influenced the manure drying rate the most were the inside wet-bulb depression and the ventilations rate. Maximum drying was possible with a high inside dry-bulb temperature, a low outside dewpoint temperature, and maximum air exchange.

Timmons and Gates (1985) studied a stochastic method for synthetic weather generation which is combined with a layer production model to illustrate the utility of risk analysis applied to animal housing. Daily mean temperatures are generated based on previous day's temperatures, the expected mean daily temperatures, and random fluctuation.

Based on simulations of layer housing and egg production using either a deterministic simulation or stochastic simulation. They conclude that large differences occur in predictions of egg production

parameters depending on the type of weather simulation model used. More reasonable predictions of egg production parameters are possible using a stochastic approach.

The use of stochastic evaluation indicates that evaporative cooling can be justified in a cool climate based on increased returns of \$.43 and \$.32 per hen per year for flock placement dates of January 1 and July 1, respectively. A minimum of 50 years of simulated production data should be used to predict expected production results

There were large differences between the two methods in predicted savings, caused by the small, but highly significant periods, when the stochastically generated outside temperature exceeded the deterministic outside temperature. Differences in predicted production occur when the higher outside stochastic temperature, caused house temperatures to significantly affect production.

## CHAPTER II

### METHODOLOGY

#### 2.1 Model Development

This study was conducted at Michigan State University Poultry Research and Teaching Farm in a commercial-type egg research facility.

The system in this study was the environment produced within a 4,100 hen operating unit. The operating unit was the house enclosing the laying hens and the equipment used to manage the operation.

The house contained two identical laying rooms. Each room was 5.5m x 31m x 2.37m. Each room contained one row of deep pyramid reverse cages 30.5 cm x 40.6 cm. These cage rows were a modified stair-step, four-tier design that contained eight lines of cages per row and 60 cages per line. Figure 2.1 shows the general cage designs for the shallow and deep cage system. Performance of different colony sizes and different bird densities was one of the other studies in the room studied. Five and six bird colonies were placed in the deep cages in alternating lines, and

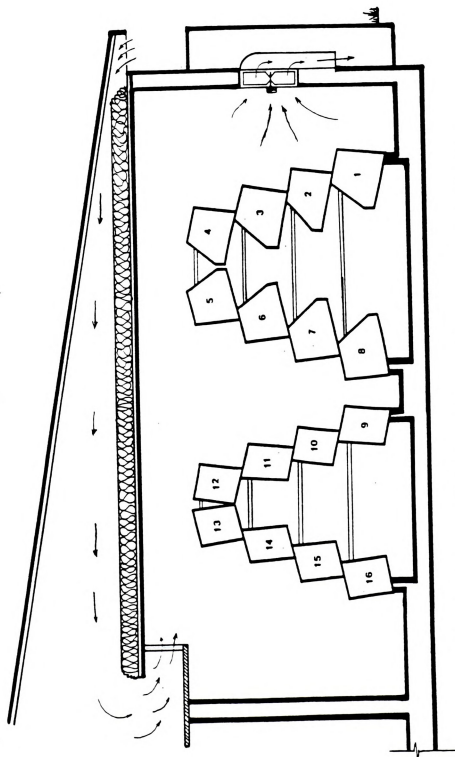


Figure 2.1. Shallow and deep cage systems labeled by line from House Seven green room.

three- and four-bird colonies were placed in the reverse cages in alternating lines. The end result was a total of two rows of deep cages with five or six birds per cage and two rows of reverse cages with three or four birds per cage and a total of 32 lines.

Figure 2.2 presents a general layout of the laying chambers. Ventilation in each room was provided by two 45 cm variable speed fans ( $4588 \text{ m}^3/\text{hr}$ ), four 60 cm ( $4950 \text{ m}^3/\text{hr}$ ), and one 90 cm ( $8411 \text{ m}^3/\text{hr}$ ), fan. The 45 cm variable speed fans operated continuously and provided a total minimum air exchange of 840 cubic meters per hour ( $.2 \text{ m}^3/\text{hr}/\text{bird}$ ). The variable speed fans were fixed on that rate. When the room temperature rose above  $26^\circ\text{C}$ , one 60 cm fan was turned on to attempt to maintain target temperatures. The in-house target temperature range was  $22$  to  $26^\circ\text{C}$ . This was regulated by thermostat controlling ventilation fans. The 90 cm fan operated only during hot weather conditions. Air inlets located near the ceiling along the north wall of the south (White) room were adjusted by an automatic system sensing static pressure. No supplemental heat was used.

Lights were provided by 33 (25 watt) white, incandescent bulbs. Intensity was adjusted to .75 foot candles as measured from the bottom tier of cages. Feed was delivered three time per day to the birds by

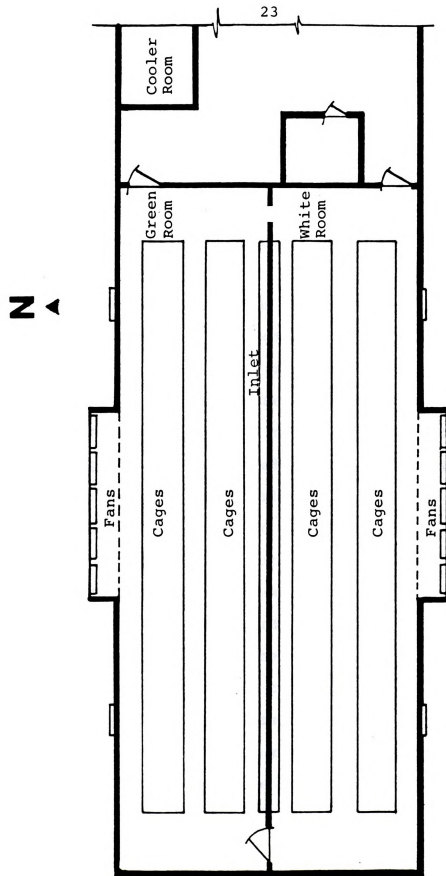


Figure 2.2 General layout of House Seven.

four automatic feed carts. One cart serviced one row of cages. Each cart was filled twice a day from separate bulk storage tank. Load cells placed under the carts at "home position" made it possible to weigh the carts before and after each feeding. Spouts from the feed cart led into each feed trough and could be adjusted separately.

Feed consumption was calculated every week. The bird inventory at the beginning of the week and at the end of the week, were used to get the average number of birds in the house during the week. The average number of birds was divided by the weight of feed disappearance (delivered) to the chickens. No feed loss adjustments were made.

Carts were controlled with time clocks and ran 1/2 hour after lights were turned on in the morning, in the early afternoon, and three hours before the lights were turned off in the evening. Water was provided from water cups placed on the side of every other cage so that one cup serviced two cages.

Average egg weight was calculated weekly. A 30 eggs flat is collected from randomly chosen cages for each line. The 30 egg flat was weighted, the empty flat also weighted in the same time. The difference in weight was the weight of 30 eggs, then this number was



divided by 30 to get the average egg weight of the line.

Manure droppings were contained in shallow pits under the cage rows. The pits were scrapped twice a day into a cross gutter at one end of the laying rooms and moved to a conventional manure spreader outside.

Birds (Hy-line variety W-36 pullets) were housed in the facility at 18 weeks of age. All the birds were from one source and had been raised according to commercial practices.

## 2.2 Weather Model

The objectives of the weather model were to give reasonable estimates of average daily and hourly outside temperature and dewpoint temperature. These were used as inputs to the laying house environmental model.

Data from both the United States Department of Commerce/National Oceanic and Atmospheric Administration/National and the Weather Service (USDC/NOHA/NWS), station for Lansing, Michigan, were used to prepare values needed for the model. Daily averages, maximum and minimum temperatures from 1941 to 1970 were used to calculate yearly average ambient temperature and yearly ambient temperature amplitude.

Diurnal dry bulb temperature fluctuation can be closely approximated by a sinusoidal function with amplitude varying equally about the daily mean temperature. During winter in Michigan, the minimum daily temperature can be expected at approximately 7 a.m. and the maximum about 3 p.m. Hill (1983) used this procedure in his paper to estimate average daily and average hourly temperatures, and found this to be a good estimation. For the prevailing conditions in this study, the following equation was used to generate the daily average ambient air temperature for any day of the year based on Hill (1983).

$$DTEMP = TA + TYRAMP * \sin [.0172142 (Day-DAV)] \quad (2.1)$$

where:

DTEMP = average daily ambient air temperature C

TA = yearly average air temperature = 8.6 C

TYRAMP = yearly ambient amplitude = -3.9 C

Day = day of year (January 1 = 1)

DAV = day of year which first reaches the annual average temperature = 107

The hourly ambient air temperature for a given day of the year is calculated as follows (Hill, 1983):

$$\begin{aligned} \text{TEMPC} = & \text{DTEMP} + \text{TDYAMP} [\sin(.2617994 (\text{HOUR} + 13))] \\ & + \sin (.2617924 (\text{Hour} + 13)2)/3] \quad (2.2) \end{aligned}$$

where:

TEMPC = hourly air temperature C  
 TDYAMP = daily ambient temperature amplitude  
 (winter only) = -13.5 C  
 HOUR = hour of day

Data from USDA/NOHA/NWS for Lansing from 1965-1984 provided the base information for the daily needed dewpoint temperature. The hourly dewpoint temperatures for each month--January, February, March, November, and December--were used to fit a regression equation for each month. Several candidate equations were evaluated. These included linear exponential, logarithmic, and power equations. The linear equations were used because the correlation coefficients were about the same as the more complex equations. These equations were used to estimate hourly dewpoint temperatures to calculate all needed psychometric properties for the incoming ventilating air. The hourly ambient dewpoint temperature for a given day during the winter were:

$$\text{DEWPT} = -1.3258 + .803381 * \text{TEMPC}$$

$$\text{For January } R = 0.93 \quad (2.3)$$

$$\text{DEWPT} = -2.8242 + .834888 * \text{TEMPC}$$

$$\text{For February } R = 0.89 \quad (2.4)$$

$$\text{DEWPT} = 4.9466 + .605923 * \text{TEMPC}$$

$$\text{For March } R = 0.76 \quad (2.5)$$

$$\text{DEWPT} = 11.6864 + .533961 * \text{TEMPC}$$

$$\text{For November } R = 0.75 \quad (2.6)$$

$$\text{DEWPT} = -3.6047 + .942597 * \text{TEMPC}$$

$$\text{For December } R = 0.92 \quad (2.7)$$

where:

DEWPT = hourly dewpoint temperature F.

Hourly relative humidity for outside air were calculated by using the hourly dry bulb temperature and dewpoint temperature for each day, by use of psychrometric equations, ASAE Standards (1984).

### 2.3 Sensible Heat Balance

The basic equations are obtained by a heat and moisture balance during short time periods considering the building as an open system. Hinkle and Good (1970) suggested that the heat balance can be represented as

Change in heat = heat entering system - heat leaving  
system

$$\Delta q = q_{in} - q_{out} \quad (2.8)$$

Several simplifying assumptions were made to develop the model. No heat storage in the building. Complete mixing of the air within the building and constant heat and moisture production of chickens during the time interval.

The systems defined by this research are the environment surrounding the layers and enclosed by interior surfaces of the animal shelter. A sensible heat balance equation can be written as

$$q = q_s + q_e + q_{\text{sup}} \pm q_w - q_b - q_{\text{sv}} - q_m \quad (2.9)$$

where:

$q_s$  = sensible heat produced by the animals kJ/hr

$q_e$  = sensible heat produced by equipment such as lights, motors kJ/hr

$q_{\text{sup}}$  = sensible heat from supplemental sources kJ/hr

$q_w$  = heat needed to change water at room temperature to water vapor at the same temperature, heat also released when water condenses kJ/hr

$q_b$  = conductive heat loss through the building, walls, floor, and ceiling kJ/hr

$q_{\text{sv}}$  = sensible heat leaving with the dry exhausted ventilation air kJ/hr

$q_m$  = sensible heat leaving with the moisture in the ventilated air kJ/hr

Sensible heat lost with the dry portion of the ventilation air,  $q_{\text{sv}}$ , can be expressed as

$$q_{\text{sv}} = q_{v_i} - q_{v_o} = C_p M (t_i - t_o) \quad (2.10)$$

where:

$C_p$  = specific heat of dry air (1.0035) kJ/kg. C

$M$  = ventilation mass air flow kg/hr

$t_i$  = inside air temperature C

$t_o$  = outside air temperature C

The equation for ventilation mass air flow rate (M) can be written as

$$M = \frac{Q_s}{V_s} \quad (2.11)$$

where:

$Q_s$  = ventilation volumetric flow rate  $m^3/hr$

$V_s$  = specific volume of inside air  $m^3/kg$

Ventilation rate needed to remove the available sensible heat and thus maintain the inside temperature at  $t_i$  calculated as

$$Q_s = \frac{V_s}{C_p (t_i - t_o)} * (q_s + q_e + Q_{sup} \pm q_w - q_b) \quad (2.12)$$

Specific volume of inside air  $V_s$  is given by ASAE 1984 standard as

$$V_s = \frac{R * T}{P_{at} - P_v} \quad (2.13)$$

where:

$T$  = absolute temperature of the dry air K

$R$  = gas constant of dry air = .287 kJ/kg.K

$P_{at}$  = atmospheric pressure = 101.325 kPa

$P_v$  = vapor pressure kPa

Vapor pressure  $P_v$  is also given by ASAE 1984 standards as

$$P_v = \frac{\phi * P_s}{100} \quad (2.14)$$

where:

$\phi$  = relative humidity %

$P_s$  = saturated vapor pressure kPa

Saturated vapor pressure is calculated by two equations for temperatures ranged -18 to -0 C as

$$\ln P_s = 31.9602 - \frac{627.3605}{T} - 4.06057 * \ln(T) \quad (2.15)$$

and for temperatures range 0 to 110 C as

$$\ln \left( \frac{P_s}{R} \right) = \frac{A + BT + CT^2 + DT^3 + ET^4}{FT - GT^2} \quad (2.16)$$

where:

$$A = -27405.526$$

$$B = 97.5413$$

$$C = -.146244$$

$$D = .12558 \times 10^{-3}$$

$$E = -.48502 \times 10^{-7}$$

$$F = 4.34903$$

$$G = 0.39381 \times 10^{-2}$$

$$R = 22105649.25$$



The enthalpy of water vapor as a function of temperature is given by ASHRAE (1967) as:

$$h = 2501 + 1.84T \quad \text{kJ/kg H}_2\text{O} \quad (2.17)$$

Then change in enthalpy due to change in both the temperature and moisture content of the incoming ( $h_{im}$ ) and outgoing ( $h_{om}$ ) water vapor would be

$$h_{im} = (W_i (2501 + 1.84 t_i)) \quad (2.18)$$

and

$$h_{om} = (W_o (2501 + 1.84 t_o)) \quad (2.19)$$

where:

W = humidity ratio in kg H<sub>2</sub>O/kg d.a.

i = incoming

o = outgoing

Then humidity ratio for outside or inside air is calculated based on ASAE 1984 standards

$$W = \frac{.619 * P_v}{P_{at} - P_v} \quad (2.20)$$

Therefore, the sensible heat  $q_m$  lost with the moisture in the ventilation air is

$$q_m = M[2501 (W_i - W_o) + 1.84 (W_i t_i - W_o t_o)] \quad (2.21)$$

where:

$q_m$  = change in heat in kJ/hr

$W_o$  = humidity ratio of outside air kg  $H_2O$ /kg d.a

$W_i$  = humidity ratio of inside air kg  $H_2O$ /kg d.a

### 2.3.1 Sensible Heat Production of Animals

Poultry produce various quantities of metabolic heat, depending on type of bird, body weight, amount of feed consumed, and environmental conditions. Data for sensible heat production published by Esmay and Dixon (1986) are used to predict the sensible heat for the model (Table 2.1). A linear regression equation has been fitted to the data. The equations are:

$$q_s = 16.4533 - .3108 * t_i \quad \text{in darkness } R = 0.97 \quad (2.22)$$

and

$$q_s = 23.4309 * t_i^{-.1558} \quad \text{in light } R = 0.96 \quad (2.23)$$

Table 2.1 Heat Production from Chickens

In Darkness		In Light	
Temp C	Sensible Heat kJ/hr. kg	Temp C	Sensible Heat kJ/hr. kg
-33.0	16.49	-33.3	25.52
0.56	16.02	1.67	19.48
8.33	44.40	8.33	17.17
12.22	12.78	12.22	15.30
17.78	12.31	17.22	15.30
27.78	8.82	22.22	15.08
34.44	3.96	27.78	13.68

### 2.3.2 Heat From Mechanical Lighting System

Use of electricity for artificial lighting and to power materials handling equipment provides a direct source of sensible heat to the system. The amount of electrical energy added during the hours of artificial daylight was estimated at  $38.7 \text{ kJ/hr. m}^2$  ( $1 \text{ watt/ft}^2$ ) by Phillips (1970). Then the amount of heat added is

$$q_e = A * 38.7 \quad (2.24)$$

where:

A = area of the floor  $m^2$

38.7 = heat produced by the lights  $\text{kJ/hr.m}^2$

Heat from the electrical motors, such as fans motors and scaper motor was assumed to be insignificant.

### 2.3.3 Conductive Heat Loss Through the Building Shell

The fundamental equation for steady-state heat conduction through the solid building boundaries is

$$q_b = - kA (dt/dx) \quad (2.25)$$

where:

$q_b$  = heat flow in one direction in Watts or J/sec

k = thermal conductivity in  $\text{W.m/m}^2\text{K}$

A = cross-sectional area in  $m^2$

$dt/dx$  = temperature gradient in  $\text{K/m}$

Overall, heat flow through ceilings, walls, and windows may be calculated for each component

$$q = U A (t_i - t_o) \quad (2.26)$$

where:

$U$  = overall coefficient of heat transfer  
 $W/m^2.K$

$A$  = area normal to direction of heat flow  $m^2$

$t_i, t_o$  = air temperature inside and outside  $C$

The overall coefficient of heat transfer may be calculated as follows:

$$U = \left[ \frac{1}{f_i} + \sum_{n=1}^x \frac{L_x}{k_x} + \frac{1}{f_o} \right]^{-1} \quad (2.27)$$

where:

$f_i, f_o$  = film or surface conductance inside and outside  
 $W/m^2.K$

$L_x$  = length of the path of heat flow  $m$

$k_x$  = coefficient of conduction of specific material  
 $W/m.K$

$n$  = number of materials needing a designation

$x$  = a specific material designation

Heat loss through the floor is based on an equation suggested by ASHRAE (ASHRAE, 1981 Handbook of Fundamentals).

$$q_{F_1} = (A_{F_1} - A_m) * U_{F_1} \quad (2.28)$$

where:

$A_{F_1}$  = floor area  $m^2$

$U_{F_1}$  = average value of heat transfer =  $3.155 \text{ W/m}^2$

$A_m$  = area covered with manure  $m^2$

$q$  = heat loss through the floor in W

Then the total heat loss through the building would be:

$$q_b = q_{w_1} + q_{c_1} + q_{F_1} + q_{op} \quad (2.29)$$

where:

$q_b$  = heat loss through the building shell W

$q_{w_1}$  = heat loss through the walls W

$q_{c_1}$  = heat loss through the ceiling W

$q_{F_1}$  = heat loss through the floor W

$q_{op}$  = heat loss through windows or fans not operating W

Substituting the components of heat balance equation and rearranging

$$q = q_s + q_e + q_{sup} + q_w - q_b - q_{sv} - q_m \quad (2.30)$$

Then the difference in rate of heat flow is

$$q = M(1.0035 (t_o - t_i) + 2501 (w_o - w_i) + 1.84 \\ * (w_o t_o - w_i t_i)) + 2431 * W_m + q_s + q_e - q_b \quad (2.31)$$

To calculate the temperature at a point in time, therefore, the change in heat content  $q$  over a small time increment is desired. This can be obtained by multiplying the heat change equation by time increment  $T$  as follows:

$$q = h / T$$

$$\Delta h = \Delta T [M(1.0035(t_o - t_i) + 2501(w_o - w_i) + 1.84 * \\ (w_o t_o - w_i t_i)) + 2431 * W_m + q_s + q_e - q_b] \quad (2.32)$$

## 2.4 Moisture Balance

The moisture balance for the system is as follows:

$$W_{ot} + W_c + W_m - W_v = 0 \quad (2.33)$$

where:

$W_{ot}$  = moisture in incoming ventilating air kg/hr

$W_c$  = moisture from animal respiration kg/hr

$W_m$  = moisture evaporated from manure and spilled water kg/hr

$W_v$  = moisture in outgoing ventilating air kg/hr

The moisture in incoming ventilating air is calculated by

$$W_{ot} = M * W_o \quad (2.34)$$

where:

$M$  = ventilation flow air mass kg d.a/hr

$W_o$  = humidity ratio of outside air kg  $H_2O$ /kg.d.a

The moisture in outgoing ventilating air is calculated by the following equation

$$W_v = M * W_i \quad (2.35)$$

where:

$W_i$  = humidity ratio of inside air kg  $H_2O$ /kg.d.a.



Air mass in the building,  $Ma$ , is calculated by the relationship

$$Ma = \frac{V_b}{V_s} \quad (2.36)$$

where:

$V_b$  = volume of the floor  $m^3$

$V_s$  = specific volume of inside air  $m^3/kg$

The moisture in the incoming ventilating air was determined from estimated data from the weather model. Dry bulb and dewpoint temperature was generated for a specific time of day.

#### 2.4.1 Moisture from Animals

The latent heat in respired air from laying hens,  $q_1$ , was determined from data presented by Esmay (1986) (Table 2.2), were used to fit a linear regression equation for latent heat production during dark hours and light. The equations were:

$$q_1 = 4.4649 + .2122 * t_i \text{ for light kJ/hr.kg} \\ R = 0.98 \quad (2.37)$$

$$q_1 = 3.8085 + .1685 * t_i \text{ for darkness kJ/hr. kg} \\ R = 0.92 \quad (2.38)$$

Table 2.2. Latent Heat from Chickens

In Darkness		In Light	
Temperature C	kJ/kg. hr	Temperature C	kJ/kg.hr
-3.33	3.71	-3.33	3.71
0.56	4.86	1.67	5.33
8.33	4.39	8.33	5.58
12.22	5.80	12.22	7.67
17.78	5.33	17.22	8.14
27.78	8.14	27.78	9.97
34.44	10.91	33.33	12.31

Then the moisture production  $W_c$  from respiration of the chickens was calculated from:

$$W_c = \frac{q_l}{h_{fg}} \quad (2.39)$$

where:

$q_l$  = latent heat produced by the chickens kJ/hr

$h_{fg}$  = latent heat of vaporation of water at saturation  
kJ/kg

Latent heat of vaporization of water at saturation based on ASAE 1984 standards is:

$$h_{fg} = 2502.535259 - 2.38576 (T - 273.16) \quad (2.40)$$

where:

T = temperature in Kelvin

#### 2.4.2 Moisture from Manure and Spilled Water

The moisture evaporated from the manure  $W_m$ , and the drinking water that spilled into the manure, and evaporated with manure water was calculated from the free water evaporation from the surfaces developed by Kadlec (1969) as follows

$$W_m = KA_m (P_m - P_p) \quad (2.41)$$

where:

$W_m$  = water evaporated from manure kg/hr

K = coefficient of evaporation  $\text{kg/m}^2/\text{hr}$

$A_m$  = area covered with manure  $\text{m}^2$

$P_m$  = partial pressure of moisture in the air near manure mm.Hg

$P_p$  = partial pressure of the moisture in the air away from the manure mm.Hg

b = barometric pressure mm.Hg

The coefficient of evaporation was calculated from the following relationship:

$$K = .018 + .015 * V \quad (2.42)$$

where:

$V$  = air velocity near the manure m/s

Partial pressure near the manure was calculated by the following relationship

$$P_m = P_{sm} * Rh_m \quad (2.43)$$

where:

$P_{sm}$  = saturated vapor pressure near the manure  
mm.Hg

$Rh_m$  = relative humidity near the manure

Relative humidity near the manure was assumed equal to the relative humidity inside based on measurements taken during winter months. The saturated vapor pressure then calculated for the temperature near the manure, which assumed less than the inside temperature by small fraction based on measurements taken in the building.

The difference in partial pressures was then calculated and used for further calculations to determine the amount of water evaporated from the manure.

The total amount of water added to the air over a small time increment  $\Delta T$  was calculated by summing the amount of water produced from the chickens' respiration, air entering the system and the amount of water evaporated from the manure, minus the moisture leaving the system.

The moisture balance can be stated as

change in moisture content = (moisture entering the  
building - moisture leaving the building)  
/building air mass

$$\frac{\Delta W}{\Delta T} = (M W_O + W_C + W_m - MW_i) / Ma \quad (2.44)$$

$$\Delta W = \Delta T [MW_O + W_C + W_m - MW_i] / Ma \quad (2.45)$$

From the basic equations for the new heat content, the change in heat, new moisture content and the change in moisture of the air in the building, at the end of time increment, the new heat and moisture content can be found.

By substituting the new values of heat content, and moisture content in the following equation, the new temperature inside the building can be calculated at the end of time increment. The new heat and moisture content is calculated as follows:

$$h_{\text{new}} = h_{\text{old}} + \Delta q \quad (2.46)$$

$$W_{\text{new}} = W_{\text{old}} + \Delta W \quad (2.47)$$

By using the relationship between enthalpy  $h = q_{\text{new}}/Ma$ , temperature and moisture content, new values of inside temperature can be calculated as follows:

$$t_i = \frac{h_{\text{new}}/Ma - 2501 * W_{\text{new}}}{1.0035 + 1.84 * W_{\text{new}}} \quad (2.48)$$

where:

$q_{\text{new}}$  = new heat content kJ

$W_{\text{new}}$  = new moisture content kg  $H_2O$ /kg d.a

$Ma$  = air mass in the building kg

Inside relative humidity is calculated from the relationship:

$$\phi = \frac{P_v}{P_s} \times 100 \quad (2.49)$$

where:

$P_v$  = existing vapor pressure kPa

$P_s$  = saturated vapor pressure kPa

The dry bulb temperature and moisture content are known, the saturated vapor pressure  $P_s$ , and existing vapor pressure  $P_v$  are calculated as previously discussed.

### 2.5 Carbon Dioxide Balance

Mitchel and Haines (1927) published early concerns about the critical temperature for hens and the carbon dioxide production of hens at different temperatures. Later in 1941, Barott and Pringle (1941) also published paper on energy and gaseous metabolism of hens. Carbon dioxide eliminated ranges from  $.46\text{cm}^3$  per hour per gram live weight at 10 C to  $.49\text{ cm}^3$  per hour per gram live weight at 16.7 C.

Rous et al. (1971) estimated carbon dioxide production for hen ranges from  $.415\text{ cm}^3/\text{hr}$  for body weight of 450 g to  $.678\text{ cm}^3/\text{hr}$  for body weight of 1,350 g (heavy breed).

Carbon dioxide balance equation could be written as:

$$C_c + C_m + C_g = C_{ve} - C_{vo} \quad (2.50)$$

where:

$C_c$  =  $\text{CO}_2$  produced by the chickens

$C_m$  =  $\text{CO}_2$  produced from manure

$C_g$  =  $\text{CO}_2$  from other sources (gas furnace)

$C_{ve}$  =  $\text{CO}_2$  in exhaust ventilation air

$C_{vo}$  =  $\text{CO}_2$  in ventilation air from outside

For this study, carbon dioxide from the manure and from other sources, e.g., heating and equipment

assumed to be zero. The only carbon dioxide production used is from the hens.

$$\frac{\Delta C}{\Delta T} = C_{ve} - C_{vo} \quad (2.51)$$

The carbon dioxide in exhaust ventilation air is set to the maximum allowable concentration of 0.35%. This value was an average of different locations concentration. To calculate ventilation rate for carbon dioxide control, the rate of CO<sub>2</sub> production is needed in m<sup>3</sup>/hr, and calculated from following equations. This rate then divided by the difference of maximum allowable CO<sub>2</sub>, and CO<sub>2</sub> in atmosphere.

Three different equations used to estimate CO<sub>2</sub> production in different temperatures based on data from Barott and Pringle (1941):

$$P_{CO_2} = .3434 * t_i^{.1317} \quad \text{for temperatures } 10 \text{ C} - 17 \text{ C} \\ R = 0.99 \quad (2.52)$$

$$P_{CO_2} = .8961 * t_i^{-.213} \quad \text{for temperatures } 18 \text{ C} - 26 \text{ C} \\ R = 0.97 \quad (2.53)$$

$$P_{CO_2} = .222 * t_i^{.2201} \quad \text{for temperatures } 27 \text{ C} - 34 \text{ C} \\ R = 0.98 \quad (2.54)$$

where:

$P_{CO_2}$  = carbon dioxide production per gram body  
weight cm<sup>3</sup>/gr.hr.



The carbon dioxide picked up by ventilation is calculated by this formula based on Kadlec (1969):

$$C_v = \frac{EP_{CO_2}}{CO_{2max} - CO_{2atm}} \quad (2.55)$$

where:

- $C_v$  = ventilation rate for  $CO_2$   $m^3/hr$   
 $EP_{CO_2}$  = total production of  $CO_2$   $m^3/hr$   
 $CO_{2max}$  = maximum  $CO_2$  allowable = 0.35%  
 $CO_{2atm}$  =  $CO_2$  concentration in the air = .0003%

## 2.6 Bodyweight

Bodyweight of the chickens was calculated as a function of age. Data used were from the DeKalb XL-Link Pullet and Layer Management Guide, 2nd edition. A linear regression equations was fitted to the data and the following equation found to be best fit.

$$BW = .39883 * Age^{.400275} \quad \text{for age 19-40 weeks} \quad (2.56)$$

R = 0.94

$$BW = 1.68548 * Age^{.011659} \quad \text{for age 41-78 weeks} \quad (2.57)$$

R = 0.99

where

BW = bodyweight of the chickens kg

Age = age of chickens weeks

Change in weight was also estimated according to the same source. An average value was used to determine the change in weight because it was not significant to use otherwise. The change in weight was estimated as:

Age (Weeks)	Gain (g/day)	S.D.
18 - 23	8.3	1.60
24 - 28	3.8	1.30
29 - 40	1.5	0.42
41 - up	.5	0.00

Mortality was estimated from the management experience, of house seven, was .8% per month or  $2.67 \times 10^{-4}$  per day.

### 2.7 Feed Consumption

Marsden and Morris (1980) fitted a third order polynomial equation to describe the response of energy intake, of white egg layers to dry bulb temperature, within the cage, from 30 experiments. Temperature within the cage were assumed the same as room temperature.

$$Y_1 = 1584.3 - 33.47 * t_1 + 1.562 t_1^2 - .0349 t_1^3 \quad (2.58)$$

At a given temperature, energy intake increases slightly if dietary energy concentration is increased, even though feed intake decreases (Morris, 1968). In

34 experiments, the average increase in energy intake was 46 kJ/day per bird for each MJ/kg increase in dietary energy concentration. Therefore, assuming that the previous equation gives the energy intake for birds eating a typical diet containing 11.3 MJ/kg of energy, then the following equation estimates the energy intake adjusted for any dietary energy level, E (MJ/kg)

$$Y_2 = Y_1 + 46.0 * E - 519.8 \quad (2.59)$$

Feed intake was estimated by

$$F = Y_2/E \quad (2.60)$$

where:

$Y_1$  = metabolizable energy intake, kJ/d per bird,  
layers feed a diet containing 11.3 MJ/kg, for  
white egg layers only

$Y_2$  = metabolizable energy intake, kJ/d per bird,  
for white egg layers

E = metabolizable energy content of diet, MJ, ME/kg

F = feed intake, g/d per bird

Feed intake also changes with age (Charles, 1984). Table 2.3 gives values of another multiplier,  $f_1$  age factor, also taken from ADAS data archives.

Feed intake estimation was taken a step further, for adjustment of feeding equipment. Many designs of feeding equipment which are standard in both

Table 2.3 Values of Factor  $f_1$ , which adjusts feed intake for age.

Period	Week of Age	White Birds
1	20-24	0.764
2	24-28	0.917
3	28-32	0.987
4	32-36	1.006
5	36-40	1.022
6	40-44	1.024
7	44-48	1.052
8	48-52	1.044
9	52-56	1.053
10	56-60	1.053
11	60-64	1.030
12	64-68	1.020
13	68-72	1.032

Note: Calculated from Gleadthorpe data for 17 flocks feed 17 g/day per bird GRP, at 24°C.

the industry and in nutrition experiments have been found to be substantially wasteful (Elson, 1980). Therefore, a second adjustment factor,  $f_2$ , was used. Values taken from the data of Elson (1980) are given in Table 2.4. Allowing for the two adjustments  $F_f$  can be finally estimated as:

$$F_f = (Y_2 * f_1 * f_2) / E \quad (2.61)$$

where:

$F_f$  = final estimate of feed intake g/day per bird

$f_1$  = age factor adjustment

$f_2$  = feeding system design factor adjustment

Table 2.4. Values of the Factor  $f_2$ , which Adjusts Feed Intake for Wastage using Various Feeding Operations

Type of Feeder	$f_2$
Hopper and trough	1.000
Chain	0.965
Hopper and trough plus grid	0.958
Spiral	0.948
Sleeve	0.986

### 2.8 Egg Production

Fisher, Morris, and Jennings (1973) presented the most fundamental model for predicting the egg output response to nutrient intake. The model was deliberately limited to a few relatively simple algebraic functions. An attempt was therefore made to find a simple function, which would simulate the shape of the responses curve described by Fisher et al. (1973).

Charles (1984) found a satisfactory approximation for protein content within the normal commercial range of feed, and for experiments carried out at optimum house temperature, using an inverse polynomial.

$$e_1 = P^2 / (4.446 - 0.417P + 0.0309P^2) \quad (2.62)$$

where:

$e_1$  = egg output response to protein (g/b/d)

P = standard protein intake g/d per bird

The standard protein intake P was adjusted from the original form to conform to the protein standard used in Charles's equation. Then the equation for the standard protein intake would be

$$P = F \cdot C / 100 \quad (2.63)$$

where:

C = protein content in the feed %

F = feed intake g/d per bird

The protein content in the feed was 16% used for this study. No attempt was made to adjust the egg output response to photoperiod. The photoperiod used in this study was considered to be near optimum.

There is insufficient evidence to make estimates with confidence about the effect of temperature upon egg production on a daily bases (Personal Communication, Flegal, 1985). The effect of temperature was used when the temperature was above to 30 C. The depression was given by subtracting the following equation from the first estimate  $e_1$ .

$$D_1 = 10.98 + 2.14t_{ia} - 0.2335t_{ia}^2 + 0.00522t_{ia}^3 \quad (2.64)$$

where

$D_1$  = depression factor for temperature g/d per bird

$t_{ia}$  = average daily inside temperature C

Morris (1968) reviewed the effects of light on poultry and described the response in egg production, on a hen-hosed basis, H, eggs per bird in 336 days, to light intensity, I, as

$$H = 232.4 + 15.18 \log_{10}(I) - 4.256 (\log_{10}(I))^2 \quad (2.65)$$

For this function, the maximum value of H occurs when I = 60.4 Lux, for which H = 245.9 eggs per 336 days. The depression factor for light intensity,  $D_2$  was calculated if the light intensity were below the 60.4 Lux. Assuming a mean egg weight of 60g, and adjusting to 364 days:

$$D_2 = 2.41 - 2.711 \log_{10}(I) + .76 (\log_{10}(I))^2 \quad (2.66)$$

where:

H = egg production per hen housed per year

I = light intensity LX

$D^2$  = depression term for light intensity g/b/d

For this model light intensity was assumed optimal, and I = 60.4.

Egg output was also adjusted for age factor A, which calculated from Gleadthorpe data for 17 flocks fed 17 g/d per gird GRP, at 24 C. Table 2.5 gives the values of A factor.

The predicted egg output  $e_3$  (g/d per bird), was therefore:



TABLE 2.5. Values of Age Factor A, which Adjusts Egg Output.

Period	Weeks of Age	White Birds
1	20-24	0.32
2	24-28	0.93
3	28-32	1.09
4	32-36	1.12
5	36-40	1.11
6	40-44	1.11
7	44-48	1.11
8	48-52	1.09
9	52-56	1.06
10	56-60	1.05
11	60-64	1.02
12	64-68	1.00
13	68-72	0.97

$$e_3 = (e_1 - D_1 - D_2) * A \quad (2.67)$$

where:

$e_3$  = egg output, final estimate g/b/d

A = egg output adjustment factor for age

## 2.9 Cost Calculations

This includes fuel, electricity, feed cost and egg revenue.

### 2.9.1 Fuel Cost

Supplemental heat was used as an option in the model. The supplemental heat needed was calculated from heat balance equation. It could be written as shown in the following:

$$q_{sp} = q_b + q_v - q_s - q_e \quad (2.68)$$

where:

$q_b$  = sensible heat from chickens kJ/hr

$q_v$  = sensible heat from lights at day time kJ/hr

$q_s$  = sensible heat loss by ventilation kJ/hr

$q_e$  = sensible heat loss by building kJ/hr

$$\begin{aligned}
 q_v &= q_{vi} - q_{vo} = C_p M (t_i - t_o) \\
 &= 1.0035 * M * (t_i - t_o)
 \end{aligned}
 \tag{2.69}$$

where:

$q_{vi}$  = sensible heat leaving the room kJ/hr

$q_{vo}$  = sensible heat entering the room kJ/hr

$M$  = ventilation air mass kg/hr

$$\begin{aligned}
 q_{sp} &= A * U (t_i - t_o) + 1.0035 * M (t_i - t_o) \\
 &- q_s - q_e
 \end{aligned}
 \tag{2.70}$$

Fuel cost was then calculated by multiplying the supplemental heat needed by its price and divided by the energy content of the fuel used:

$$F_{uc} = (q_s * P_f) / E_f \tag{2.71}$$

where:

$P_f$  = fuel price \$/m<sup>3</sup>

$E_f$  = energy content in fuel kJ/m<sup>3</sup>

### 2.10 Electricity Cost

The two 45 cm variable speed fans were fixed at constant rate, and they operated continuously as minimum ventilation rate. Minimum ventilation rate cost was calculated by measuring power in watts consumed at low air flow rate on the variable speed fan

and multiplied by electricity price in dollars per kilowatt hour for each fan.

$$E_c = (E_p * .135) * N \quad (2.72)$$

where:

$E_c$  = electricity cost \$/hr

$E_p$  = electricity price \$/kW hr

0.135 = power measured at min. vent. rate kW

$N$  = number of fans operating  $N=2$

For fans operated to control the temperature, electricity cost calculated according to information supplied by the fan manufactures performance tables, it was 11.81 cubic feet per min, per watt was used to calculate electricity usage per hour, which then multiplied by electricity price. The daily electricity cost was calculated by summing the cost for every hour for both fans during one day.

$$KWH = (Vrate \times Eusag)/1000 \quad (2.73)$$

where:

$Vrate$  = ventilation rate above minimum ventilation rate cfm

$Eusag$  = electricity consumption = 0.0847 W/cfm

$KWH$  = electricity usage in kw

### 2.11 Feed Cost

Feed cost was calculated by multiplying feed intake by feed price.

$$F_{dc} = (F_{in} * F_{dp}) \times 1000 \quad (2.74)$$

where:

$F_{dc}$  = feed cost 1,000      \$/day

$F_{in}$  = feed intake              kg/day

$F_{dp}$  = feed price              \$/kg

### 2.12 Egg Revenue

Average egg weight was estimated from data published by Hy-Line management guide, third edition, for variety W 36. Two equations were used to estimate average egg weight based on age of the bird.

$$\begin{array}{ll} \text{Egw} = 13.5203 * \text{Age}^{.4087} & \text{for age 22 to 40 weeks} \\ R = 0.98 & (2.75) \end{array}$$

$$\begin{array}{ll} \text{Egw} = 36.1114 * \text{Age}^{.1371} & \text{for age 41 to 80 weeks} \\ R = 0.99 & (2.76) \end{array}$$

where:

Egw = average egg weight      gr

Age = Age of birds              weeks

The number of eggs was determined by dividing egg production estimated from the model by the average

weight calculated from the standards and then calculated per 1,000 chickens. Number of dozens was also calculated by dividing number of eggs for (1,000 chickens) by 12. Then the revenue was calculated by multiplying number of dozens by nest run price.

Cost was estimated for that day by summing the electricity cost, feed cost, and fuel cost (if used). Then this amount was subtracted from the revenue for the same day, and reported as (revenue margin).

### 2.13 Outline of Computer Program

The mathematical algorithms discussed early were incorporated into subroutines for computer computation. In the simulation these subroutines were activated and controlled by a main or executive program. A flow chart of the main program and the subroutines are shown by Figures 2.3 to 2.26.

The computer program was set up to either operate in a verification mode based on actually recorded(measured) input ventilation rate, inside and outside average daily temperature or a simulation mode based on Weather model.

The input routine was designed to be used interactively to enter all information needed to run the main program. The input routine may use old files stored on a disk, change some parameters from an old

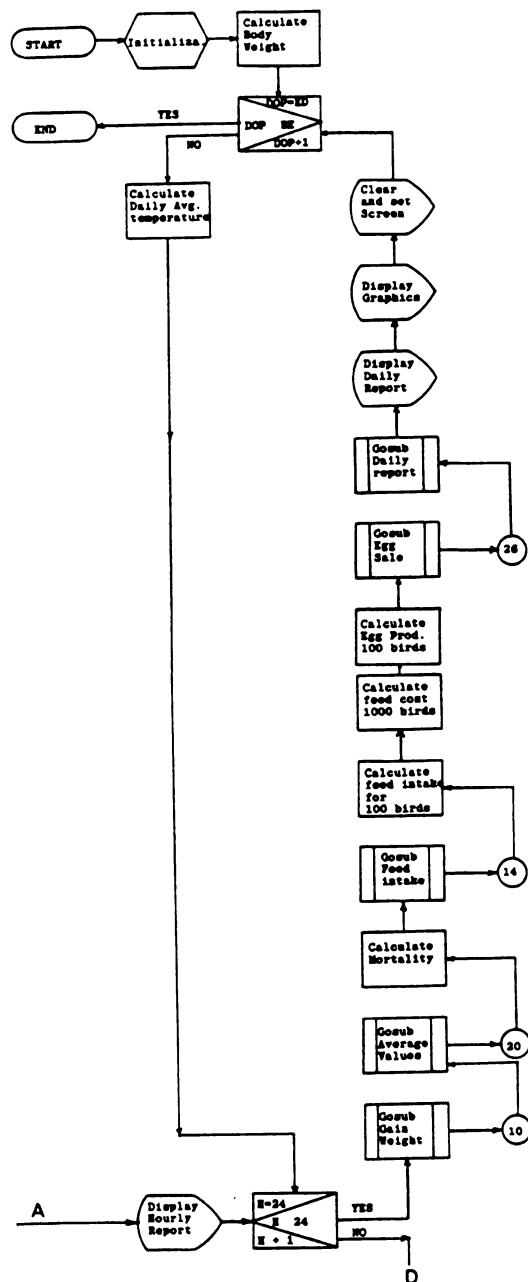


Figure 2.3 Main Program

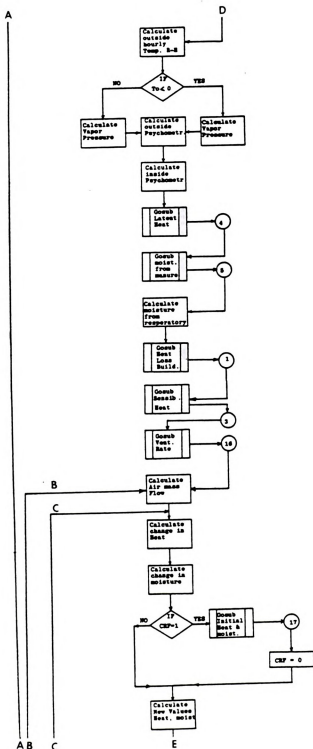


Figure 2.3. Continued



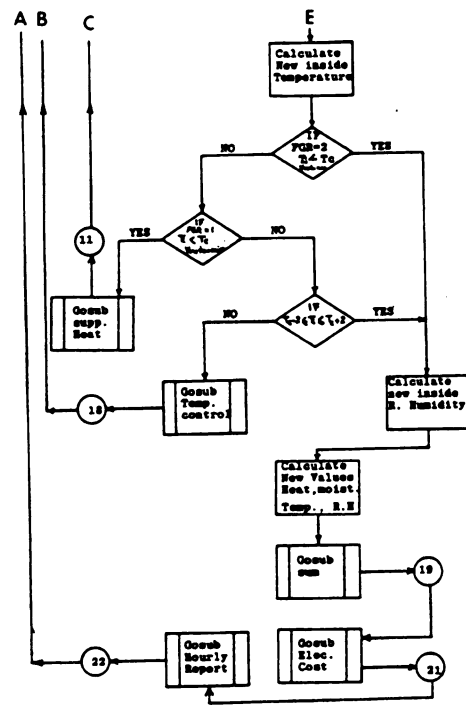


Figure 2.3. Continued.

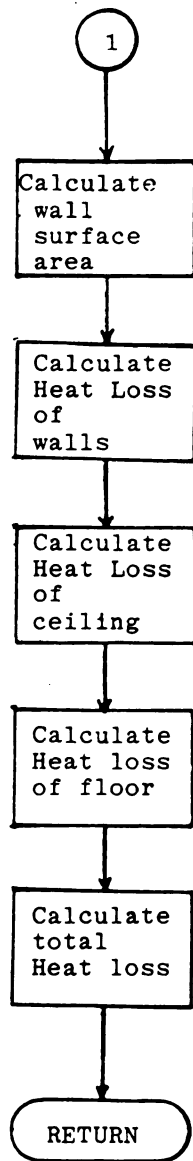


Figure 2.4. Subroutine Number 1--Heat Loss Through Building.

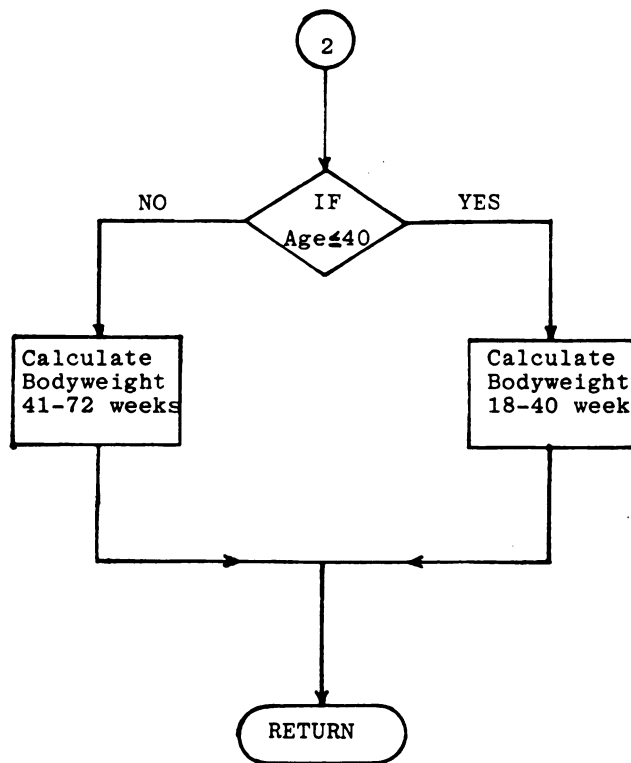


Figure 2.5. Subroutine Number 2--Body Weight of Chickens.

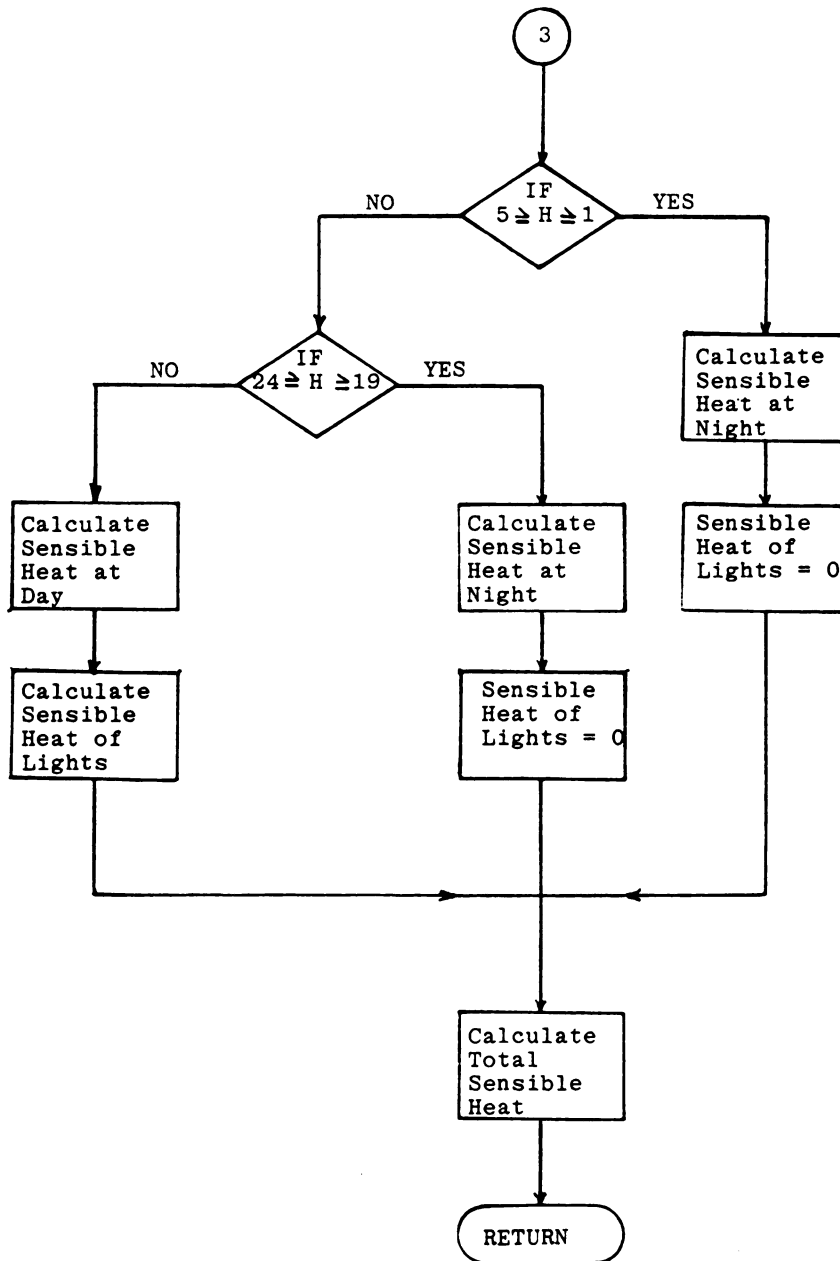


Figure 2.6. Subroutine Number 3--Sensible Heat from Chickens.

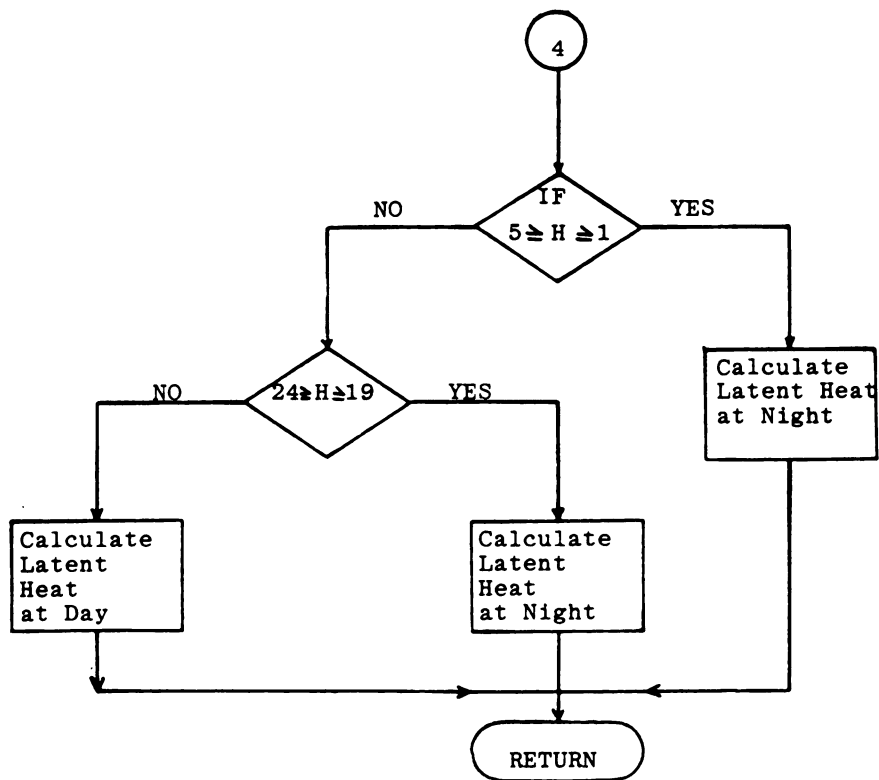


Figure 2.7. Subroutine Number 4--Latent Heat from Chickens.

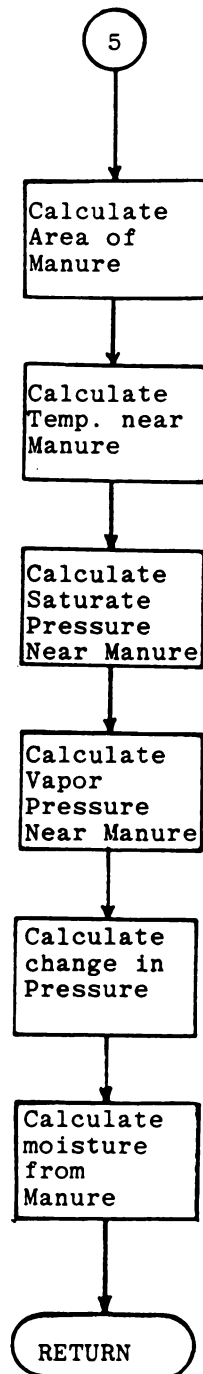


Figure 2.8. Subroutine Number 5--Water Evaporation from Manure.

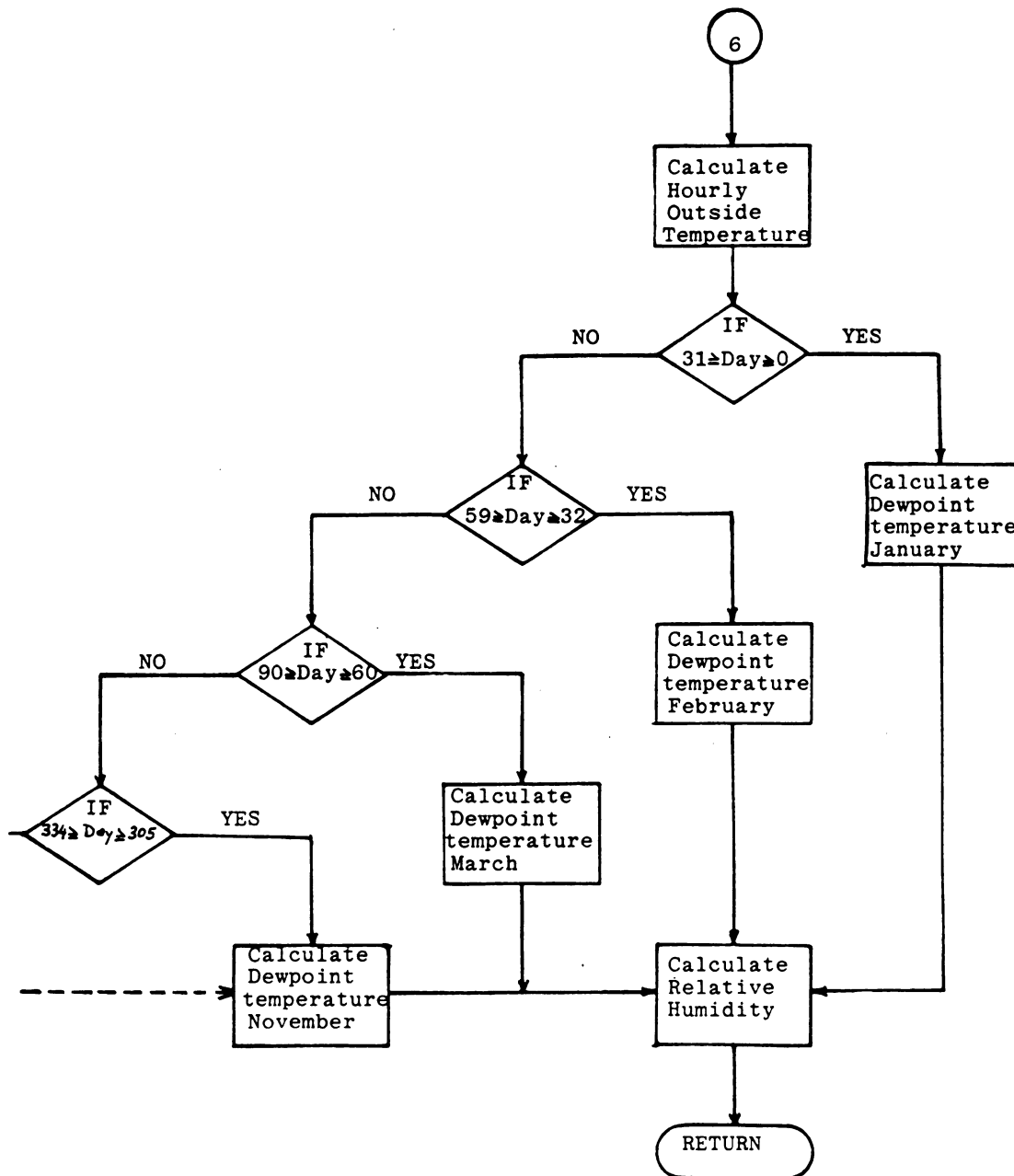


Figure 2.9. Subroutine Number 6--Outside Hourly Ambient Temperature and Relative Humidity.

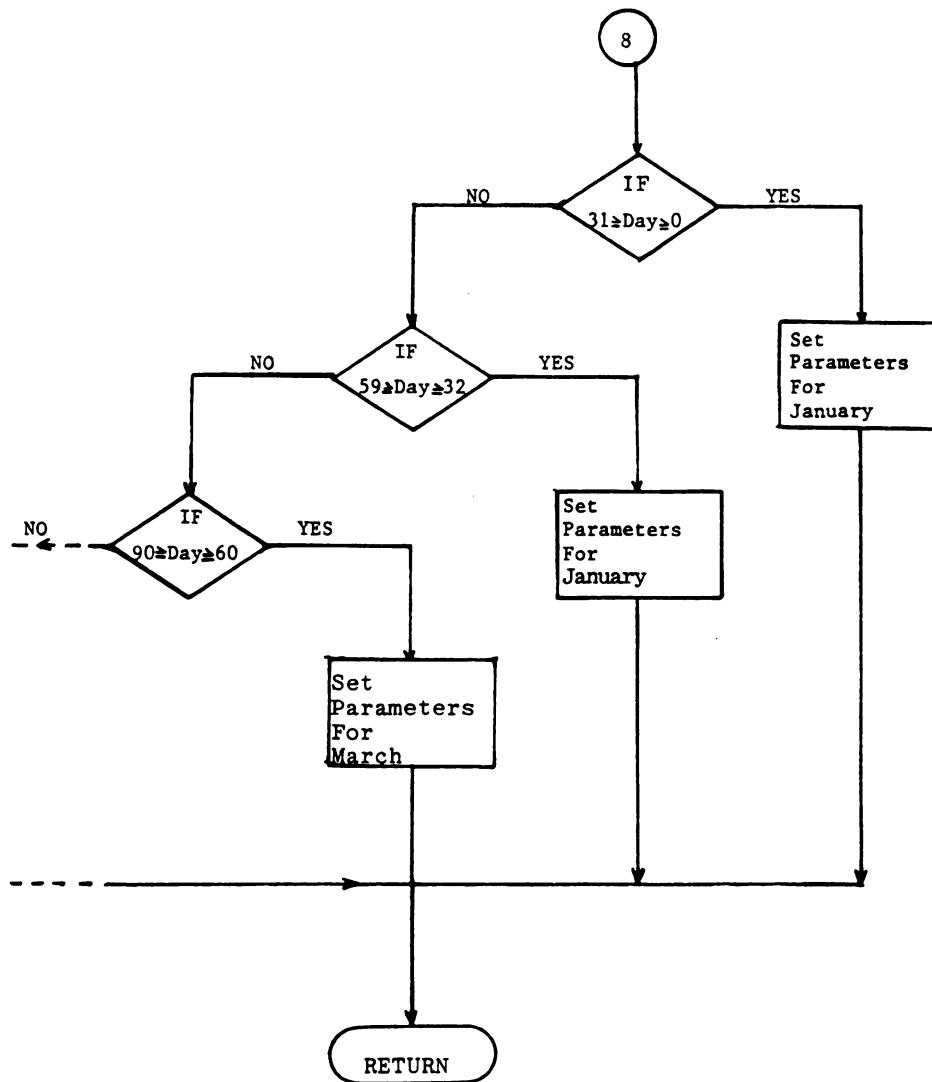


Figure 2.10. Subroutine 8: Julian Day (Calendar)



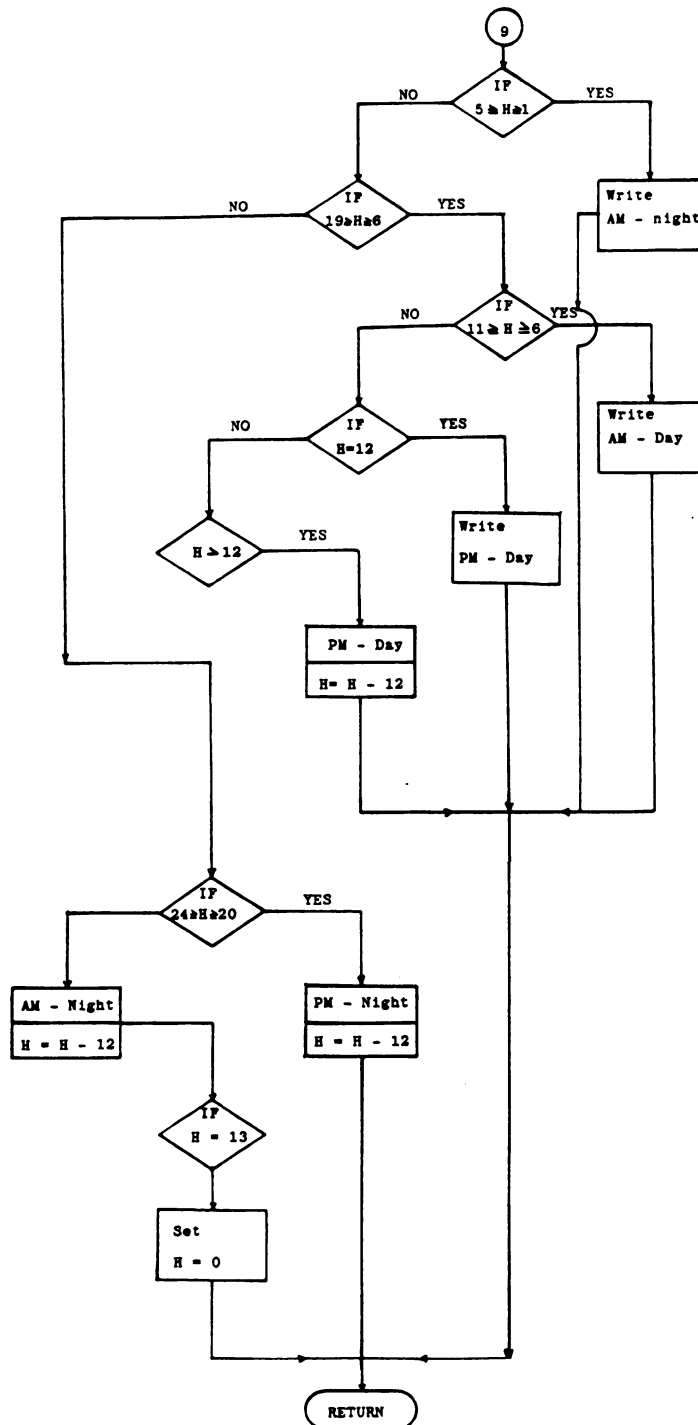


Figure 2.11. Subroutine Number 9--Day and Night.

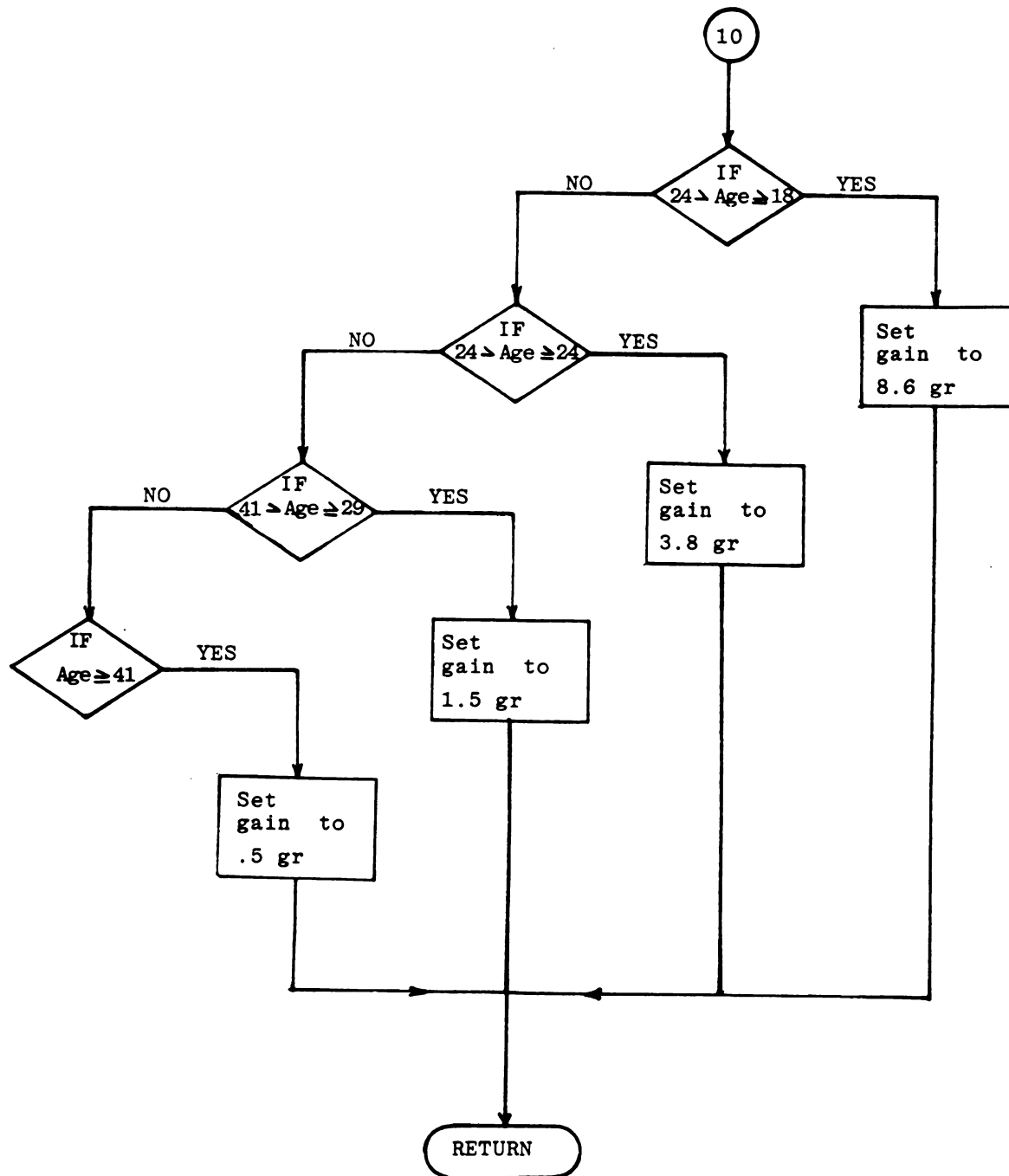


Figure 2.12. Subroutine Number 10--Gain in Weight.

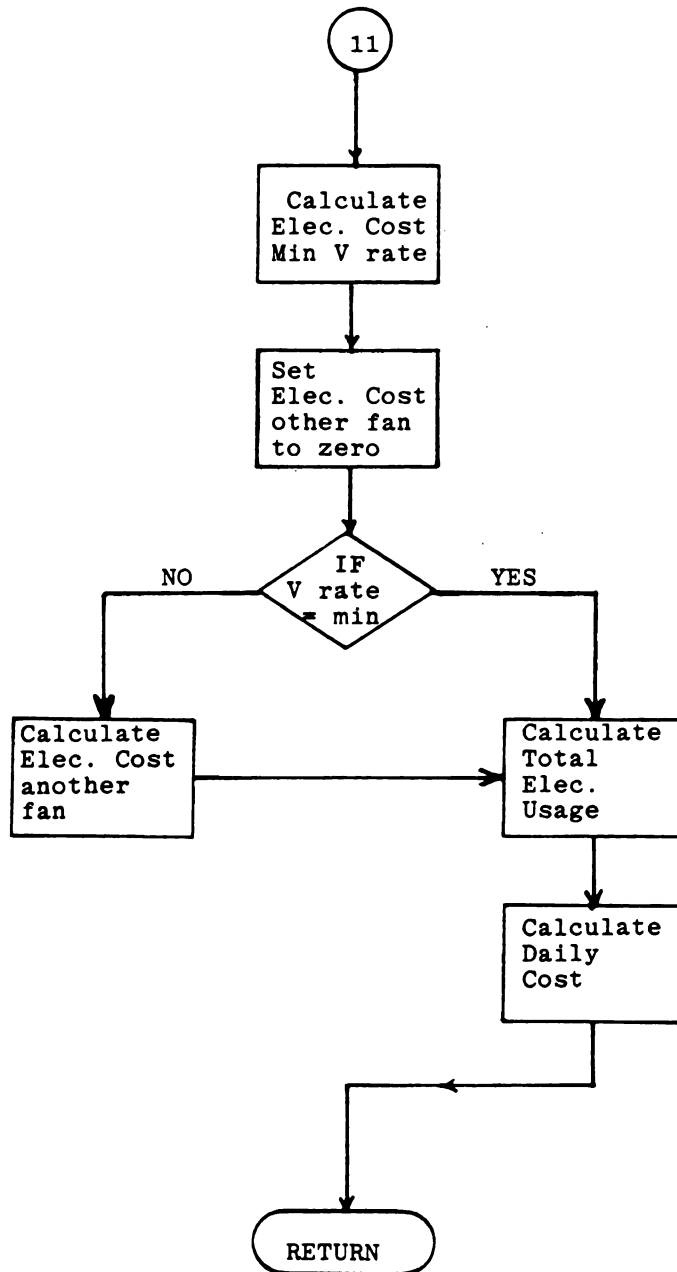


Figure 2.13. Subroutine Number 11--Electricity Cost.

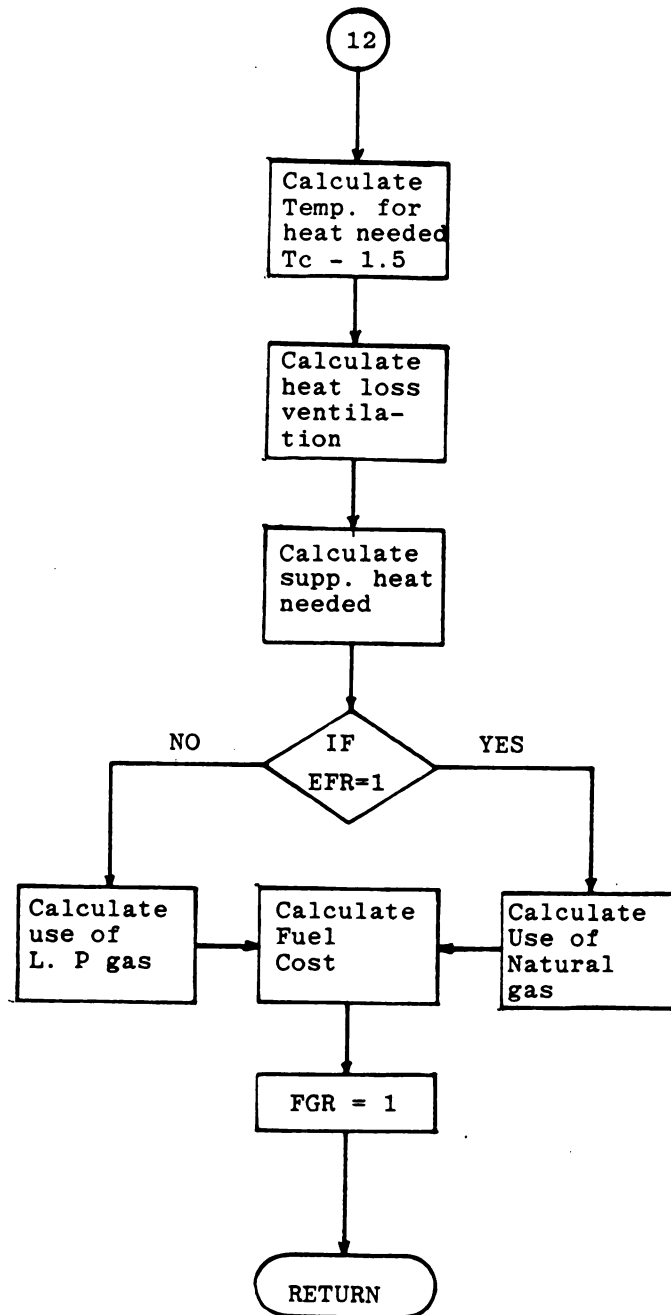


Figure 2.14. Subroutine Number 12: Supplemental Heat Needed.

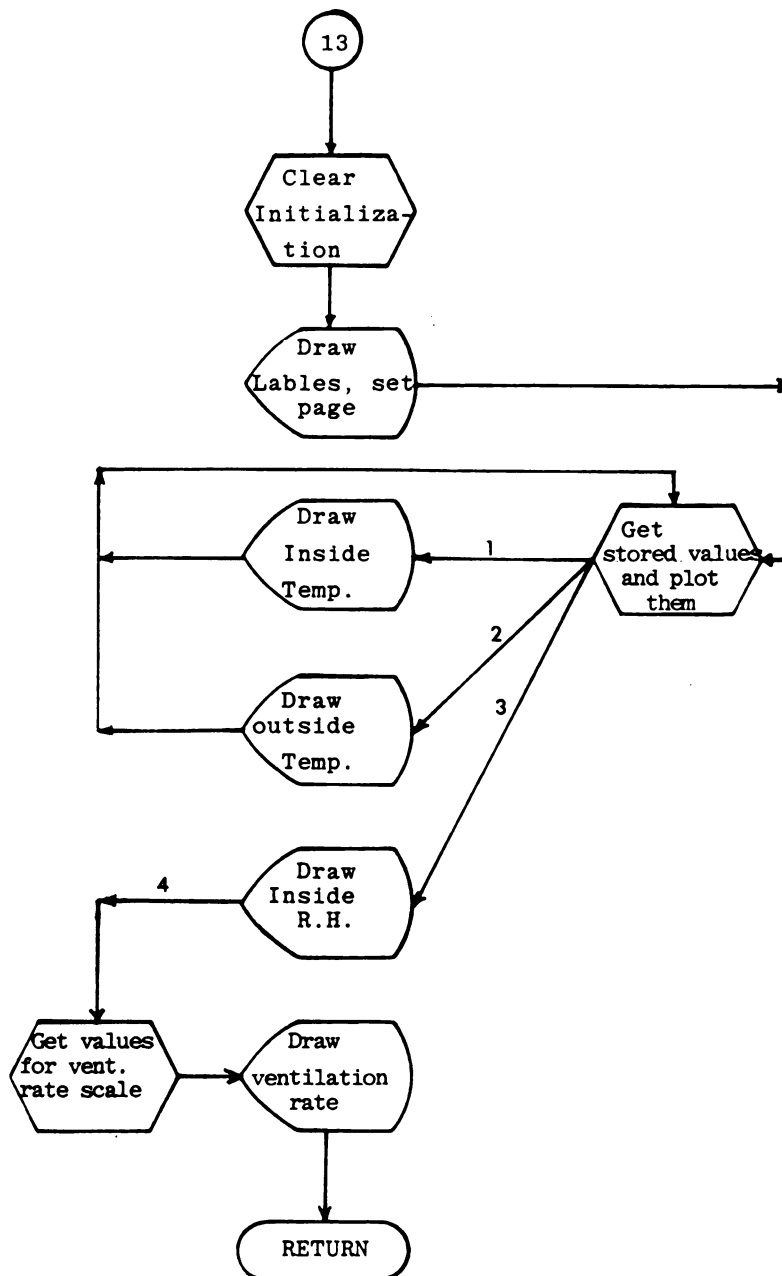


Figure 2.15. Subroutine Number 13: Graphics Presentation.

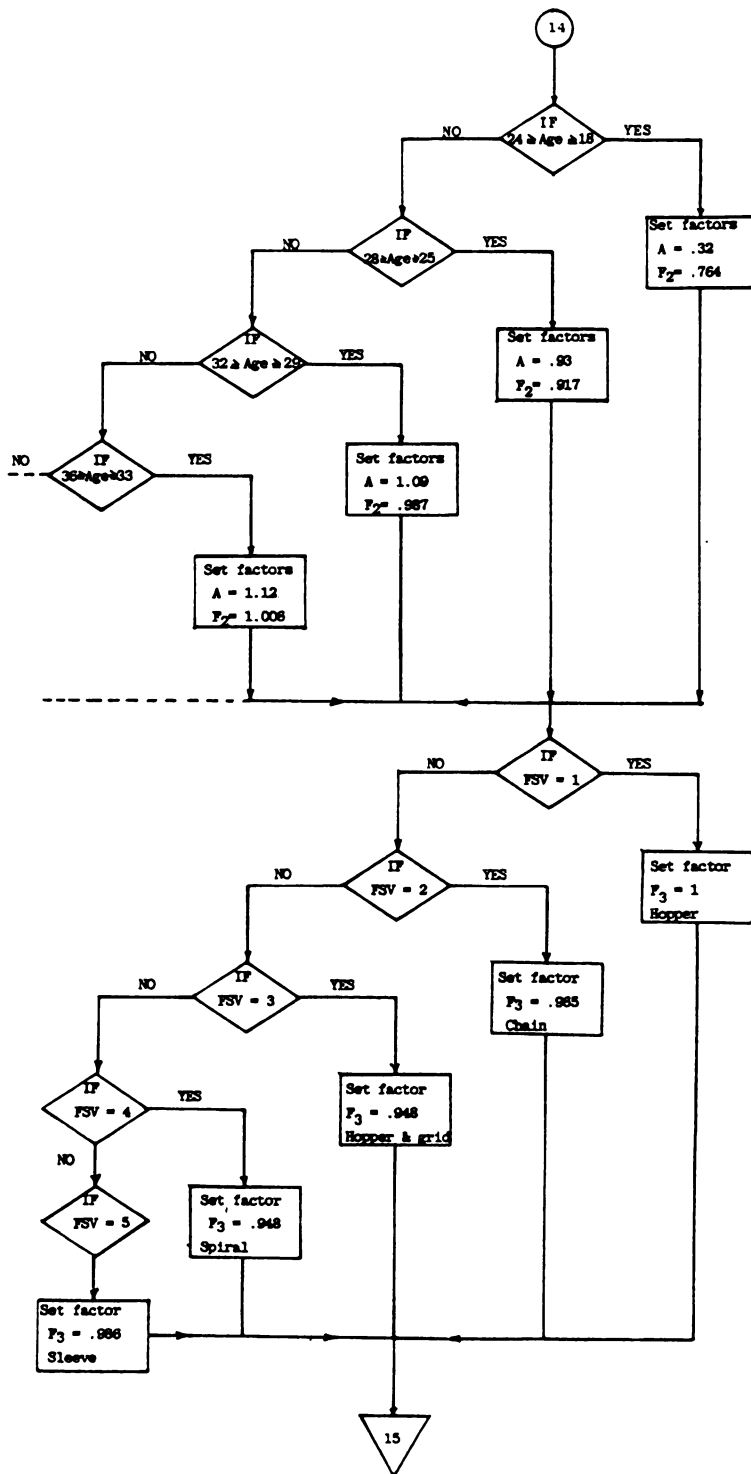


Figure 2.16. Subroutine Number 14: Estimate of Age and Feed System Factors.

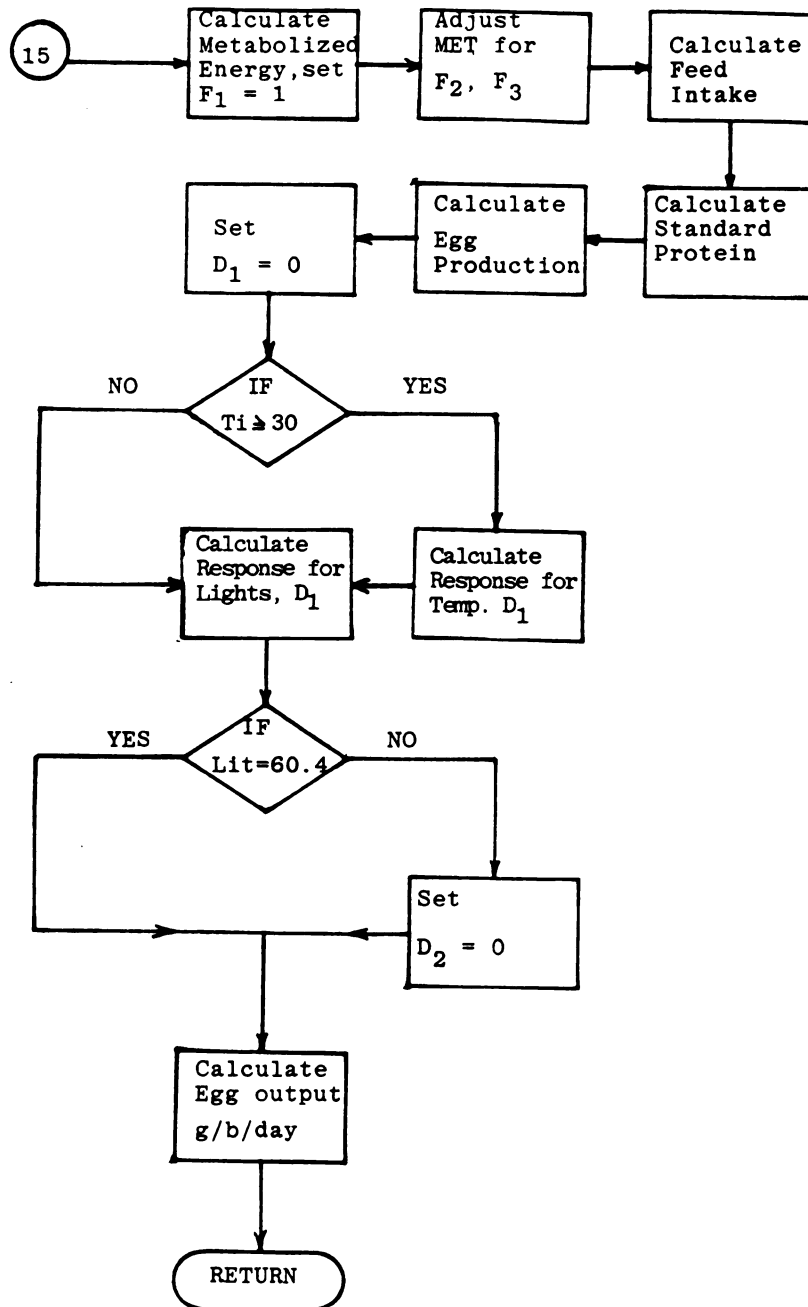


Figure 2.17. Subroutine Number 15: Feed Intake and Egg Production.

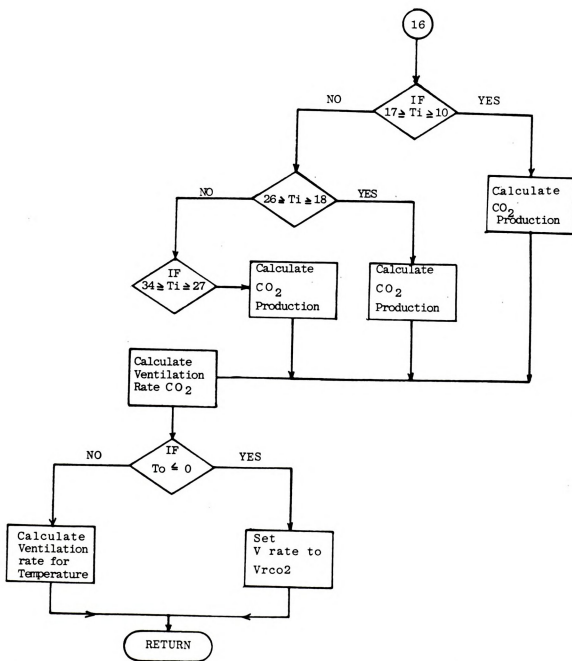


Figure 2.18. Subroutine Number 16: Ventilation Rate.



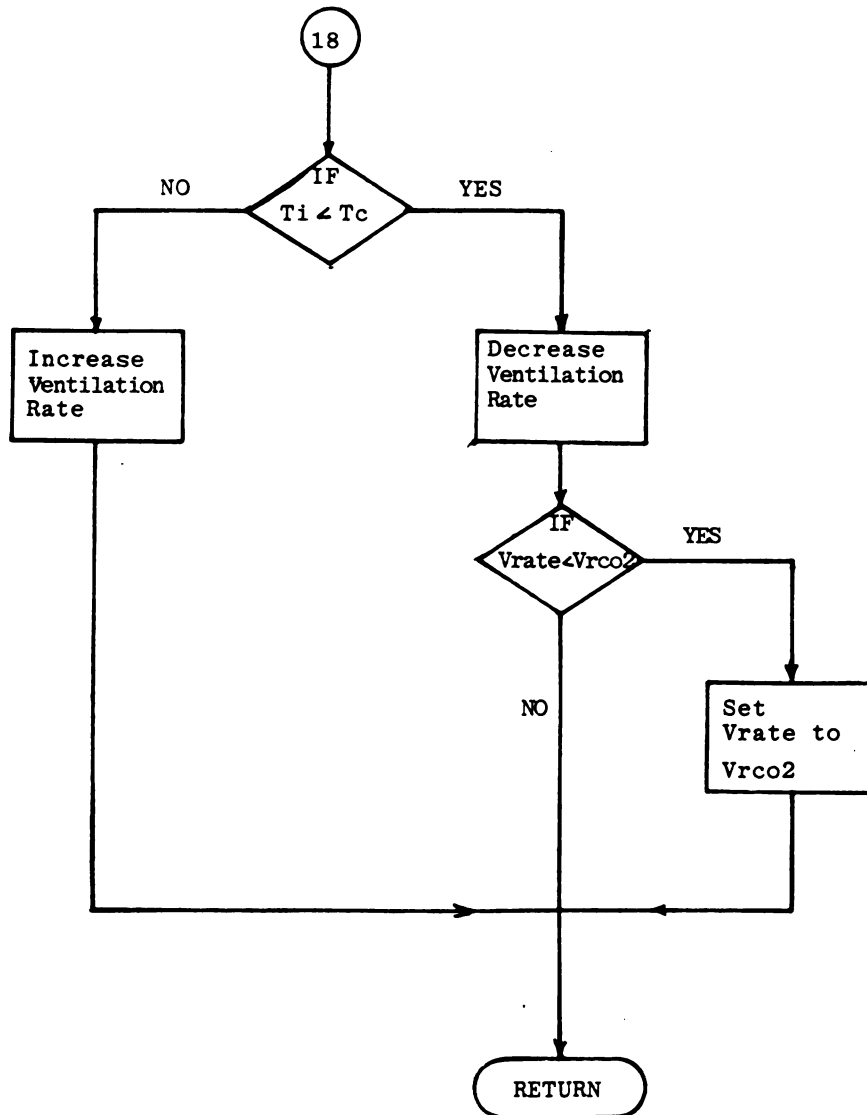
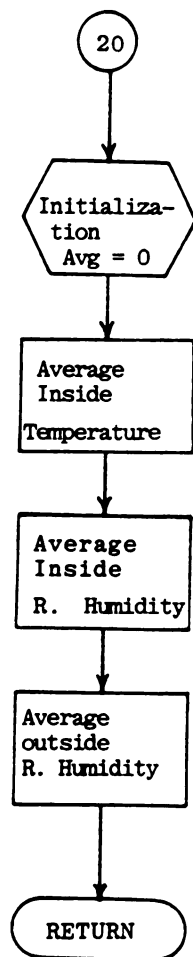
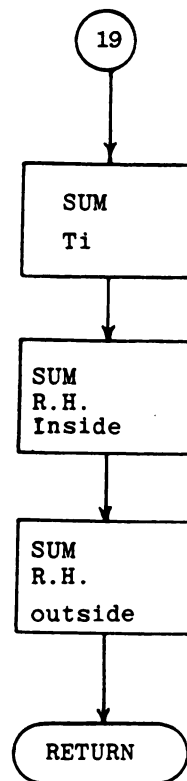


Figure 2.19.--Subroutine Number 18: Control Inside Temperature.



Subroutine Number 20  
Averaging the Values



Subroutine Number 19  
Summing the Values.

Figure 2.20. Subroutine Number 19: Summing the Values.



Figure 2.21. Subroutine Number 21: Design Hourly Output Page.

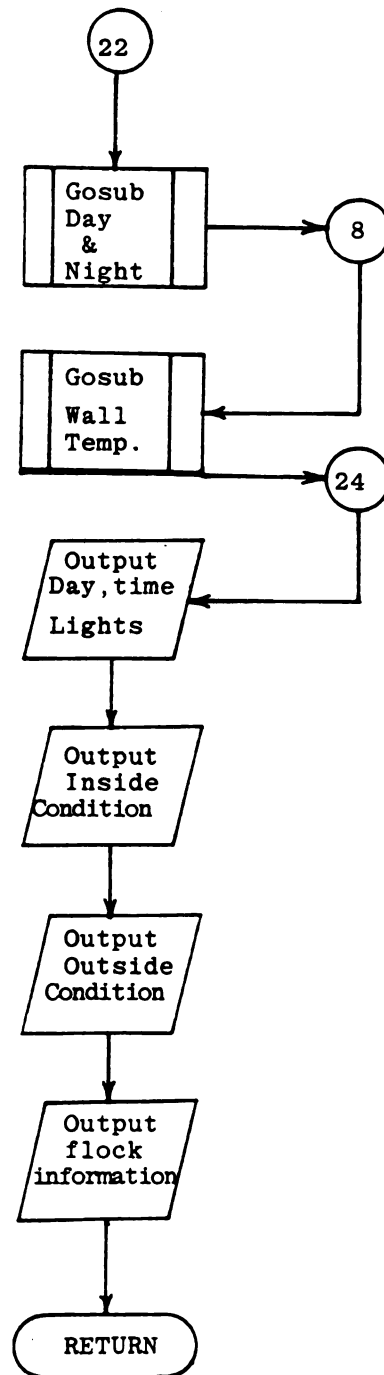


Figure 2.22. Subroutine Number 22: Hourly Report.

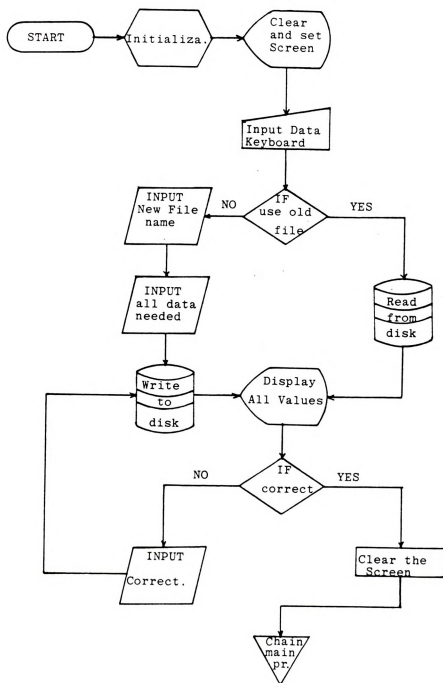


Figure 2.23. Subroutine Number 23--Input Program.

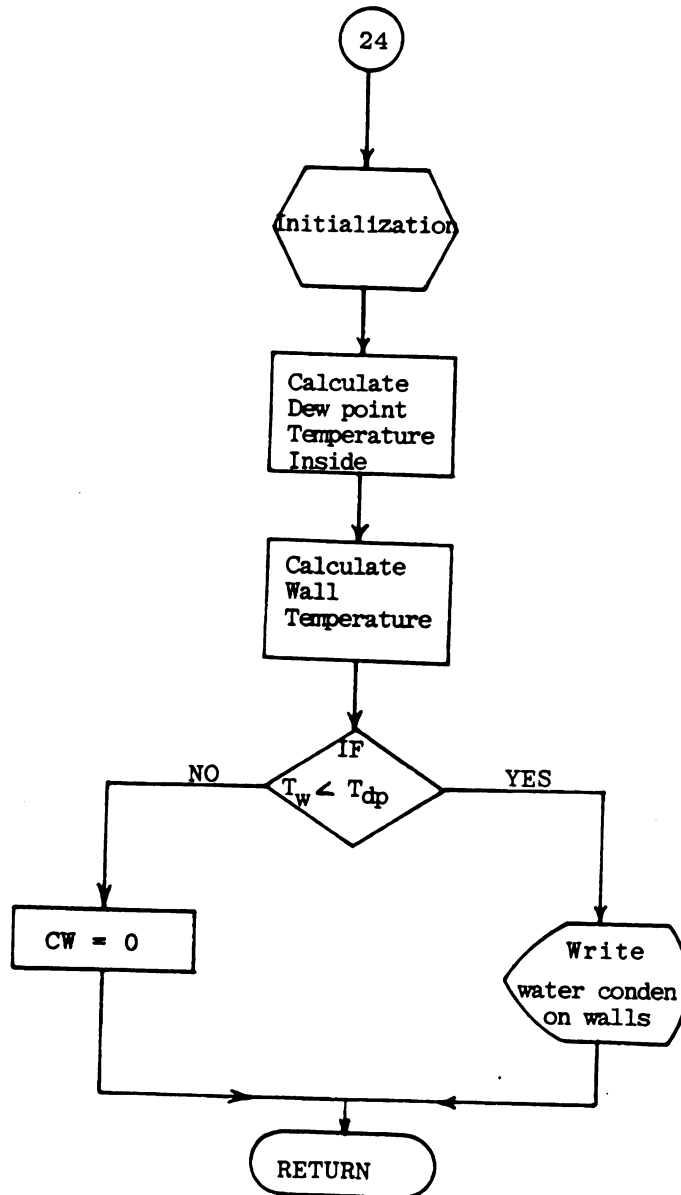


Figure 2.24. Subroutine Number 24: Wall Temperature.

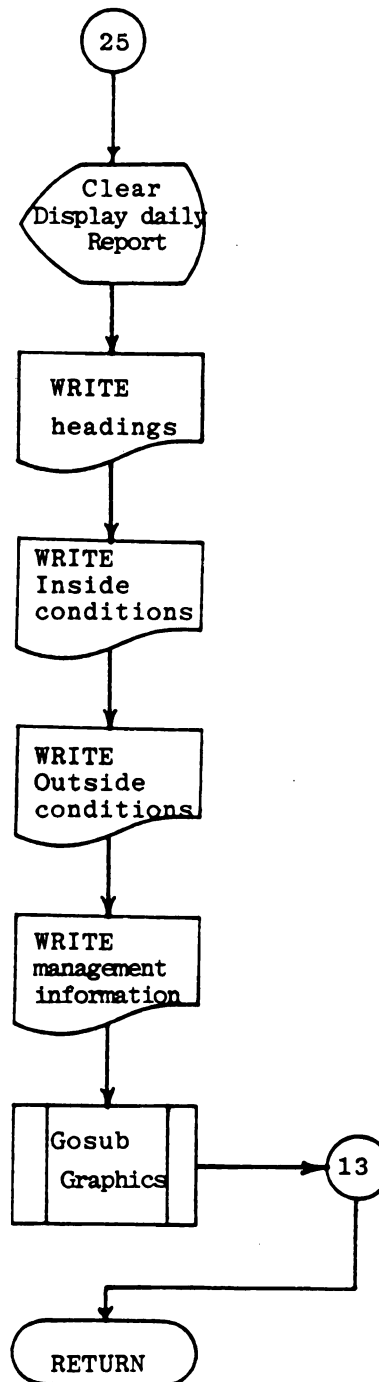


Figure 2.25. Subroutine Number 25: Daily Report.

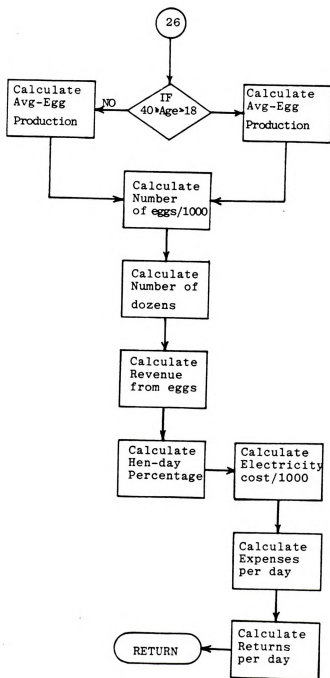


Figure 2.26. Subroutine Number 26: Costs.



file or allow the user to create new files. After all the information have been entered, the input routine will activate the simulation model (main program).

The first operation for starting the simulation on a daily bases was to initialize the fixed parameters. First, the body weight of chickens is calculated based on age of bird. Then the daily simulation started for the period needed. The screen is cleared, and the hourly report displayed (see Figure 2.27), and prepared for further calculations. Average daily temperature for outside was then calculated using the weather model. This was followed by determining the appropriate psychometric properties for the outside air for that hour for the specific day.

The appropriate psychometric properties for the inside air for that hour and day also was calculated.

Heat loss through the building, sensible heat from birds, and if the lights were on, the heat from lights was estimated, then the total sensible heat calculated.

The ventilation rate for temperature control was determined, and the minimum ventilation rate to control carbon dioxide is calculated, if outside hourly temperature were below 0 C. For temperatures above 0 C, ventilation rate is calculated from equation

derived from heat balance equation. Before using any ventilation rate, the ventilation rate was checked, and not allowed to be less than the ventilation rate for carbon dioxide control.

The change in heat and moisture was calculated and added to initial values, then the new heat and moisture content of air was used to determine the new inside temperature. This value was checked, if it was in the range previously set, then it was passed for further calculations and to determine the new relative humidity. If it was not, a control subroutine was used to increase or decrease ventilation rate, and checked against the minimum allowed, then returned to the main program to calculate a new inside temperature.

The new values of heat, moisture, inside temperature, and relative humidity were set to be initial values for the next hour, and stored in an array for further use in graphics.

The wall temperature and dewpoint temperature inside was calculated and compared to determine if water condensation may occur. Then the inside and outside conditions were displayed on a previously prepared screen.

After 24 hours of calculations, the age of chickens was determined, the gain in bodyweight was

estimated and mortality per day calculated. Feed intake was then calculated based on average daily inside temperature and feed cost for 1,000 birds was calculated. Egg production and egg sale for 1,000 bird was also calculated. Figures 2.27 and 2.28 show a typical output.

The daily report then displayed, included average inside temperature and relative humidity, maximum and minimum temperature that occurred on that day, the outside conditions, average daily temperature, and relative humidity.

The management information was also displayed, which included feed intake per 100 birds, metabolizable energy intake per bird, estimated egg production per 100 bird, percent of hen day production, feed cost, electricity cost, fuel cost if used, and egg revenue for 1,000 bird was calculated and displayed.

The flock information also displayed. That included number of birds, age in weeks, average body weight, and mortality rate calculated on that day.

Then the model will clear the screen and draw the graphics for inside, outside hourly temperature, the relative humidity inside, and ventilation rate on hourly base was also displayed.

DATE :		TIME:		FARM NAME:	
HOURLY REPORT				LIGHTS:	
<b>INSIDE CONDITIONS:</b> 1-Previous temperature C 2-New temperature C 3-Previous rel humidity % 4-New rel humidity % 5-Ventilation rate m3/hr			<b>OUTSIDE CONDITIONS:</b> 1-Avg daily temperature C 2-Previous temperature C 3-New temperature C 4-Previous rel humidity % 5-New rel humidity %		
<b>FLOCK INFORMATION:</b> 1-Number of birds Birds 2-Age of birds Weeks 3-Avg bodyweight kg 4-Fed consumption g/d/b 5-Egg production g/d/b 6-H D production %					

Figure 2.27. Typical Hourly Report Output.

DATE :	FARM NAME:	
DAILY REPORT		
<p>INSIDE CONDITIONS:</p> <p>1-Avg temperature C</p> <p>2-Avg rel humidity %</p> <p>3-Maximum temp C</p> <p>4-Minimum temp C</p> <p>OUTSIDE CONDITIONS:</p> <p>1-Avg daily temp C</p> <p>2-Avg rel humidity %</p> <p>FLOCK INFORMATION:</p> <p>1-Number of birds Birds</p> <p>2-Age of birds Weeks</p> <p>3-Avg bodyweight kg</p> <p>4-Bird mortality Birds</p>	<p>MANAGEMENT INFORMATION:</p> <p>1-Feed intake /100 kg/day</p> <p>2-MET energy /bird kJ/day</p> <p>3-H D production %</p> <p>4-Est egg prod/100 kg/day</p> <p>5-Feed cost /100 \$/day</p> <p>6-Elec cost /1000 \$/day</p> <p>7-Fuel cost /1000 \$/day</p> <p>8-Egg revenue /1000 \$/day</p> <p>9-Revenues - cost \$/day</p> <p># Hours of water condensation</p>	

Figure 2.28. Typical Daily Report Output.

After a pause of about 30 seconds, a new hourly report displayed, and all the calculations repeated for new conditions of outside and inside.

#### 2.14 Model Calibration and Verification

The model was calibrated during winter months, and especially adjusted on February 8. This day was used as calibration of the model. Other days selected for validation were February 13, 16, 27, and March, 3 days only.

The model was verified by operating a commercial-type cage laying houses from January 1986 through March 1986. At various time throughout this period, psychometric data were collected for analysis. The principal data collected were dry-bulb, wet-bulb temperature and ventilation rate. Carbon dioxide and ammonia were measured during minimum ventilation rate.

Management information also collected by the poultry department for the same period, and that includes bodyweight, feed consumption, egg production, feed energy, and also prices for feed, egg, and electricity

### 2.15 Experimental Facilities and Equipment

The floor plan of experimental facilities is illustrated by Figure 2.29. Dry and wet bulb temperature data were collected with CR-21 instrument manufactured by Campbell Scientific, Inc. The temperature was measured with thermister sensors: one dry and one with a cotton wick kept wet with distilled water from a continuous source. The results of these measurements were transferred to the CR-21 and then to a tape recorder. The data logger was programmed to collect data for every 10 minutes. The instrument was set to recover temperatures in degrees Celsius. Since some temperatures for outside air were expected to be below 0 C, relative humidity measured directly by special sensor design for this purpose (201 sensor).

Wet bulb temperature for inside air was measured by temperature probe (101 sensor) covered with a cotton wick kept wet by an instrument designed in Agricultural Engineering Department at Michigan State University, and a special circuit was built to turn the wet bulb fan on 5 minutes before the reading and turn it off after that.

A 5 volt pulse from CR-21 to transistor 2N2222 turns on LED in OPTO-ISOLATOR which turns on trigger triac. This turns on 1 amp 200 volt triac which

- Temperature
- ▲ Relative humidity or wet-bulb temperature
- + CO<sub>2</sub>

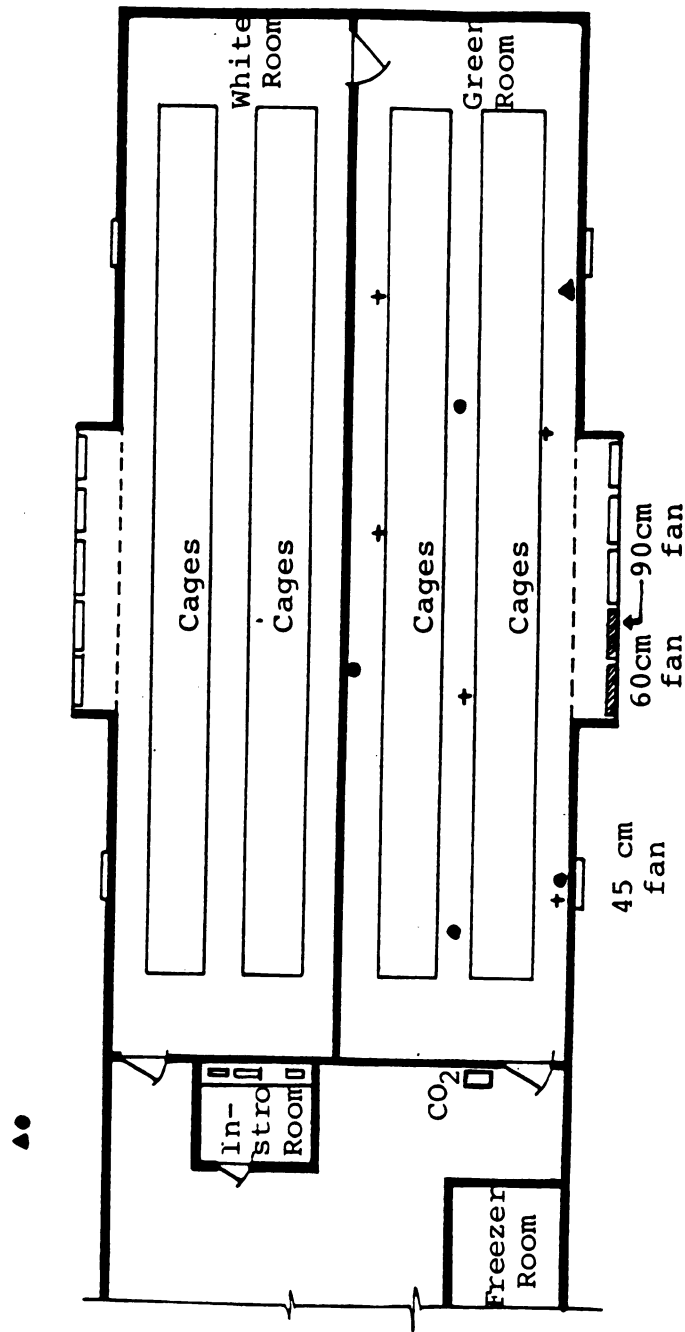


Figure 2.29 Floor plan of the commercial-type poultry house used as base for the simulation.



controls fan motor (see Figure 2.30) holding it on for as long as 5 volt output for CR-21 is present.

For air flow measurements, the variable fans (45 cm) were fixed on fixed rate of 900 cubic meters per hour. Air velocity were measured near the inlet openings and the area of the inlet was measured, then the airflow was calculated by multiplying the area by air velocity. This procedure was repeated several times until the appropriate ventilation rate was achieved.

This ventilation rate was the minimum ventilation rate and for ventilation rate above that, two pieces of equipment designed to interface the fan circuit. The first circuit was the current sensor which connected to circuit breaker of 60 cm fan (see Figure 2.31 for each fan).

When any current passes through Diode resistor assembly, a constant AC voltage is presented to OPTO-ISOLATOR and external LEDs. This causes output triac to switch on feeding 120 VAC to input of CR-21 logic interface.

The second device was the logic interface, Figure 2.32, which connected to the data logger CR-21 input channels. Current sensor (in 240 V fan power line) senses fan "ON" condition and causes 120 VAC

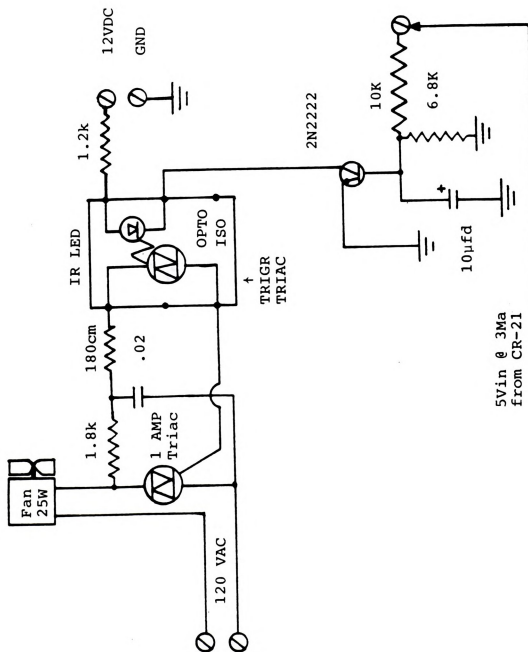


Figure 2.30. Psychrometric Fan Control Circuit.

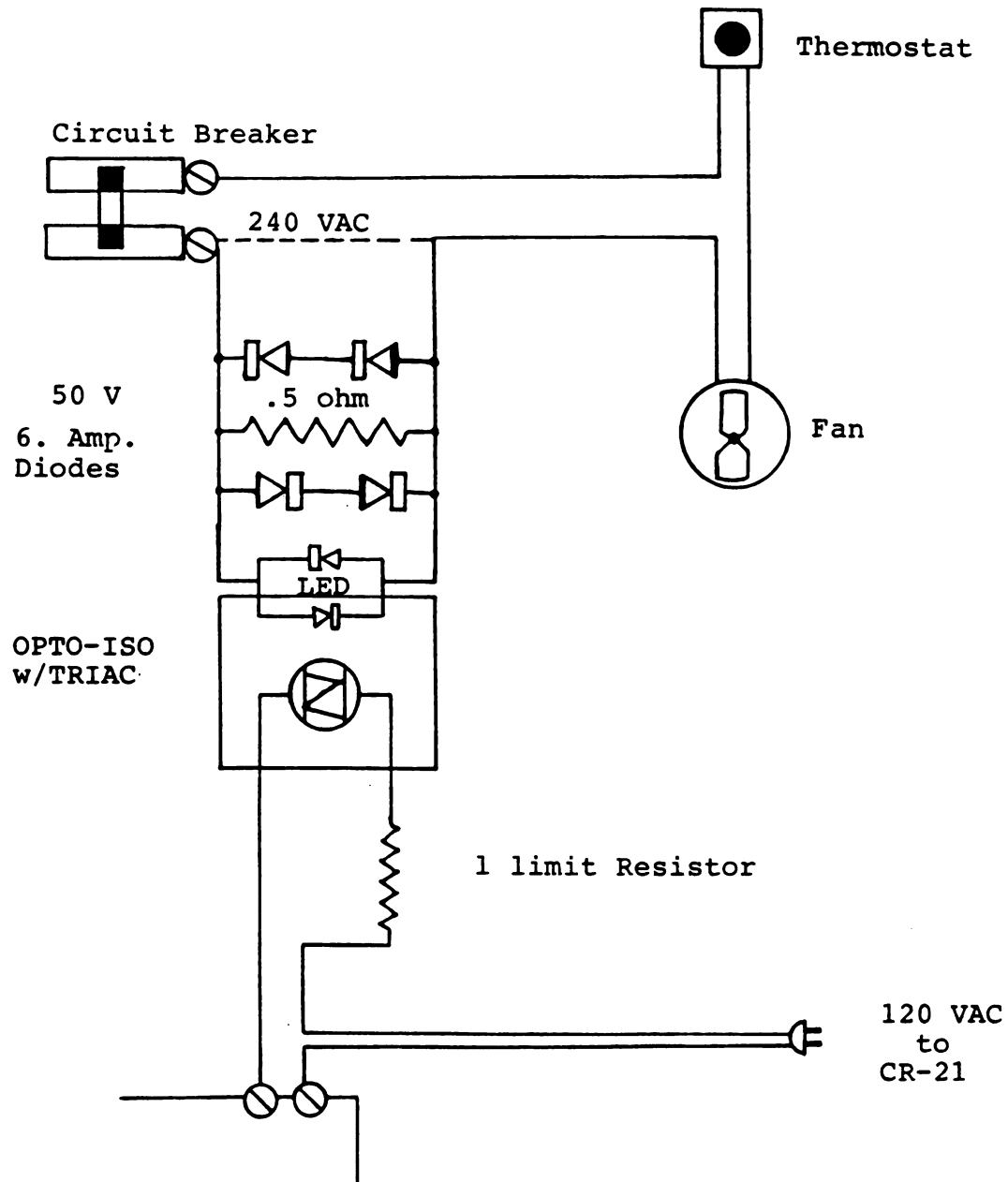


Figure 2.31 Current (I) Sensor circuit.

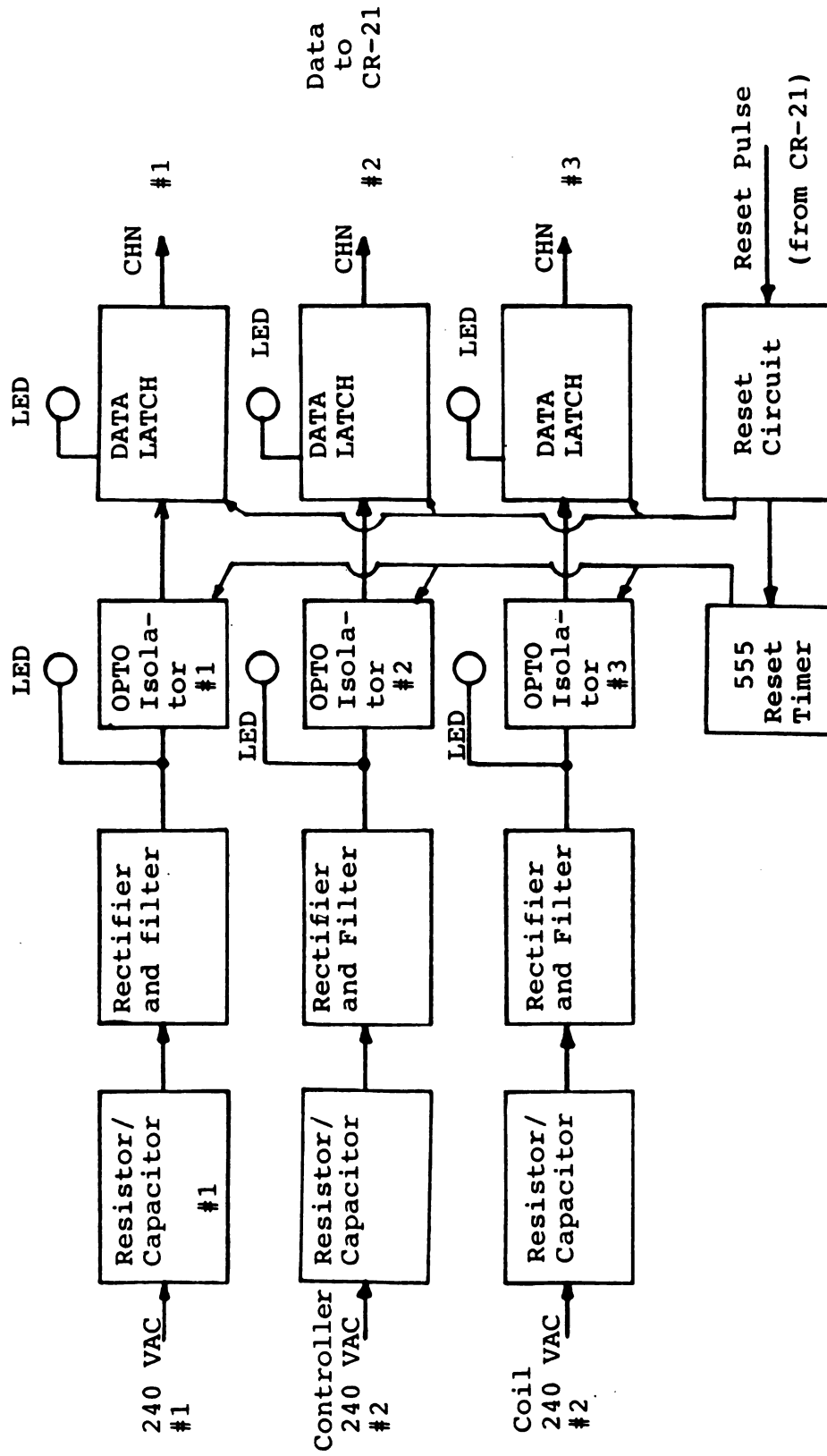


Figure 2.32 Current (I) to CR-21 interface diagram.

(approximately) to appear at the Attenuator inputs (numbers 1 through 3). This voltage is then rectified and filtered, then it is applied (as low voltage, DC) to both on light Emitting Diode and the input of an OPTO- ISOLATOR. The output of the OPTO-ISO is a small pulse (from a capacitor) to the data latch, which holds the (PULSE/information) condition until the CR-21 scans latches for present/absent of fan "ON" condition. At the end of the scan, the CR-21 pulses to "RESET CIRCUIT" causing the "LATCHES" to return to the wait state (Yellow Led ON).

The reset pulse also starts a "555" timer which holds any information that may be present in the OPTO-ISO for approximately 10 seconds. If the fan is still on or comes on during the time period (after reset) then the information is not lost, but is passed on to the latches after "time out" of the reset timer (555).

The 60 cm fan, when it was on, assumed to operate on maximum capacity of 4950 cubic meter per hour. That was the same for the 90 cm fan. Both fans were connected to the CR-21 circuit.

To measure carbon dioxide concentration in the poultry house at the minimum ventilation rate, a gas system collection was designed and built in the poultry house. There was a set of filters (5) placed in

different locations and different heights on the cases (see Figure 2.33). Every filter was connected to a P.V.C. tube which then connected to a main panel with valves, each valve controls one filter. All five tubes led to outside the room. A vacuum compressor was connected to the main valve panel through a fine filter. The compressor then pumps the air to an aquarium (see Figure 2.34), which puts upside down. Another tube was placed on the base of the aquarium to allow taking the samples.

There was flush filter placed outside the poultry room to flush the system after each sample.

#### 2.16 Data Collection and Analysis

Dry bulb and wet bulb temperatures were measured at various locations in the poultry house (see Figure 2.29). Data were collected every ten minutes. Temperature at each hour calculated by two data sets, at the end of each hour and the reading from the ten minutes before were averaged and used as representative temperature of that hour.

Wet bulb temperature was measured in two ways: by using a thermistor prob manufactured by Campbell Scientific, Inc., covered with wet wick and a thermocouple sensor covered with the same wick as a back up sensor. Both sensors placed in the same

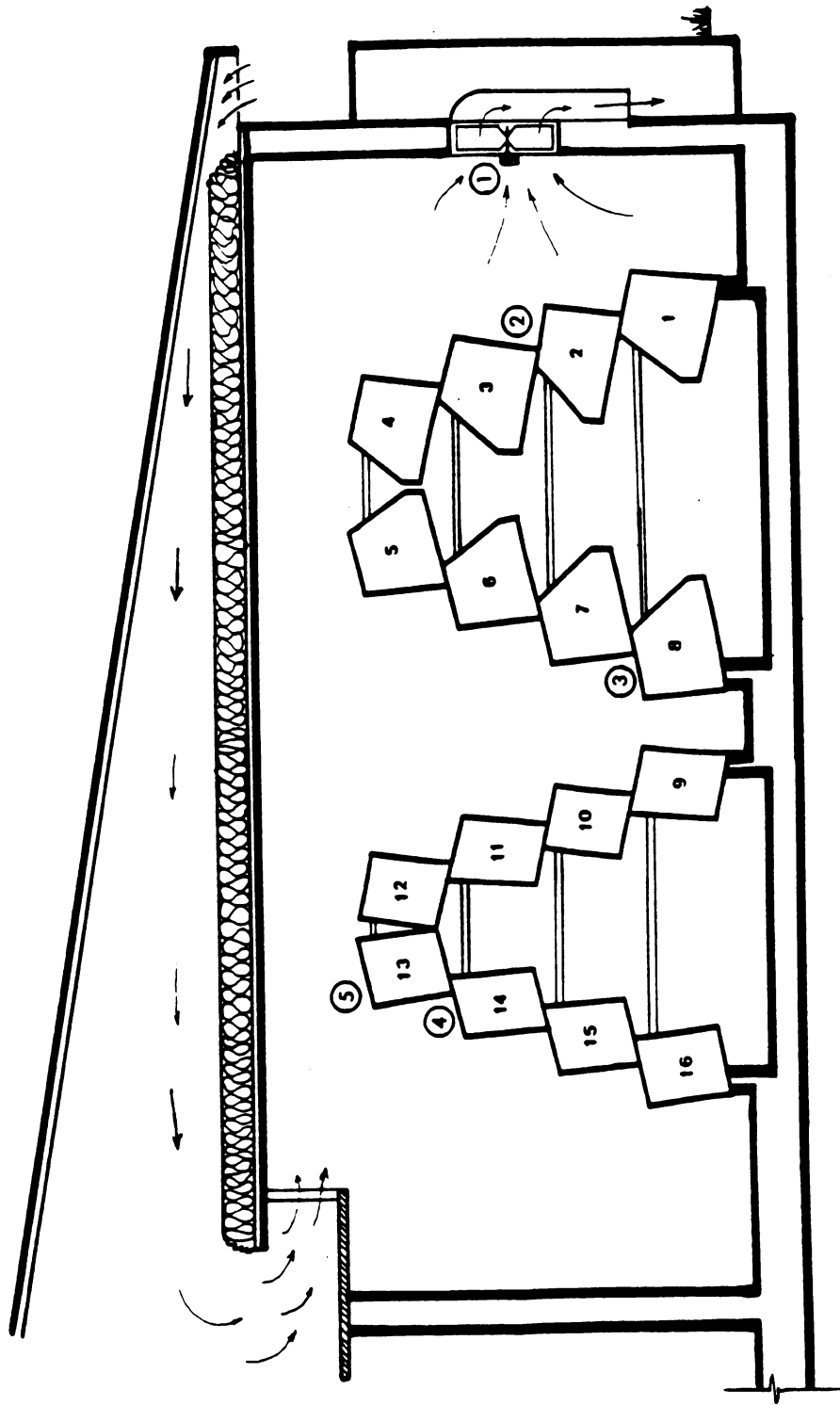


Figure 2.33. Carbon Dioxide Sampling Locations.

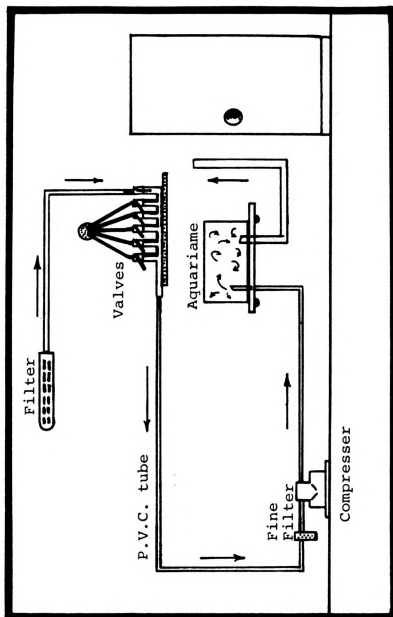


Figure 2.34. Carbon Dioxide Sampling Instrumentation.



location close to exhaust fan. Readings were taken twice a day for the back up sensor manually at 8 a.m. in the morning and 4 p.m. in the afternoon.

Because of the failure in some channels of data logger not registered, specially for the outside temperature and relative humidity and the wet bulb temperature for inside. The back-up data for wet bulb temperature then was used to calculate the average daily inside relative humidity.

Outside temperature and relative humidity data were taken from the National Oceanic and Atmospheric Administration (NDAA), from Lansing, Michigan, during February and March 1986. The average daily temperature and the amplitude of the daily temperature were calculated and used in the weather model to predict the hourly outside temperature and relative humidity. The dewpoint temperature first calculated and then by using the dry bulb temperature on that hour, the relative humidity calculated from psychrometrics. The hourly temperature and relative humidity were used as inputs to the main model to calculate psychrometric data needed to complete the calculation for outside conditions.

Carbon dioxide was measured on different days of January 17 and 31, and several days in February, 11, and 21, for coldest days. Samples were taken several

times a day from 9 a.m. in the morning, 3 p.m. in the afternoon, and from 6 p.m. until 7 a.m. of the next day, every three hours. It takes one hour to complete a scan of all five locations (see Figure 2.33 for carbon dioxide and ammonia locations). The interval between each scan was about 15 minutes. The emphasis was on night hours when the poultry house was in stable conditions almost all the time and the ventilation rate was a minimum  $0.2 \text{ m}^3/\text{hr bird}$ .

During working hours, it is difficult to control or measure exact amount of airflow because of the workers and other researchers which who should do their jobs. Several times the doors were opened which could effect the carbon dioxide concentration.

The samples were analyzed by using a commercial colorometer (chemically). The instrument was manufactured by Matheson (Model No. 8014-400a) using carbon dioxide tube model 126SA ranges from 0.1 - 2.6%. The ammonia tube model 105SC ranges from 5 to 260 PPM.

After each sample, the system was flushed with clean air from the outside room for about 8 minutes and then proceeded to the next location (see Figure 2.34). Measurements with very low readings were repeated and the average of the two were considered as representative value of that sample.

To estimate moisture from the manure, 4 to 5 samples each time of manure has been taken on a time interval of 3 p.m., 8 p.m., 12 midnight, and 6 a.m. The samples were weighed in aluminum cans. The cans were cleaned, dried, numbered, and weighted empty. This was the empty can weight. Then the sample was placed in each can and immediately sealed and then weighed. This weight was the weight of the can full of manure. A preheated oven for 103 C used to dry the cans for 24 hours. Then the samples were taken from the oven, cooled, and weighed again. This weight was the weight of the dried manure with the can. The dry manure weight was calculate by subtracting the weight of the can empty from the weight of the can plus manure dried. Then the moisture content in percent was calculated for all 22 samples This process was repeated for other days for more data.

Electricity consumption also was measured for the 45 cm fan and assumed to be constant for all day. For the 60 cm fan, data from the manufacturing company were used to calculate electricity consumption, which was based on the number of minutes the fan was operating.

## CHAPTER III

### VERIFICATION

#### 3.1 Simulation Model Evaluation

The model was evaluated by comparing a performance variable as determined from measured data to that same variable as calculated by the simulation model. The important variables to compare were the hourly inside temperature during the test day, average daily inside temperature ventilation rates and average daily inside relative humidity. Another performance variable was the feed intake of 100 chickens and egg production. Intermediate calculation from the model were compared, for example, bodyweight.

The verification measurements were combined with comparable calculations from the simulation model and plotted to form a graph for review.

The principal input variables for the model, for inside conditions, were initial dry-bulb temperature, relative humidity, age of the birds, number of chickens, building parameters, insulation values of the walls and ceiling, feed metabolizable energy and length, width of manure pit. Inputs for outside conditions were average

daily dry-bulb temperature and amplitude of outside temperature. Other input variables were considered constant; for example, feeding system, feed prices, electricity prices, egg sale price, and ventilation rate (Tables 5A to 7A in the Appendix).

### 3.2 Results and Discussion

Actual and predicted outside and inside temperatures are plotted in Figures 3.1 through 3.4. Output information for all runs are tabulated (Tables 3.1 to 3.5). The input information is tabulated in Appendix A.

The absolute mean deviation between actual and predicted hourly inside temperature for February 13 was 0.148 C and standard deviation of 1.758; for February 16 was 0.077 C and standard deviation of 1.884; for February 27 it was 0.016 C and standard deviation of 1.776; and on March 3 was 0.204 C and standard deviation of 1.954.

The average daily inside relative humidity, (Table 3.1) measured was 72% and the simulated was 71%, average daily relative humidity for outside, measured was 78% and the simulated was 79%. The mean daily inside temperature simulated and measured were 24.61 and 24.46 C, respectively. The daily average for outside temperature was -11.46 C, which was the same used to

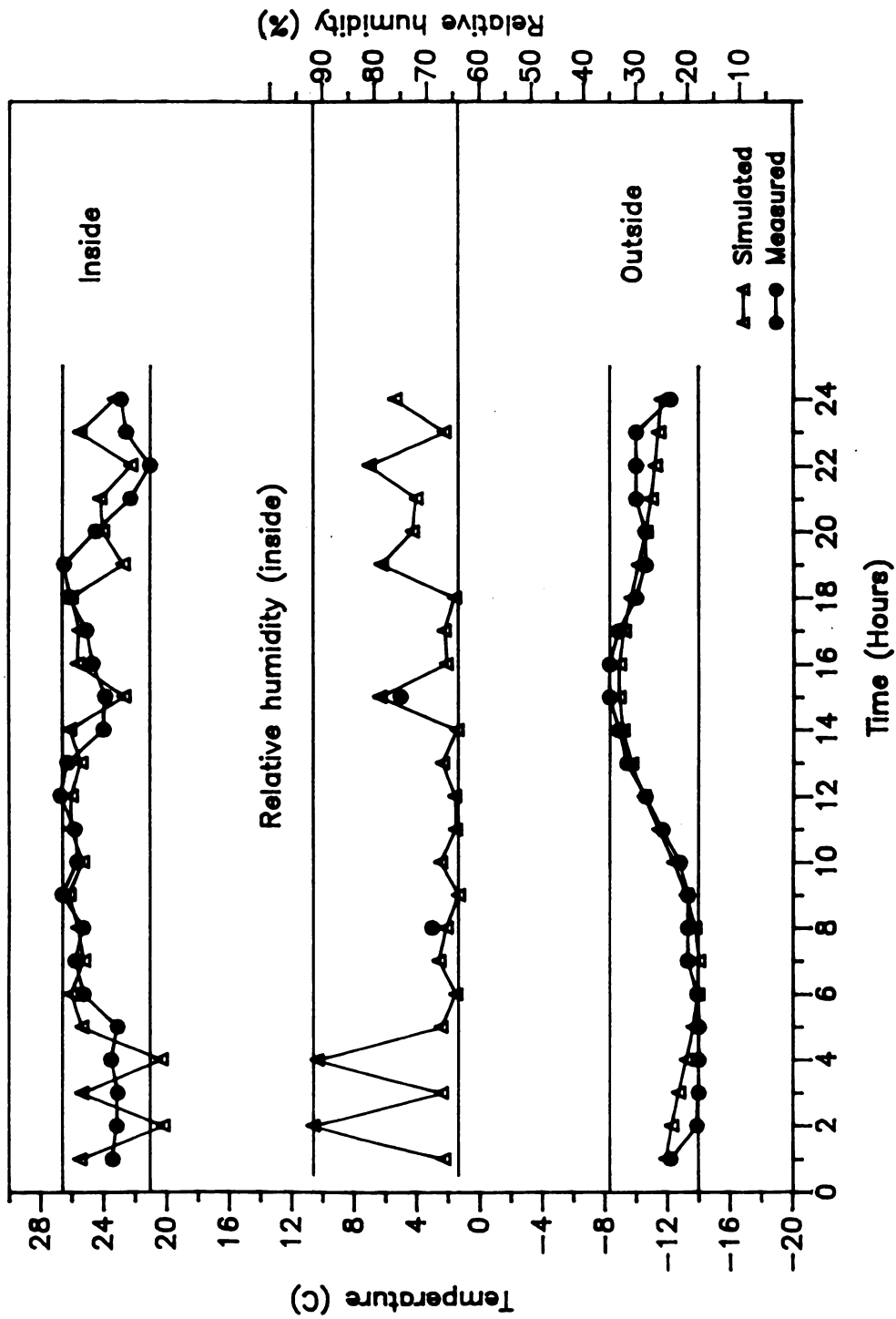


Figure 3.1. Simulated vs. measured temperature, and relative humidity February-13-1986.



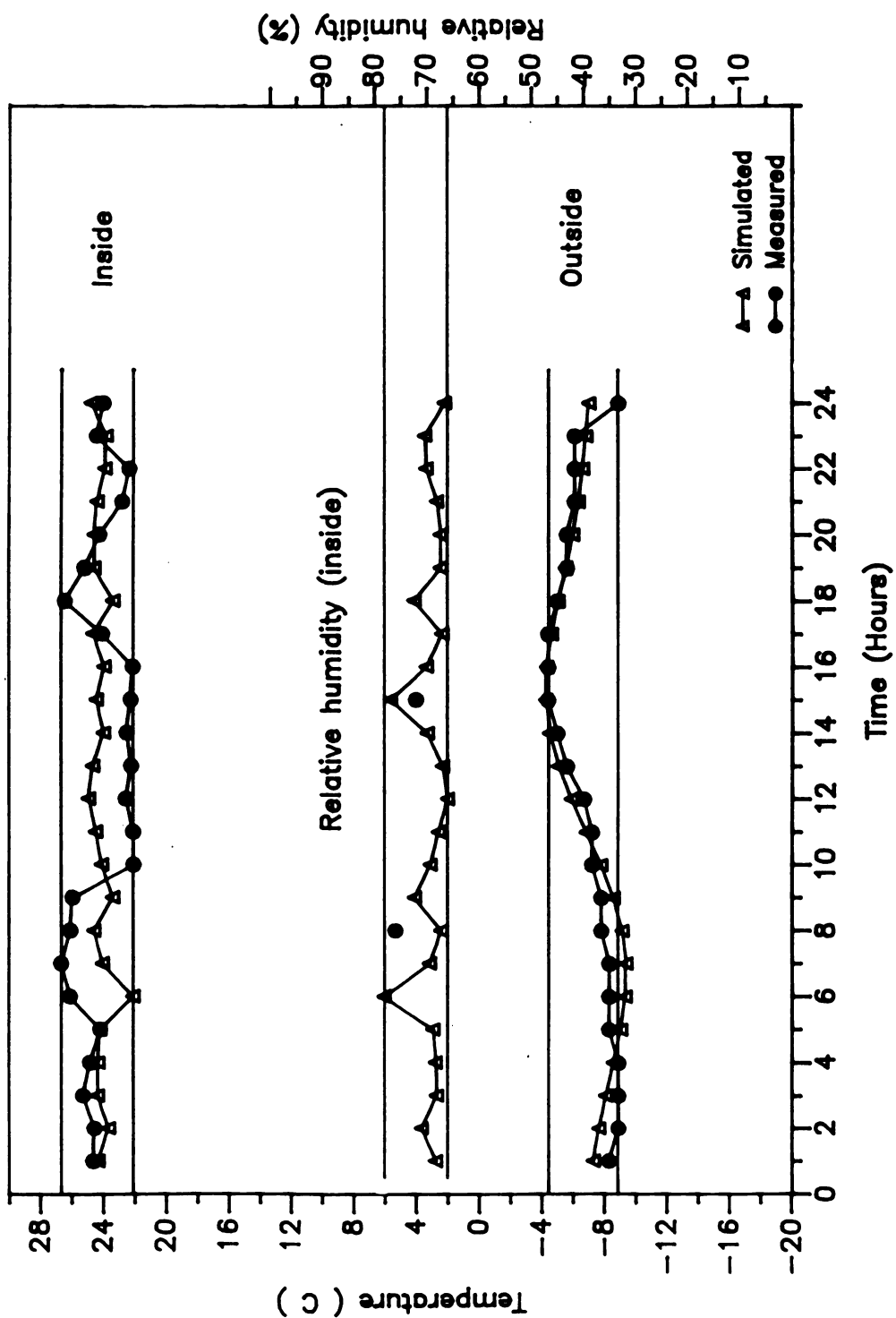


Figure 3.2. Simulated vs. measured temperature, and relative humidity February-16-1986.





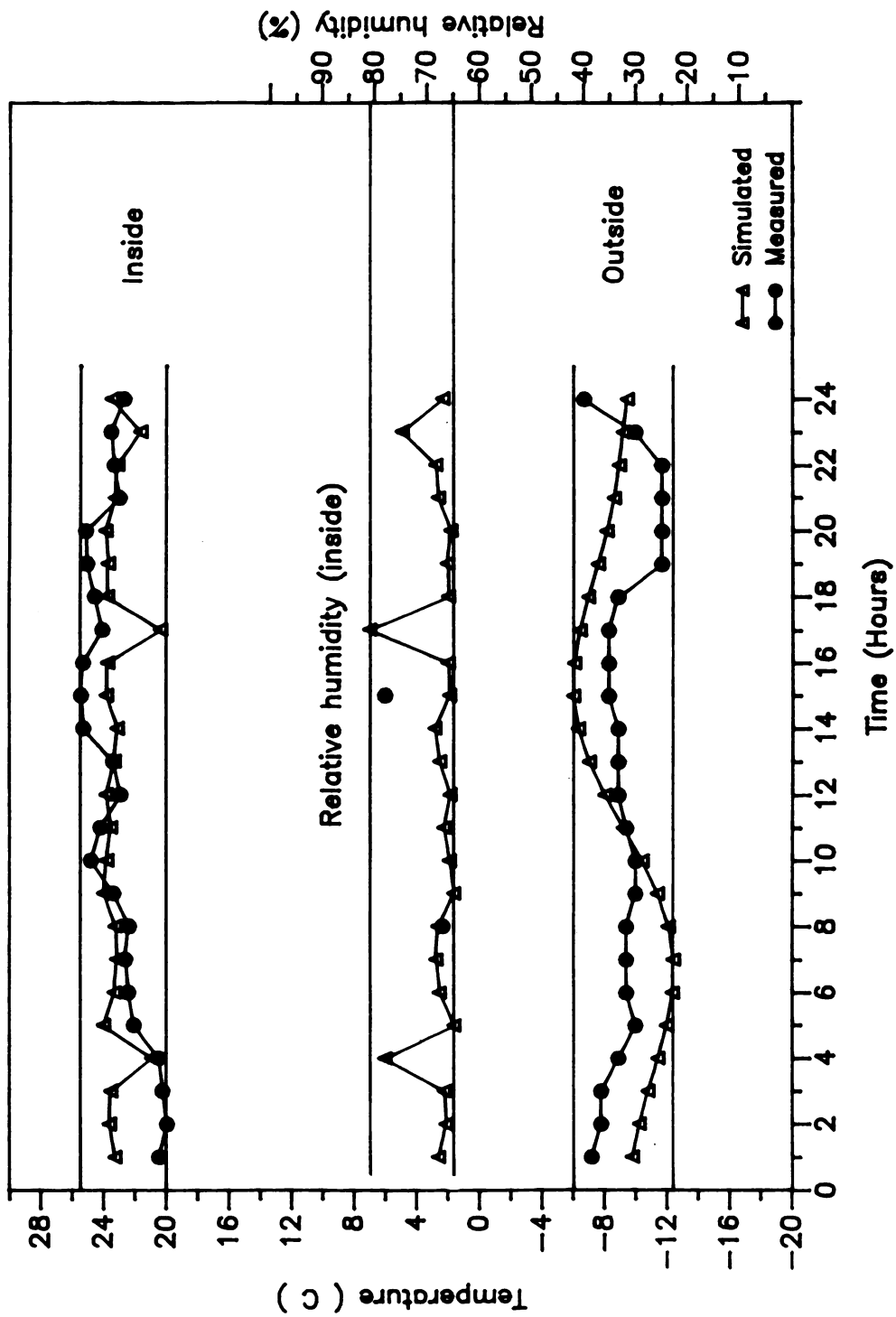


Figure 3.3. Simulated vs. measured temperature, and relative humidity February-27-1986.

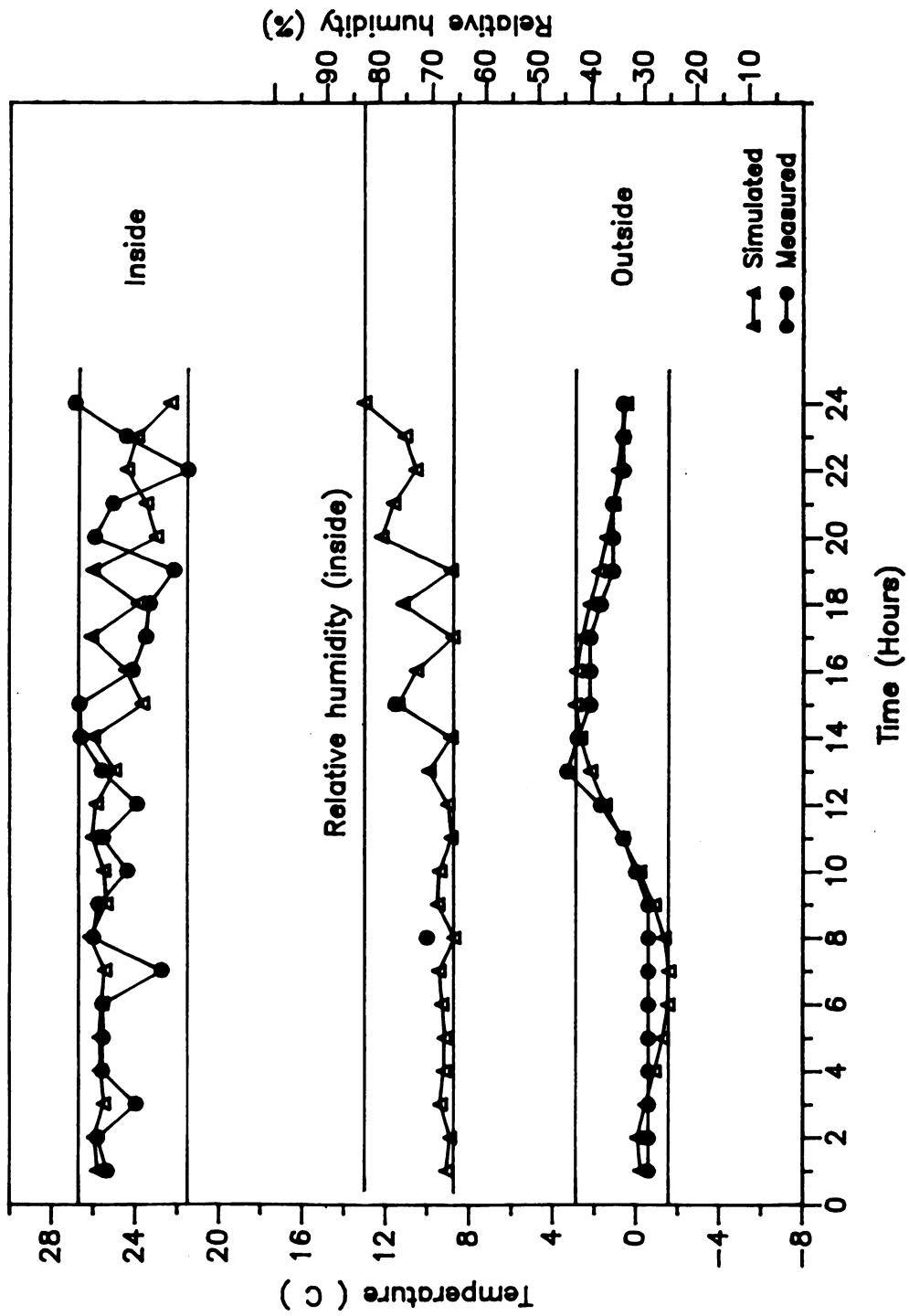


Figure 3.4. Simulated vs. measured temperature, and relative humidity March-3-1986.



Table 3.1. Output Values Simulated and Measured on February 13, 1986

Time Hours	Temperature in Degree C			
	Inside		Outside	
	Measured	Simulated	Measured	Simulated
1am	12.41	25.49	-12.2	-11.93
2	23.14	20.20	-13.9	-12.29
3	23.09	25.37	-14.0	-12.74
4	23.51	20.33	-14.0	-13.23
5	23.09	25.35	-14.0	-13.68
6	25.25	26.06	-13.9	-13.97
7	25.78	25.24	-13.3	-14.02
8	25.28	25.60	-13.3	-13.77
9	26.62	26.20	-13.3	-13.21
10	25.66	25.31	-12.8	-12.40
11	25.81	26.06	-11.7	-11.46
12pm	26.73	26.02	-10.6	-10.51
1	26.27	25.41	- 9.4	- 9.70
2	23.97	26.14	- 8.9	- 9.14
3	23.86	22.66	- 8.3	- 8.89
4	24.66	25.61	- 8.3	- 8.94
5	25.05	25.51	- 8.9	- 9.23
6	26.13	26.02	-10.0	- 9.68
7	26.48	22.72	-10.6	-10.17
8	24.48	24.05	-10.6	-10.62
9	22.28	24.21	-10.0	-10.99
10	21.04	22.24	-10.0	-11.25
11	22.57	25.51	-10.0	-11.46
12	22.89	23.28	-12.2	-11.66
Avg. inside temperature simulated				
				24.61 C
Avg. inside temperature measured				
				24.46 C
Avg. inside relative humidity simulated				
				70.72 %
Avg. inside relative humidity measured				
				72.00 %
Avg. outside temperature simulated				
				-11.46 C
Avg. outside temperature measured				
				-11.46 C
Avg. outside relative humidity simulated				
				78.94 %
Avg. outside relative humidity measured				
				78.00 %
Feed intake simulated (100 birds)				
				10.84 kg/d
Feed intake measured (100 birds)				
				9.92 kg/d
Percent hen - day production simulated				
				81.56 %
Percent hen - day production measured				
				74.51 %
Avg. egg weight simulated				
				61.77 gr
Avg. egg weight measured				
				59.70 gr
Avg. bodyweight simulated				
				1.77 kg
Avg. bodyweight measured				
				1.71 kg

Table 3.2. Output Values Simulated and Measured on February 16, 1986

Time Hours	Temperature in Degree C			
	Inside		Outside	
	Measured	Simulated	Measured	Simulated
1am	24.66	24.34	-8.3	-7.30
2	24.58	23.68	-8.9	-7.66
3	25.31	24.38	-8.9	-8.11
4	24.84	24.33	-8.9	-8.60
5	24.20	24.21	-8.3	-9.05
6	26.13	22.10	-8.3	-9.34
7	26.70	24.06	-8.3	-9.39
8	26.09	24.60	-7.8	-9.14
9	25.95	23.38	-7.8	-8.58
10	22.06	24.10	-7.2	-7.77
11	22.09	24.47	-7.2	-6.83
12pm	22.56	24.92	-6.7	-5.88
1	22.22	24.66	-5.6	-5.08
2	22.50	23.96	-5.0	-4.52
3	22.24	24.42	-4.4	-4.26
4	22.11	23.92	-4.4	-4.31
5	24.07	24.64	-4.4	-4.61
6	26.44	23.36	-5.0	-5.05
7	25.18	24.58	-5.6	-5.54
8	24.24	24.57	-5.6	-5.99
9	22.80	24.40	-6.1	-6.34
10	22.35	23.90	-6.1	-6.62
11	24.44	23.84	-6.1	-6.83
12	24.00	24.78	-8.9	-7.03
Avg. inside temperature simulated				
				24.07 C
Avg. inside temperature measured				
				24.15 C
Avg. inside relative humidity simulated				
				69.09 %
Avg. inside relative humidity measured				
				74.00 %
Avg. outside temperature simulated				
				-6.83 C
Avg. outside temperature measured				
				-6.83 C
Avg. outside relative humidity simulated				
				77.68 %
Avg. outside relative humidity measured				
				87.00 %
Feed intake simulated (100 birds)				
				10.86 kg/d
Feed intake measured (100 birds)				
				10.67 kg/d
Percent hen - day production simulated				
				81.39 %
Percent hen - day production measured				
				74.61 %
Avg. egg weight simulated				
				61.93 gr
Avg. egg weight measured				
				60.15 gr
Avg. bodyweight simulated				
				1.77 kg
Avg. bodyweight measured				
				1.71 kg

Table 3.3. Output Values Simulated and Measured on February 27, 1986

Time Hours	Temperature in Degree C			
	Inside		Outside	
	Measured	Simulated	Measured	Simulated
1am	20.45	23.25	- 7.2	- 9.82
2	19.95	23.61	- 7.8	-10.27
3	20.24	23.51	- 7.8	-10.82
4	20.49	20.91	- 8.9	-11.45
5	22.06	23.98	-10.0	-12.01
6	22.41	23.28	- 9.4	-12.38
7	22.60	23.12	- 9.4	-12.44
8	22.35	23.22	- 9.4	-12.12
9	23.36	23.97	-10.0	-11.42
10	24.79	23.76	-10.0	-10.42
11	24.18	23.50	- 9.4	- 9.23
12pm	22.89	23.80	- 8.9	- 8.05
1	23.38	23.29	- 8.9	- 7.04
2	25.28	23.07	- 8.9	- 6.34
3	25.42	23.78	- 8.3	- 6.03
4	25.28	23.70	- 8.3	- 6.09
5	24.04	20.33	- 8.3	- 6.46
6	24.54	23.72	- 8.9	- 7.01
7	25.03	23.67	-11.7	- 7.63
8	25.12	23.84	-11.7	- 8.20
9	22.97	23.23	-11.7	- 8.65
10	23.31	23.11	-11.1	- 8.98
11	23.51	21.62	-10.0	- 9.23
12	22.69	23.46	- 6.7	- 9.49
Avg. inside temperature simulated				
				23.20 C
Avg. inside temperature measured				
				23.18 C
Avg. inside relative humidity simulated				
				68.01 %
Avg. inside relative humidity measured				
				73.00 %
Avg. outside temperature simulated				
				-9.23 C
Avg. outside temperature measured				
				-9.23 C
Avg. outside relative humidity simulated				
				80.71 %
Avg. outside relative humidity measured				
				69.71 %
Feed intake simulated (100 birds)				
				11.10 kg/d
Feed intake measured (100 birds)				
				10.23 kg/d
Percent hen - day production simulated				
				79.13 %
Percent hen - day production measured				
				76.56 %
Avg. egg weight simulated				
				62.26 gr
Avg. egg weight measured				
				60.80 gr
Avg. bodyweight simulated				
				1.77 kg
Avg. bodyweight measured				
				1.71 kg

Table 3.4. Output Values Simulated and Measured on March 3, 1986

Temperature in Degree C				
Time Hours	Inside		Outside	
	Measured	Simulated	Measured	Simulated
1am	23.33	25.80	-0.6	-0.24
2	25.80	25.96	-0.6	-0.08
3	23.96	25.49	-0.6	-0.47
4	25.57	25.66	-0.6	-0.90
5	25.52	25.69	-0.6	-1.29
6	25.56	25.57	-0.6	-1.55
7	22.73	25.43	-0.6	-1.60
8	26.01	26.15	-0.6	-1.37
9	25.75	25.38	-0.6	-0.88
10	24.35	25.48	0.0	-0.18
11	25.52	26.02	0.6	0.65
12pm	23.90	25.85	1.7	1.48
1	25.59	24.97	3.3	2.18
2	26.61	26.00	2.8	2.67
3	26.66	23.64	2.2	2.90
4	24.10	24.43	2.2	2.85
5	23.47	26.09	2.2	2.59
6	23.30	23.85	1.7	2.20
7	22.13	26.02	1.1	1.77
8	25.93	22.99	1.1	1.38
9	25.05	23.47	1.1	1.06
10	21.47	24.40	0.6	0.83
11	24.44	23.93	0.6	0.65
12	26.90	22.31	0.6	0.47
Avg. inside temperature simulated			25.02	C
Avg. inside temperature measured			24.82	C
Avg. inside relative humidity simulated			70.62	%
Avg. inside relative humidity measured			74.00	%
Avg. outside temperature simulated			0.65	C
Avg. outside temperature measured			0.65	C
Avg. outside relative humidity simulated			68.74	%
Avg. outside relative humidity measured			92.00	%
Feed intake simulated (100 birds)			10.78	kg/d
Feed intake measured (100 birds)			9.81	kg/d
Percent hen - day production simulated			78.58	%
Percent hen - day production measured			75.36	%
Avg. egg weight simulated			62.26	gr
Avg. egg weight measured			61.10	gr
Avg. bodyweight simulated			1.77	kg
Avg. bodyweight measured			1.77	kg



Table 3.5. Average Daily Inside Temperatures Measured and Simulated from February 13 to March 3, 1986

Date	Average Daily Temperature °C	
	Measured	Simulated
February 13	24.46	24.61
16	24.15	24.07
27	23.18	23.20
March 3	24.82	25.02
Mean	24.15	24.22
SD	0.704	0.786

Average hourly deviation = 0.11

Average daily deviation = 0.18

Percent of error for hourly deviation = 0.5%

predict the hourly outside temperature and relative humidity. Ventilation rate calculated from the model (February 13) for early morning hours (1 a.m. to 5 a.m.) was between 0.2 and 0.29 m<sup>3</sup>/hr/bird, the measured was fixed on 0.2 m<sup>3</sup>/hr/bird, but the air infiltration could add to it and increase the air flow. The maximum air flow predicted at 4 p.m. was 0.5 m<sup>3</sup>/hr/bird.

The model had a tendency to fluctuate in the morning hours, especially on day February 13, Figure 3.1, which may be caused by the model's trying to adjust the temperature inside while the temperature outside was going down (simulated). The control routine of the model has a fixed increment to control the air flow, which may not be good for all the times to adjust the ventilation rate to keep the inside temperature in the specified range. So the temperature was allowed to drop to the minimum allowed. This air flow rate was assumed to occur for the entire hour. However, the real temperature (measured) was about constant for about 5 hours. Otherwise, the model predicted very good estimates of hourly inside temperatures after that.

On day March 3, Figure 3.4, the model and the measured data followed each other until 3 p.m. (hour 15) which then the measured and the simulated starts to fluctuate. The measured data could be effected by the

thermostat setting when outside temperature is high. But the fluctuation of the model is still in the range of the measured data, Table 3.4, the daily average of inside temperature measured and simulated were 25.02 C and 24.82 C, respectively, with a difference of 0.2 C. The average relative humidities were 74.00% and 70.62% measured and simulated, respectively.

Mean deviation between actual and predicted average daily inside temperature for all runs was 0.18 C with standard deviation of 0.43. Table 3.5 shows the average daily temperatures measured and simulated for the period from February 13 to March 3.

Percent of error for the same period for the average hourly deviation was 0.5%, compared to 5% from Phillips (1970). The results also statistically tested by paired comparison, for all runs and found that the means of these examples were not significantly different.

The model predicting very accurate average daily temperatures compared to the actual average temperatures. This will support the prediction of feed consumption which is calculated based on the daily average temperature.

It was necessary to adjust the simulation model to give results similar to the collected data. During this period of evaluation, it was found useful to compare

initial inputs values and intermediately calculated values. Special adjustment made on day February 8, an increase in moisture evaporation from the manure made the model predict inside temperatures more closely to the actual.

The inputs for this model were average daily temperatures and the temperature amplitude. To evaluate the model's ability to predict inside conditions, these inputs were taken from the NOAA for Lansing, Michigan, and used to predict hourly outside temperature and relative humidity. The weather model was predicting very close to data. The curve shape matched the actual data closely in Figure 3.1, 3.2, and 3.4.

The feed consumption and egg production models (management model), which include prediction of feed consumption based on 100 bird per day in kg, metabolizable energy per bird in kJ per day, hen-day production in percent, estimated egg production for 100 bird in kg per day. The second part of this model is the cost calculations and that includes feed cost per 1,000 bird as a common base, electricity cost/1,000 bird in dollars per day, and egg sale calculated based on nest run price for that day, then the revenue margin (revenues-cost) for that day is calculated and the value is displayed in \$/day.

The above parameters were compared to measured data or supplied by the management manual for Hy-Line chickens breed W-36. Tables 3.1 to 3.4 shows the simulated values and the measured values for each day.

Feed intake for February 13, Table 3.2, (age 50 weeks) was 10.83 kg/day/100 bird simulated, the measured was 9.92 kg/day/100 birds, and comparing with the management manual was 9.9 kg/day/100 bird. The percent hen per day production was 81.56% simulated comparing to 74.51% measured on 50th week, and the manual estimated it to be 80%. Egg production prediction from the model was 61.77 g/da/bird, the measured was 59.70 g/day/bird, and the management manual for this breed estimate was 61.70 g/day/bird.

Bodyweight was also calculated based on age of the chickens. The simulated value was 1.77 kg, comparing with 1.71 kg according to the management manual. Electricity costs were calculated based on number of hours the fans were operated. The simulated value was 0.134 \$/day/1,000 bird, the measured was 0.10 \$/day. No fuel costs were calculated.

The mean deviation for all runs between measured and simulated were, for feed intake 0.796 kg/100 bird, egg weight 1.708 g/day/bird and for the bodyweight 0.06 kg.

Some of the differences in the management information could be caused by conditions that may have occurred that week; for example, health, stress, feed, and management practices. In general, the model is a useful tool to evaluate different parameters, for instance, inside temperature, ventilation rate, feed intake, and egg production. The model gives very accurate average daily inside temperatures.

Carbon dioxide concentration could vary by using different ventilation rates. Allowable concentration of  $\text{CO}_2$  in hen houses were discussed in Kadlec (1969). Concentrations in the range 0.25% to 0.5% have no harmful effect on production. Concentration between 0.5% to 2.5% have a small effect on production between 2.5%, and above 5%,  $\text{CO}_2$  concentration is dangerous and will effect health, production, and may increase mortality, especially with combination of other gases and high temperature.

The minimum ventilation rate for carbon dioxide control was  $0.2 \text{ m}^3/\text{hr}/\text{bird}$ . When air flow was reduced below that necessary for control of moisture ( $0.43 \text{ m}^3/\text{hr}/\text{bird}$ ), uniform distribution of fresh air throughout the room may not be achieved. Measurement of  $\text{CO}_2$  in various locations were made to determine the adequacy of

CO<sub>2</sub> removal from all locations of the room, and to appraise the air distribution.

For February 13, Figure 3.5, CO<sub>2</sub> concentration in location #2, ranged from 0.41% to 0.70%. Location #3 from 0.42% to 0.55%, location #4 from 0.30% to 0.52%, and location #5 from 0.5% to 0.6%. All these ranges fall in the allowable concentration of CO<sub>2</sub>, where no effect on health or production would be anticipated. Other day, Figure 3.6 has similar patterns.

The sudden drop in CO<sub>2</sub> level in location #2, Figure 3.5, was caused by operation of second phase fan in the adjacent room (white) at 4 a.m.

Carbon dioxide could be deadly in case of electricity failure or stoppage of fans. Figure 3.7 shows the quick increase in CO<sub>2</sub> concentration reaching the harmful level of 2% in about 2 hours and 20 minutes. The rate of CO<sub>2</sub> production calculated was 714 cm<sup>3</sup>/hr/bird measured and the simulated was 734 cm<sup>3</sup>/hr/bird. A combination of high levels of CO<sub>2</sub> from 2% to 5% and high temperature (30 C) in tight buildings will contribute to very high mortality. The highest level of CO<sub>2</sub> was in location #5, and the lowest at location #3 at 10 p.m.

Ammonia concentration was constant about all the time during the test days, and it was always below the maximum limit of 50 PPM. This could be effected by the





kind of feed used, and the two time cleaning the manure pit.

Using low ventilation rate of  $0.2 \text{ m}^3/\text{hr}/\text{bird}$  in winter as ventilation rate for carbon dioxide control (minimum ventilation rate) will give better manipulation of air exchange in the poultry house, and to maintain the temperature in the thermoneutral zone, without exceeding the maximum allowable concentration of  $\text{CO}_2$ .

The mean deviation between the average hourly carbon dioxide concentration measured for both days Figures 3.5 and 3.6, and the simulated were 10.05%. The prediction of carbon dioxide for both days was satisfactory and fell in the range of  $\text{CO}_2$  measured.



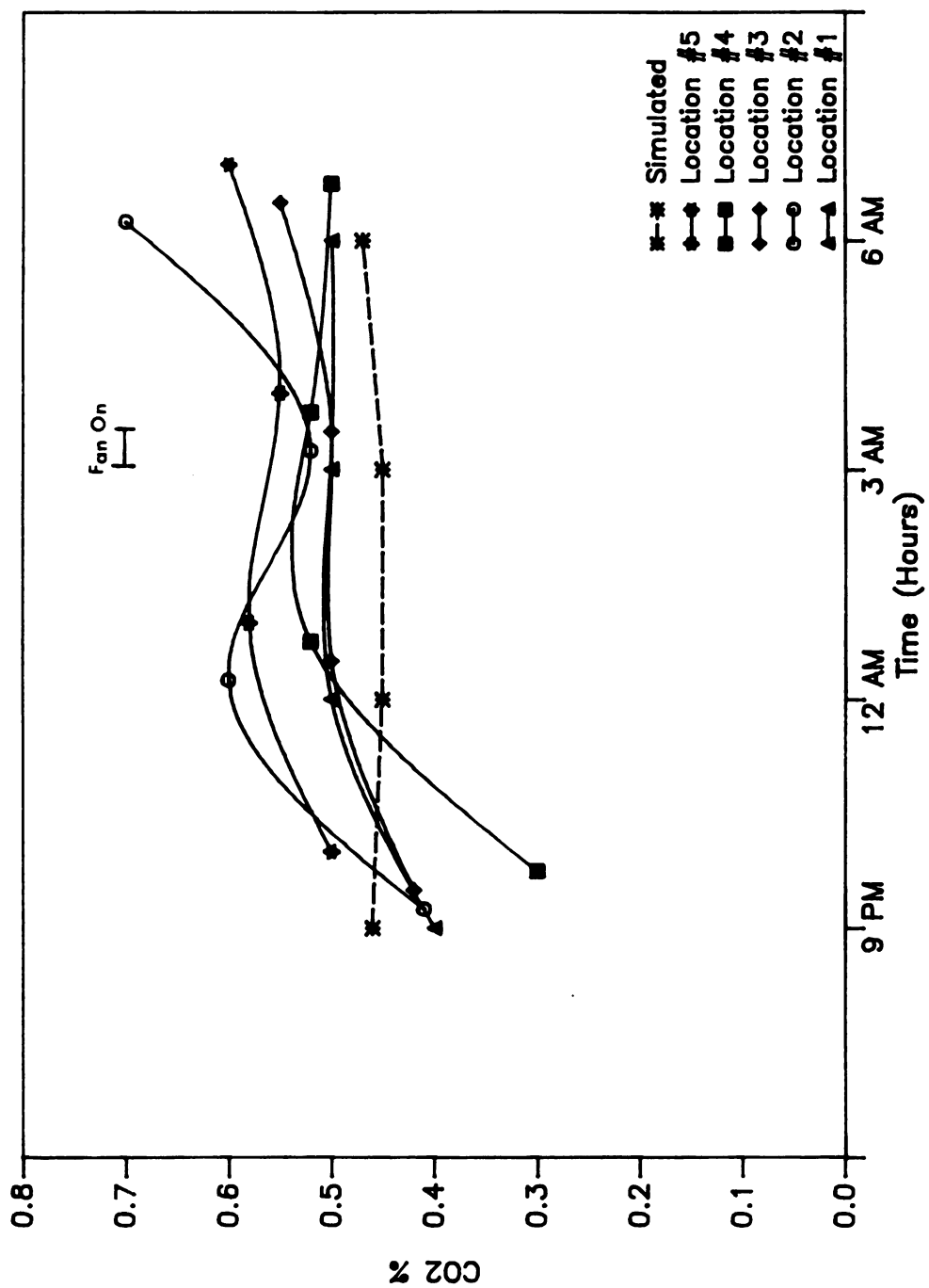


Figure 3.5. Carbon dioxide concentration vs. time  
February-11-1986

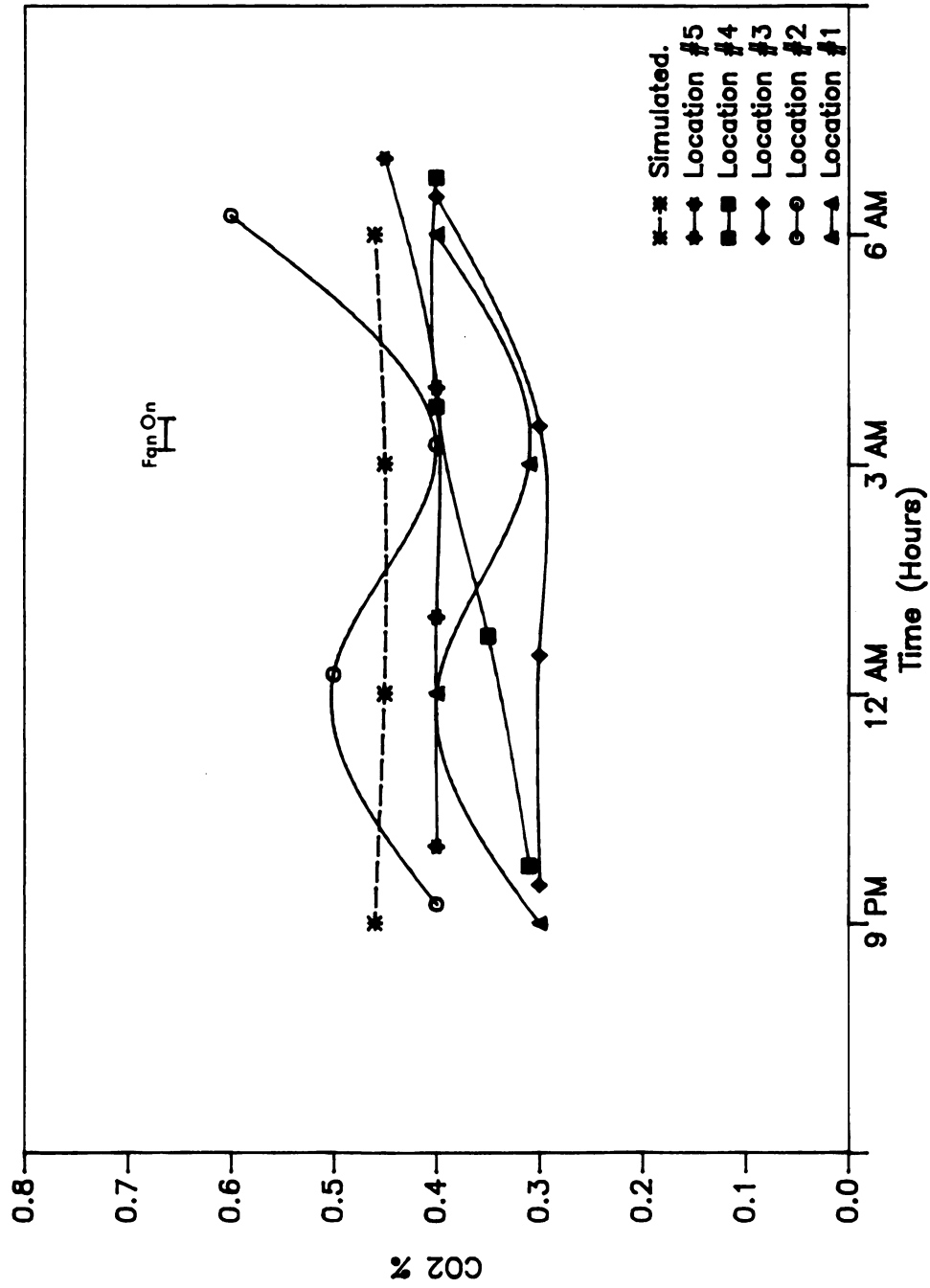


Figure 3.6. Carbon dioxide concentration vs. time  
February-21-1986

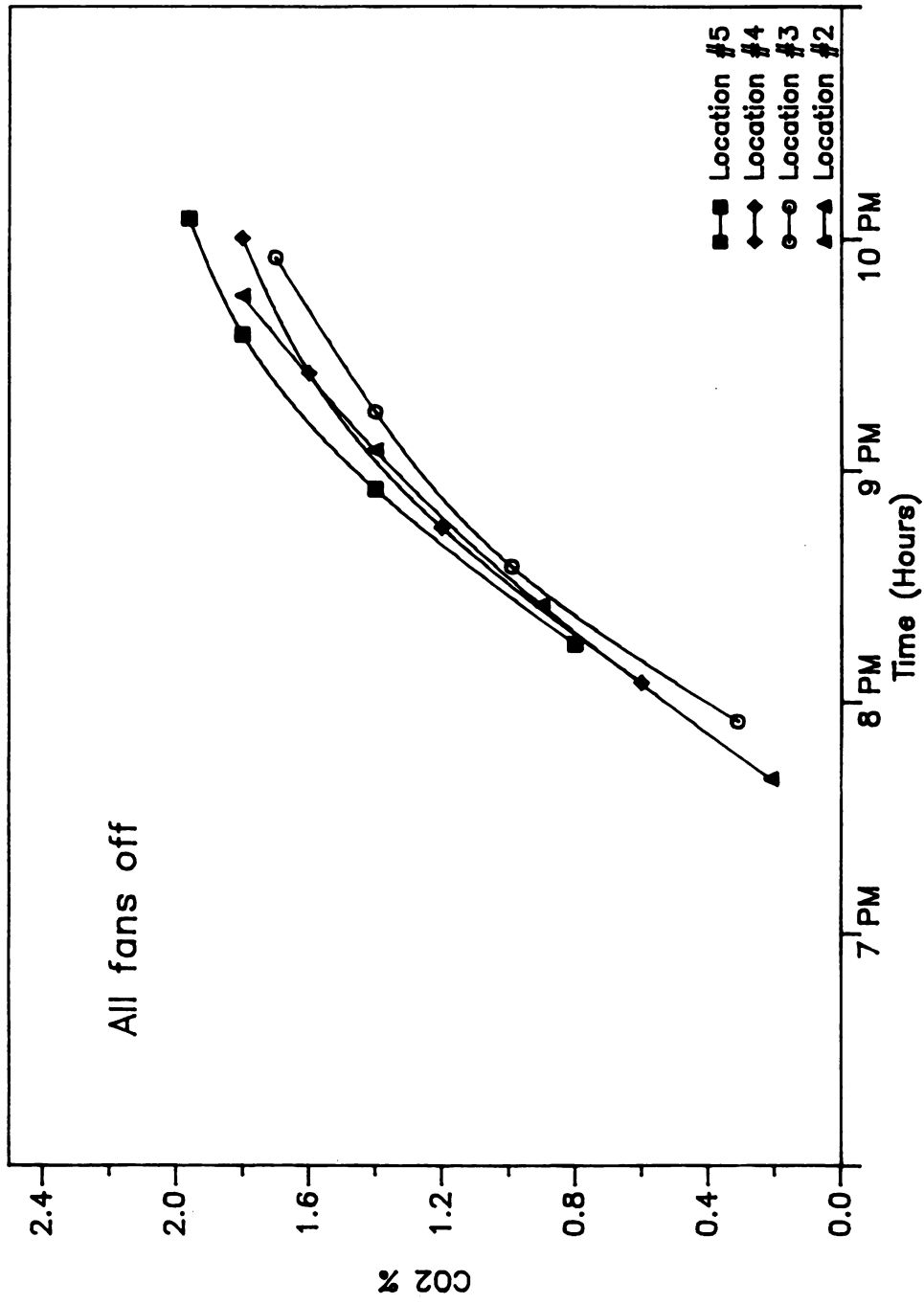


Figure 3.7. Carbon dioxide concentration vs. time  
February-18-1986

## CHAPTER IV

### RESULTS FROM MODEL USE

One of the applications of the model is to decide what ventilation rate should be used to maximize revenues over costs when the outside temperature is very low. Two alternatives that may be considered are:

1. Ventilate at a rate to control carbon dioxide.
2. Ventilate at a rate that will control moisture. (Fixed ventilation rate.)

The simulation model was used to estimate and evaluate differences in revenue margins between the two control strategies. A common base for expressing financial performance measures in the commercial egg industry is per 1,000 bird units. This base will be used in calculating and presenting the evaluation criterion. The revenue margin (RM) is defined as value of egg sales minus feed and electricity costs per 1,000 birds.



$$RM = ES - (FC + EC) \quad (4.1)$$

where

FC = Feed cost \$/day

ES = Egg sale \$/day

EC = Electricity cost \$/day

Decision analysis has become an important technique in the solution of business problems of this type. The decision analysis method is accomplished by listing available courses of action, expressing subjective variables quantitatively, and determining possible economic returns.

When the data are put in order, the result is that decision analysis becomes a powerful tool for determining optimal courses of action. The returns of laying hen operation is dependent on the biological response of chickens to their environment and to market conditions.

The evaluation criterion used for this application is the Expected Value (EV). This criterion incorporates the probability of an event (state of nature) occurring into the decision or evaluation process. The probability is a quantitative measurement of the degree of certainty associated with the occurrence of an event. The evaluation decision rule is to select



the alternative that has the greatest revenue margin. A decision tree is a graphic presentation that shows a sequence of strategic decisions and the expected consequences under each possible state of nature or circumstances. A decision is symbolized by a square and noncontrollable events by a circle. The revenue margin of each branch is multiplied by its joint probability of possible state of nature and then summed with other branches to get the expected value (EV) of each age, and each strategy. The equation of EV would be as follows:

$$EV = \sum_{i=1}^n P_i \times V_i \quad (4.2)$$

where

$P_i$  = Probability of event  $V_i$  occurring.

Then the expected value for age 25 weeks will be calculated as:

$$\begin{aligned} EV_{25} &= (0.03 \times 14.93) + (0.24 \times 15.03) + (0.73 \times 15.07) \\ &= 15.06 \text{ \$/day} \end{aligned}$$

A summary of E.V. calculations is in Table 4.1 and the decision analysis is in Figures 4.1. and 4.2.

The usual laying period for the hens is about 76 weeks, when pullets are put in production from 18 weeks of age. Some assumptions have been made for the duration



Table 4.1. Output Values for Decision Analysis for Expected Values (E V)

Ventilation Rate m <sup>3</sup> /hr	Age Weeks	Avg. Temperature C		Expected Values	Total
		Outside	Inside		
Carbon Dioxide Ventilation Rate (840)	25	-20	19.70	0.45	
		-15	22.05	3.61	
		-10	23.45	11.00	
					15.06
	40	-20	22.88	0.44	
		-15	24.28	3.59	
		-10	24.58	10.92	
					14.95
Moisture Control Ventilation Rate (1394)	25	-20	17.94	0.44	
		-15	21.42	3.58	
		-10	22.99	10.92	
					14.97
	40	-20	19.45	0.43	
		-15	22.43	3.51	
		-10	24.36	10.86	
					14.80

Revenue Margin

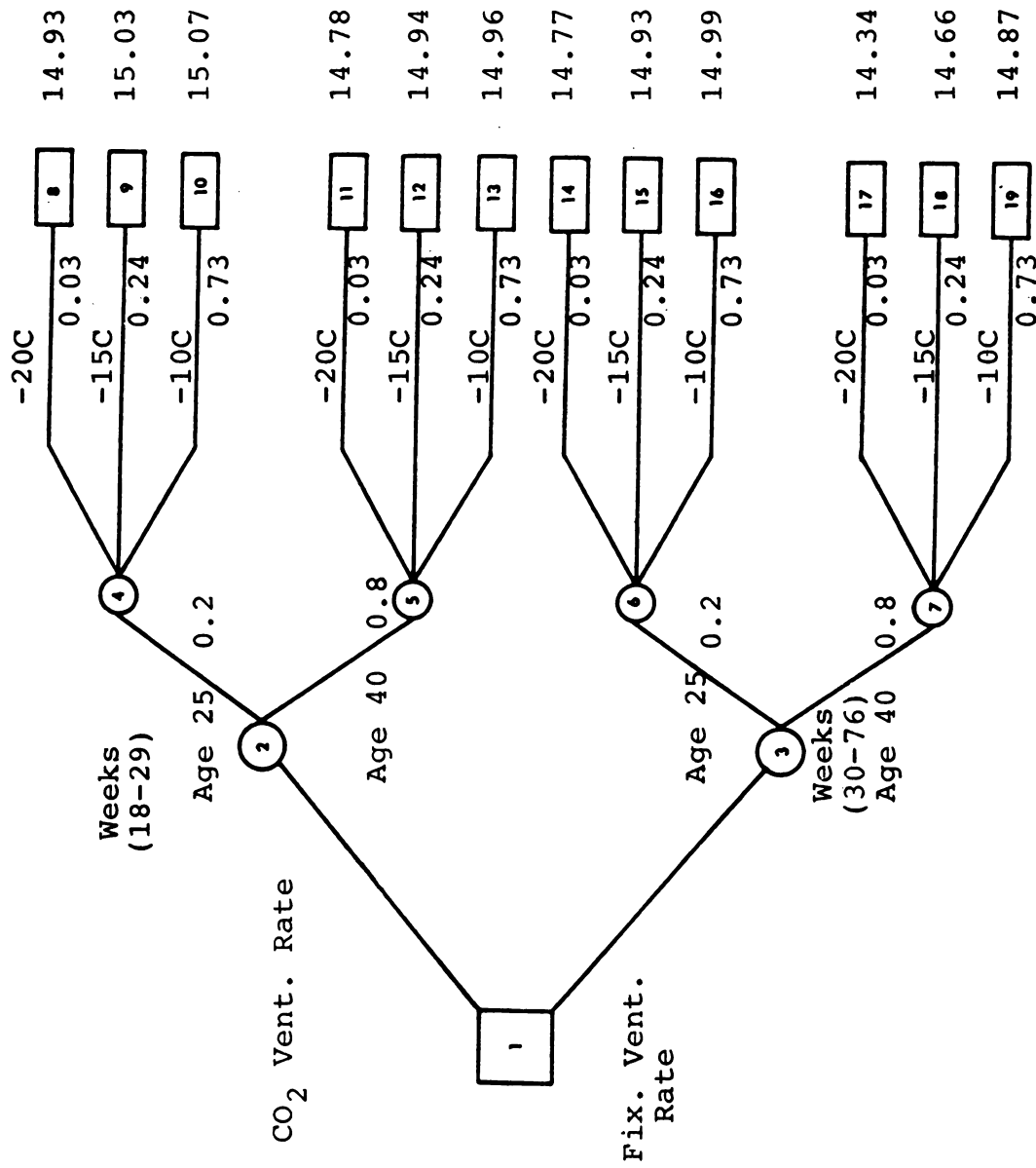


Figure 4.1. Decision Analysis Inputs, Revenue Margins and Probabilities.

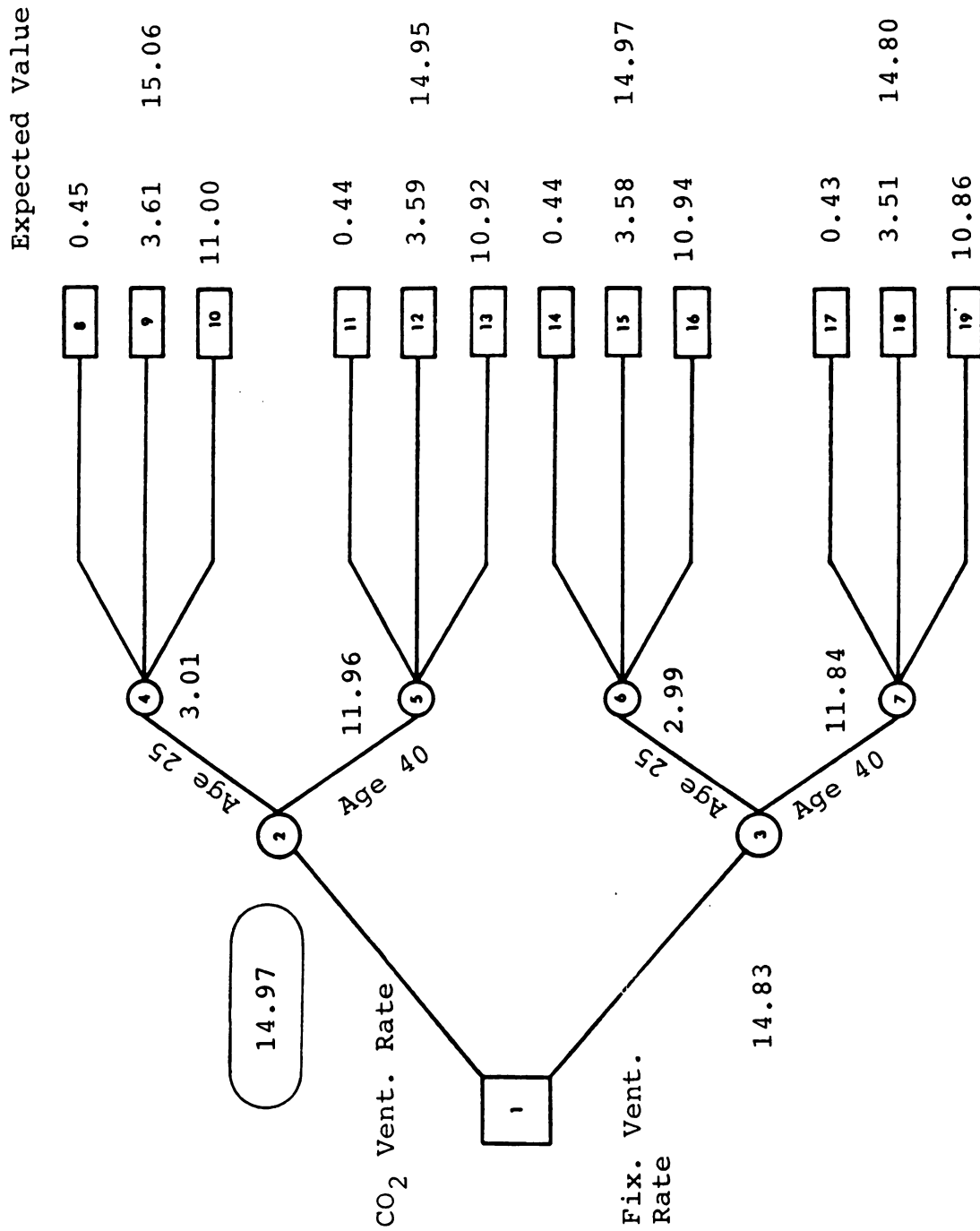


Figure 4.2. Decision Analysis Expected Values

of age. The laying period is divided into two periods. First period from age 18 through 29 weeks, which encompasses 11 weeks of production. In this period the chickens are small in size, their bodyweight is not reached the standard (growing) and they are not mature. A representative age is chosen for this period (18 to 29 weeks) and that is 25 weeks. This age reflects the variability in bodyweight and production. The second period, 30 to 78 weeks, when the chickens reach their stable bodyweight, maturity, and they are well adapted to production conditions. The representative age chosen for this period (47 weeks) is 40 weeks.

The duration proportions calculated for each period are as follows:

$$29 - 18 = 11 \text{ weeks first period duration}$$

$$76 - 30 = 47 \text{ weeks second period duration}$$

$$11 + 47 = 58 \text{ weeks production period duration}$$

then

$$\frac{11}{58} = 0.19 \approx 0.2 \text{ duration proportion for first period}$$

$$\frac{47}{58} = 0.81 \approx 0.8 \text{ duration proportion for second period}$$

These duration proportions will be used to weight the two alternatives selected as representative production situations.

The weather data used in this evaluation are based on 83 years (1889 - 1980) for Jackson, Michigan, supplied by NOAA and NWS, Table 4.2 is used to calculate the probabilities for outside temperatures.

Three ranges of temperatures were chosen to represent outside conditions. They are from  $>0$  to  $<-10$  C, from  $-10$  to  $<-20$  and from  $-20$  to  $-30$ . The representative temperature for each range used in the model were  $-10$ ,  $-15$ , and  $-20$  C, respectively. The probability for each range then calculated by dividing the total number of days for each range by the number of winter days in 83 years for the period from November through March (5 months).

$$\text{Number of days} = 151 \times 83 = 12,533 \text{ days}$$

For  $-20$  C range, the probability is calculated as:

$$\frac{(328 + 42)}{12,533} = 0.0296 \approx 0.03$$

The same procedure is used to calculate other range probabilities. They are 0.03, 0.24, and 0.73 from the lowest to the highest range.

Assumptions were also made for the market price of product and input factors. A representative price level for egg, feed, and electricity were used: 0.45 \$/doz for

Table 4.2. Weather Information Used in Decision  
Analysis 1889-1980 (83 Years)

Ranges C	Jan.	Feb.	Mar.	Nov.	Dec.	Total
Frequencies of Occurrences						Days
> 0 to <-5	697	612	1061	1055	886	4311
- 5 to <-10	771	755	700	418	816	3460
-10 to <-15	645	561	307	83	469	2065
-15 to <-20	373	332	76	7	214	1002
-20 to <-25	141	122	15	2	48	328
-25 to -30	18	23	0	0	1	42
Number of Years with Hits						Years
> 0 to <-5	79	81	82	82	82	83
- 5 to <-10	82	82	82	79	82	83
-10 to <-15	82	82	72	37	81	83
-15 to <-20	72	69	34	6	55	82
-20 to <-25	49	44	11	2	26	65
-25 to -30	13	13	0	0	1	23



nest run egg price, 0.16 \$/kg for feed, and 0.06 \$/kWh for electricity.

The expected values for the two strategies being evaluated in this application are 14.97 \$/day for carbon dioxide control ventilation rate, and 14.83 \$/day for moisture control ventilation rate. The maximum expected value revenue margin (MEVRM) of 14.97 \$/day was achieved by using or implementing the carbon dioxide control ventilation rate. The difference of the two strategies in RM is 0.14 \$/day. This value becomes more significant in a large production operation, where a 100,000 bird house capacity or greater may be utilized. The number of cool days in the winter season has an important impact on choosing the appropriate ventilation rate. Other factors that could be listed in this discussion are: age of chickens, production level, feed prices, egg and other inputs which the manager must take into consideration.

To evaluate this problem for different conditions, egg sale price was fixed as 0.45 \$/dozen nest run price for all following runs. The feed and electricity prices were doubled and then the model used to predict the new revenue margins. The expected values were calculated by using equation (4.2). When the price of the feed doubled to 0.32 \$/kg, both strategies lost money. The minimum losses were with using lower ventilation rates to control



carbon dioxide, with minimum expected value of -1.50 \$/day, compared to -1.64 \$/day. The difference between both values was 0.14 \$/day.

Another run was made to evaluate the two strategies under electricity price change only. The price of electricity was doubled to 0.12 \$/kW hr. The expected values also calculated, and the final evaluation was to use lower ventilation rates to control carbon dioxide instead of moisture control ventilation rate. The maximum expected value achieved with low ventilation rate was 14.88 \$/day, compared to 14.74 \$/day, and the difference was 0.14 \$/day, the same as previous runs.

Using lower ventilation rates ( $0.2 \text{ m}^3/\text{hr}/\text{bird}$ ) could cause water condensation on the walls or equipment, but this problem was not serious from the observations made during the data collection and also from the model prediction. Hours of water condensation predicted for the runs from February 13 through March 3 were 10, 1, 3, and 0 hours, respectively. The water condensation usually occurred in early morning hours and in the night. From the observation made, water condensation occurred on the lower part of the walls and outside door. No water condensation was as noted on the cages or other equipment in the poultry house.

Higher ventilation rates ( $0.43 \text{ m}^3/\text{hr}/\text{bird}$ ) did not prevent water condensation on the walls; predicted hours of water condensation were between 6 and 4 hours.

Lower ventilation rates based on controlling carbon dioxide in poultry houses could be used to achieve higher temperatures, and savings without effecting egg production, or creating health problems.

However, for prudent management at low ventilation rates of  $0.2 \text{ m}^3/\text{hr}/\text{bird}$ , monitoring  $\text{CO}_2$  is mandatory. The width of commercial layer houses are typically more than the 17 m width structure used in this study. With low ventilation rates, it is possible that the carbon dioxide levels in the middle of the poultry house could exceed allowable levels. This may result in increased mortality or reduced performance levels unless special provisions are made for effective air distribution at these low air flow rates.

Table 4.3. Output Values from the Model Used in Decision Analysis

Ventilation rate m <sup>3</sup> /hr	Age Weeks	Avg. Temperature C		Feed Intake kg/day/100 b
		Outside	Inside	
Carbon Dioxide Control Ventilation Rate (840)	25	-20	19.70	10.138
		-15	22.05	9.878
		-10	23.45	9.693
	40	-20	22.88	10.678
		-15	24.28	10.459
		-10	24.58	10.407
	25	-20	17.94	10.304
		-15	21.42	9.953
		-10	22.99	9.756
Moisture Control Ventilation Rate (1394)	40	-20	19.45	11.105
		-15	22.43	10.742
		-10	24.36	10.444

## CHAPTER V

### SUMMARY AND CONCLUSIONS

#### 5.1 Summary

A simulation model which predicts hourly temperature, relative humidity, maximum, minimum temperatures, average daily temperature for inside and outside conditions, and management information, including feed consumption, feed costs, metabolizable energy, egg production, and electricity costs, bodyweight, mortality rate, and ventilation rates used in evaluation of poultry laying house was prepared and verified. The simulation model was based on psychrometric and biological relationships for laying hens.

The basis of the simulation model and the test facilities for model verification was a commercial-type laying house near East Lansing, Michigan. The laying house has a capacity of approximately 4,100 hens in each room: system was managed as small commercial unit at Michigan State University Poultry Science Research and Training Center.

Verification data collected on five winter days compared satisfactorily with the simulation.

The carbon dioxide ventilation rate control was used as minimum ventilation rate in cool days to replace the ventilation rate for moisture control. Carbon dioxide and ammonia were under control with a ventilation rate of  $0.2 \text{ m}^3/\text{hr}/\text{bird}$  ( $0.12 \text{ CFM}/\text{bird}$ ).

The model gives very close predictions of feed consumption, H-D production, metabolizable energy, and egg production compared with the measured data and management manual for the Hy-Line breed W-36.

## 5.2 Conclusions

The following conclusions are the result of preparing and verifying the simulation model of estimate the hourly inside, outside dry-bulb temperature and relative humidity, and management information.

1. Ventilating at 47% of the rate commonly used for moisture control to provide adequate environmental conditions was accomplished successfully under the climatic conditions that existed.

2. Lower ventilation rates helped maintain higher inside temperature which lowered feed consumption and improved revenue margins for cooler days.

3. The data from the simulation model matched the experimental winter psychrometric data satisfactorily.

4. Ammonia concentrations were well below maximum allowable concentrations (<35 PPM) even with low ventilation rate which was used in this study.

5. For the climatic conditions studied, water condensation occurred only for short durations, but it did not last all day.

6. At the low air flow rate, mixing of outside air with the inside was very good, and adequate, based on uniformity of CO<sub>2</sub> and temperature in various locations.

7. Carbon dioxide did not exceed the maximum allowable level in any location.

8. The simulation model provided a means of effectively evaluating the controllable management and design factors for the environment in a poultry house.

9. Data generated from the simulation model is useful in making economical analysis to evaluate different strategies or situations.

### 5.3 Recommendations for Further Research

The results of this research suggests the need for additional work in the following areas:

1. This model was not tested or evaluated for options already built in the simulation. It is recommended to explore this simulation model for different conditions.



2. Additional studies be conducted to determine and improve the egg production model.

3. Investigation of bird heat production under conditions of diurnally varying temperatures.

4. Develop a single function which can make a smoother transition between day and night rates than the two separate linear interpolations used in this study.

5. Expansion of the model so that it could be used to simulate environment conditions, feed consumption and egg production responses throughout an entire year. This would allow evaluation of alternative energy and environmental management strategies for any period of time.



## APPENDICES



## APPENDIX A

### TABLES

Table A.1. Carbon Dioxide and Ammonia Concentration  
Measured on February 11, 1986

Time	Location	CO <sub>2</sub> %	NH <sub>3</sub> ppm	Temperature C
9:00 pm	1	0.40	20	22.92
9:15 pm	2	0.41	15	22.52
9:30 pm	3	0.42	15	22.87
9:45 pm	4	0.30	20	21.85
10:00 pm	5	0.50	15	22.48
12:00 am	1	0.50	30	23.66
12:15 am	2	0.60	20	23.56
12:30 am	3	0.50	20	23.66
12:45 am	4	0.52	20	23.71
1:00 am	5	0.58	15	23.56
3:00 am	1	0.50	30	23.41
3:15 am	2	0.52	23	23.41
3:30 am	3	0.50	23	23.46
3:45 am	4	0.52	23	23.56
4:00 am	5	0.55	23	23.66
6:00 am	1	0.50	25	24.39
6:15 am	2	0.70	18	25.21
6:30 am	3	0.55	18	25.20
6:45 am	4	0.50	18	24.70
7:00 am	5	0.60	18	24.63

Table A.2. Carbon Dioxide and Ammonia Concentration  
Measured on February 21, 1986

Time	Location	CO <sub>2</sub> %	NH <sub>3</sub> ppm	Temperature C
9:00 pm	1	0.30	20	22.83
9:15 pm	2	0.40	20	23.16
9:30 pm	3	0.30	20	23.26
9:45 pm	4	0.31	20	23.35
10:00 pm	5	0.40	20	23.04
12:00 am	1	0.40	20	24.42
12:15 am	2	0.50	20	24.07
12:30 am	3	0.30	20	24.17
12:45 am	4	0.35	20	23.98
1:00 am	5	0.40	20	23.04
3:00 am	1	0.31	--	23.80
3:15 am	2	0.40	--	23.84
3:30 am	3	0.30	--	24.04
3:45 am	4	0.40	--	24.07
4:00 am	5	0.40	--	24.19
6:00 am	1	0.40	--	25.77
6:15 am	2	0.60	--	26.11
6:30 am	3	0.40	--	26.39
6:45 am	4	0.40	--	25.99
7:00 am	5	0.45	--	26.06

Table A.3. Carbon Dioxide and Ammonia Concentration  
Measured on February 18, 1986 (All fans off)

Time	Location	CO <sub>2</sub> %	NH <sub>3</sub> ppm	Temperature C
7:40 pm	2	0.21	20	23.21
8:20 pm		0.90		28.90
9:00 pm		1.40		31.45
9:40 pm		1.80		33.47
7:50 pm	3	0.31	20	26.78
8:30 pm		0.99		29.73
9:10 pm		1.40		31.83
9:50 pm		1.70		33.88
8:00 pm	4	0.60		27.03
8:40 pm		1.20		30.46
9:20 pm		1.60		32.61
9:55 pm		1.80		33.90
8:10 pm	5	0.80	20	28.09
8:50 pm		1.40		31.00
9:30 pm		1.80		33.07
10:00 pm		1.96		34.22



Table A.4 Management Factors, Design, and Input Values as  
Used for Verifying the Model on February 13,  
1986

---

Building:		
Length, m		31.00
Width, m		5.50
Height, m		2.37
Insulation:		
Walls, $\text{W/m}^2\cdot\text{C}$		0.54
Ceiling, $\text{W/m}^2\cdot\text{C}$		0.32
Simulation Period:		
Beginning day		44.00
Ending day		45.00
Initial Inside Conditions:		
Average daily temperature, $^{\circ}\text{C}$		24.20
Average daily rel. humidity, %		72.00
Initial Outside Conditions:		
Average daily temperature, $^{\circ}\text{F}$		11.38
Amplitude temperature, $^{\circ}\text{F}$		4.00
Flock Information:		
Number of chickens		4038.00
Age of chickens		50.00
Feed Information:		
Feed metabolized energy, $\text{MJ/da}$		11.532
Crude protein content, %		0.16
Manure Pit:		
Length, m		25.00
Width, m		3.44
Lights:		
Lights intensity, $\text{Lx}$		60.40
Feeding System:		
Hopper and trough system		
Prices:		
Feed, $\$/\text{kg}$		0.16
Electricity, $\$/\text{kW}\cdot\text{hr}$		0.06
Egg Prices:		
Nest run price, $\$$		0.45

---

Table A.5. Management Factors, Design, and Input Values as Used for Verifying the Model on February 16, 1986

---

Building:		
Length, m		31.00
Width, m		5.50
Height, m		2.37
Insulation:		
Walls, $W/m^2 \cdot C$		0.54
Ceiling, $W/m^2 \cdot C$		0.32
Simulation Period:		
Beginning day		47.00
Ending day		48.00
Initial Inside Conditions:		
Average daily temperature, C		23.00
Average daily rel. humidity, %		74.00
Initial Outside Conditions:		
Average daily temperature, F		19.71
Amplitude temperature, F		4.00
Flock Information:		
Number of chickens		4031.00
Age of chickens		51.00
Feed Information:		
Feed metabolized energy, MJ/da		11.532
Crude protein conten, %		0.16
Manure Pit:		
Length, m		25.00
Width, m		3.44
Lights:		
Lights intensity, Lx		60.40
Feeding System:		
Hopper and trough system		
Prices:		
Feed, \$/kg		0.16
Electricity, \$/kW.hr		0.06
Egg Prices:		
Neat run price, \$		0.45

---

Table A.6. Management Factors, Design, and Input Values  
as Used for Verifying the Model on February 27,  
1986

---

Building:	
Length, m	31.00
Width, m	5.50
Height, m	2.37
Insulation:	
Walls, $W/m^2.C$	0.54
Ceiling, $W/m^2.C$	0.32
Simulation Period:	
Beginning day	58.00
Ending day	59.00
Initial Inside Conditions:	
Average daily temperature	22.00
Average daily rel. humidity, %	73.00
Initial Outside Conditions:	
Average daily temperature, F	15.38
Amplitude temperature, F	5.00
Flock Information:	
Number of chickens	4020.00
Age of chickens	53.00
Feed Information:	
Feed metabolized energy, mJ/da	11.532
Crude protein content, %	0.16
Manure Pit:	
Length, m	25.00
Width, m	3.44
Lights:	
Lights intensity, Lx	60.40
Feeding System:	
Hopper and trough system	
Prices:	
Feed, \$/kg	0.16
Electricity, \$/kW.hr	0.06
Egg Prices:	
Nest run price, \$	0.45

---

Table A.7. Management Factors, Design, and Input Values  
as Used for Verifying the Model on March 3,  
1986

---

Building:	
Length, m	31.00
Width, m	5.50
Height, m	2.37
Insulation:	
Walls, $\text{W/m}^2\cdot\text{C}$	0.54
Ceiling, $\text{W/m}^2\cdot\text{C}$	0.32
Simulation Period:	
Beginning day	62.00
Ending day	63.00
Initial Inside Conditions:	
Average daily temperature, C	24.20
Average daily rel. humidity, %	74.00
Initial Outside Conditions:	
Average daily temperature, F	33.17
Amplitude temperature, F	3.50
Flock Information:	
Number of chickens:	4009.00
Age of chickens	53.00
Feed Information:	
Feed metabolized energy, $\text{MJ/da}$	11.532
Crude protein content, %	0.16
Manure Pit:	
Length, m	25.00
Width, m	3.44
Lights:	
Lights intensity, Lx	60.40
Feeding System:	
Hopper and trough system	
Prices:	
Feed, \$/kg	0.16
Electricity, \$/kW.hr	0.06
Egg Prices:	
Nest run price, \$	0.45

---

APPENDIX B

LIST OF THE MODEL

```

10 '-----:
20 '      SUBROUTINE TO INPUT INITIAL DATA FOR SIMULATION      :
30 '      MODEL AND TO DRAW HEN PICTURE (INTRODUCTION)          :
40 '      AL-CHALABI DHIA 1985                                   :
50 '      SUBROUTINE      023                                     :
60 '-----:
70 CLS:SCRN$="HENS.SCR":REM Name of file to Load in
80 SCRNFS="R":REM set screen function to "R" for Read
90 GOSUB 110
100 FOR LOOP=1 TO 5000:NEXT LOOP:CLS:GOSUB 160
110 OPEN"R",1,"SAVESCR.ADR",2:FIELD 1,2 AS SCRNADR$:GET 1:
115 SCRNADR=CVI (SCRNADR$):CLOSE:
120 REM SCRN$=FILE NAME OF SCREEN YOU WANT TO READ IN OR WRITE OUT
130 REM SCRNFS=FUNCTION YOU WISH TO DO "R" FOR READ "W" FOR WRITE
140 DEF SEG=SCRNADR:CALL 256,SCRN$,SCRNFS
150 RETURN
160 CLS :DIM XX(27)
170 'DRAW THE BOUNDRY OF THE PAGE
180 LOCATE 2,2 :PRINT CHR$(201)
190 'Upper line
200 '
210     FOR X=3 TO 78
220     IF X=40 THEN 230 ELSE 250
230     LOCATE 2,X:PRINT CHR$(203)
240     GOTO 260
250     LOCATE 2,X :PRINT CHR$(205)
260     NEXT X :LOCATE 2,78:PRINT CHR$(187)
270 '
280 'Right line
290 '
300     FOR Y=3 TO 22
310     LOCATE Y,78:PRINT CHR$(186)
320     NEXT Y :LOCATE 23,78 :PRINT CHR$(188)
330 '
340 'Lower line
350 '
360     FOR X=77 TO 3 STEP -1
370     IF X=40 THEN 380 ELSE 400
380     LOCATE 23,X:PRINT CHR$(202)
390     GOTO 410
400     LOCATE 23,X:PRINT CHR$(205)
410     NEXT X
420     LOCATE 23,2 :PRINT CHR$(200)
430 '
440 'Left line
450 '
460     FOR Y=22 TO 3 STEP -1
470     LOCATE Y,2 : PRINT CHR$(186)
480     NEXT Y
490     LOCATE 8,3
500 '

```

```

510 'Middel line
520 '
530     FOR Y=3 TO 22
540         LOCATE Y,40 :PRINT CHR$(186)
550     NEXT
560 '
570 'Write the headings
580     GOSUB 3650 :GOSUB 3530
590     IF M=1 THEN 2160 ELSE 600
600 'BEGINING OF DATA INPUT
610     ROW =4
620     FOR I=1 TO 22
630         IF I=1 THEN 640 ELSE 680
640         COLOR 3:LOCATE 3,4:PRINT "Building features"
650         LOCATE 4,4:PRINT "-----" :COLOR 2
660         LOCATE ROW+1,4 :INPUT "1-Length in m | ";LENG: XX(1)=LENG
670     NEXT
680     IF I=2 THEN 690 ELSE 720
690     LOCATE ROW+1,4
700     INPUT "2-Wiedth in m | ";WEDT: XX(2)=WEDT
710     NEXT
720     IF I=3 THEN 730 ELSE 760
730     LOCATE ROW+1,4
740     INPUT "3-Hight in m | ";HIGT: XX(3)=HIGT
750     NEXT
760     IF I=4 THEN 770 ELSE 810
770     COLOR 3:ROW=7:LOCATE 9,4 :
775     PRINT "Thermal conductivity (U-value) of"
780     LOCATE 10,4:PRINT "-----" :COLOR 2
790     LOCATE ROW+1,4:
795     INPUT "4-Walls in W/m2xC |";UWALL:XX(4)=UWALL
800     NEXT
810     IF I=5 THEN 820 ELSE 850
820     LOCATE ROW+1,4
830     INPUT "5-Ceilling in W/m2xC |";UCEIL:XX(5)=UCEIL
840     NEXT
850     IF I=6 THEN 860 ELSE 910
860     COLOR 3:ROW=10:LOCATE 8+1,4:
865     PRINT "Simulation period (Julian days)"
870     LOCATE 15,4:PRINT "-----" :COLOR 2
880     LOCATE ROW+1,4
890     INPUT "6-Beging day |";BG :XX(6)=BG
900     NEXT
910     IF I=7 THEN 920 ELSE 950
920     ROW=12:LOCATE 10+1,4:INPUT "7-Endding day |";ED :XX(7)=ED
930     COLOR 2
940     NEXT
950     IF I=8 THEN 960 ELSE 1000
960     COLOR 3:LOCATE 19,4 :PRINT "Initial inside conditions"
970     LOCATE 20,4 :PRINT "-----" :COLOR 2
980     LOCATE 21,4 :INPUT "8-Avg. daily temperature |";TINS:XX(8)=TINS

```

```

990 NEXT
1000 IF I=9 THEN 1010 ELSE 1040
1010 LOCATE 22,4
1020 INPUT "9-Avg. relative humidity |";RHIN :XX(9)=RHIN
1030 NEXT
1040 IF I=10 THEN 1050 ELSE 1090
1050 COLOR 3:LOCATE 3,42:PRINT "Flock informations"
1060 LOCATE 4,42:PRINT "-----":COLOR 2
1070 LOCATE 5,42:
1075 INPUT "10-Number of chickens |";NCHKN :XX(10)=NCHKN
1080 NEXT
1090 IF I=11 THEN 1100 ELSE 1130
1100 LOCATE 6,42
1110 INPUT "11-Age of chickens |";AGE :XX(11)=AGE
1120 NEXT
1130 IF I=12 THEN 1140 ELSE 1190
1140 COLOR 3:LOCATE 8,42:PRINT "Feed informations"
1150 LOCATE 9,42:PRINT "-----":COLOR 2
1160 LOCATE 10,42
1170 INPUT "12-Feed MET. energy |";MEDIT :XX(12)=MEDIT
1180 NEXT
1190 IF I=13 THEN 1200 ELSE 1230
1200 LOCATE 11,42
1210 INPUT "13-Crude protein content % |";NSCP :XX(13)=NSCP
1220 NEXT
1230 IF I=14 THEN 1240 ELSE 1330
1240 LOCATE 13,42:COLOR 3:PRINT"14-Supplemental heat "
1250 LOCATE 14,42:PRINT "-----":COLOR 2
1260 LOCATE 15,42:PRINT "1-Natural gas |"
1270 LOCATE 16,42:PRINT "2-L.P gas |"
1280 LOCATE 17,42:PRINT "3-No suppl. heat |"
1290 LOCATE 19,42:INPUT "Choose one option please";FGR
1300 XX(14)=FGR
1310 IF FGR<=0 OR FGR>=4 GOTO 1290
1320 NEXT
1330 IF I=15 THEN 1350 ELSE 1410
1340 'Clean the screen
1350 GOSUB 3540
1360 COLOR 3:LOCATE 3,4 :PRINT "Information about manure area"
1370 LOCATE 4,4:PRINT "-----":COLOR 2
1380 LOCATE 5,4
1390 INPUT "15-Length of pit in m |";LENM :XX(15)=LENM
1400 NEXT
1410 IF I=16 THEN 1420 ELSE 1450
1420 LOCATE 6,4
1430 INPUT "16-Wiedth of pit in m |";WEDM :XX(16)=WEDM
1440 NEXT
1450 IF I=17 THEN 1460 ELSE 1500
1460 COLOR 3:LOCATE 8,4:PRINT "Information about Lights"
1470 LOCATE 9,4:PRINT "-----":COLOR 2
1480 LOCATE 10,4:INPUT "17-Light intensity in Lx |";LIT :XX(17)=LIT

```



```

1490 NEXT
1500 IF I=18 THEN 1510 ELSE 1620
1510 COLOR 3:LOCATE 12,4 :PRINT "18-Feeding systems "
1520 LOCATE 13,4 :PRINT "-----" :COLOR 2
1530 LOCATE 14,4 :PRINT "1-Hopper and trough system"
1540 LOCATE 15,4 :PRINT "2-Chain system"
1550 LOCATE 16,4 :PRINT "3-Hopper and trough + grid"
1560 LOCATE 17,4 :PRINT "4-Spiral system"
1570 LOCATE 18,4 :PRINT "5-Sleeve system"
1580 LOCATE 20,4 :INPUT "Choose one feed system Please ";FSV
1590 XX(18)=FSV
1600 IF FSV<=0 OR FSV>=6 GOTO 1580
1610 NEXT
1620 IF I=19 THEN 1630 ELSE 1670
1630 COLOR 3:LOCATE 3,42:PRINT "Information about costs"
1640 LOCATE 4,42 :PRINT "-----":COLOR 2
1650 LOCATE 5,42 :INPUT "19-Feed cost $/Kg ";FPRIC:XX(19)=FPRIC
1660 NEXT
1670 IF I=20 THEN 1680 ELSE 1710
1680 LOCATE 6,42
1690 INPUT "20-Electricity cost ";ELPRC:XX(20)=ELPRC
1700 NEXT
1710 IF I=21 THEN 1720 ELSE 1740
1720 LOCATE 7,42:INPUT "21-Fuel cost $/m3 ";FUPRC:XX(21)=FUPRC
1730 NEXT
1740 IF I=22 THEN 1750 ELSE 1800
1750 COLOR 3:LOCATE 9,42
1760 PRINT "Information about egg prices"
1770 LOCATE 10,42:PRINT "-----":COLOR 2
1780 LOCATE 11,42:
1785 INPUT "22-Nest run price ";VEGG1:XX(22)=VEGG1
1790 NEXT
1800 '
1810 OPEN "O", 1,N$+".SIM"
1820 FOR I=1 TO 22
1830 WRITE 1,XX(I)
1840 NEXT I
1850 CLOSE 1
1860 '
1870 LOCATE 17,42:PRINT "Are these values correct (Y/N) ?"
1880 LOCATE 17,75:QQ$=INKEY$ :IF QQ$="" THEN 1890
1890 IF QQ$="Y" OR QQ$="y" THEN CHAIN "HOUSIMUL",,ALL
1900 'Correct the wrong values
1910 '
1920 OPEN "O", 1,N$+".SIM"
1930 LOCATE 18,42:INPUT"Enter number,new value ";I,XX(I)
1940 FOR I=1 TO 22
1950 WRITE 1,XX(I)
1960 NEXT I
1970 CLOSE 1
1980 '
1990

```

```

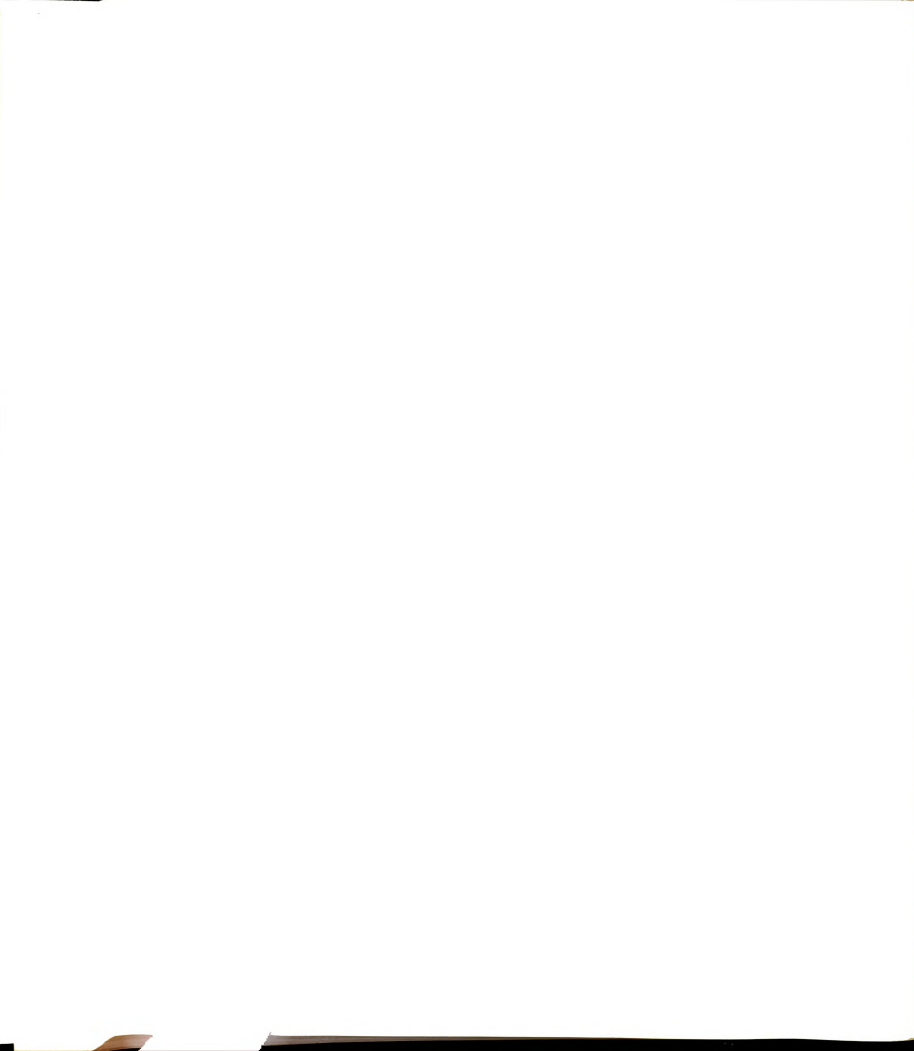
2100 OPEN "1", 2,N$+".SIM"
2110 GOSUB 3540
2120 INPUT 2,XX(1)
2130 GOSUB 2250
2140 CLOSE 2
2150 GOTO 1980
2160 'Read the old file from the disk
2170 LOCATE 1,30:PRINT "WAIT loading file ";N$
2180 OPEN "1", 1,N$+".SIM"
2190 FOR I=1 TO 22
2200 INPUT 1,XX(1)
2210 NEXT I
2220 CLOSE 1
2230 LOCATE 1,30:PRINT" "
2235 GOSUB 2250:GOTO 1980
2240 'Write the data to the screen
2250 ROW =4
2260 FOR I=1 TO 22
2270 IF I=1 THEN 2280 ELSE 2320
2280 COLOR 3:LOCATE 3,4:PRINT "Building features"
2290 LOCATE 4,4:PRINT "-----" :COLOR 2
2300 LOCATE ROW+1,4 :PRINT "1-Length in m | ";XX(1)
2310 NEXT
2320 IF I=2 THEN 2330 ELSE 2360
2330 LOCATE ROW+1,4
2340 PRINT "2-Width in m | ";XX(2)
2350 NEXT
2360 IF I=3 THEN 2370 ELSE 2400
2370 LOCATE ROW+1,4
2380 PRINT "3-Hight in m | ";XX(3)
2390 NEXT
2400 IF I=4 THEN 2410 ELSE 2450
2410 COLOR 3:ROW=7:LOCATE 9,4 :
2415 PRINT "Thermal conductivity (U-value) of"
2420 LOCATE 10,4:PRINT "-----" :COLOR 2
2430 LOCATE ROW+1,4:PRINT "4-Walls in W/m2xC |";XX(4)
2440 NEXT
2450 IF I=5 THEN 2460 ELSE 2490
2460 LOCATE ROW+1,4
2470 PRINT "5-Ceilling in W/m2xC |";XX(5)
2480 NEXT
2490 IF I=6 THEN 2500 ELSE 2550
2500 COLOR 3:ROW=10:LOCATE 8+1,4:
2505 PRINT "Simulation period (Julian days)"
2510 LOCATE 15,4:PRINT "-----" :COLOR 2
2520 LOCATE ROW+1,4
2530 PRINT "6-Beging day |";XX(6)
2540 NEXT
2550 IF I=7 THEN 2560 ELSE 2590
2560 ROW=12:LOCATE 10+1,4:PRINT "7-Endding day |";XX(7)
2570 COLOR 2

```

```

2580 NEXT
2590   IF I=8 THEN 2600 ELSE 2640
2600   COLOR 3:LOCATE 19,4 :PRINT "Initial inside conditions"
2610   LOCATE 20,4 :PRINT "-----" :COLOR 2
2620   LOCATE 21,4 :PRINT "8-Avg. daily temperature |";XX(8)
2630 NEXT
2640   IF I=9 THEN 2650 ELSE 2680
2650   LOCATE 22,4
2660   PRINT "9-Avg. relative humidity |";XX(9)
2670 NEXT
2680   IF I=10 THEN 2690 ELSE 2730
2690   COLOR 3:LOCATE 3,42:PRINT "Flock information "
2700   LOCATE 4,42:PRINT "-----" :COLOR 2
2710   LOCATE 5,42:PRINT "10-Number of chickens |";XX(10)
2720 NEXT
2730   IF I=11 THEN 2740 ELSE 2770
2740   LOCATE 6,42
2750   PRINT "11-Age of chickens |";XX(11)
2760 NEXT
2770   IF I=12 THEN 2780 ELSE 2830
2780   COLOR 3:LOCATE 8,42:PRINT "Feed information "
2790   LOCATE 9,42:PRINT "-----" :COLOR 2
2800   LOCATE 10,42
2810   PRINT "12-Feed MET. energy |";XX(12)
2820 NEXT
2830   IF I=13 THEN 2840 ELSE 2870
2840   LOCATE 11,42
2850   PRINT "13-Crude protein content % |";XX(13)
2860 NEXT
2870   IF I=14 THEN 2880 ELSE 2950
2880   LOCATE 13,42:COLOR 3:PRINT"14-Supplemental heat "
2890   LOCATE 14,42:PRINT "-----":COLOR 2
2900   LOCATE 15,42:PRINT "1-Natural gas |"
2910   LOCATE 16,42:PRINT "2-L.P gas |"
2920   LOCATE 17,42:PRINT "3-No suppl. heat |"
2930   LOCATE 19,42:PRINT "Your choise is |";XX(1)
2940 NEXT
2950   IF I=15 THEN 2970 ELSE 3030
2960   'Clean the screen
2970   GOSUB 3590: GOSUB 3540
2980   COLOR 3:LOCATE 3,4 :PRINT "Information about manure area"
2990   LOCATE 4,4:PRINT "-----" :COLOR 2
3000   LOCATE 5,4
3010   PRINT "15-Length of pit in m |";XX(15)
3020 NEXT
3030   IF I=16 THEN 3040 ELSE 3070
3040   LOCATE 6,4
3050   PRINT "16-Width of pit in m |";XX(16)
3060 NEXT
3070   IF I=17 THEN 3080 ELSE 3120
3080   COLOR 3:LOCATE 8,4:PRINT "Information about Lights"

```



```

3090     LOCATE 9,4:PRINT "-----":COLOR 2
3100     LOCATE 10,4:PRINT "17-Light intensity in Lx |";XX(17)
3110 NEXT
3120     IF I=18 THEN 3130 ELSE 3220
3130     COLOR 3:LOCATE 12,4 :PRINT "18-Feeding systems "
3140     LOCATE 13,4 :PRINT "-----":COLOR 2
3150     LOCATE 14,4 :PRINT "1-Hopper and trough system |"
3160     LOCATE 15,4 :PRINT "2-Chain system                |"
3170     LOCATE 16,4 :PRINT "3-Hopper and trough + grid  |"
3180     LOCATE 17,4 :PRINT "4-Spiral system              |"
3190     LOCATE 18,4 :PRINT "5-Sleeve system              |"
3200     LOCATE 20,4 :PRINT "Your choise is      ";XX(1)
3210 NEXT
3220     IF I=19 THEN 3230 ELSE 3270
3230     COLOR 3:LOCATE 3,42:PRINT "Information about costs"
3240     LOCATE 4,42 :PRINT "-----":COLOR 2
3250     LOCATE 5,42 :PRINT "19-Feed cost  $/Kg      |";XX(19)
3260 NEXT
3270     IF I=20 THEN 3280 ELSE 3310
3280     LOCATE 6,42
3290     PRINT "20-Electricity cost  |";XX(20)
3300 NEXT
3310     IF I=21 THEN 3320 ELSE 3340
3320     LOCATE 7,42:PRINT "21-Fuel cost  $/m3      |";XX(21)
3330 NEXT
3340     IF I=22 THEN 3350 ELSE 3400
3350     COLOR 3:LOCATE 9,42
3360     PRINT "Information about egg prices"
3370     LOCATE 10,42:PRINT "-----":COLOR 2
3380     LOCATE 11,42:PRINT "22-Nest run price          |";XX(22)
3390 NEXT
3510 '
3520     RETURN
3530 'Clean the screen
3540         SR=0
3550         FOR J=3 TO 22:LOCATE J,4+SR
3560         PRINT "
3570         NEXT :IF SR=38 THEN RETURN
3580         SR =38 : GOTO 3550
3590 'This subroutine will wait for input to continue
3600         COLOR 0,5:LOCATE 22,47:PRINT" Hit space bar to continue "
3610         FOR D=1 TO 1500:NEXT :COLOR 2,0
3620         LOCATE 22,47:PRINT "
3630         QQ$=INKEY$:IF QQ$="" THEN 3630
3640         IF QQ$=" " THEN RETURN
3650 'This subroutine will aske the user if he wants to use an old file
3660     COLOR 7
3670     LOCATE 3,4:INPUT "Enter Farm name |";FARM$
3680     LOCATE 22,4:PRINT"OLD files on this disk are|-"
3690     LOCATE 24,4:ON ERROR GOTO 3760 :FILES"*SIM"
3700     LOCATE 5,4:PRINT "Do you want an old file (Y/N)?" :LOCATE 5,34

```

```
3710 QS=INKEY$:IF QS="" THEN 3710
3720 IF QS="Y" OR QS="y" THEN 3730 ELSE 3760
3730 LOCATE 6,4:INPUT "OLD file name (8 Chr.)";N$:LOCATE 24,4
3740 FOR FG=4 TO 80:PRINT" ";:NEXT
3750 COLOR 2:M=1:RETURN
3760 COLOR 5:LOCATE 5,42:
3765 INPUT"NEW file name (8 Chr.)";N$:LOCATE 24,4
3770 COLOR 2:M=0:FOR FG=4 TO 80:PRINT" ";:NEXT :RETURN
```



```

1  ' :-----:
2  ' :   THIS IS THE MAIN PROGRAM TO CALCULATE PSYCHROMETRIC :
3  ' :   PARAMETERS AND CONTROL THE MODEL :
4  ' : :
5  ' :   WRITTEN BY DHIA AHMED AL-CHALABI 1985-1986 :
6  ' :-----:
7  CLS: DIM Y1 (26) ,Y2 (26) ,Y3 (26) ,Y4 (26) ,VRATE (26) ,TINS (26)
8      DIM TOUT (26) ,RHIN (26) ,RHOUT (26)
10     A =-27405.526      :NRPRC= XX (22)
12     B = 97.5413       :LENG=XX (1) :WEDT=XX (2) :HIGT=XX (3)
14     C =-.146244       :UCEIL=XX (5) :BG =XX (6) :ED =XX (7)
16     D = .00012558     :RHIN =XX (9) :NCHKN=XX (10) :AGE=XX (11)
18     E =-.000000048502 :NSCP=XX (13) :FGR =XX (14) :LENM=XX (15)
20     F = 4.34903       :LIT=XX (17) :FSV=XX (18) :FPRIC=XX (19)
22     G = .0039381      :FUPRC=XX (21) :UWALL=XX (4) :TINS=XX (8)
25     R = 22105649.25   :MEDIT=XX (12) :WEDM=XX (16) :ELPRC=XX (20)
30 '
44     TINEW=TINS :MEANT=TINS:ELSUM=0: CW=0: COUNT=0: QSUPL=0: FLAG=0: FGR=2
160 'Calculate body weight of chickens      subroutine 2      in kg
180     GOSUB 12000
200 'Starting DAILY simulation  *.*.*.*.*.*.*.*.*.*.*.*.*.*.*.*
210 '
220     FOR DOP =BG TO ED
225     TISUM=0 :RHSUM=0 :VRSUM=0 :CRF=1 :QMOLD=0 :
226     QHOLD=0 :RHOSM=0: COUNT=0
230     GOSUB 31000
240 'Calculate daily average temperature      subroutine 7      in C
250 '
260     GOSUB 17000
270 '
280 'Calculate body weight in kg and change in gaine in gr
290     GOSUB 20000
300     BWEIT=(BWEIT + DTW/1000)
310     BODYW=BWEIT* NCHKN
320 'Starting HOURLY simulation  *.*.*.*.*.*.*.*.*.*.*.*.*.*.*.*
330 '
340     FOR H=1 TO 24
350 '
360 'Calculate outside hourly temperature      subrotine 6      in C
370 ' and relative humidity
380     GOSUB 16000
390 '
400     TOUT=TEMPC :TOUT (H) =TOUT :RHOUT (H) =RHOUT
410 '
420 'Psychrometric calculation                      in SI units
430 'for outside conditions
520 '
530 'Calculate outside absolute temperature      in Kelvin
540 '
550     TOKVN=TOUT+273.16
560 '

```



```

570 'Atmospheric pressure                                in kPa
580 '
590   PATMO= 101.325
600 '
610 'Calculate saturated vapor pressure temp.  range (-18 - 0)    in kPa
620 '
630   IF TOUT <=0 AND TOUT >=-18 THEN 640 ELSE 690
640     LTOK=LOG (TOKVN)
650     PSOUT=EXP (31.9602- (6270.3605 /TOKVN) - (4.6057*LTOK))
660     GOTO 710
670 '
680 'Calculate saturated vapor pressur temp.  range  (0 - 110)    in kPa
690 '
700   Z = (A + (B *TOKVN)+(C *(TOKVN^2))+(D *(TOKVN^3))+(E *(TOKVN^4)))
703   Y = ((F *TOKVN) - (G *(TOKVN^2)))
705   L =Z /Y      :PSOUT=R *CDBL (EXP (L ))
710   PSOUT=PSOUT/1000
720 'Calculate actual vapor pressure                                in kPa
730 '
740   PVOUT=(RHOUT*PSOUT)/100
750 '
760 'Calculate humidity ratio of outside air                      in kg/kg da
770 '
780   HOUT=(.6219*PVOUT)/(PATMO-PVOUT)
790 '
800 'Calculate specific volume of outside air                      in m3/kg
810 '
820   VSOUT=(.287*TOKVN)/(PATMO-PVOUT)
830 '
840 'CALCULATE INSIDE CONDITIONS *.*.*.*.*.*.*.*.*.*.*.*.*.*.
850 'Calculate absolute inside temperature                        in Kelvin
860 '
870   TNKVN=TINS+273.16
880 '
890 'Calculate saturation vapor pressure                            in kPa
900 '
903   K = (A + (B *TNKVN)+(C *(TNKVN^2))+(D *(TNKVN^3))+(E *(TNKVN^4)))
906   M = ((F *TNKVN) - (G *(TNKVN^2)))
910   S =K /M      :PSINS=R *CDBL (EXP (S ))
920   PSINS=PSINS/1000
930 'Calculate vapor pressure                                      in kPa
940 '
950   PVINS=(RHIN*PSINS)/100
960 '
970 'Calculate humidity ratio of inside air                        in kg/kg d.a.
980 '
990   HINS=(.6219*PVINS)/(PATMO-PVINS)
1000 '
1010 'Calculate specific volume of inside air                      in m3/kg
1020 '
1030   VSINS=(.287*TNKVN)/(PATMO-PVINS)

```

```

1040 '
1050 'Calculate air mass in the building                      in kg
1055 '
1060     VOLUM=HIGT*LENG*WEDT-(BODYW/1000)-5.599
1070     AMI=VOLUM/VSINS
1080 '
1090 'Calculate latent heat of vaporization                  in kJ/kg
1100 'of water at saturation
1110     HFG=2502.535259 -2.38576*(TNKVN-273.16)
1120 '
1130 'Calculate latent heat from birds      subroutine    4    in kJ/hr
1140 '
1150     GOSUB 14000
1160 '
1170 'Calculate moisture from manure          subroutin    5    in kg/hr
1180 '
1190     GOSUB 15000
1200 '
1210 'Calculate moisture production from respiration        in kg/hr
1220 '
1230     WECHK=QLATB/HFG
1240 '
1250 'Calculate total moisture added to the air              in kg/hr
1260 '
1270     WETOT=WECHK+WEMNR
1273 '
1275 'Calculate building heat loss          subroutine    1    in kJ/hr
1280 '
1285     GOSUB 11000
1287 '
1290 'Calculate sensible heat from birds      subroutine    3    in kJ/hr
1300 '
1310     GOSUB 13000
1320 '
1330 'Calculate ventilation rate              subroutine    16   in m3/hr
1340 '
1350     GOSUB 26000
1360 '
1370 'Calculate ventilation air flow                      in kg/hr
1380 '
1390     MAV=VRATE/VSINS
1400 '
1410 'Calculate rate of change for heat content inside        in kJ
1420 'Change in time =1 hour                                in hr
1430 '
1440     DTIME=1
1450     DAH=1.0035*(TOUT-TINS)
1453     MAH=2501*(HOUT-HINS)+1.775*((HOUT*TOUT)-(HINS*TINS))
1455     LHA=2430 * WECHK
1457     QHCHG=DTIME*((MAV*(DAH+MAH))+LHA-QTOTB+QSNCL+QSUPL)
1460 '

```

```

1470 'Calculate rate of change for moisture content           in kg/kg d.a
1480 '
1490     QMCHG=DTIME*((MAV*HOUT+WETOT)-(MAV*HINS))/AMI)
1500 '
1502     IF CRF=1 THEN 1504 ELSE 1550
1504     TOUT(O)=TOUT :TINS(O)=TINS :RHIN(O)=RHIN :RHOUT(O)=RHOUT
1506 '
1510 'Calculate initial values for                               subroutine 17
1520 'heat and moisture
1530     GOSUB 27000
1540 '
1550 'Calculate new values for heat and moisture content
1560 '
1570     QHNEW=QHOLD+QHCHG
1580     QMNEW=QMOLD+QMCHG
1590 '
1600 'CALCULATE NEW INSIDE TEMPERATURE                               in C
1610 '
1620     TINEW=((QHNEW/AMI)-(2501* QMNEW))/(1.0035+1.775* QMNEW)
1630 '
1640 'Check temperature range inside
1650 '
1671     IF FGR=2 AND TINEW<MEANT-2 AND VRATE<1100 THEN 1710 ELSE 1672
1672     IF FGR=1 AND TINEW<MEANT-2 AND VRATE<1100 THEN 1673 ELSE 1677
1673     GOSUB 22000
1674     GOTO 1410
1675 '
1677     IF TINEW <=MEANT+2 AND TINEW >=MEANT-2 THEN 1710 ELSE 1680
1678 '
1680 'GO to the control subroutine 18
1690     GOSUB 28000
1700     GOTO 1390
1710     TINS(H)=TINEW :VRATE(H)=VRATE/3600
1720 'Calculate inside relative humidity
1730 'Calculate absolute temperture for new inside
1740 'temperature in Kelvin
1750     TNEWK=TINEW+273.16
1760 '
1770 'Calculate actual vapor pressure                               in kPa
1780 '
1790     PVACT=(HINS*PATMO)/(HINS+.6219)
1800 '
1810 'Calculate saturated vapor pressure                               in kPa
1820 '
1830     NE =(A +(B *TNEWK)+(C *(TNEWK^2))+(D *(TNEWK^3))+(E *(TNEWK^4)))
1833     PW =(F *TNEWK)-(G *(TNEWK^2))
1836     UA =NE /PW
1840     PSNEW=R *CDBL(EXP(UA )) : PSNEW=PSNEW/1000
1850 'Calculate new relative humidity inside %
1860 '
1870     RHNEW=(PVACT/PSNEW)*100

```

```

1875     IF RHNEW >99 THEN RHNEW=95
1880     RHIN(H)=RHNEW
1890 'Exchange the values
1900 '
1910     QHOLD=QHNEW
1920     QMOLD=QMNEW
1930     TINS =TINEW
1940     RHIN =RHNEW
1950 '
1960 'Calculate the sum of values                subroutine    19
1970 '
1980     GOSUB 29000
1990 'Save the data in array
2000     Y1(H)=TINS(H)
2010     Y2(H)=TOUT(H)
2020     Y3(H)=RHIN(H) :Y4(H)=VRATE(H) :QSUPL=0
2022     TOLD=TOUT(H-1):TILD=TINS(H-1) :RHILD=RHIN(H-1) :
2023     RHOLD=RHOUT(H-1)
2025     GOSUB 21000 : GOSUB 32000 : 'Print out hourly report
2030     NEXT H : 'Next hour  *.*.*.*.*.*.*.*.*.*.*.*.*.*.*.*
2040 'Calculate age of the birds in weeks
2050     AGE=AGE+(1/7)
2056 'Calculate maximum and minimum temperatures
2058 '
2060     TIMIN=TINS(1)
2062     FOR H=1 TO 24
2064         IF TINS(H)>=TIMIN THEN 2068
2066         TIMIN=TINS(H)
2068     NEXT H
2070     TIMAX=TINS(1)
2072     FOR H=1 TO 24
2074         IF TINS(H)<=TIMAX THEN 2078
2076         TIMAX=TINS(H)
2078     NEXT H
2080 'Calculate change in body weight            subroutine    10      in gr/da
2090 '
2100     GOSUB 20000 :GOSUB 30000
2110 '
2120 'Calculate mortality of the birds per day (assumed .008/month)
2150 '
2155     MORCH=NCHKN * .0003 :MORCH=INT(MORCH)
2160     NCHKN=NCHKN - MORCH
2165 '
2170 'Calculate feed intake and egg production  subroutine    14 & 15
2180 '
2190     GOSUB 24000
2200 '
2300 'Calculate feed intake for 1000 birds                in kg/day
2310 '
2320     FE100= FETAK*1000
2330 '

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```

2340 'Calculate feed cost consumed by 1000 birds           in $/day
2350 '
2360     FCOST=(FPRIC*FE100)/1000
2370 '
2380 'Calculate total egg production                       in kg/day
2390 '
2400     EGTOT=(E30FE*NCHKN)/1000
2410 '
2420 'Calculate egg production for 100 birds               in kg/day
2430 '
2440     EG100= E30FE*100
2445 'Calculate egg sale and display daily report
2447     GOSUB 40000 : GOSUB 39000
2450 NEXT DOP
2460 END
2470 '
2480 ' Where:-----
2490 ' QLATB ----- latent heat production      in kJ/hr
2500 ' QTOTB ----- heat loss through buliding in kJ/hr
2510 ' QSNCL ----- total sensible heat prod.   in kJ/hr
2515 ' QSUPL ----- supplemental heat needed    in kJ/hr
2520 ' PRCO2 ----- carbon dioxide production  in m3/g/hr
2530 ' VRCO2 ----- ventilation rate for CO2    in m3/sce
2540 ' MWATR ----- rate of water production    in kg/hr
2550 ' WEMNR ----- water vaopr from manure      in kg/hr
2560 ' VRMIS ----- venti. rate for moisture    in m3/sce
2570 ' VSINS ----- specific volume in air      in m3/kg
2580 ' VRTMP ----- venti.rate for temperature  in m3/sce
2590 ' HINS ----- humidity ratio inside air    in kg/kg
2600 ' HOUT ----- humidity ratio outside air   in Kg/Kg
2610 ' TINS ----- inside temperaturet         in C
2620 ' TOUT ----- outside temperaturet        in C
2630 ' HFG ----- latent heat of evaporation   in kJ/kg
2640 ' DAH ----- heat of dry air flow          in kJ
2650 ' MAH ----- heat from moisture change    in kJ
2655 ' LHA ----- heat from moisture of hens   in kJ
2660 ' -----
2670 ' End of subroutine
11000 ' :-----:
11010 ' :     SUBROUTINE OF HEAT LOSS THROUGH THE BUILDING kJ/hr :
11020 ' :           AL-CHALABI DHIA                               :
11030 ' : :                                                         :
11040 ' :     SUBROUTINE      01                                   :
11050 ' : :-----:
11060 '
11070 'Calculate surface area of the walls in m2
11080 '
11090     AWALL=2*HIGT*(LENG+WEDT)
11100 '
11110 'Calculate heat loss through the walls    QWALL  in W
11120 '

```

```

11130      QWALL=AWALL*UWALL*(TINS-TOUT)
11140
11150 ' Calaulate heat loss through the ceiling QCEIL in W
11160
11170      QCEIL=(LENG*WEDT)*UCEIL*(TINS-TOUT)
11180
11190 ' Calculate heat loss through the floor QFLOR in W
11200      UFLOR=3,155
11210      QFLOR=((LENG * WEDT) - (LEMN * WEDM)) * UFLOR
11220
11230 ' Calculate total heat loss through the building in kJ/hr
11240
11250      QTOTB=QWALL+QCEIL+QFLOR
11260      QTOTB=QTOTB * 3.6
11270      RETURN
11280
11290 ' Where:
11300 ' AWALL ----- surface area of the walls in m2
11310 ' HIGT ----- height of the building in m
11320 ' WEDT ----- width of the building in m
11330 ' LENG ----- length of the building in m
11340 ' UWALL ----- wall coef.of heat trans. in W/m2.C
11350 ' UCEIL ----- ceiling coef.of heat trans.in W/m2.C
11355 ' UFLOR ----- flor heat loss coef. in W/m2
11360 ' QWALL ----- heat loss through walls in W
11370 ' QCEIL ----- heat loss through ceiling in W
11380 ' QFLOR ----- heat loss through floor in W
11385 ' QTOTB ----- heat loss through building in kJ/hr
11390 '
11400 ' End of subroutine
12000 ' :-----:
12010 ' : SUBROUTINE OF BODY WEIGHT CALCULATION in kg :
12020 ' : AL-CHALABI DHIA :
12030 ' : :
12040 ' : SUBROUTINE 02 :
12050 ' :-----:
12060
12070 ' Calculate body weigth for hens from age 19 - 40 weeks in kg
12080
12090      IF AGE >=19 AND AGE <=40 THEN 12100 ELSE 12130
12100      BWEIT=.41583 * (AGE^ .400275) : 'R=.94
12110      GOTO 12180
12120
12130 ' Calculate body weight for hens from age 41 - 78 weeks in kg
12140
12150      BWEIT=1.68548 * (AGE^ .011659) : 'R=1.0
12160
12170
12180      RETURN
12190
12200

```

```

12210 | Where|-----|
12220 | AGE  ----- age of the hens           in weeks
12230 | BODYW ----- body weight of the hens   in kg
12240 | R      ----- correlation coef. of dody
12250 |                weight and age
12260 |-----|
12270 | End of subroutine
13000 |-----|
13010 | :          SUBROUTINE TO CALCULATE SENSIBLE HEAT in kJ/hr :
13020 | :          AL-CHALABI DHIA :
13030 | : :
13040 | :          SUBROUTINE      03 :
13050 |-----|
13060 |          H=INT(H)
13070 | Calculate sensible heat from the hens at night           in kJ/hr
13080 |
13090 |          IF H <5 AND H >=1 THEN 13100 ELSE 13122
13100 |          QSNSB=(16.4533 - .3108 * TINS) * BODYW           : 'R=.97
13110 |          FLAG=0 : QSNSL=0 :GOTO 13230
13120 |
13122 |          IF H <=24 AND H>=19 THEN 13124 ELSE 13130
13124 |          QSNSB=(16.4533 - .3108 * TINS) * BODYW           : 'R=.97
13126 |          FLAG=0 : QSNSL=0 :GOTO 13230
13128 |
13130 | Calculate sensible heat from the hens at day time in kJ/hr
13140 |
13150 |          IF H <19 AND H >=5 THEN 13160
13160 |          QSNSB=(23.4309 * (TINS^-.1558 )) * BODYW           : 'R=.96
13170 |          FLAG=1 : 'LIGHTS ON
13180 |
13190 | Calculate sensible heat from the lights                   in kJ/hr
13200 |
13210 |          QSNSL=(LENG*WEDT) * 38.744
13220 |
13230 | Calculate total sensible heat                             in kJ/hr
13240 |
13250 |          QSNCL=QSNSB + QSNSL
13260 |
13270 |          RETURN
13280 |
13290 |
13300 | Where|-----|
13310 | QSNSB ----- sensible heat production   in kJ/hr
13320 | QSNSL ----- sensible heat from lights   in kJ/hr
13330 | QSNCL ----- total sensible heat         in kJ/hr
13340 | TINS  ----- inside temperature         in C
13350 | H      ----- time of the day           in Hours
13360 | R      ----- correlation coef. of sensible
13365 |                heat and inside temperature
13370 | 38.744----- heat generated by lights in kJ/hr.m2
13380 |-----|

```

```

13390 ' End of subroutine
14000 '-----:
14010 '      SUBROUTINE TO CALCULATE LATENT HEAT in kJ/hr      :
14020 '      AL-CHALABI DHIA                                     :
14030 '      :                                                    :
14040 '      SUBROUTINE      04                                     :
14050 '-----:
14060 '
14070 ' Calculate latent heat from the hens at night      in kJ/hr
14080 '
14090 '      IF H>=1 AND H <5 THEN 14100 ELSE 14120
14100 '      QLATB=(3.8085 +.1685 * TINS) * BODYW      : 'R=.92
14110 '      FLAG=0: GOTO 14190
14120 '
14122 '      IF H<=24 AND H>=19 THEN 14124 ELSE 14140
14124 '      QLATB=(3.8085 +.1685 * TINS) * BODYW
14126 '      FLAG=0: GOTO 14190
14128 '
14130 ' Calculate latent heat from the hens at day time in kJ/hr
14140 '
14150 '      IF H >=5 AND H <19 THEN 14160
14160 '      QLATB=(4.4649 +.2122 * TINS) * BODYW      : 'R=.97
14170 '      FLAG=1 : 'Lights ON
14180 '
14190 '
14200 '      RETURN
14210 '
14220 '
14230 ' Where |-----:
14240 ' QLATB |----- latent heat production      in kJ/hr |
14250 ' TINS  |----- inside temperature          in C      |
14260 ' H     |----- time of the day              in Hours  |
14270 ' R     |----- correlation coef. of latent      |
14280 '       |----- heat and inside temperature      |
14290 ' |-----:
14300 ' End of subroutine
15000 '-----:
15010 '      SUBROUTINE OF WATER EVAPORATION FROM MANURE in kg/hr:
15020 '      AL-CHALABI DHIA                                     :
15030 '      :                                                    :
15040 '      SUBROUTINE      05                                     :
15050 '-----:
15060 ' This subroutine will calculate water from manure in kg/hr
15070 ' Calculate area covered with manure      in m2
15080 '      RFTOR=1.5
15090 '      ARAM=LENM * WEDM * RFTOR
15100 '
15110 ' Calculate temperature near the manure      in C
15120 '
15130 '      CHTMP=.09
15140 '      TMNR=TINS-CHTMP

```



```

15150 '
15160 ' Calculate absolute temperature near the manure      in Kelvin
15170 '
15180      TMNRK=TMNR+273.16
15190 '
15200 ' Calculate saturated vapor pressure near the manure  in torr
15210 '
15220      P =(A +(B *TMNRK)+(C *(TMNRK^2))+(D *(TMNRK^3))+(E *(TMNRK^4)))
15225      Q =((F *TMNRK)-(G *(TMNRK^2)))
15230      V =P /Q      :      PSMNR=R *CDBL (EXP (V ))
15240      PSMNR=PSMNR/133.322
15250 '
15260 ' Calculate partial vapor pressure near the manure    in torr
15270      RHMNR=RHIN/100
15280      PVMNR=PSMNR * RHMNR
15290 '
15300 ' Calculate partial pressure in the house              in torr
15310 '
15320      PVINT=PVINS/.1333
15330 '
15340 ' Calculate change in pressure                        in torr
15350 '
15360      DPSSR=PVMNR - PVINT
15370 '
15380 ' Calculate barometric pressure                      in torr
15390 '
15400      BPRSS=PATM0*(760/101.325)
15410 '
15420 ' Calculate evaporation coefficient in kg/m2/hr
15430      AVELC=.06
15440      SIGMA=.018 + .015 * AVELC
15450 '
15460 ' Calculate water evaporation from the manure         in kg/hr
15470 '
15480      WEMNR=SIGMA * ARAM * DPSSR *(760/BPRSS)
15490 '
15500 '
15510      RETURN
15520 '
15530 '
15540 ' Where:-----
15550 ' LENM  ----- length of the manure area   in m
15560 ' WEDM  ----- wedth of the manure arae    in m
15570 ' ARAM  ----- area covered with manure    in m2
15580 ' TMNR  ----- temperature near manure     in C
15590 ' TINS  ----- inside temperaturet        in C
15600 ' TMNRK ----- absolute temp. near manure  in K
15610 ' DTEMP ----- change in temperature      in C
15620 ' PSMNR ----- saturated pres.near manure  in torr
15630 ' PVMNR ----- partial pres. near manure   in torr
15640 ' PVINT ----- partial pres. in the house in torr

```

```

15650 ' DPSSR ----- change in pressure           in torr
15660 ' BPRSS ----- barometric pressuer           in torr
15670 ' SIGMA ----- coefficient of evaporation in kg/m2/h
15680 ' AVELC ----- air velocity near manure      in m/sce
15690 ' WEMNR ----- water evapo. from manure      in kg/hr
15700 ' RFTOR ----- manure roughness factor
15710 ' UNITS ----- 1 torr =.1333 kPa = 1 mm Hg abs
15720 '              760 torr =101.325 kPa= 1 atm
15730 ' -----
15740 ' End of subroutine
16000 ' :-----:
16010 ' :      SUBROUTINE OF TEMPERATURE & REL.HUM.  OUTSIDE in C  :
16020 ' :              AL-CHALABI DHIA                          :
16030 ' :                                                                 :
16040 ' :      SUBROUTINE      06                                  :
16050 ' :-----:
16060 ' Calculate hourly ambient air temperature in F
16070 '
16080 '      TDAMP= 7.71
16090 ' TEMPF= DTEMP+TDAMP*(SIN(.261799*(H+13))+SIN(.261792*(H+13)*2)/3)
16100 '
16110 ' KD= TEMPF
16120 ' TEMPC=(KD-32)*5/9      : 'Convert to C
16130 ' Dew point temp Vs Dry bulb Temperature (1965-1984)
16140 '
16150 ' IF DOP>=0 AND DOP<=31 THEN 16160 ELSE 16190 : 'FOR JANUARY
16160 ' DEWPT= -1.3258+(.803381*KD) : 'LINEAR EQUATION(R=.93) FOR January
16170 ' GOTO 16340
16180 '
16190 ' IF DOP>=32 AND DOP<=60 THEN 16200 ELSE 16230 : 'FOR FEBRUARY
16200 ' DEWPT= -2.8242+(.834888*KD) : 'LINEAR EQUATION(R=.89) FOR February
16210 ' GOTO 16340
16220 '
16230 ' IF DOP>=61 AND DOP<=90 THEN 16240 ELSE 16270 : 'FOR MARCH
16240 ' DEWPT= 4.94659+(.605923*KD) : 'LINEAR EQUATION(R=.76) FOR March
16250 ' GOTO 16340
16260 '
16270 ' IF DOP>=305 AND DOP<=334 THEN 16280 ELSE 16310 : 'FOR NOVEMBER
16280 ' DEWPT= 11.6864+(.533961*KD) : 'LINEAR EQUATION(R=.75) FOR November
16290 ' GOTO 16340
16300 '
16310 ' IF DOP>=335 AND DOP<=365 THEN 16320 ELSE 16480 : 'FOR DECEMBER
16320 ' DEWPT= -3.6047+(.942594*KD) : 'LINEAR EQUATION(R=.92) FOR December
16330 '
16340 ' CALCULATE RELATIVE HUMIDITY OUTSIDE
16350 '
16360 ' TDPO=459.69+DEWPT
16370 ' PDP=EXP(23.3924-(11286.6489 /TDPO) -.46057*LOG(TDPO))
16380 '
16390 ' TDBO=459.69+KD
16400 ' PDB=EXP(23.3924-(11286.6489 /TDBO) -.46057*LOG(TDBO))

```

```

16410 '
16420 ' Calculate relative humidity outside in %
16430 '
16440 '      RHOUT= (PDP/PDB) *100
16450 '
16460 ' IF RHOUT>=100 THEN RHOUT=99
16470 '
16480 ' RETURN
16490 '
16500 ' WHERE|-----|
16510 ' TEMPC ----- hourly ambient air temperature in C |
16520 ' TDAMP ----- daily ambient temp. amplitude in F |
16530 ' DTEMP ----- average daily ambient air temp. in F |
16540 ' DEWPT ----- dew point temperature outside in F |
16550 ' TDPO ----- absolute temperature in R |
16560 ' DOP ----- day of production of the year in day |
16570 ' RHOUT ----- relative humidity outside in % |
16580 ' X ----- outside temperature converted in F |
16590 ' -----|
16600 ' END OF SUBROUTINE
17000 ' :-----:
17010 ' : SUBROUTINE OF AVERAGE DAILY TEMPERATURE in C :
17020 ' : AL-CHALABI DHIA :
17030 ' : :
17040 ' : SUBROUTINE 07 :
17050 ' :-----:
17060 ' Calculate daily average ambient air temperature in C
17070 ' YTA= 47.5
17080 ' TYAMP= 25
17090 ' DTEMP=YTA + TYAMP * SIN(.017214 *(DOP-107))
17100 ' DTMPC= (DTEMP-32) *5/9
17110 '
17120 ' RETURN
17130 '
17140 ' WHERE|-----|
17150 ' TYAMP ----- yearly ambient amplitude temp. in F |
17160 ' DTEMP ----- average daily ambient air temp. in F |
17165 ' DTMPC ----- average daily ambient air temp. in C |
17170 ' YTA ----- yearly average air temperature in F |
17180 ' -----|
17190 ' END OF SUBROUTINE
18000 ' :-----:
18010 ' : SUBROUTINE TO CALCULATE DAY OF THE YEAR in DAYS :
18020 ' : AL-CHALABI DHIA :
18030 ' : :
18040 ' : SUBROUTINE 08 :
18050 ' :-----:
18060 ' This subroutine convert the julian day to a calender day
18070 '
18080 '
18090 ' IF DOP>=0 AND DOP<=31 THEN 18100 ELSE 18120

```

```

18100      GOSUB 19000 :S$="JANUARY ":SDOP=DOP
18110      GOTO 18550
18120      IF DOP>=32 AND DOP<=59 THEN 18130 ELSE 18160
18130      GOSUB 19000 :S$="FEBRUARY "
18140      SDOP=DOP-31
18150      GOTO 18550
18160      IF DOP>=60 AND DOP<=90 THEN 18170 ELSE 18200
18170      GOSUB 19000 :S$="MARCH "
18180      SDOP=DOP-59
18190      GOTO 18550
18200      IF DOP>=91 AND DOP<=120 THEN 18210 ELSE 18240
18210      GOSUB 19000 :S$="APRIL "
18220      SDOP=DOP-90
18230      GOTO 18550
18240      IF DOP>=121 AND DOP<=151 THEN 18250 ELSE 18280
18250      GOSUB 19000 :S$="MAY "
18260      SDOP=DOP-120
18270      GOTO 18550
18280      IF DOP>=152 AND DOP<=181 THEN 18290 ELSE 18320
18290      GOSUB 19000 :S$="JUNE "
18300      SDOP=DOP-151
18310      GOTO 18550
18320      IF DOP>=182 AND DOP<=212 THEN 18330 ELSE 18360
18330      GOSUB 19000 :S$="JULY "
18340      SDOP=DOP-181
18350      GOTO 18550
18360      IF DOP>=213 AND DOP<=243 THEN 18370 ELSE 18400
18370      GOSUB 19000 :S$="AUGUST "
18380      SDOP=DOP-212
18390      GOTO 18550
18400      IF DOP>=224 AND DOP<=273 THEN 18410 ELSE 18440
18410      GOSUB 19000 :S$="SEPTEMBER "
18420      SDOP=DOP-243
18430      GOTO 18550
18440      IF DOP>=274 AND DOP<=304 THEN 18450 ELSE 18480
18450      GOSUB 19000 :S$="OCTOBER "
18460      SDOP=DOP-273
18470      GOTO 18550
18480      IF DOP>=305 AND DOP<=334 THEN 18490 ELSE 18520
18490      GOSUB 19000 :S$="NOVEMBER "
18500      SDOP=DOP-304
18510      GOTO 18550
18520      IF DOP>=335 AND DOP<=365 THEN 18530
18530      GOSUB 19000 :S$="DECEMBER " :SDOP=DOP-334
18540
18550      RETURN

```

```

18570      WHERE!-----
18580      DOP  ----- day of production in the year
18590      SDOP ----- calender day associaated with
18600      the day of production.

```

```

18610 ' -----
18620 '
18630 '   END OF SUBROUTINE
19000 ' :-----:
19010 ' :   SUBROUTINE TO CALCULATE DAY AND NIGHT TIME   :
19020 ' :   AL-CHALABI DHIA                               :
19030 ' :
19040 ' :   SUBROUTINE      09                               :
19050 ' :-----:
19060 '
19070 '
19080 '   SDF=H
19090 '   IF SDF>=1 AND SDF<=5 THEN 19100 ELSE 19110
19100 '   D$=" AM-Night"                                     :RETURN
19110 '   IF SDF>=6 AND SDF<=19 THEN 19120 ELSE 19170
19120 '   IF SDF>=6 AND SDF<=11 THEN 19130 ELSE 19140
19130 '   D$=" AM-Day "                                     :RETURN
19140 '   IF SDF= 12 THEN D$=" PM-Day" ELSE 19150 :RETURN
19150 '   IF SDF> 12 THEN SDF=SDF-12
19160 '   D$=" PM-Day "                                     :RETURN
19170 '   IF SDF>=20 AND SDF<=23 THEN 19180 ELSE 19190
19180 '   D$=" PM-Night":SDF=H-12                           :RETURN
19190 '   D$=" AM-Night":SDF=H-12
19200 '   IF SDF=13 THEN SDF=0 : D$=" " :RETURN
19210 '
19220 ' END OF SUBROUTINE
20000 ' :-----:
20010 ' :   SUBROUTINE TO CALCULATE CHANGE IN WEIGHT  in grams :
20020 ' :   AL-CHALABI DHIA                               :
20030 ' :
20040 ' :   SUBROUTINE      010                               :
20050 ' :-----:
20060 '
20070 '   IF AGE> 18 AND AGE<24 THEN 20080 ELSE 20090
20080 '   DTW=8.6 :GOTO 20160
20090 '   IF AGE>=24 AND AGE<29 THEN 20100 ELSE 20110
20100 '   DTW=3.8 :GOTO 20160
20110 '   IF AGE>=29 AND AGE<41 THEN 20120 ELSE 20130
20120 '   DTW=1.5 :GOTO 20160
20130 '   IF AGE>=41 THEN 20140
20140 '   DTW=.5
20150 '
20160 '
20170 ' RETURN
20180 '
20190 '   Where:-----
20200 '   DTW  ----- change in weight in gr |
20210 '   AGE  ----- bird's age           in weeks|
20220 '   -----
20230 '
20240 ' END OF SUBROUTINE

```

```

21000 :-----:
21005 :      SUBROUTINE TO CALCULATE ELECTRICITY COST      :
21010 :      AL-CHALABI DHIA                                :
21020 :                                                    :
21030 :      SUBROUTINE      011                            :
21040 :-----:
21060 :
21080 'Calculate cost for minimum ventilation rate
21082   ELCS1=ELPRC*(.135*2)           :ELCS2=0
21084   IF VRATE <1050 THEN GOTO 21094 ELSE 21086
21086   CFMRT=VRATE*.589               : 'Convert to CFM
21088   KWHRC=((CFMRT*.0847)/1000)
21090 'Calculate electricity cost per day
21092   ELCS2=KWHRC*ELPRC
21094   ELTOT=ELCS1+ELCS2
21096   ELSUM=ELTOT+ELSUM
21098 :
21120 :
21130 RETURN
21140 'Where|-----:
21150 'VRATE ----- ventilation rate in m3/hr |
21160 'CFMRT ----- ventilation rate in CFM   |
21170 'KWHRC ----- electr. consum.   in kW/h  |
21180 'ELCST ----- electr. cost      in $/day  |
21190 'ELPRC ----- electr. price     in $/kW.hr |
21200 :-----:
21210 :
21220 'END OF SUBROUTINE
22000 :-----:
22010 :      SUBROUTINE TO CALCULATE SUPPLEMENTAL HEAT      :
22020 :      AL-CHALABI DHIA                                :
22030 :                                                    :
22040 :      SUBROUTINE      012                            :
22050 :-----:
22060 'Calculate heat loss though ventilation              in kJ/hr
22070 :
22080   TSUPL=MEANT -1.5
22090   QHVRT=1.0035 * MAV * (TSUPL - TOUT)
22100 :
22110 'Calculate supplement heat needed
22120 :
22130   QSUPL=(QHVRT + QTOTB) - QSNCL
22140 :
22150 'Calculate fuel cost                                in $/hr
22160   IF EFR=1 THEN FENRG=37252! ELSE FENRG=25529138
22170   FCOST=(QSUPL * FPRIC)/FENRG
22220 :
22230 RETURN
22240 :
22250 'Where|-----:
22260 'QHVRT ----- heat loss in ventilation |

```

```

22270 ' TSUPL ----- temperature needed
22280 ' QSUPL ----- supplemental heat kJ/hr
22290 ' -----
22300 'END OF SUBROUTINE
23000 '-----:
23010 ' SUBROUTINE TO DRAW A GRAPH FROM THE DATA :
23020 ' AL-CHALABI DHIA :
23030 ' :
23040 ' SUBROUTINE 013 :
23050 '-----:
23060 '
23070 'This subroutine will plot the data into line graph
23080 '
23090 CLS:'Clear the screen
23100 '
23110 WINDOW(0,0)-(639,459):VIEW(0,0)-(639,199)
23120 DATA 1,2,3,4,5,6,7,8,9,10,11,12,1,2,3,4,5,6,7,8,9,10,11,12
23130 '
23140 'Draw lables and axis
23150 '
23160 GOSUB 23430
23170 '
23180 'Draw inside temperature in deg. F
23190 '
23200 FOR H=1 TO 24:Y1(H)=((Y1(H) * 9/5)+32):NEXT H
23210 K=3:Z=0:N$="Tin" :CLR=1
23220 GOSUB 23670
23230 '
23240 'Draw outside temperature in deg. F
23250 FOR H=1 TO 24:Y1(H)=Y2(H):NEXT H
23260 FOR H=1 TO 24:Y1(H)=((Y2(H) * 9/5)+32):NEXT H
23270 Z=55:N$="Tout" :CLR=2
23280 GOSUB 23670
23290 '
23300 'Draw relative humidity in %
23310 FOR H=1 TO 24:Y1(H)=Y3(H):NEXT H
23320 FOR H=1 TO 24:Y1(H)=(Y3(H)):NEXT H
23330 Z=145:N$="R.H" :CLR=3
23340 GOSUB 23670
23350 '
23360 'Draw ventilation rate in m3/sec
23370 '
23380 FOR H=1 TO 24:Y1(H)=(Y4(H)*15):NEXT H
23390 Z=210:N$="Vrt" :CLR=4
23400 GOSUB 23810
23410 FOR JJ=1 TO 5000:NEXT
23420 RETURN
23430 ' Draw lables and axis
23440 SYMBOL (1,350)," Out -In Temp. R.H",2,2,3,3
23450 SYMBOL (35,400),"A.M. Hours P.M.",1,2,5
23460 FOR C= 7 TO 77 STEP 3

```

```

23470         LOCATE 20,C :PRINT "!";
23480         LOCATE 21,C-1 :READ M :PRINT M ;
23490     NEXT C:L=0
23500     LINE (50,359)-(146,364),1,BF
23510     LINE (148,359)-(482,364),6,BF
23520     LINE (484,359)-(605,364),1,BF
23530     LOCATE 3,10:PRINT S$;" / ";SDOP
23540     FOR Y=352 TO 44 STEP -30
23550         SYMBOL (32,Y),CHRS(196),1,1,2
23560         SYMBOL (630,Y),CHRS(196),1,1,2
23570     NEXT Y
23580     LOCATE 3,2:PRINT "100"
23590     LOCATE 12,3:PRINT "50"
23600     LOCATE 20,3:PRINT "0"
23610     SYMBOL(80,8),"AVERAGE HOURLY TEMPERATURE & R.H ",2,2,5
23620     SYMBOL(82,10),"AVERAGE HOURLY TEMPERATURE & R.H ",2,2,7
23630     LINE (35,30)-(35,356):LINE-(630,356):LINE-(630,30)
23640     RESTORE
23650     RETURN
23660 '
23670 'Plot the data
23680 '
23690     LINE(48,(356-Y1(1)*K)-2)-(52,(356-Y1(1)*K)+2),CLR,B
23700     C=1:M=1
23710     SYMBOL(300+Z,30),N$,2,2,CLR
23720     PSET(50,356-Y1(1)*K)
23730     FOR X=78 TO 654 STEP 24
23740         C=C+1 :M=M+1
23750     FOR I=C TO M
23760         IF X=630 THEN GOTO 23800
23770         LINE-(X,356-Y1(1)*K),CLR
23780         LINE(X-2,(356-Y1(1)*K)-2)-(X+2,(356-Y1(1)*K)+2),CLR,B
23790     NEXT I:NEXT X
23800     RETURN
23810     CC=-1 :MM=-1
23820     SYMBOL(300+Z,30),N$,2,2,CLR
23830     PSET(50,356-Y1(1)*K)
23840     FOR X=78 TO 654 STEP 24
23850         CC=CC+1 :MM=MM+1
23860     FOR I=CC TO MM
23870         IF X=630 THEN GOTO 23930
23880         IF X=78 THEN GOTO 23900
23890         LINE-(X-24,356-Y1(I+1)*K),CLR
23900 '****
23910         LINE -(X,356-Y1(I+1)*K),CLR
23920     NEXT I:NEXT X :CLR=3
23930     RETURN
24000 '-----:
24010 ' : SUBROUTINE TO ESTIMATE FACTORS EFFECTING FEED INTAKE :
24020 ' : AL-CHALABI DHIA :
24030 ' :

```



```

24040 ' :      SUBROUTINE      014      :
24050 ' :-----:
24060      AGEI=INT(AGE)
24070 'Values of factor f2 ,which adjusts  feed intake for age ,and
24080 'values of factor A ,which adjusts egg output for age.
24090 '
24100 'Bird's age 20-72 weeks                      Period
24110 '
24120      IF AGEI>=20 AND AGEI<=24 THEN 24130 ELSE 24150      : ' 1
24130          F2FCT=.764      :AEFCT=.32
24140          GOTO 24550
24150      IF AGEI>=25 AND AGEI<=28 THEN 24160 ELSE 24180      : ' 2
24160          F2FCT=.917      :AEFCT=.93
24170          GOTO 24550
24180      IF AGEI>=29 AND AGEI<=32 THEN 24190 ELSE 24210      : ' 3
24190          F2FCT=.987      :AEFCT=1.09
24200          GOTO 24550
24210      IF AGEI>=33 AND AGEI<=36 THEN 24220 ELSE 24240      : ' 4
24220          F2FCT=1.006      :AEFCT=1.12
24230          GOTO 24550
24240      IF AGEI>=37 AND AGEI<=40 THEN 24250 ELSE 24270      : ' 5
24250          F2FCT=1.002      :AEFCT=1.11
24260          GOTO 24550
24270      IF AGEI>=41 AND AGEI<=44 THEN 24280 ELSE 24300      : ' 6
24280          F2FCT=1.024      :AEFCT=1.11
24290          GOTO 24550
24300      IF AGEI>=45 AND AGEI<=48 THEN 24310 ELSE 24330      : ' 7
24310          F2FCT=1.052      :AEFCT=1.11
24320          GOTO 24550
24330      IF AGEI>=49 AND AGEI<=52 THEN 24340 ELSE 24360      : ' 8
24340          F2FCT=1.044      :AEFCT=1.09
24350          GOTO 24550
24360      IF AGEI>=53 AND AGEI<=56 THEN 24370 ELSE 24390      : ' 9
24370          F2FCT=1.046      :AEFCT=1.06
24380          GOTO 24550
24390      IF AGEI>=57 AND AGEI<=60 THEN 24400 ELSE 24420      : ' 10
24400          F2FCT=1.053      :AEFCT=1.05
24410          GOTO 24550
24420      IF AGEI>=61 AND AGEI<=64 THEN 24430 ELSE 24450      : ' 11
24430          F2FCT=1.03      :AEFCT=1.02
24440          GOTO 24550
24450      IF AGEI>=65 AND AGEI<=68 THEN 24460 ELSE 24480      : ' 12
24460          F2FCT=1.02      :AEFCT=1
24470          GOTO 24550
24480      IF AGEI>=69 THEN 24490                      : ' 13
24490          F2FCT=1.032      :AEFCT=.97
24500 '
24510 '      end of values f2
24520 'Values of factor f3 ,which adjusts feed consumption for wastage
24530 'in various feeding systems .
24540 '

```

```

24550 '
24560 'Hopper and trough system
24570 '    IF FSV=1 THEN F3FCT=.1 ELSE 24590
24580 '
24590 'Chain system
24600 '    IF FSV=2 THEN F3FCT=.965 ELSE 24620
24610 '
24620 'Hopper and trough plus grid system
24630 '    IF FSV=3 THEN F3FCT=.948 ELSE 24650
24640 '
24650 'Spiral system
24660 '    IF FSV=4 THEN F3FCT=.948 ELSE 24680
24670 '
24680 'Sleeve system
24690 '    IF FSV=5 THEN F3FCT=.986
24700 '
25000 ' :-----:
25010 ' : SUBROUTINE TO ESTIMATE EGG OUTPUT in g/b/day :
25020 ' : AL-CHALABI DHIA :
25030 ' : :
25040 ' : SUBROUTINE 015 :
25050 ' :-----:
25060 'This subroutine will estimate feed consumption and egg
25070 'production for the white breed chickens
25080 '
25090 'Breed factor for white birds
25100 '
25110 '    F1FCT=1
25120 '
25130 'Calculate metabolizable energy intake for white egg layer fed
25140 '11.3 MJ/kg in kJ/d per bird
25150 '
25160 '    METAK=1584.3 - 33.47*TI AVG + 1.562*(TI AVG^2) - .0349*(TI AVG^3)
25170 '
25180 'Adjust the energy intake for any dietary energy level
25190 '
25200 '    ADJFD=METAK + 46 * MEDIT - 519.8
25210 '
25220 'Calculate feed intake for the chickens in g/d per bird
25230 '
25240 '    FETAK=(F1FCT*F2FCT*F3FCT*ADJFD)/MEDIT
25250 '
25260 'Calculate the standard protein intake g/day
25270 '
25280 '    STRDP=FETAK *(NSCP/100)
25290 '
25300 'Calculate egg output response to protein g/b/day
25310 '
25320 '    E1ORP=(STRDP^2)/(4.446-(.417*STRDP)+(.0309*(STRDP^2)))
25330 '
25340 'Calculate egg output response to temperature g/b/day

```

```

25350 D1ORT=0
25360 IF TIAVG>=30 THEN 25370 ELSE 25400
25370
25380 D1ORT=10.98-(2.14*TIAVG)-(.02335*(TIAVG^2))+(.00522*(TIAVG^3))
25390
25400 Calculate egg output response to light intensity g/b/day
25410
25420 D2ORL=2.41-(2.711*LOG(LIT)*.434294)+(.76*((LOG(LIT)*.434294)^2))
25430
25440 IF LIT=60.4 THEN D2ORL=0
25450
25460 Calculate egg output the final estimet g/b/day
25470
25480 E30FE=(E1ORP-D1ORT-D2ORL) * AEFCT
25490
25500 RETURN
25510
25520 WHERE!-----
25530 F1FCT ----- breed factor for white chickens
25540 F2FCT ----- adjust feed intake for age f2
25550 F3FCT ----- adjust feed intake for wastage in
25560 FETAK ----- feed intake in g/b/day
25570 METAK ----- metabolizable energy intake in kJ/b/da
25580 AEFCT ----- adjust egg output for age A
25590 MEDIT ----- metabolizable energy of diet in MJ/kg
25600 STRDP ----- standard protein intake
25610 E1ORP ----- egg output response to protein g/b/da
25620 D1ORT ----- egg output response to temp. g/b/da
25630 D2ORL ----- egg output response to light g/b/da
25640 E30FE ----- egg output final estimate
25650 -----
25660 END OF SUBROUTINE
26000 :-----:
26010 : SUBROUTINE TO CALCULATE VENTILATION RATE m3/hr :
26020 : AL-CHALABI DHIA :
26030 : :
26040 : SUBROUTINE 016 :
26050 :-----:
26060
26070 Calculate ventilation rate for carbon dioxide
26120 Check for inside temperature and calculate CO2 production
26130 for hens (10-17 C) in cm3/gr.hr
26140 IF TINEW>=10 AND TINEW<=17 THEN 26150 ELSE 26180
26150 PRCO2=.34344 * (TINEW^.1317) : 'R=.99
26160 GOTO 26290
26170
26180 Calculate CO2 production for hens (18-26 C) in cm3/gr.hr
26190
26200 IF TINEW>=18 AND TINEW<=26 THEN 26210 ELSE 26240
26210 PRCO2=.8961 * (TINEW^-.213) : 'R=.97
26220 GOTO 26290

```

```

26230 '
26240 'Calculate CO2 production for hens (27-34 C)           in cm3/gr.hr
26250 '
26260 '    IF TINEW>=27 AND TINEW<=34 THEN 26270
26270 '        PRC02=.222 * (TINEW^.2201)                   : 'R=.98
26280 '
26290 'Calculate total CO2 production in the house           in m3/hr
26300 '
26310 '    TPC02=PRC02 * .001 * BODYW
26320 '
26330 'Calculate ventilation rate for carbon dioxide         in m3/hr
26340 '
26350 '    VRC02=TPC02/ (.0035-.0003)
26360 '    IF TOUT<= 0 THEN 26400 ELSE 26660
26400 '    VRATE=VRC02
26410 'Go back to maine program
26420 '
26430 '    RETURN
26440 '
26450 'Check for relative humidity inside
26460 '
26470 '    IF RHIN > 90 THEN 26490 ELSE 26660
26480 '
26490 'Calculate ventilation rate for moisture                 in m3/hr
26500 '
26600 '    VRMIS=(VSINS * WETOT) / (HINS-HOUT)
26605 '
26610 '    VRATE=VRMIS
26620 'Go back to maine program
26630 '
26640 '    RETURN
26650 '
26660 'Calculate ventilation rate for temperature              in m3/hr
26700 '
26710 '    VRTMP=(VSINS/(1.0035 *(TINS -TOUT))) * (QSNCL-QTOTB)
26720 '    VRATE=VRTMP
26730 'Go back to maine program
26740 '
26750 '    RETURN
26760 '
26770 '
26780 'Where|-----|
26790 'QLATB ----- latent heat production      in kJ/hr |
26800 'QTOTB ----- heat loss through building in kJ/hr |
26810 'QSNCL ----- total sensible heat prod.   in kJ/hr |
26820 'PRC02 ----- carbon dioxide production   in m3/kghr |
26830 'VRC02 ----- ventilation rate for CO2    in m3/hr  |
26840 'WETOT ----- rate of water production    in kg/hr  |
26860 'VRMIS ----- venti. rate for moisture    in m3/hr  |
26870 'VSINS ----- specific volume of air      in m3/kg   |
26880 'VRTMP ----- venti.rate for temperature in m3/hr |

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```

26890 | HINS ----- humidity ratio inside air in kg/kg |
26900 | HOUT ----- humidity ratio outside air in kg/kg |
26910 | TINS ----- inside temperature in C |
26920 | TOUT ----- outside temperature in C |
26930 | HFG ----- latent heat of evaporation in kJ/kg |
26940 | R ----- correlation coef. of CO2 |
26950 | ----- production and inside temperature |
26960 | -----
26970 | End of subroutine
27000 | :-----:
27010 | : SUBROUTINE TO CALCULATE INITIAL HEAT & MOISTURE :
27020 | : CONTENT :
27030 | : AL-CHALABI DHIA :
27040 | : SUBROUTINE 017 :
27050 | :-----:
27060 |
27070 | Calculate initial value for heat content in kJ
27080 |
27090 | IF CRF=1 THEN 27100 ELSE 27200
27100 |
27110 | QHOLD=AMI* (TINS * (1.007 + 1.84* HINS) + 2501* HINS - .026)
27120 |
27130 | Calculate initial value for moisture content in kg H2O/kg d.a
27140 |
27150 | QMOLD=HINS
27160 |
27170 | Go back to main program
27180 | CRF=0
27190 |
27200 | RETURN
27210 |
27220 | Where!-----
27230 | QHOLD ----- initial heat content in kJ
27240 | QMOLD ----- initial moisture content in kg
27250 | HINS ----- humidity ratio inside air in kg/kg
27260 | TINS ----- inside temperature in C
27270 | AMI ----- air mass in the building in kg
27290 | CRF ----- flag
27300 | -----
27310 | End of subroutine
28000 | :-----:
28010 | : SUBROUTINE TO CONTROL INSIDE TEMP.,MOISTURE & CO2 :
28020 | : AL-CHALABI DHIA :
28030 | : :
28040 | : SUBROUTINE 018 :
28050 | :-----:
28060 |
28170 | Decrease ventilation rate for low temperatures
28180 |
28190 | IF TINEW < MEANT-2 THEN 28200 ELSE 28280
28200 | VRTMP=VRTMP -153.83

```

```

28210     VRATE=VRTMP
28220 '
28230 'Check for CO2 level
28240 '
28250     IF VRATE < VRCO2 THEN 28260 ELSE 28270
28260     VRATE=VRCO2
28270     RETURN
28280 '
28290 'Increase ventilation rate for high temperatures
28300 '
28310     VRTMP=VRTMP +12
28320     VRATE=VRTMP
28330     RETURN
28340 '
28350 'CONTROL FOR MOISTURE (RELATIVE HUMIDITY)
28360 '
28370     IF RHIN <=95 THEN 28380 ELSE 28400
28380     RETURN
28390 '
28400 'Increase ventilation rate
28410 '
28420     VRMIS=VRMIS +15
28430     VRATE=VRMIS
28440 '
28450 'Go back to main program
28460 '
28470 RETURN
28480 '
28490 ' Where:-----
28500 ' VRCO2 ----- ventilation rate for CO2    in m3/hr
28510 ' VRMIS ----- venti. rate for moisture    in m3/hr
28520 ' VRTMP ----- venti.rate for temperature in m3/hr
28530 ' MEANT ----- temp. to be controled      in C
28540 ' TINS  ----- inside temperature          in C
28550 ' TOUT  ----- outside temperature         in C
28560 ' -----
28570 ' End of subroutine
29000 '-----:
29010 ' : SUBROUTINE TO SUM THE VALUES TO CALCULATE MEANS :
29020 ' : AL-CHALABI DHIA :
29030 ' : :
29040 ' : SUBROUTINE 019 :
29050 ' :-----:
29060 '
29070 'Temperature summation
29080 '
29090     TISUM=TISUM+TINS
29100 '
29110 'Realtive humidity sumation
29120 '
29130     RHSUM=RHSUM+RHIN

```

```

29140    RHOSM=RHOSM+RHOUT
29150 'Ventilation rate summation
29160 '
29170    VRSUM=VRSUM+VRATE
29180 '
29190    RETURN
29200 '
29210 ' Where|-----|
29220 ' RHNEW ----- new inside relative humidity in % |
29230 ' TINEW ----- new inside temperature      in C  |
29240 ' VRATE ----- ventilation rate             in m3/hr |
29250 ' |-----|
29260 ' End of subroutine
30000 ' :-----|
30010 ' :      SUBROUTINE TO CALCULATE HOURLY AVERAGES      :
30020 ' :      AL-CHALABI DHIA                               :
30030 ' : : : : : : : : : : : : : : : : : : : : : : : : : : : : :
30040 ' :      SUBROUTINE      020                           :
30050 ' : :-----|
30060 TIAVG=0 :RHAvg=0 :VRAVG=0 :RHOVG=0
30070 'Temperature mean
30080 '
30090    TIAVG =TISUM/24
30100 '
30110 'Realtive humidity mean
30120 '
30130    RHAvg=RHSUM/24
30140    RHOVG=RHOSM/24
30150 'Ventilation rate mean
30160 '
30170    VRAVG=VRSUM/24
30180 '
30190    RETURN
30200 '
30210 ' Where|-----|
30220 ' RHAvg ----- hourly average relativ humi.  in %  |
30230 ' TINS  ----- hourly average temperature   in C  |
30240 ' VRAvg ----- hourly average venti.  rate   in m3/hr |
30250 ' |-----|
30260 ' End of subroutine
31000 ' :-----|
31010 ' :      SUBROUTINE TO DESIGN OUTPUT HOURLY REPORT      :
31020 ' :      AL-CHALABI DHIA                               :
31030 ' : : : : : : : : : : : : : : : : : : : : : : : : : : : : :
31040 ' :      SUBROUTINE      021                           :
31050 ' : :-----|
31060 CLS:WINDOW(0,0) - (639,459) :VIEW(0,0) - (639,199)
31070 'Draw the boundry of the page
31080 '
31090 LOCATE 2,2 :PRINT CHR$(201)
31100 '

```

```

31110 'Upper line
31120 '
31130     FOR X=3 TO 78
31140         LOCATE 2,X :PRINT CHR$(205)
31150     NEXT X :LOCATE 2,78:PRINT CHR$(187)
31160 '
31170 'Right line
31180 '
31190     FOR Y=3 TO 22
31200         IF Y=8 THEN 31210 ELSE 31230
31210         LOCATE Y,78:PRINT CHR$(185)
31220         GOTO 31240
31230         LOCATE Y,78:PRINT CHR$(186)
31240     NEXT Y :LOCATE 23,78 :PRINT CHR$(188)
31250 '
31260 'Lower line
31270 '
31280     FOR X=77 TO 3 STEP -1
31290         IF X=40 THEN 31300 ELSE 31320
31300         LOCATE 23,X:PRINT CHR$(202)
31310         GOTO 31330
31320         LOCATE 23,X:PRINT CHR$(205)
31330     NEXT X
31340 LOCATE 23,2 :PRINT CHR$(200)
31350 '
31360 'Left line
31370 '
31380     FOR Y=22 TO 3 STEP -1
31390         IF Y=8 THEN 31400 ELSE 31420
31400         LOCATE Y,2:PRINT CHR$(204)
31410         GOTO 31430
31420         LOCATE Y,2 : PRINT CHR$(186)
31430     NEXT Y
31440 LOCATE 8,40 :PRINT CHR$(203)
31450 LOCATE 8,3
31460 '
31470 'Upper middel line
31480 '
31490     FOR X=3 TO 77
31500         IF X=40 THEN 31510 ELSE 31520
31510         GOTO 31530
31520         LOCATE 8,X :PRINT CHR$(205)
31530     NEXT X
31540 LOCATE 9,40
31550 '
31560 'Middel line
31570 '
31580     FOR Y=9 TO 22
31590         LOCATE Y,40 :PRINT CHR$(186)
31600     NEXT
31610 '

```



```

31620 'Write the headings
31630 '
31640 LOCATE 4,4 :PRINT "DATE:" :LOCATE 4,20 :PRINT "/"
31650 LOCATE 4,26:PRINT "TIME:"
31660 LOCATE 4,45:PRINT "FARM NAME:"
31670 SYMBOL (50,100)," HOURLY REPORT",3,3,5 :COLOR 2,0
31675 SYMBOL (52,101)," HOURLY REPORT",3,3,7 :COLOR 2,0
31680 LOCATE 6,65:PRINT "LIGHTS:"
31690 LOCATE 9 ,4:COLOR 3,4:PRINT " INSIDE CONDITIONS:      ":COLOR 2,0
31700 LOCATE 10,4:PRINT "1-Previous  temperature"
31710 LOCATE 11,4:PRINT "2-New          temperature"
31720 LOCATE 12,4:PRINT "3-Previous rel humidity"
31730 LOCATE 13,4:PRINT "4-New          rel humidity"
31740 LOCATE 14,4:PRINT "5-Ventilation      rate"
31750 LOCATE 15,4:PRINT "                                "
31760 LOCATE 16,4:COLOR 0,5:PRINT " FLOCK INFORMATION :":COLOR 2,0
31770 LOCATE 17,4:PRINT "1-Number of  birds"
31780 LOCATE 18,4:PRINT "2-Age      of  birds"
31790 LOCATE 19,4:PRINT "3-Avg    bodyweight"
31800 LOCATE 20,4:PRINT "4-Feed consumption"
31810 LOCATE 21,4:PRINT "5-Egg    production"
31820 LOCATE 22,4:PRINT "6-H D    production"
31830 'Write outside conditions
31840 '
31850 LOCATE 9 ,42:COLOR 4,6:PRINT " OUTSIDE CONDITIONS:  ":COLOR 2,0
31860 LOCATE 10,42:PRINT "1-Avg daily temperature"
31870 LOCATE 11,42:PRINT "2-Previous  temperature"
31880 LOCATE 12,42:PRINT "3-New          temperature"
31890 LOCATE 13,42:PRINT "4-Previous rel humidity"
31900 LOCATE 14,42:PRINT "5-New          rel humidity"
31910 '
31920 RETURN
31930 '
31940 '
31950 'END OF SUBROUTINE
32000 '-----:
32010 '      SUBROUTINE TO OUTPUT HOURLY REPORT      :
32020 '      AL-CHALABI DHIA                          :
32030 '      :                                           :
32040 '      SUBROUTINE      022                        :
32050 '-----:
32060 'This subroutine will print out the digits for the simulation
32070 'go to subroutine 8 to calculate the calender day and to
32080 'subroutine 24 to calculate wall temperature if there is
32081 'condenzation
32090 GOSUB 18000 :GOSUB 38000
32100 '
32110 'Write the month's name ,time ,day and hour
32120 '
32130 LOCATE 4,10:COLOR 1:PRINT $$:LOCATE 4,21:COLOR 5:
32135 PRINT SDOP:COLOR 2

```



```

32140 LOCATE 4,32:COLOR 7:PRINT SDF:LOCATE 4,35:COLOR 4 :PRINT D$
32150 COLOR 2:LOCATE 4,56:COLOR 3:PRINT FARM$
32160 IF FLAG=0 THEN 32170 ELSE 32190
32170 LOCATE 6,73:COLOR 0,5:PRINT " OFF":COLOR 2
32180 GOTO 32200
32190 LOCATE 6,73:COLOR 1,6:PRINT " ON ":COLOR 2,0
32200 '
32210 IF CW=1 THEN 32220 ELSE 32250
32220 LOCATE 19,43:COLOR 6,1
32230 PRINT " WATER CONDENZATION ON THE WALLS " :COLOR 2,0
32240 GOTO 32260
32250 COLOR 2,0:LOCATE 19,43:PRINT "
32260 KK$=" . m3/hr"
32270 DD$=" . m3/s"
32280 FF$=" . C"
32290 SS$=" . %"
32300 COLOR 4,0
32310 LOCATE 10,28:PRINT USING FF$;TILD :LOCATE 10,35:PRINT CHR$(248)
32320 LOCATE 11,28:PRINT USING FF$;TINW :LOCATE 11,35:PRINT CHR$(248)
32330 LOCATE 12,28:PRINT USING SS$;RHLD
32340 LOCATE 13,28:PRINT USING SS$;RHNEW
32350 LOCATE 14,28:PRINT USING DD$;VRATE/3600
32360 '
32370 COLOR 3,0
32380 LOCATE 17,24:PRINT USING " Birds";NCHKN
32390 LOCATE 18,24:PRINT USING " Weeks";AGE
32400 LOCATE 19,24:PRINT USING " . Kg";BODYW/NCHKN
32410 LOCATE 20,24:PRINT USING " . g/d/b ";FETAK
32420 LOCATE 21,24:PRINT USING " . g/d/b ";EGADJ/100
32425 LOCATE 22,24:PRINT USING " . % ";HDPOD
32430 COLOR 5,0
32440 LOCATE 10,67:PRINT USING FF$;DTMPC :LOCATE 10,74 :PRINT CHR$(248)
32450 LOCATE 11,67:PRINT USING FF$;TOLD :LOCATE 11,74 :PRINT CHR$(248)
32460 LOCATE 12,67:PRINT USING FF$;TOUT :LOCATE 12,74 :PRINT CHR$(248)
32470 LOCATE 13,67:PRINT USING SS$;RHOLD
32480 LOCATE 14,67:PRINT USING SS$;RHOUT
32490 COLOR 2,0
32500 CW=0
32510 RETURN
32520 '
32530 'END OF SUBROUTINE
38000 '-----:
38010 ' SUBROUTINE TO CALCULATE DEW POINT TEMPERATURE in C :
38020 ' AL-CHALABI DHIA :
38030 ' :
38040 ' SUBROUTINE 24 :
38050 '-----:
38060 'Calculate Dew point temperature for inside conditions in deg.C
38070 TDB=TINS:RH=RHIN :USFC=2.46
38072 GOSUB 38130
38080 'Calculate wall surface temperature in deg. C

```

```

38090      WALTP=TINS-((UWALL * (TINS-TOUT))/USFC)
38100      IF WALTP+1 <TDP THEN CW=1 ELSE CW=0
38110      IF WALTP+1 <TDP THEN COUNT=COUNT+1
38120      RETURN
38130      '-----SUBROUTINE HUMIDT-----
38140          PATM = 101.325
38150          P = PATM
38160          JR = .28705
38170      'CALCULATE SATURATION VAPOR PRESSURE FOR DRY BULB TEMPERATURE
38180          TDBK = TDB + 273.16
38190          T = TDBK
38200          GOSUB 38400
38210          PSDB = PRES
38220          WSDB = .62198 * PSDB / (P - PSDB)
38230      'CALCULATE PROPERTIES AT DESIRED STATE POINT
38240          RH = RH / 100
38250          PW = RH * PSDB
38260          W = .62198 * PW / (P - PW)
38270          DEGSAT = W / WSDB
38280          ENTH = 1.006 * TDB + W * (2501 + 1.775 * TDB)
38290          SPVOL =JR * TDBK * (1 + 1.6078 * W) / P
38300          ALFA = LOG(PW)
38310          IF PW > .611 THEN GOTO 38340
38320          TDP = 5.994 + 12.41 * ALFA + .4273 * ALFA^2
38330          GOTO 38390
38340          IF PW > 8.08 THEN GOTO 38370
38350          TDP = 6.983 + 14.38 * ALFA + 1.079 * ALFA^2
38360          GOTO 38390
38370          TDP = 13.8 + 9.478 * ALFA + 1.991 * ALFA^2
38380          TWB = TEMP
38390          RETURN
38400      '----- SUBROUTINE PRESSURE -----
38410          IF T > 273.16 THEN GOTO 38440
38420          PRES = EXP(24.2779 - 6238.64 / T - .344438 * LOG(T))
38430          GOTO 38450
38440          PRES = EXP(-7511.52/T+89.6312+.023999*T-.000011654551 *T^2-
          .000000012810336 *T^3+2.0998405D-11*T^4-LOG(T)*12.1507992 )
38450          RETURN
38460      '
38470      'Where |-----
38480      'WALTP ----- Wall temperature      in C |
38490      'USFC ----- Heat transf.coeffi.  in W/m2C |
38500      'RHIN ----- Relative humidity    in %  |
38510      'TINS ----- Inside temperature   in C  |
38520      'TDP ----- Dew point temperature in C  |
38530      '-----
38540      '
38550      'END OF SUBROUTINE
38560      '
39000      '-----
39010      ' SUBROUTINE TO PRINT OUT DAILY REPORT      '

```



```

39020 ' :          AL-CHALABI DHIA :
39030 ' : :
39040 ' :          SUBROUTINE      025 :
39050 ' :-----:
39060 'This subroutine will print out daily report
39070 'Write the headings
39080 FF$="      C      ":SS$="      %      ":DD$="      m3/s "
39090 LOCATE 4,26:PRINT "      "
39095 LINE (50,100)-(455,125),0,BF :COLOR 2,0
39100 SYMBOL (50,100)," DAILY REPORT ",3,3,1 :COLOR 2,0
39105 SYMBOL (52,101)," DAILY REPORT ",3,3,6 :COLOR 2,0
39110 LOCATE 6,65:PRINT "      "
39120 LOCATE 9, 4:COLOR 1,3:PRINT " INSIDE CONDITIONS:      ":COLOR 2,0
39130 LOCATE 10,4:PRINT "1-Avg temperature      ":LOCATE 10,28:
39135 PRINT USING FF$;TIAVG:LOCATE 10,35:PRINT CHR$(248)
39140 LOCATE 11,4:PRINT "2-Avg rel Humidity      ":LOCATE 11,28:
39145 PRINT USING SS$;RHAvg
39150 LOCATE 12,4:PRINT "3-Maximum      temp      ":LOCATE 12,28:
39155 PRINT USING FF$;TIMAX:LOCATE 12,35:PRINT CHR$(248)
39160 LOCATE 13,4:PRINT "4-Minimum      temp      ":LOCATE 13,28:
39165 PRINT USING FF$;TIMIN:LOCATE 13,35:PRINT CHR$(248)
39170 LOCATE 14,4:COLOR 3,1:PRINT " OUTSIDE CONDITIONS:      ":COLOR 2,0
39175 LOCATE 14,29:PRINT "      ":COLOR 2,0
39180 LOCATE 15,4:PRINT "1-Avg daily temp      ":LOCATE 15,28:
39185 PRINT USING FF$;DTMPC:LOCATE 15,35:PRINT CHR$(248)
39190 LOCATE 16,4:PRINT "2-Avg rel humidity      ":LOCATE 16,28:
39195 PRINT USING SS$;RHOVG
39200 LOCATE 17,4:PRINT "      "
39210 LOCATE 18,4:COLOR 0,7:PRINT "FLOCK INFORMATION:      ":COLOR 2,0
39215 LOCATE 18,28:PRINT "      ":COLOR 2,0
39220 LOCATE 19,4:PRINT "1-Number of birds      ":LOCATE 19,28:
39225 PRINT USING "      Birds";NCHK
39230 LOCATE 20,4:PRINT "2-Age      of birds      ":LOCATE 20,28:
39235 PRINT USING "      Weeks";AGE
39240 LOCATE 21,4:PRINT "3-Avg      bodyweight      ":LOCATE 21,28:
39245 PRINT USING "      Kg";BODYW/NCHK
39250 LOCATE 22,4:PRINT "4-Bird      mortality      ":LOCATE 22,28:
39255 PRINT USING "      Birds";MORCH
39260 '
39270 'Write management information
39280 '
39290 LOCATE 9 ,42:COLOR 4,6:PRINT " MANAGEMENT INFORMATION: ":
39295 COLOR 2,0
39300 LOCATE 10,42:PRINT "1-Feed intake /100      ":LOCATE 10,63:
39305 PRINT USING "      kg/day";FE100/10000
39305 LOCATE 11,42:PRINT "2-MET energy /bird      ":LOCATE 11,63:
39306 PRINT USING "      kJ/day";METAK
39310 LOCATE 12,42:PRINT "3-H D      production      ":LOCATE 12,63:
39315 PRINT USING "      %      ";HDPOD
39320 LOCATE 13,42:PRINT "4-Est egg prd/100      ":LOCATE 13,63:
39325 PRINT USING "      kg/day";EGADJ/1000

```

```

39340 LOCATE 14,42:PRINT "5-Feed cost /1000      ":LOCATE 14,63:
39345 PRINT USING "      .    $/day ";FCOST
39350 LOCATE 15,42:PRINT "6-Elec cost /1000      ":LOCATE 15,63:
39355 PRINT USING "      .    $/day";ELSUM
39360 LOCATE 16,42:PRINT "7-Fuel cost /1000      ":LOCATE 16,63:
39365 PRINT USING "      .    $/day";FUCOST
39380 LOCATE 17,42:PRINT "8-Egg revenue/1000     ":LOCATE 17,63:
39385 PRINT USING "      .    $/day";EGGSL
39385 LOCATE 18,42:PRINT "9-Revenues - costs   ":LOCATE 18,63:
39387 PRINT USING "      .    $/day";PROFT:ELSUM=0
39388 LOCATE 19,42:PRINT "                               ":
39389 LOCATE 21,43:COLOR 0,7 : PRINT COUNT
39390 LOCATE 21,46:COLOR 4,7:PRINT " Hours of water condenzation" :
39391 COLOR 2,0
39392 FOR X=1 TO 10000 :NEXT:GOSUB 23000 : RETURN
39400 'END OF SUBROUTINE
40000 '-----:
40010 '      SUBROUTINE TO CALCULATE EGG PRODUCTION      :
40020 '      AL-CHALABI DHIA                               :
40030 '      :                                              :
40040 '      SUBROUTINE      026                             :
40050 '-----:
40060 'Calculate average egg weight                        in gr
40070 '
40080 '      IF AGE>=22 AND AGE<=40 THEN 40090 ELSE 40110
40090 '      EGGWT=13.5203*(AGE^.4087) : 'For age 22-40 weeks (R2=.98)
40100 '      GOTO 40120
40110 '      EGGWT=36.1114*(AGE^.1371) : 'For age 41-80 weeks (R2=.99)
40120 'Calculate number of eggs for 1000 birds            in gr
40130 '      EGNBR=(EG100 /EGGWT)*10
40140 'Calculate number of dozens                        in dozens
40150 '      DOZNO=EGNBR/12
40160 'Calculate returns from eggs sale                  in $/100 birds
40170 '      EGGSL=DOZNO*NRPRC
40180 'Calculate hen/day production                      in %
40190 '      HDPOD=EGNBR/10
40195 '      EGADJ=(EG100/HDPOD)*100
40200 'Calculate electricity cost/1000 birbs             in $/day
40202 '      ELSUM= (ELSUM/NCHKN)*1000
40204 'Calculate sum of      cost/1000 birds             in $/day
40206 '      PRCOST=ELSUM+FUCOST+FCOST
40210 'Calculate revenues over cost                      in $/day
40212 '      PROFIT=EGGSL-PRCOST
40220 RETURN
40230 'Where:-----
40240 'E3FKG ----- egg weight /100 birds
40250 'NRPRC ----- nest run price   in $
40260 'EGNBR ----- egg number
40270 'EGGWT ----- egg weight       in gr
40280 'EGGSL ----- egg sale         in $/100 bird
40290 'DOZNO ----- dozen number

```

```
40300 'HDP0D ----- hen/day production in % |
40310 '-----
40320 'END OF SUBROUTINE
*EOS
*EOP
----- hen
```





## REFERENCES

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- Anderson, D. P., Beard, C. W., and Hanson, R. P. (1964). Adverse effects of ammonia on chickens including resistance to infection with new-castle disease virus. *Avian Diseases*, 8, 369-379.
- Arad, Z., Marder, J., and Soller, M. (1981). Effect of gradual acclimation to temperatures up to 44 C on productive performance of the desert bedouin fowl, the commercial white Leghorn and the two reciprocals. *British Poultry Science*, 22, 511-520.
- Ariel, A., Meltzer, A., and Bearman, A. (1980). The thermoneutral temperature zone and seasonal acclimatization of the hen. *British Poultry Science*, 21, 471-478.
- Barott, H. G., and Prince, E. M. (1941). Energy and gaseous metabolism of the hen as effected by temperature. *Journal of Agricultural Research*, Washington, D.C.
- Bary, D. J., and Gesell, J. A. (1961). Environmental temperature--A factor affecting performance of pullets fed diets suboptimal in protein. *Poultry Science*, 40, 1328-1335.
- Brooker, D. B. (1967). Mathematical model of the psychrometric chart. *Transaction of the ASAEA*, 10(4), 558-560.
- Bouchillon, C. W., Reece, N. F., and Deaton, J. W. (1970). Mathematical modeling of thermal homeostasis in chicken. *Transaction of the ASAE*, 13, 648-652.
- Byerly, T. J., Kessler, R. M., and Thomas, O. P. (1980). Feed requirements for egg production. *Poultry Science*, 59, 2500-2507.

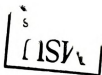
- Charles, D. R. (1984). A model of egg production. British Poultry Science, 25, 309-321.
- Charles, D. R., and Payne, C. G. (1966). The influence of the graded levels of atmospheric ammonia on chickens. I. Broilers and replacement growing stock. British Poultry Science, 7, 177-187.
- Cole, G. W. (1980). The application of control systems theory to the analysis of ventilated animal housing environments. Transaction of the ASAE, 23, 431-436.
- Cowan, P. J., and Michie, W. (1980). Increasing the environmental temperature later in lay and performance of the fowl. British Poultry Science, 21, 339-343.
- Deaton, J. W., Reece, F. N., McNaughton, J. L., and Cott, B. D. (1981). Effect of differing temperature cycles on egg shell quality and layer performance. Poultry Science, 60, 733-737.
- DeShazer, J. A., Jordan, K. A., and Suggs, C. W. (1970). Effect of acclimation on partitioning of heat loss by the laying hen. Transaction of the ASAE, 13, 82-84.
- Dixon, J. E., and Esmay, M. L. (1979). Design and management affect laying house moisture removal. ASAE Summer Meeting of ASAE and CSAS, June 24-27, 1979, Paper No. 79.4020.
- Esmay, M. L. (1978). Principles of Animal Environment. Textbook Edition. Westport: AVI.
- Esmay, M. L., and Dixon, J. (1986). Environmental Control for Agricultural Buildings. Westport: AVI.
- Greninger, T. J., DeShazer, J. A., and Gleaves, E. W. (1982). Simulation model of poultry energetics for developing environmental recommendation. Livestock Environment II, Second International Livestock Environment Symposium, April 20-23. ASAE, 234-240.

- Hahn, R. H., Purschwitz, M. A., and Rosentreter, E. E., eds. (1984). ASAE Standards 1984. Michigan: ASAE.
- Harsh, S. B., Connor, L. J., and Schwab, G. D. (1981). Managing the Farm Business. Englewood Cliffs, N.J.: Prentice-Hall.
- Heady, E. O., and Balloun, S. L. (1980). Egg production functions a time variable. Poultry Science, 59, 224-230.
- Helback, N. V., Casterline, J. L., Jr., and Casterline, C. J. (1963). The effect of the high CO<sub>2</sub> atmosphere on the laying hen. Poultry Sciences, 43, 1082-1084.
- Hellickson, M. A., and Walker, J. N., eds. (1983). Ventilation of Agricultural Structures. Michigan: ASAE.
- Henken, A. M., Groot Schaarsbserg, A. M. J., and Van der Hel, W. (1982). The effect of environmental temperature on immune response and metabolism of young chicken. 4. Effect of environmental temperature on some aspects of energy and protein metabolism. Poultry Science, 62, 59-67.
- Hiestand, W. A., and Randall, W. C. (1941). Species differentiation in the respiration of birds following CO<sub>2</sub> administration and the location of inhibitory receptors in the upper respiratory tract. Journal of Cellular and Comparative Physiology, 17(3), 333-340.
- Hill, D. T. (1983). Energy consumption relationships for mesophilic and thermophilic digestion of animal manures. Transaction of the ASAE, 26, 841-848.
- Hinkle, N. C., and Good, L. D. (1970). A comparison of ventilation control systems.. Transaction of the ASAE, 13, (4), 365-368.
- Hy-Line Layers. (1986). Management guide, Chick, Pullet, Layer. Variety W-36. (3rd). Iowa: Hy-Line Indian Revier Comp.

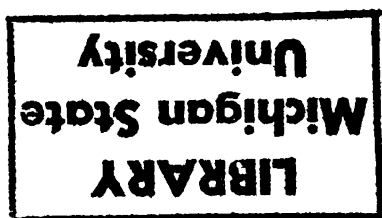
- Kotula, A. W., Drewinak, E. E., and Davis, L. L. (1957). Effect of immobilization on the bleeding of chickens. *Poultry Science*, 36 (3), 585-589.
- Longhouse, A. D. (1967). Design of poultry laying g house ventilation and insulation requirements based on calorimetric data and psychrometric relationship. *Transaction of the ASAE*, 10, 512-516.
- Longhouse, A. D., Ota, H., Emerson, R. E., and Heishman, J. D. (1968). Heat and moisture design data for broiler house. *Transaction of the ASAE*, 11, 694-700.
- Marsden, A., and Morris, T. R. (1980). Egg production at high temperatures. *Intensive livestock in developing countries*. British Society of Animal Production.
- Meltzer, A., Goodman, G., and Fistool, J. (1982). Thermoneutral zone and resting metabolic rate of growing with leghorn-type chickens. *British Poultry Science*, 23, 383-391.
- Midwest Plan Service. *Structure and Environment Handbook* (10th ed.). Iowa: ISU.
- Mitchell, H. H., and Haines, W. T. (1927). The critical temperature of chicken. *Journal of Agricultural Research*, Washington, D.C., 34 (6), 549-557.
- Mueller, W. J. (1961). The effect of constant and fluctuating environmental temperatures on the biological performance of laying pullets. *Poultry Science*, 40(6), 1562-1571.
- Mueller, W. J. (1967). The effect of two levels of methionine on the biological performance of laying pullets in controlled environments. *Poultry Science*, 45(1) 82-88.
- North, M. O. (1979). New method of estimating feed consumption as temperature changes. *Poultry Tribune*, p. 18.

- Phillips, R. E., and Esmay, M. L. (1973). Systems model of environment in egg production facility. Transaction of ASAE, 16, 152-157.
- Prince, R. P., Whitaker, J. H., Matterson, L. D., and Luginbuhl, E. (1965). Response of chickens to temperature and relative humidity environments. Poultry Science, 44, 73-77.
- Regnault, V., and Reiset, J. (1850). Chemische untersuchungen uber die respiration der thierte aus verschiedenen klassen. Ann. Chem. U. Pharm. 73, 92-123; 129-179; 257-321.
- Rouse, J., et al. (1971). Chov drubeze. (Growing Poultry). Prague: SZN.
- Timmons, M. B., and Gates, R. S. (1985). Risk analysis methodology applied to environmental control options for animal housing. Part 1. Poultry Layers ASAE Winter Meeting December 17-20, 1985, Paper No. 85-4507.
- Valencia, M. E., Maiorino, P. M., and Reid, B. L. (1980). Energy utilization in laying hens. III. Effect of dietary protein level at 21 C and 32 C. Poultry Science, 59, 2508-2513.
- Vohra, P., Wilson, W. O., and Siopes, T. D. (1979). Egg production, feed consumption, and maintenance energy requirements of leghorn hens as influenced by dietary at temperatures of 15.6 C and 26.7 C. Poultry Science, 58, 674-680.
- White, D. H., Oleary, G. J., Bartlett, B. E., and Abu-Serewa, S. (1978). Simulation of poultry egg production. Agricultural Systems, 3, 85-102.

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