A STUDY OF THE HELIUM - JET RECOIL - TRANSPORT METHOD

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This is to certify that the

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ABSTRACT

A STUDY OF THE HELIUM-JET RECOIL-TRANSPORT METHOD

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The Helium-Jet Recoil-transport (HeJRT) system has been studied for the purposes of discovering more of the detail of the mechanism of its operation and to facilitate its further development. The major portion of this thesis is a report of a series of experiments in which the operation of the HeJRT system was defined and in which the effects of varying the operating parameters of the system were recorded. This has provided an experimental basis that has allowed us to make statements on possible mechanisms of operation and the importance of certain features of the system. Of course, also included are a detailed description of our HeJRT system and sections discussing some of the extensions of HeJRT techniques that have resulted, such as those allowing the performance of on-line aqueous chemistry with the system.

The initial motivations for the construction of a HeJRT system here was its intended use as a subsystem in an on-line mass identification system to be used in conjuction with conventional nuclear counting experiments. Our present thoughts on this application are included in the introductory chapter of this thesis.

A STUDY OF THE HELIUM-JET RECOIL-TRANSPORT METHOD

Ву

Kenneth Lee Kosanke

A THESIS

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CHAPTER I

Introduction

I. a. General

There remain approximately 2000 unknown nuclides with half-lives in the range between 10^2 and 10^{-2} seconds [BeI66a]. This includes all the remaining unknown β unstable nuclei, except some superallowed β decays which may have half-lives as short as 10^{-3} seconds, in addition to proton, neutron, and γ emitters. Figure 1 (taken from [RuG67]) is an approximate breakdown of stable or very long-lived $(t_{1/2}>10^9 \text{ years})$ nuclides and unknown nuclides lying between the limits of the neutron drip line and proton stability. Further, there is an indication of expected half-lives. Clearly most of these remaining unknown nuclides are expected to have half-lives of less than one second and they will outnumber the nuclides presently known. The remainder of this introduction will be devoted to a short discussion of why and how these nuclides should be investigated.



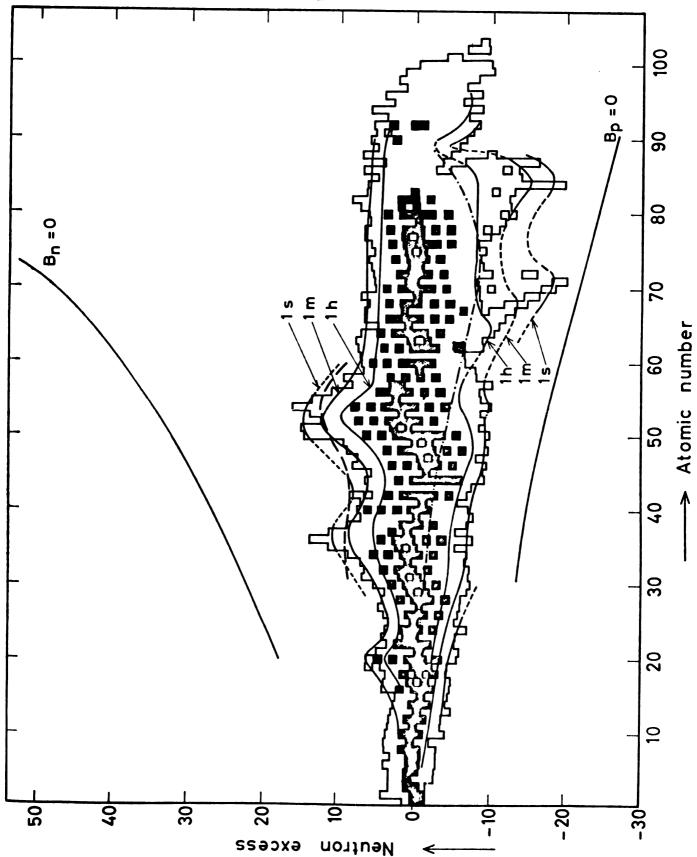


Figure 1. Approximate breakdown of nuclides lying between the neutron drip line and proton stability according to half-life. This figure is taken from [BeI66a].

I. b. Why Nuclides far from β Stability Should be Studied β -Delayed Particle Emission

Beta-delayed particle emission occurs when as a result of β -decay the nucleus is left in an excited state, one for which the binding energy for the last neutron, proton, or α particle is negative and Coulomb barrier penetration in the case of protons or α particles competes with γ deexcitation. Cases of β -delayed particle emission have been observed for each type particle.

These decays are accessible to study using techniques designed for working with activities with half-lives greater than 10^{-2} seconds because the overall half-life for these processes is determined by the half-life of the β decay. Most of these cases found thus far are in the low-Z region where the energy available for decay and the average level spacings are large; however, now cases are being reported in the higher-Z region. Also found are regions where the binding energy for an α particle or the last proton or neutron is low, such as just above a closed shell.

The number of unknown delayed particle emitters should be quite large [BeI66a][BeD65]. Through a careful mapping of these nuclides and consideration of their particle emission energies, further refinement of the parameters in the semiempirical mass formula should be possible. Also, as far as these parameters relate to nuclear structure, further refinement there may be possible.

Particle Emission

In addition to delayed particle emission, proton and α emission begin to compete successfully as modes of decay as one proceeds further from β stability. Many of the least energetic of these decays will have half-lives in the 10^2-10^{-2} second range because of the difficulty of Coulomb barrier penetration. A study of these nuclides should yield information on both nuclear masses from the energetics of the decays and on nuclear wave functions from half-lives, which reflect the ability of the emitted particle to penetrate the Coulomb barrier.

New Doubly Magic Regions

It should be possible to reach the doubly magic 28-28 region using proton reactions and the 50-50 region using heavy ion reactions. Several of the nuclides only one or two nucleons removed from ⁵⁶Ni and most of the nuclides of the ¹⁰⁰Sn region remain unknown. A study of these nuclides one nucleon removed from doubly magic will of course involve a determination of their levels. Accordingly, these experimentally determined levels can then be used to extend calculations to the levels in nuclides further removed.

Transition Region Nuclides and New Deformed Regions

It is known in at least one case that practically spherical eveneven nuclei may remain spherical as nucleon pairs are added until it very suddenly "collapses" with the addition of another nucleon pair to a shape of stable deformation. This is evidenced by the vibrational nuclear structure suddenly changing to a rotational one with the addition of a nuclear pair. The example of this "collapse" or transition between essentially spherical and permanently deformed nuclei takes place in the beginning of the rare earth region between neutron numbers 88 and 90 [BeI66a]. (A second example of the sudden onset of deformation may be occurring at about 135Nd [EkC72].) Nuclear states in the region of this sudden transition should not be amenable to either purely vibrational or rotational description. There have not been many of the nuclides of this type experimentally investigated and many more experimental studies are needed. Further, expanding decay studies to nuclides further from \$\beta\$ stability will yield information on many more deformed nuclides including many in new deformed regions, such as the one starting in the extremely neutron deficient Xe- and Ba- isotopes [MoH65][ShR61].

Access to Highly Excited States

Because of the high energies associated with β decay far from the stability line, it will be possible to populate highly excited states in this decay. Beta decay will then complement nuclear reaction studies in examining these states. If one also considers the difficulty in obtaining suitable, i.e., stable or long-lived targets for nuclear reaction studies on nuclei far from β stability, it is probable that

 β -decay studies will become the primary means of investigating these states.

Nuclear Masses from Q-values

The semi-empirical mass formula is in a sense a measure of a quantitative understanding of nuclei. Nested in the upwards of 40 parameters necessary to get accurate predictions are liquid drop model effects, shell model effects, and effects from other models. Accurate experimental masses measured in regions chosen to test specific parameters are thereby testing nuclear models and conceivably may lead to a more fundamental composite model. Many of the most interesting mass measurements will be made on nuclei far from β stability and can be made through determination of reaction Q values.

Results of Interest in Astrophysics

One of the more basic goals of astrophysics is that of developing models that will account for the relative abundances of elements in the universe. Two of the most important types of experimental information necessary to develop such a model are decay half-lives and cross-sections. Many of the more important half-lives, in particular those necessary to account for the build-up of elements above 209 Bi are of nuclei lying far from β stability [BeI66a].

In addition, there are many specific bits of nuclear information missing about nuclear reactions, decay energies, branching ratios, etc.,

that are necessary to check and extend current astrophysical theories. Much of this needed information is about nuclei lying far from $\boldsymbol{\beta}$ stability.

I. c. How Nuclides Far From β Stability Can be Studied

There are several difficulties associated with the study of nuclides far from β stability which have definitely limited their study using standard nuclear techniques. Accordingly, any serious attempt at extending nuclear investigations to regions far from β stability will have to provide new or improved techniques to overcome these difficulties. The degree of success in overcoming these difficulties will determine the profitability of any attempt at studying nuclei far from β stability. The remainder of this introduction will be devoted to a short discussion of the requirements these difficulties impose on any system to study nuclides far from β stability and how our proposed systems meet these requirements. A discussion of those techniques proposed or being implemented by other researchers studying nuclides far from β stability is beyond the scope of this thesis [MaR72b][AnG66].

The most obvious requirement of any system designed to study nuclides far from β stability is that it must provide a method of generating these nuclei in sizeable number. In a paper prepared for presentation at the International Symposium on Why And How Should We Investigate Nuclides Far Off The Stability Line [RuG67], Rudstam presents a comparison of several possible methods for producing nuclides far from β stability. The processes considered are medium energy (<50 MeV) charged particle (p,d,α) reactions like (p,xn); high energy proton reactions like (p,2p), spallation (p,2pxn), and proton induced fission;

heavy ion induced reactions like (HI,m); thermal neutron fission; and (n,p) reactions with energetic (14-MeV) neutrons. The comparison between these processes is made for target material between Z=25 to 75.

While Rudstam's comparison is based on estimates of cross-sections and more or less typical beam intensities of different types of machines used to generate radionuclides, a presentation of a summary of his conclusions may be helpful. For the production of moderately neutron-deficient isotopes (≤10 neutrons deficient) throughout the range of Z=25 to Z=75, medium energy charged particles (p,d,α) should prove to be best by far. However, as one proceeds to extremely neutron deficient isotopes, heavy-ion and spallation reactions should compete well with medium-energy proton reactions for the best production rates, with heavy-ion reaction producing better yields than spallation. For the production of neutron-rich isotopes throughout the range Z=35 to Z=55, thermal fission should prove to be best by far. However, in the region below Z=35, high-energy proton and spallation reactions are favored and in the region above Z=55 high energy proton reactions like (p,2p) are favored. One of Rudstam's figures (that for Z=55) has been Rudstam's figure of merit (FM) is defined by the included as Fig. 2. relation

$$FM = \int_0^d I(x) \sigma(x) \rho dx,$$

where I is the particle density, σ is the reaction cross-section, ρ is the target density, and d is the thickness. Rudstam assumed the following beam intensities:

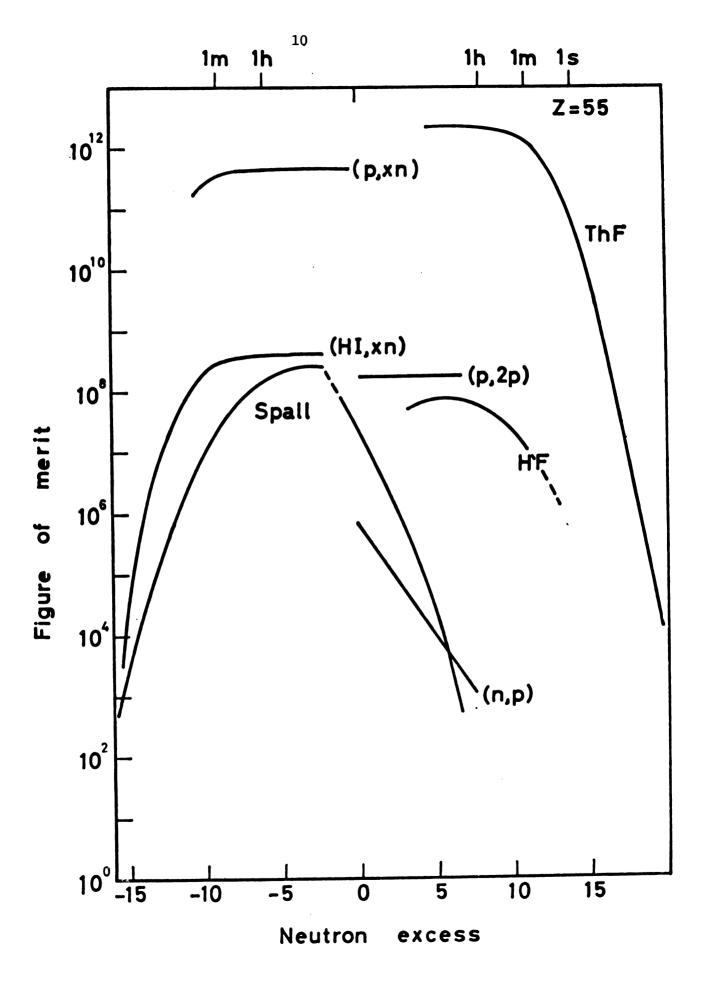


Figure 2. Graphic display of the usefulness of various techniques for generating radionuclides from targets with Z=55. This figure

Med. energy p or d 100 μ A

High energy p 1 μ A

Heavy ions 6×10^{12} HI/sec

Thermal n $10^{14} n/\text{cm}^2\text{sec}$

High energy n (14-MeV) 10^{10} $n/\text{cm}^2\text{sec}$

In those instances where experimental cross-sections were not available, Rudstam used extrapolated or estimated values.

A second requirement for the system is that it be capable of providing the radionuclides in a form suitable for study in times approximately equal to their half-lives. If we wish to consider β unstable nuclides out to the limits of the neutron drip line and proton stability, then it is necessary to consider times as short as 10⁻² seconds (and possibly even as short as 10⁻³ sec for a few superallowed transitions). To the extent that it is desirable not to count in beam or to use pulsed beam techniques, it is necessary to transport the activities to low background areas. In addition, for charged particle spectroscopy, it is necessary to accomplish a removal of the radionuclides from the target material in order to make a suitable source for counting, all in these short times. Further, in that daughter activities will be rapidly built up, it is necessary to provide for the continuous removal of old source material after being counted for some time interval.

For each of the possible mechanisms for generating nuclides far from β stability (proton or heavy ion induced reactions or fission), a large number of different product nuclei will result and in most

instances the interfering products will greatly out-number the desired products. Thus, an additional requirement of the system is that it provide some means of isolating or at least enriching the desired product nuclei in order to limit interfering radiations. Ideally this would be accomplished using a combination of chemical and isotopic separations.

The earlier discussion of Rudstam's paper suggests that it will be possible to produce nuclei far from β stability in good yields using proton beams with energies <50 MeV or ³He beams with energies <75 MeV (with currents <5 μ A on target) from the Michigan State University Sector Focused Isochronous Cyclotron to initiate (p,xn) or $(^3\text{He},xn)$ reactions. Table 1 (in Chapter II) provides a listing of some of the reactions that are possible using these beams from the MSU Cyclotron. In most regions of the nuclear chart it should be possible to reach from one to four nuclei beyond those presently reported and several nuclei beyond those for which fairly complete data are available. In addition, it is anticipated that the MSU Cyclotron will be capable of producing heavy ion (carbon, etc.) beams before too long. It may then be possible to extend even further into the extremely neutron-deficient regions. However, the yields for these reactions will be less than those with p or ³He beams.

Block and schematic drawings of one of two on-line mass separation systems presently under consideration are shown in Figure 3. At this time the system and the operation of its component parts will only be

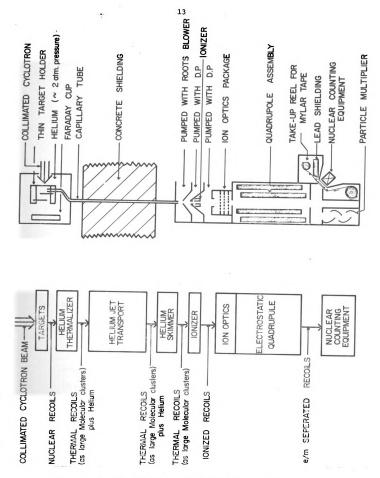


Figure 3. Sketch and block drawing of a proposed on-line system employing an electric quadrupole for mass filtering.

discussed briefly. A more detailed discussion of its construction and operation will follow in later sections.

In the Helium Jet Recoil Transport (HeJRT) portion of the system a collimated cyclotron beam enters the apparatus, striking a thin target (or a series of thin targets) in an atmosphere of helium. Those nuclei near the back of the target that interact with the beam will recoil out of the target into the helium atmosphere. Some of the characteristics of these nuclear recoils for a few representative targets and beams are listed in Table 1. The nuclear recoils are slowed to thermal energies by collisions with the helium atoms. cent work by R. D. Macfarlane [JuH71] and in this lab suggest the next step is the attachment of the thermal recoils to large molecule clusters (with masses up to 10^8 amu). These cluster molecules are formed in the plasma generated by the cyclotron beam passing through the helium atmosphere from impurities added to the helium. The nuclear recoils are then removed from the target chamber by differentially pumping the helium containing the molecular clusters out through a polyethylene capillary. The capillary is run through concrete shielding to a low background area about 40 feet away.

At the end of the capillary most of the helium will be removed using a one or two stage skimmer. Quite efficient skimming should be possible by just directing the flow coming from the capillary at a coincal orifice [MaR72] [NiJ70]. The molecular clusters with their enormous masses are extremely well collimated (see Section II. g.

"Capillary Considerations") and will be passed quite efficiently through the orifice, whereas the helium will have a much larger angle of divergence as it leaves the capillary and will therefore largely be pumped off. If our pumping capacity is not sufficient to reduce the pressure after the first skimmer stage to the low pressures required to operate the electric quadrupole, a second skimmer stage will be used.

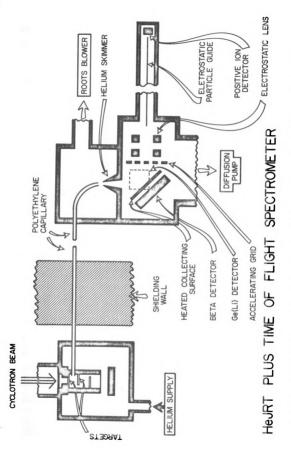
The molecular cluster will be broken up and the nuclear recoils ionized using a discharge set up in one of the skimmer stages, with the recoils directed into the ion optics associated with the electric quadrupole. With the quadrupole set up properly, only selective masses (e/m) will be transmitted through it [PaW58]. At the exit of the quadrupole the mass separated ions will be deflected either into an electron multiplier such that it will be possible to obtain a mass scan or onto paper or aluminized mylar tape for conventional nuclear counting.

It appears this system will be capable of providing mass-separated nuclear reaction products, separated from the target and transported to a low background area, in very short times (>100 msec, Section II.g. "Capillary Considerations"), continuously, and with daughter activities removed. Thus, this system should meet all the requirements mentioned previously, with the exception of providing a chemical separation in addition to the mass separation provided by the electric quadrupole. It now seems that it may be possible to accomplish this chemical separation at the time of attachment of the nuclear recoil to the molecular cluster during thermalization (see Section II.o. "Plasma Chemistry").

A second system, and the one we will most probably construct first and patterned directly after R. D. Macfarlane's "MAGGIE" system [JuH71], is sketched in Figure 4. At this time the system and the operation of its components will be discussed only briefly. A more detailed discussion of its construction and operation will follow in later sections.

The first portion of this system as in the first system described is the Helium Jet Recoil Transport (HeJRT) subsystem; its operation was described above. Again, as in the first system described, the flow from the capillary is directed at a conical orifice (helium skimmer) to remove most of the helium from the flow and allowing most of the large molecular clusters with their nuclear recoil atoms attached to pass to the next stage of the system.

The next stage of the system is a time-of-flight spectrometer. The molecular clusters with their nuclear recoils still attached are collected on a metal plate just after the helium skimming orifice. The clusters stick to the surface on impact with it. Macfarlane has found that if the proper impurities were used to generate the molecular clusters and if the collecting surface is heated to about 200° C, the cluster molecule is broken up and driven off, leaving the nuclear recoil bound very weakly to the collecting surface. As the activities on the collecting surface β decay, the portion that decay with the proper geometry will recoil from the collecting surface. Some fraction of these β recoils will become ionized by shake-off and will be accelerated away from the collecting surface, using an accelerating grid. The



Sketch of a proposed on-line system employing a recoil time-of-flight spectrometer for mass identification. Figure 4.

accelerated β recoils are electrostatically focused and enter a particle guide which consists primarily of a charged wire running down the center of a grounded metal pipe. The β recoils follow the trajectory of a helix about the central wire. A detector for the β recoils is placed at the end of the particle guide.

If the β particle from the decay is observed in the detector behind the collecting surface, it can be used to fix the time of the decay. The time of flight of the β recoil can then be established using the output of the positive-ion detector at the end of the particle guide. Knowing the accelerating voltage and the length of the flight path, the mass of the β recoil can be determined. The outputs from the β and positive-ion detector will provide start and stop signals for a time to amplitude converter (TAC) where the output in this case will be proportional to the mass of the β recoil. Then if a γ detector is placed in the region of the collecting surface where the decay is taking place and the output of the TAC is used to route the ADC output from the γ detector into different memory locations a series of γ spectra will be recorded, each associated with a particular mass β recoil.

It appears this system will be capable of providing mass identified Y spectra in very short times (≥100 msec), continuously and without significant interference from daughter activities. As in the previously described system, it is possible to consider performing a chemical separation at the time of attachment of the nuclear recoil to the molecular cluster in the target assembly. However, this may

be a more difficult task in view of the added requirement that the cluster molecules break up on heating of the collecting surface.

CHAPTER II

HELTIM JET RECOTL TRANSPORT SYSTEM

II. a. General

Quite apart from its intended use as the first stage of the isotope separator described at the close of the introduction, the helium jet recoil transport (HeJRT) system can be used to provide sources suitable for most nuclear counting experiments. It can provide sources in which the radionuclides have been physically separated from the target and continuously transported to a low background in times <250 msec. Accordingly, the HeJRT system has been used with increasing frequency to provide α , β , and γ sources for study in this lab [Gig71], [B1J72], [KoK72].

While in essence the operation of the HeJRT system is quite simple, much of the detail of its operation is not understood. Thus, satisfactory operation of the system is achieved more by using techniques that are better described as artful rather than scientific. As a result, when one collects the thoughts and impressions of researchers using some form of HeJRT system, one gets a collection in which much of the fine detail of its operation and many of the corresponding "best recipes" are not widely accepted. What follows in this Chapter are my thoughts and impressions on the construction, operation, and use of the HeJRT system we have constructed.

II. b. Calculation of Recoil Characteristics

Table 1 was prepared to point out possible nuclear reactions and to display some of the expected characteristics of the recoiling reaction products. The targets were chosen to approximately span the mass range of targets we expect to use in the HeJRT system. While the highest beam energies listed in the Table are not the upper limit of the MSU cyclotron, they are nearly the highest energies run routinely. Also, possible reactions and recoil characteristics for deuteron and α beams were omitted to keep the table short.

Probable (p, xn) and $(^3\text{He}, xn)$ reactions were determined solely on the basis of Q values (Q values were determined by Clare Morgan [MoC71] using the mass tables of Garvey, Grace, and Talmi or of Harvey). Where Q values were not known an estimate was made based on an extrapolarion from known Q values following systematically from other known Q values in the region. In several cases for the beam energies listed it may be possible to boil out an additional neutron. However, the yields for these reactions should be smaller than for those listed in the table. There was no attempt to account for any additional energies needed over the Q value to initiate the reaction, such as overcoming the centrifugal barrier. Also, there was no attempt made to determine the extent to which reactions involving the loss of charged particles will compete with the reactions listed. It should be expected that reactions involving the loss of charged particles will compete favorably with most of the xn reactions, particularly for those that involve

Reactions and Recoil Characteristics Expected Using the MSU Cyclotron Table 1.

y Reaction Energy of Energy of Energy of Energy of Energy of Energy of England In Target In			Probable		Initial	Maximum	Maximum Range of Recoils [c]	coils [c]	
10 NeV p (p,2n) 23A1 1.11 0.37 0.065 45 MeV p (p,3n) 22A1 1.11 0.37 0.082 0.082 35 MeV 3He (3He,3n) 22A1 1.15 0.50 0.082 0.124 0.69 0.124 0.69 0.124 0.69 0.124 0.69 0.124 0.69 0.124 0.69 0.124 0.69 0.124 0.69 0.124 0.69 0.124 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.013 0.69 0.014 0.000 0.24 0.000 0.0		Finerov	xx Reaction	Reaction	Energy of	In Ta	rget	In Helium	
30 MeV p ($p,2n$) 2^3A_1 1.1 0.37 0.065 45 MeV p ($p,3n$) 2^4S_1 1.6 0.50 0.082 35 MeV p ($p,3n$) 2^4S_1 3.4 0.69 0.124 70 MeV p ($p,3n$) 4^9M_1 0.57 0.20 0.20 0.138 35 MeV p ($p,3n$) 4^9M_1 0.57 0.20 0.20 0.013 35 MeV p ($p,3n$) 4^9M_1 0.57 0.20 0.29 0.013 35 MeV p ($p,3n$) 4^9M_1 0.84 0.95 0.013 0.84 0.29 0.013 35 MeV p ($p,2n$) 4^9M_1 0.84 0.95 0.013 0.084 0.95 0.013 30 MeV p ($p,2n$) 9^5R_1 0.30 0.30 0.08 [d] 0.002 [d] 30 MeV p ($p,4n$) 9^5R_1 0.30 0.45 0.11 [d] 0.003 [d] 45 MeV p ($p,4n$) 9^6P_1 0.45 0.11 [d] 0.005 [d] 30 MeV p ($p,4n$) 9^6P_1 0.14 0.014 0.057 0.14 0.08 [d] 0.001 [d] 35 MeV p ($p,4n$) p	Target	Particle	[a]	Product	(MeV)	(mg/cm^2)	(Mils)	(Mils)	
45 MeV p (7,37) $2^{2}A_{1}$ 1.6 0.50 0.082 35 MeV $^{2}B_{1}$ (7,127) $^{2}A_{2}$ 1.6 0.69 0.124 70 MeV $^{2}B_{1}$ (7,127) $^{2}A_{2}$ 1.19 0.188 30 MeV $^{2}B_{1}$ (7,127) $^{4}B_{1}$ 0.57 0.20 $^{[4]}$ 0.09 0.124 45 MeV $^{2}B_{1}$ (7,127) $^{4}B_{1}$ 0.57 0.20 $^{[4]}$ 0.009 $^{[4]}$ 0.009 $^{[4]}$ 0.009 0.013 30 MeV $^{2}B_{1}$ (3,124) $^{4}B_{1}$ 0.30 0.03 0.03 0.041 0.057 0.027 0.027 0.027 0.041 0.057 0.041 0.009 0.045 0.041 0.009 0.045 0.041 0.009 0.045 0.041 0.009 0.045 0.011 0.009 0.045 0.011 0.009 0.045 0.011 0.009 0.014 0.001 0.098 0.014 0.001 0.098 0.014 0.001 0.098 0.017 0.009 0.098 0.017 0.009 0.098 0.017 0.009 0.098 0.017 0.009 0.098 0.017 0.009 0.098 0.017 0.009 0.098 0.009	24Ma	30 MeV n	(n 2n)	2341	1.1	0.37	0.065	750	
35 MeV ⁵ He ⁽⁵ He, 3n) ²⁴ Si 3.4 0.69 0.124 70 MeV ³ He ⁽⁵ He, 3n) ²⁴ Si 3.4 0.69 0.124 70 MeV ³ He ⁽⁵ He, 3n) ⁴ 9Mn 0.57 0.20 [d] 0.009 [d] 45 MeV ⁶ He ⁽⁵ He, 3n) ⁴ 9Mn 0.57 0.29 0.013 35 MeV ⁷ He ⁽⁵ He, 3n) ⁴ 9Fe 1.9 0.58 0.027 70 MeV ⁷ He ⁽⁵ He, 5n) ⁴ 9Fe 3.6 0.007 30 MeV ⁷ P ⁽⁶⁾ He, 5n) ⁹⁵ Rh 0.30 0.08 [d] 0.002 [d] 45 MeV ⁷ P ⁽⁶⁾ He, 3n) ⁹⁵ Rh 0.45 0.11 [d] 0.003 [d] 50 MeV ⁷ P ⁽⁶⁾ He, 5n) ⁹⁵ Rh 0.45 0.11 [d] 0.003 [d] 70 MeV ⁷ P ⁽⁷⁾ He, ²⁰⁰ Pb 0.14 0.00 [d] 70 MeV ⁷ P ⁽⁷⁾ He, ²⁰⁰ Pb 0.14 0.00 [d] 45 MeV ⁷ P ⁽⁷⁾ He, ²⁰⁰ Pb 0.14 0.00 [d] 70 MeV ⁷ P ⁽⁷⁾ He, ²⁰⁰ He ⁽³⁾ He, 4n) ²⁰⁰ Pb 0.21 0.00 [d] 70 MeV ⁷ P ⁽⁷⁾ He, ²⁰⁰ He ⁽³⁾ He, 4n) ²⁰⁰ He ⁽³⁾ He ⁽³⁾ He, 4n) ⁽³⁾ He ⁽³⁾ He ⁽³⁾ He, 4n) ⁽³⁾ He ⁽³⁾	911	MeV	(p,3n)	22A1	1.6	0.50	0.082	770	
70 MeV ³ He (³ He, 5n) ² S ₅ I 6.4 1.19 0.188 30 MeV ^p (p, 3n) ^{4,9} Mn 0.57 0.20 [d] 0.009 [d] 45 MeV ^p (p, 3n) ^{4,9} Mn 0.84 0.29 0.013 35 MeV ³ He (³ He, 3n) ^{4,8} Fe 3.6 0.057 30 MeV ^p (p, 2n) ^{9,5} Rh 0.30 0.08 [d] 0.002 [d] 45 MeV ^p (p, 4n) ^{9,5} Rh 0.45 0.11 [d] 0.003 [d] 45 MeV ^p (p, 4n) ^{9,6} Rh 0.45 0.11 [d] 0.006 [d] 30 MeV ^p (³ He, 3n) ^{9,6} Rh 0.45 0.14 0.00 [d] 30 MeV ^p (p, 6n) ^{19,8} Pb 0.21 0.00 [d] 45 MeV ^p (p, 6n) ^{19,8} Pb 0.21 0.00 [d] 30 MeV ^p (p, 6n) ^{19,8} Pb 0.21 0.00 [d] 35 MeV ^p (p, 6n) ^{19,8} Pb 0.21 0.00 [d] 35 MeV ^p (³ He, 4n) ^{20,2} Bi 0.50 0.08 [d] 36 MeV ^p (³ He, 4n) ^{20,2} Bi 0.50 0.00 [d] 37 MeV ³ He (³ He, 4n) ^{20,2} Bi 0.50 0.00 [d] 38 MeV ³ He (³ He, 4n) ^{20,2} Bi 0.50 0.00 [d]		MeV	$(^{5}$ He, $3n)$	24S1	3.4	0.69	0.124	1300	
30 MeV p $(p,2n)$ $^{4}9Mn$ 0.57 $0.20^{[d]}$ $0.009^{[d]}$ $4.9Mn$ 0.84 0.29 0.013 $4.8Mn$ 0.84 0.84 0.29 0.013 0.0013 $0.08 - 1.9$ $0.08 - 1.9$ 0.0013		MeV	$(^{3}\text{He}, 5n)$	22 S1	7.9	1.19	0.188	1700	
45 MeV p (p , 3 n) 48 Mm 0.84 0.29 0.013 50 He, 3 n) 50 He (5 He, 3 n) 50 He (50 He, 3 n) 50 He (5 He, 5 n) 50 He (5 He, 3 n) 50 He (5 He, 4 n) 50 He (5 He, 8 n) 50 He (5 He) 50	⁵⁰ C r	30 MeV p	(p, 2n)	4 9 _{Mn}	0.57	0.20[4]	0.009 ^[d]	180 ^[d]	
35 MeV 3 He 3 He 3 He, 4 He 4		MeV	(p,3n)	$^{ m h}_{ m W}$	0.84	0.29	0.013	280	
70 MeV 3 He 3 He, 5 π) 48 Fe 5 Fe 5 3.6 0.041 30 MeV p p p p 4.7) 95 Rh 0.30 0.08 [d] 0.002 [d] 45 MeV p p p p 4.7) 95 Rh 0.45 0.11 [d] 0.003 [d] 55 MeV p 3 He 3 He, 5 6π) 93 Pd 2.0 0.24 [d] 0.006 [d] 70 MeV p p p p p 4.5 MeV p p p 6.7 p 4.7) p 6.7 p 6.0 0.14 0.001 [d] 45 MeV p p p p 6.7 p 6.7 p 7 0.005 [d] 50 MeV p p p p 6.7 p 6.7 p 7 0.005 [d] 50 MeV p $^{$		MeV	$(^3\text{He}, 3n)$	50Fe	1.9	0.58	0.027	530	
30 MeV p ($p,2n$) 95Rh 0.30 0.08[d] 0.002[d] 45 MeV p ($p,4n$) 95Rh 0.45 0.11[d] 0.003[d] 0.003[d] 35 MeV 3 He (3 He,3 n) 96Pd 1.0 0.24[d] 0.006[d] 0.006[d] 0.006[d] 0.006[d] 0.006[d] 0.014 0.52 0.014 0.02[d] 0.001[d] 0.001[d] 0.001[d] 0.001[d] 0.003[d] 0.005[d]		MeV	$(^{3}\text{He}, 5n)$	⁴⁸ Fe	3.6	0,95	0.041	970	
45 MeV $\stackrel{p}{p}$ ($\stackrel{p}{p}$, 4 n) 93Rh 0.45 0.11[d] 0.003[d] 35 MeV 3 He (3 He, 3 n) 96Pd 1.0 0.24[d] 0.006[d] 0.006[d] 0.006[d] 0.014 0.52 0.014 0.52 0.014 0.014 0.02[d] 0.001[d] 0.014 0.02[d] 0.001[d] 0.001[d] 0.001[d] 0.003[d] 0.003[d] 0.003[d] 0.005[d] 0.005	96Ru	30 MeV p	(p, 2n)	⁹⁵ Rh	0.30	0.08[4]	0.002[4]	60 [4]	
35 MeV 3 He $^{(3)}$ He, $^{(3)}$ n) 96 Pd 1.0 0.24 $^{[d_1]}$ 0.006 $^{[d_1]}$ 70 MeV $^{(3)}$ He, $^{(6)}$ n) $^{(2)0}$ Pb 0.14 0.02 $^{[d]}$ 0.001 $^{[d]}$ 45 MeV $^{(2)}$ ($^{(2)}$ 6n) $^{(2)}$ 6n) $^{(2)2}$ 81 0.50 0.08 $^{[d]}$ 0.003 $^{[d]}$ 70 MeV $^{(3)}$ He, $^{(3)}$		MeV	(p,4n)	$^{93}\mathrm{Rh}$	0.45	0.11[4]	0.003[4]	80[4]	
70 MeV 3 He $^{(3)}$ He, $^{(6)}$ N) 93 Pd 2.0 0.52 0.014 30 MeV $^{(6)}$ Ph 0.14 0.02 [d] 0.001 [d] 45 MeV $^{(6)}$ Ph 0.21 0.04 [d] 0.001 [d] 35 MeV $^{(6)}$ Ph 0.281 0.50 0.08 [d] 0.003 [d] 70 MeV $^{(3)}$ He $^{(3)}$ He, $^{(3)}$		MeV	$(^{3}_{He}, 3n)$	Pd_{96}	1.0	0.24 ^[d]	0.006141	200[d]	
30 MeV p ($p,4n$) 200 Pb 0.14 0.02[d] 0.001[d] 45 MeV p ($p,6n$) 198 Pb 0.21 0.04[d] 0.001[d] 35 MeV 3 He (3 He,4 n) 2 02Bi 0.50 0.50 0.08[d] 0.005[d] 198Bi 0.98		MeV	$(^3$ He, $6n)$	Pd_{E6}	2.0	0.52	0.014	390	
45 MeV \dot{p} (\dot{p} ,6 n) $^{198}{Pb}$ 0.21 0.04[d] 0.001[d] 35 MeV $^{3}{He}$ ($^{3}{He}$,4 n) $^{202}{Bi}$ 0.50 0.08[d] 0.003[d] 70 MeV $^{3}{He}$ ($^{3}{He}$,8 n) $^{198}{Bi}$ 0.98 0.17[d] 0.005[d] 1	203T1	30 MeV p	(p,4n)	200 Pb	0.14	0.02[4]	0.001[4]	20[4]	
MeV 3 He (3 He, $^4\pi$) 202 Bi 0.50 0.08[4] 0.003[4 J MeV 3 He (3 He, $^8\pi$) 198 Bi 0.98 0.17[4 J 0.005[4 J]		MeV	$(\bar{p},6n)$	^{198}Pb	0.21	0.04[4]	0.001[4]	20 ^[d]	
MeV 3 He (3 He, 8π) 198 Bi 0.98 0.17 ^[4] 0.005 ^[4]		MeV	$(^3$ He, $4n)$	202B1	0.50	0.08[4]	0.003[4]	60[4]	
	**	MeV	(3He,8n)	198 B1	0.98	0.17[4]	0.005141	110[4]	

In several cases for the beam energies used in this table, it may be possible to boil out an addi-Probable (p,xn) or $(^3\text{He},xn)$ reactions were determined on the basis of Q values determined using the mass tables of Garvey, Gerace and Talmi or of Harvey [MoC71]. Where Q values were not known an estimate was will compete with each of the xn reactions listed. However, some of the reactions involving the loss of charged particles are expected to compete well with the xn reactions at high energies, low-2 targets, or tional neutron. However the yields for these reactions should be smaller than for the reactions listed. There was no attempt to determine the extent to which reactions involving the loss of charged particles very neutron-deficient regions.

The initial recoil energies were determined on the basis of conservation of linear momentum between the particles of the beam and the compound nucleus and considering no additional sources of momentum in the breakup of the compound nucleus.

[P]

В

- Corrections to the range were made to account for the mass of the recoil differing from the mass of the isotope reported Also, interpolation was done between the stopping media reported in the table to obtain the ranges in the in the table. The corrections assumed the primary source of energy loss to be from electronic stopping. [c] Recoil ranges were determined using the range tables of Northcliff and Schilling [NoL70].
- further complicated by the nuclear stopping collisions occurring between approximately equal mass particles. tables. These results have particularly large uncertainties associated with them due to a large portion [d] For particularly low values of e/m ($e/m \le 0.0125$ MeV/amu) the ranges were obtained by extrapolating the of their range being determined by nuclear stopping. In the case of the ranges in the targets this is

high beam energies, low-Z targets, and very neutron-deficient regions.

Parameters such as target thickness, target separation, and helium pressure used in setting up the target chamber for a run are based on calculations of the energy for the nuclear recoils. For several reasons these calculations were kept simple and contain many assumptions. The foremost reason was the large uncertainties associated with the range of very low energy, high mass particles, which makes precise calculation of recoil energy unrewarding. Second, in most instances it is possible to use values in setting up the experiment that are on the safe side of the calculated values by factors of 2 or 3 without seriously impairing the operation of the HeJRT system.

As a result of the medium energies of the particle beams generated by the cyclotron, the primary mechanism for the nuclear reactions involves compound nucleus formation. It is a simple matter to calculate the recoil energy of the compound nucleus by just considering linear momentum conservation (effects such as the energy transferred to the lattice holding the target nucleus are too small to be considered). The most extreme assumption made in calculating recoil energies is that there are no additional sources of momentum for the recoil associated with the breakup of the compound nucleus. This is clearly not the case and further this source of momentum can be quite large. However, in that the breakup of the compound nucleus will be roughly isotropic, the gross features of the energy distribution of recoils leaving the target will be unchanged. The exception would be the

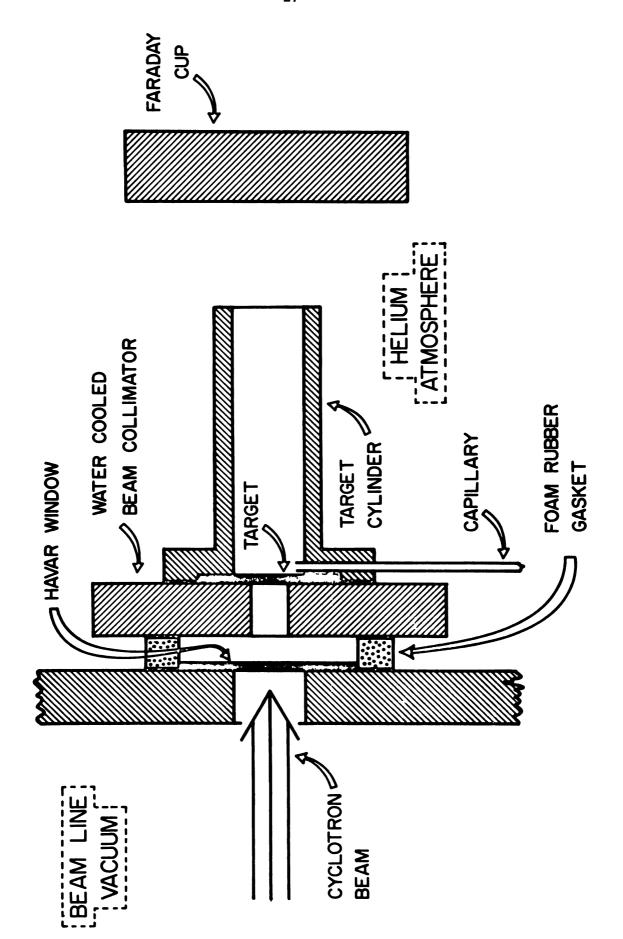
high energy tail corresponding to recoils generated at backside of the target that have had their recoil energies altered in the breakup of the compound nucleus.

Maximum recoil ranges in the target and in He(STP) were determined using maximum recoil energies. The ranges were obtained from the range tables of Northcliffe and Schilling [NoL70]. In many instances the maximum recoil energies fall below the lowest reported in these tables. For these cases the ranges reported were extrapolated off the end of the tables. It should be expected that the uncertainties associated with recoil ranges in the target determined by extrapolation are large. Within the limits of the tables, Northcliffe and Schilling determine their ranges considering energy losses occurring through both electronic and nuclear stopping mechanisms. in the case of very low energy recoils (recoil velocities $<10^8$ cm/sec [HaB60]) the energy loss mechanism is primarily through nuclear stopping. In the case of the recoils traveling through the target, the mass of the recoil and the mass of nuclei in the stopping medium are essentially equal and the recoil can lose up to half its energy in a single collision. Accordingly, the ranges for these recoils will vary considerably recoil to recoil and the calculated ranges can only be considered an average effect.

II. c. Target Assemblies

A sketch of a target assembly employing a single target is included as Figure 5. Here the cyclotron beam enters from the left through a Havar window (0.001 in. in practice) separating the vacuum of the beam line from the helium atmosphere (1 to 4 atm pressure, typically run at 3 atm). See Sections II. i. "Efficiency vs. Target Assembly Pressure" and II. g. "Capillary Considerations" for discussions of the effect of He pressure on transport efficiency and on transport times, respectively. The volume between the Havar window and the target is sealed with a foam rubber gasket. This is to prevent those recoils from the window that are thermalized in this volume from entering the bulk helium supply and being swept out of the assembly along with recoils from the target.

As a result of interaction with the cyclotron beam, product nuclei recoil from the back surface of the target into the helium. Through collisions with helium atoms the recoils lose their initially high kinetic energies and are reduced to thermal energies. The approximate ranges for some typical recoils carrying a maximum energy are listed in Table 1. By pumping on the capillary, located immediately behind the target, a flow of helium down the target cylinder, mounted behind the target, and out the capillary is established. Recoils in the helium are swept with the helium from the volume behind the target and out the capillary typically used has an inside diameter of 0.055 in. and is made of polyethylene).



igure 5. Single target assembly of the HeJRT system.

A major time consuming step in the process of thermalizing recoils and transporting them from the target area to low background
counting areas is the time necessary to sweep the recoils from the
thermalizing volume behind the target into the capillary. Accordingly,
it is desirable to keep this thermalizing volume to a minimum by reducing the diameter of the target cylinder. To facilitate this, the
cyclotron beam is collimated using a water cooled collimator before
it is allowed to strike the target.

Initially, the target cylinder was intended to help concentrate the most recently thermalized recoils in the flow of helium leaving through the capillary and keep them from diffusing throughout the chamber containing the target assembly. However, it was subsequently learned that it is necessary to attach the recoils to large molecular clusters (cluster of masses up to 10⁸ amu [JuH71]) in order to achieve efficient transport of the recoils through the 40 ft of capillary leading to the low background counting area (see Section II. f. "Cluster Molecules" [MaR72, WiK72, BoW72]). These molecular clusters are generated from impurities in the helium in the plasma provided by the cyclotron beam passing through the helium behind the target. It is presently intended that the target cylinder help concentrate the molecular clusters as well as the recoils in the flow of helium leaving through the capillary.

Figure 6 displays the result of an experiment to test the effectiveness of the target cylinder in concentrating suitable molecular clusters

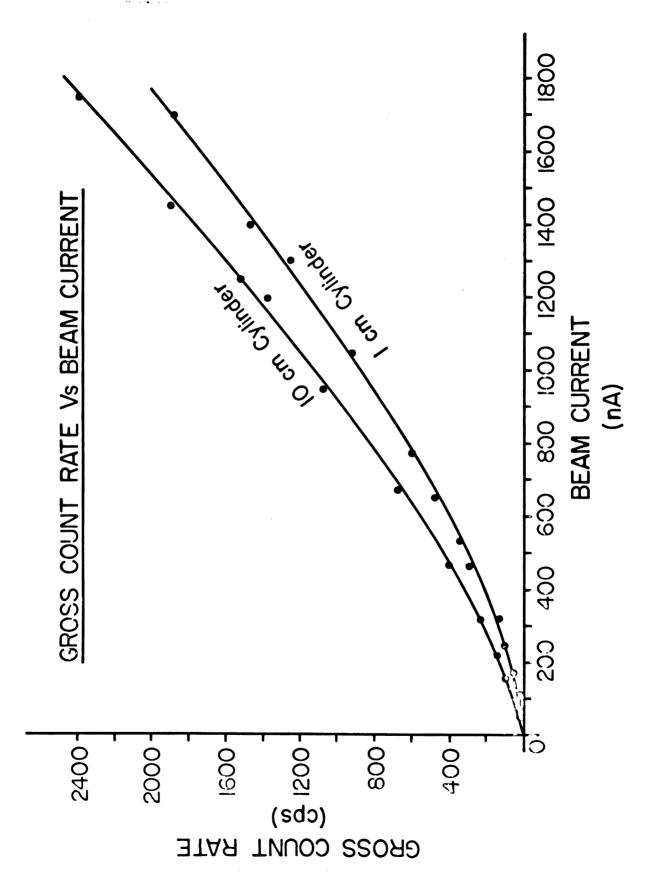


Figure 6. Gross count rate vs beam current compared for long and short target cylinders

in the helium flow leaving through the capillary. For this experiment a silicon (quartz) target was bombarded with 30-MeV protons to generate 28 P ($t_1/_2$ = 280 msec). Two different target cylinders were used: one was 1 cm long and the other was 10 cm long. Both cylinders were 2 cm in diameter. The maximum range for the ²⁸P recoils, was less than 1/2 cm for 3 atm helium pressure. After considering the magnitude of the flow of helium leaving through the capillary (120 standard cm³/ second) and the maximum range for the 28P recoils it is apparent that a very small number of, if any, recoils could have diffused out of either target cylinder and not have been swept with the helium into the capillary. Relative efficiencies for the system when run using each of the two cylinders were determined by just comparing the gross γ count rates observed. Spectra were recorded to make certain that peak areas for the 1.78-MeV peak of ²⁸P followed the gross y count rate. The improved efficiency for the system when run using the long cylinder is obvious from Figure 6.

It is possible to attribute the improved efficiency of the target assembly when using the 10 cm cylinder to something other than concentrating suitable molecular clusters in the thermalizing volume. However, upon considering the increase in the relative efficiency of the system using the long cylinder as less beam current was run (at 1.6 μ A the long cylinder system was 21% more efficient at transporting recoils than when the short cylinder was used, as compared with 75% more efficient at a 0.2 μ A), it does seem likely that the improved transport

efficiency for the long cylinder system is related to the generation and/or concentration of suitable cluster molecules in the thermalizing volume. If the transport efficiency improvement were associated with an improvement in the flow characteristics along the long cylinder and into the capillary (which could significantly improve transport efficiency), it would be expected that the transport efficiency improvement would not be beam current dependent. A more detailed discussion of the shape of the curves presented in Figure 6 will be presented in Section II. f. "Cluster Molecules".

The capillary presently being used has an inside diameter of 0.055 in. and, with the exception of a short stainless steel end that attaches to the target cylinder, is made of polyethylene (Clay-Adams Intermedic) tubing. The coupling between the stainless steel and polyethylene capillaries is made by first cutting the polyethylene and grinding the stainless steel tubing in special jigs so that they are cut off perpendicular to their axes. The two pieces of tubing are then brought together by inserting them in a tight fitting sleeve, see Figure 7.

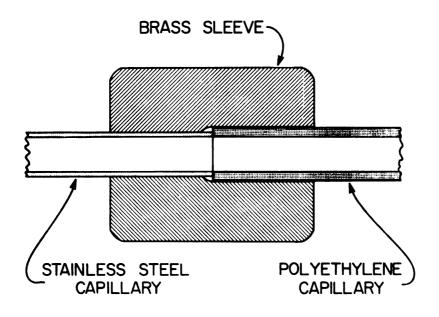


Figure 7.

Stainless steel to

polyethylene capil
lary coupling sleeve.

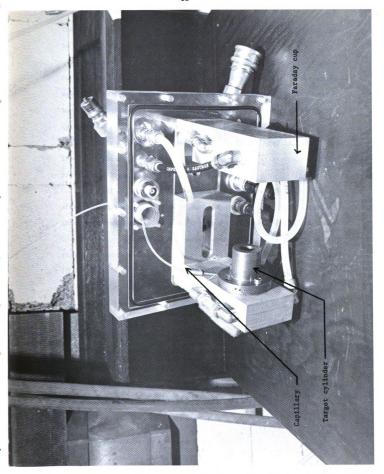


Figure 8. Target assembly components mounted on lid of target assembly chamber.

The requirements and flow considerations in the capillary are discussed in Section II. g. "Capillary Considerations".

The beam is stopped and the current mointored by a water cooled Faraday cup located in the helium atmosphere. While it is not necessary to have the Faraday cup in the helium atmosphere, it was convenient and a historical carryover from earlier target configurations (discussed later in this section).

The target assembly drawn in Figure 5 is pictured in Figure 8.

The components are mounted on the lid of the target assembly chamber, pictured in Figure 9, to allow easy access.

The initial target configuration used in this lab was patterned after an early configuration of R. D. Macfarlane [MaR69]. Although this configuration has not been used here for two or three years, it does represent a satisfactory target assembly with possibly very short recoil collecting times and has been used recently by other groups [BoW72] [JuH71]. The basic mechanism for generating and collecting recoils is the same as described above with the exception that recoils ejected from the target are thermalized between the target and a chrome plated aluminum hemisphere and are then swept into the capillary through an orifice in the rear of the hemisphere. The hemisphere serves double duty as recoil collector and as Faraday cup, see Figures 10 and 11. The main reason for changing to our present configuration was that it provided for an easy expansion to a multiple target assembly, which is not possible with the initial configuration.

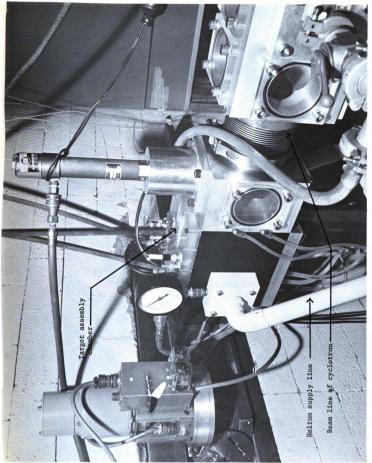
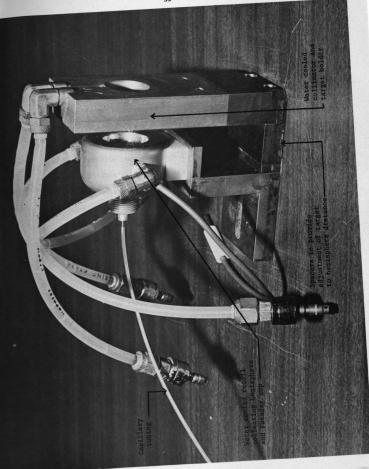


Figure 9. Target assembly chamber on cyclotron beam line.



The necessity for considering a target assembly using multiple targets is born out of the short range of recoils in thin targets. Clearly, no higher yield of recoils is to be gained by increasing the target thickness beyond the range of the most energetic recoils created by the cyclotron beam. For most cases this maximum usable target thickness is from 10⁻⁵ to 10⁻⁴ cm (see Section II. b. "Recoil Characteristics"). Even though most experiments will be possible with the HeJRT system using a single target, cases are anticipated where the number of recoils generated from a single target will be a serious limitation. This will be especially true when the HeJRT system is feeding a mass separator. Also, in general it would be wise to have a surplus of recoils generated, making it possible to tolerate larger inefficiencies in other components of an experimental set up. Accordingly, it is desirable to consider multiple target assemblies for the HeJRT system.

The simplest multiple target assembly considered is sketched in Figure 12. Here the helium exiting the target assembly first sweeps back and forth in front of each of the separate targets in sort of an S pattern. This is accomplished by simply staggering the targets and leaving small spaces, through which the helium can flow, on alternate sides of the target assembly. The thickness of the spacers between the targets must be adjusted to provide sufficient distance in order that recoils from the preceding target are thermalized within the distance to the next target. However, a major portion of the time



Figure 11. Recoil collecting/Faraday Cup Hemisphere.

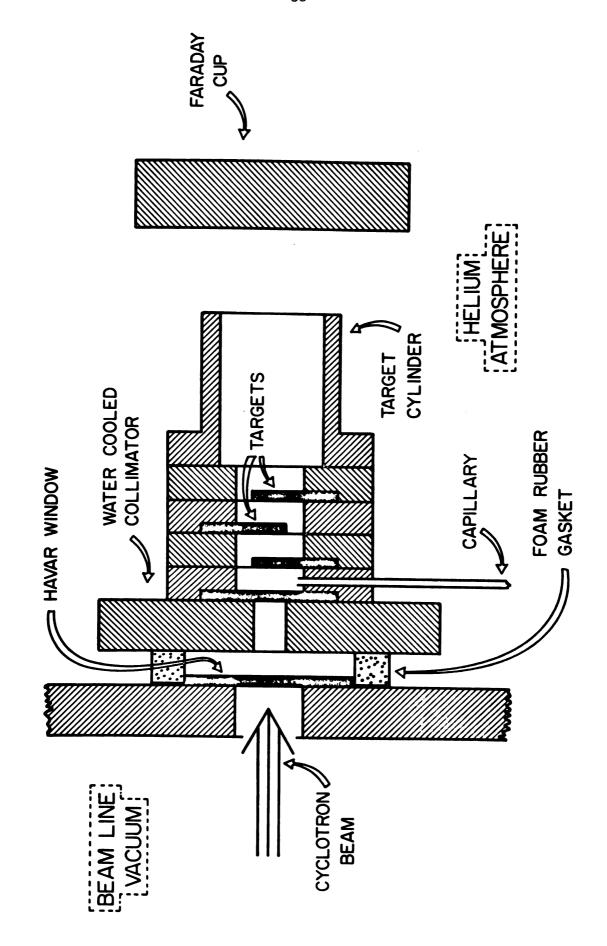


Figure 12. Multiple target assembly of the HeJRT system.

elapsing between the generation of the recoils and having them ready for counting in the low background area is the time necessary to sweep the recoils into the capillary. (See Section II. g. "Capillary Considerations".) Thus, in an attempt to keep this time to a minimum the separation of the targets should not be any greater than necessary for the recoil to be thermalized before striking the next target.

While multiple target assemblies have been used here for some time [GiG71], a detailed study of their characteristics has not been conducted. It is known that yields from the multiple target assemblies used are up from single target assemblies; however, the exact relationship between the number or type of targets used and their yield has not been determined. It is also necessary to determine if modifications of the assembly can further improve its efficiency. The initial multiple target assembly used [GiG71] is shown in Figure 13. The one presently being used is essentially the same but looks more like the sketch in Figure 11.

The average time necessary to sweep recoils into the capillary increases with each additional target because as each target is added the total volume from which recoils must be swept is increased. If the half-life of the activity desired is of the order of the time necessary to sweep the recoils from a single target into the capillary, then adding additional targets in the manner described above may produce little increase in the total yield. Accordingly, it may be necessary to add additional capillaries as well as targets. Figure 14 is a sketch of a multiple target assembly employing as many

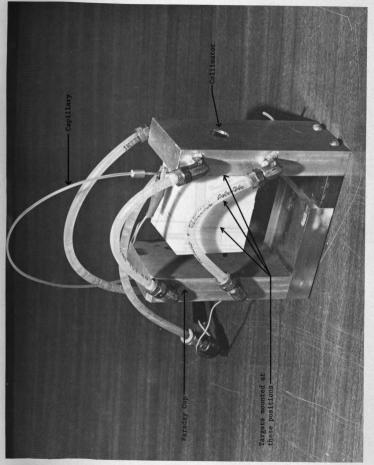


Figure 13. Picture of initial multiple target assembly using three targets.

MULTIPLE TARGET/CAPILLARY ASSEMBLY

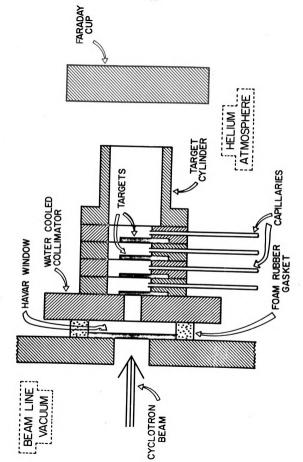


Figure 14. Multiple target/capillary assembly proposed for the HeJRT system.

capillaries as targets; however, if the half life restriction is not too severe it may only be necessary to use a capillary for every second or third target. In addition to the half life limiting the number of targets that can be swept with a single capillary there is a second limitation to the total number of targets used. This is a result of the energy degradation occurring in the targets and the helium, shifting the reaction products toward fewer neutrons boiling off. Of course, this restriction can be partially alleviated by using thinner targets, ones approaching the maximum recoil range.

II. d. Gas Supplies

Initially the helium used in the HeJRT system has a purity >99.995%; however, this is typically doped with benzene vapor to a level of 10-20 ppm. This is accomplished using the gas mixing set up shown in Figure 15. The process is a two-step procedure. First, a supply of helium is made up containing about 1 ppt benzene vapor by adding a known amount of liquid benzene into the flow of helium to a storage tank pressurized to > 100 psig. Initially, a compressor was used (as in Figure 15) to pressurize the tank; however, because of the uncertainties about the amount of pump oil this was adding to the helium, the compressor has been replaced with a high pressure regulator on a tank of pure helium. The second step is to take the heavily doped helium from the storage tank and dilute it with pure helium as it is fed to the target assembly. This is accomplished by taking the pressure regulated flow from the supply tank through a needle valve and flow gauge and adding it to the pressure regulated flow of pure helium, which also passes through a flow gauge. The final benzene concentration is determined and maintained using the flow gauge readings. For those runs in which the helium is doped with compressed air and water vapor, the compressed air is supplied by the compressor and is fed through the needle valve and flow gauge, while the water vapor is added by just passing the helium supplied to the detector assembly over or through a container of water.

It was originally intended that the gas mixing set-up described above be used to add target gases (e.g., Ne for a $^{20}\text{Ne}(p,n)^{20}\text{Na}$

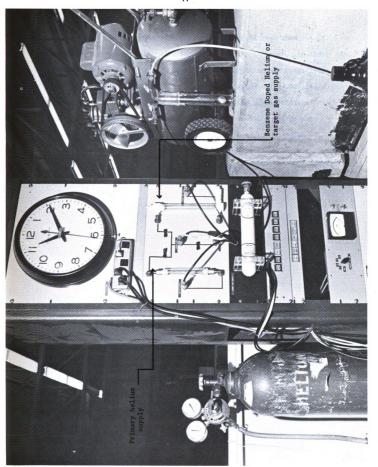


Figure 15 Target Assembly Gas Mixing Apparatus.

reaction) to the target assembly. This ability was lost when the necessity for adding controlled impurities became apparent. In order to regain the ability to add target gases in addition to impurities, the gas mixing apparatus is being expanded to allow the controlled addition of up to three gaseous components to the primary helium supply. An additional source of motivation for expanding the gas mixing set—up comes from the desire to try more exotic mixtures of impurities in the helium. This is necessitated by the desire to follow up the possibility of performing "Plasma Chemistry" (see Section II. o. "Plasma Chemistry").

II. e. Detector Assembly and Tape Transport

The physical relation between the components of the HeJRT system and the detector assembly with its tape transport is shown in Figure The capillary is run from the target assembly up into the detector assembly (a distance of ~45 ft) where the flow of helium containing cluster-nuclear recoil combinations is directed at a collecting surface. The cluster molecules are accelerated as they are carried along in the helium flow to about the speed of sound in helium at room temperature (see Section II. g. "Capillary Considerations"). Because of their very large mass, up to above 108 amu [JuH71], this corresponds to very high kinetic energies for the cluster, $^{2}1.1 \text{ MeV}$ for 10^{8} amu clusters. In turn, these high kinetic energies of the clusters cause them to stick well to collecting surfaces with which they collide. The most frequently used collecting surface is 1-in. paper tape, which is fed through the detector assembly by a tape drive mechanism. Thus, it is possible to continuously expose detectors to fresh sources or to stop the system repeatedly for half life determinations, etc. The tape transport system is discussed later in this section.

Figures 17 and 18 are pictures of two of the possible set-ups for the detector assembly. The first was a set-up used in the search for β -delayed protons. The activities are collected on an aluminum wheel that is being rotated by advancing paper tape in order to expose a fresh collecting surface continuously. A detector telescope has been set up to look for the protons. The second was a set-up used in a simple γ singles experiment and is essentially the set-up used in the collection of the efficiency information in Sections II. h.

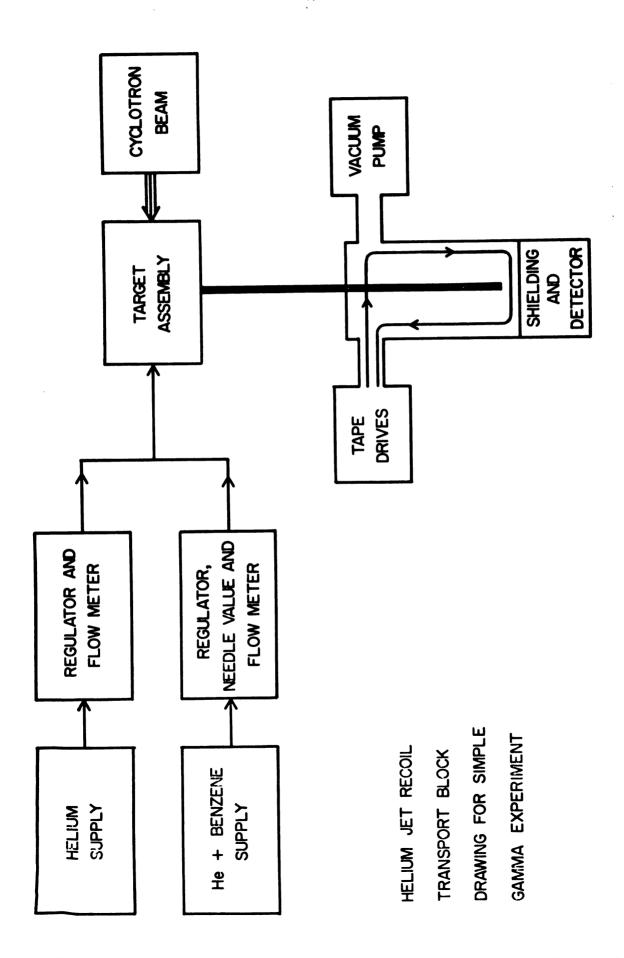


Figure 16. Block diagram of HeJRT system set-up for a simple γ experiment.

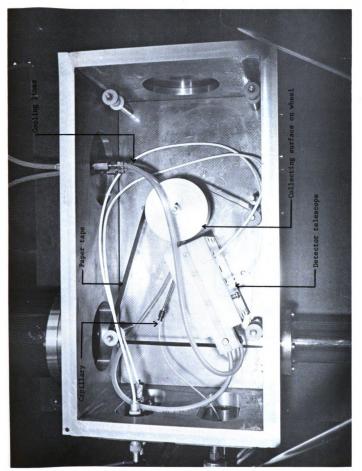


Figure 17. Detector assembly set-up in a search for β -delayed protons.

Figure 18. Detector assembly set-up in a simple γ singles run.

through II. 1. The activities are collected on paper tape just out of view of a collimated Ge(Li) detector located just outside the detector assembly chamber. The capillary to tape angle and distance has been adjusted so that the tip of the capillary (where activities sometimes collect) is out of view of the detector. In both figures the end of the capillary has been run through a slightly larger diameter metal tube. This has been done to hold the end of the capillary straight to facilitate aiming the capillary and to minimize the problem of activities collecting on the end of the capillary (see Section II. g. "Capillary Considerations"). An overall view of the detector assembly area is shown in Figure 19.

The tape transport system is shown in Figure 20. It is designed to handle up to 1-in. tape and has been used with paper and aluminized mylar tape. The tape is advanced using a capstan-pinch roller assembly that is driven by a stepping motor. The accuracy to which the tape speed is known is the accuracy of the pulse generator (±1%), assuming the tape does not slip or the stepping motor does not miss steps.

This is a good assumption providing the proper tension is maintained on the tape and the tape speed is not excessive (<10 inches per second). The tape transport system has the ability to move the tape in either direction at speeds up to about 15 inches per second. The recent addition of a 16-channel programmable sequencer allows for quite complex motions of the tape and can also control other functions, such as gating detectors, routing spectra, and operating other mechanical devices.

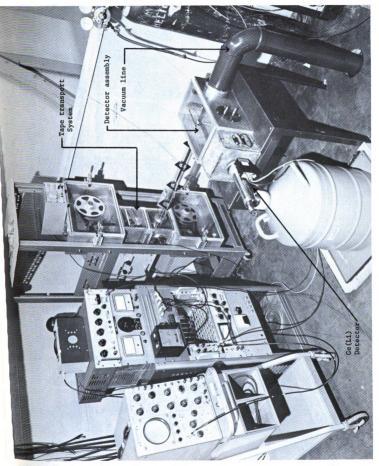


Figure 19. Overall view of detector assembly area set up for a γ singles experiment.

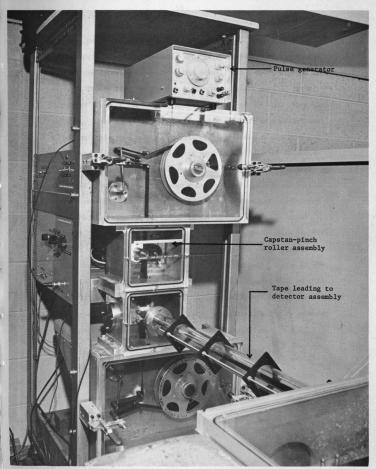


Figure 20. Tape transport system.

The pumping station for the HeJRT system is located on a platform below the detector assembly area in order to reduce the vibration of the detector assembly by the pumps. The pumping station is shown in Figure 21. The pumping system consists of an *300 l/sec. (measured capacity for helium) Roots blower backed by a 15 cfm mechanical pump. The vacuum line to the detector assembly is provided with a Chevron-style cold trap to prevent back streaming of oil from the pumps when solid state detectors are used in the detector assembly. Typically, only the 15 cfm mechanical pump is used for experiments using the HeJRT system, since the lower operating pressure offered by the Roots blower provides no increase in the total transport efficiency of the HeJRT system (see Section II. j. "Efficiency vs. Detector Assembly Pressure"). However, when the HeJRT system becomes the first stage of an on-line mass determination system, the added pumping capacity of the Roots blower will be necessary. When the HeJRT system is expanded to the on-line mass system, the additional pumps will also be placed on the HeJRT pumping station platform. Because of the possibility of the pump exhaust containing activities, all pump exhausts are ducted to a filter and pumped out of the building.

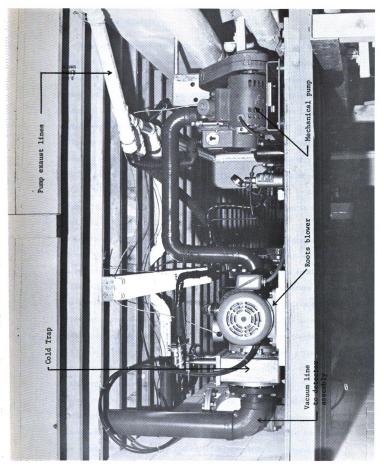


Figure 21. HeJRT pumping station on a platform located below the detector assembly area.

II. f. Cluster Molecules

Most simply stated, the role of cluster molecules in the HeJRT system is to aid in the efficient transport of recoil activities through the system and to help hold these activities on collecting surfaces. However, a good deal of detail of the mechanism is not known for certain. It can be argued the details of the mechanism are not important so long as the system works efficiently, which it does. However, we feel that when the HeJRT system is expanded to being part of an on-line mass identification system or when it is used in conjunction with aqueous chemistry and possibly plasma chemistry (see Sections II. m. "Aqueous Chemistry" and II. o. "Plasma Chemistry") this detailed information will be at least helpful if not in fact necessary. Accordingly, the program to fill in these gaps is continuing.

The possible presence of molecular cluster has been considered since Ghiorso [GhA59-69] observed that a fraction of recoils produced in heavy ion reactions on Pb targets apparently had masses as large as 10³ amu. In 1962 Macfarlane reported results that indicated the clusters played a role in the collection of recoils when he observed that Tb recoils produced in heavy-ion reactions could be collected electrostatically as either positive or negative ions [MaR62]. Subsequently, Mikheev demonstrated that the efficiency of transport was markedly reduced when extremely pure (non-cluster generating) helium was used [MiV67]. However, the importance of the large cluster molecules was not fully realized until the HeJRT systems grew in length to their present size (capillaries with lengths in the range of 20-200 ft). In these systems the total transport efficiencies were only a few percent, and not until specific impurities were added to the helium did the efficiencies climb back toward 100%.

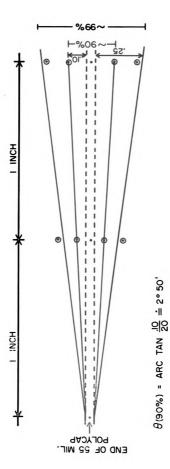
In our system the total transport efficiency increases by a factor of about 20 upon changing from pure helium (purity ≥99.995%) to helium containing a few parts per million benzene vapor. In addition to the dramatic increase in efficiency observed for our system we also observe the buildup of solid material (cluster molecules) at each of the points where activities are deposited. In all respects the increase in efficiency for the system is tied to the presence of cluster molecules. Those factors that foster the generation of cluster molecules increase the efficiency of the system, and the activities generated in the system "tag along" with the cluster molecules. Thus, it seems apparent that the increase in efficiency is a result of the generation of cluster molecules and the attachment of recoiling activities to these molecular clusters. Macfarlane undertook a study of the masses of the cluster molecules and found them to range upward beyond 10⁸ amu [JuH71].

Once the importance of having the nuclear recoil attached to large cluster molecules was demonstrated, it was a relatively simple matter to explain why this should have been expected all along. Initially the explanation was that the large mass of the cluster molecules reduced the transverse diffusion rate in the capillary, thus reducing the chance that activity would be lost through collision with the capillary wall. Macfarlane made the additional observation that the clusters were concentrated nearer the center of the capillary [JuH71]. After some additional thought, the current concensus of people using HeJRT systems is that it is the focusing effect of laminar flow for massive objects transported in the flow that is the reason the cluster molecules drastically improve the system's efficiency. This focusing effect arises from an imbalance of forces on the large object accelerating in the flow as a result of it being acted on by laminae flowing at different speeds [CoW56]. The

direction of the imbalance is toward the laminae with the higher speed, i.e., toward the center of the capillary. For the HeJRT system as it is currently set up, the Reynolds number is just between Reynolds numbers indicating laminar flow and those indicating turbulent flow (see Section II. g. "Capillary Considerations"). However, even if the flow in the center of the capillary tended toward being turbulent, the forcing effect would still be present in the laminar sublayers along the walls of the capillary.

An additional benefit resulting from the attachment of recoil activities to massive cluster molecules lies in the relative ease one has in separating clusters (and therefore activities) from the helium used to transport the cluster molecules. Owing to their enormous masses the clusters will diverge only slightly as they exit the capillary into a vacuum, whereas the helium will suffer a much greater divergence. Macfarlane has been successful in achieving good separations of recoil-carrying clusters from helium using a conical oriface (helium skimmer) with a diameter only slightly larger than the capillary diameter and at a distance of several millimeters from the end of the capillary [JuH71]. We made an attempt at determining the angle of divergence of the clusters in our system by merely observing the diameter of cluster build-ups at varying distances from the end of the capillary. For this determination the assumption was made that the clusters were not concentrated in the central regions of the capillary and that turbulence created by placing a collecting surface in the path of the flow did not affect the paths of the clusters. The result of these assumptions is the determination will yield a larger diameter than would be observed for a properly designed skimmer. The results of this determination are shown in Figure 22 which indicates an angle of divergence of ≥3° for about 90% of the clusters and an angle of





Approximate angle of divergence of molecular clusters leaving the HeJRT capillary. Figure 22.

ARC TAN $\frac{25}{2.0} = 7^{\circ}$ 10'

e (%66) e

divergence of ≥7° for 99% of the clusters.

In our case cluster molecules are generated from benzene vapor added to the HeJRT helium supply to a concentration of 10-20 ppm. Sugihara's group at Texas A & M also uses benzene vapor but at a much higher concentration. They bubble their helium through a container of benzene [BoW72] such that their benzene concentration is probably in the range of 0.1 to 1%. Macfarlane's group at Texas A & M initially used compressed air and water vapor. They added about 1% compressed air and had an open dish of water in their target assembly (private communication) (the important ingredient in the compressed air most probably was pump oil). More recently Macfarlane has been bubbling his helium through water and adding 2200 ppm CH, [MaR72a] or using commercial grade helium and water vapor [WiK72]. A group at Simon Fraser University used ethylene in concentrations up to 100% as their cluster generating gas [DaH73a]; however, the mechanism for generating the clusters is quite different than we are now considering. Quite obviously the cluster molecules must be primarily composed of the elements making up the impurities added to the HeJRT helium supply. Thus, the clusters would seem to be organic in nature. In addition, the improvement they bring to the total transport efficiency would not seem to depend on their exact composition. One of the things that is not known at this time is the possible importance of trace impurities in the generation of molecular clusters in providing sites for attachment of thermal recoils to the clusters.

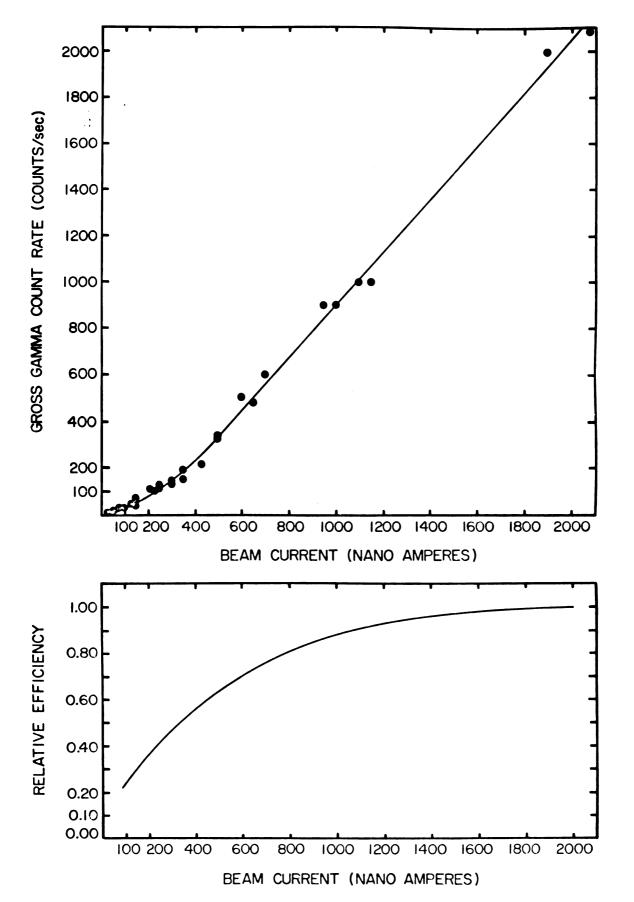
In our case cluster growth is initiated by the passage of the cyclotron beam through the impurity-containing helium. Other researchers report the use of hard ultra-violet [WiK72] and gas discharges [WeC72] to initiate the growth of molecular clusters. Presumably cluster generation is a result of creating free radicals and/or carbonium ions and carbanions

within the plasma, formed by the beam passing through the helium from the organic impurities present. These highly reactive species then apparently react chemically to buildup the cluster molecules. Except for the necessity of the cyclotron beam (or some other source of energy input as discussed below), there is no direct information on the mechanism of cluster generation. The suggestion that it involves the formation and subsequent reaction of highly reactive organic species is made only on the basis that it seems logical. The group of Simon Fraser suggests their clusters are generated upon the expansion of ethylene gas from pressures and temperatures above the critical point [DaJ73].

Studies have been conducted to determine the relationship between beam current on target (plasma density) and system performance and between benzene concentration and system performance. In each case the HeJRT system was set up using an aluminum target, the beam was 30-MeV protons, a 45-foot long 0.055-in I.D. polyethylene capillary was used, and the activities were collected on moving paper tape such that the source material spent about 1.5 sec in view of the Ge(Li) detector. The detector assembly was pumped to ²⁷ torr, and the target assembly was maintained at 2 atm. For the series of determinations seeking the relationship between beam current and transport efficiency the helium was doped with ²⁵⁰ ppm benzene vapor. For the series of determinations seeking the relationship between benzene concentration and transport efficiency the beam current was held at very nearly 1 μA. Several spectra were recorded during each series of runs to be certain the gross γ count rate followed the intensity of the 820-keV peak of ²⁶Si.

The results from the first series of runs are shown in Figure 23.

It is quite apparent the amount of activity transported through the system is not linearly dependent on beam current. The production of recoils from

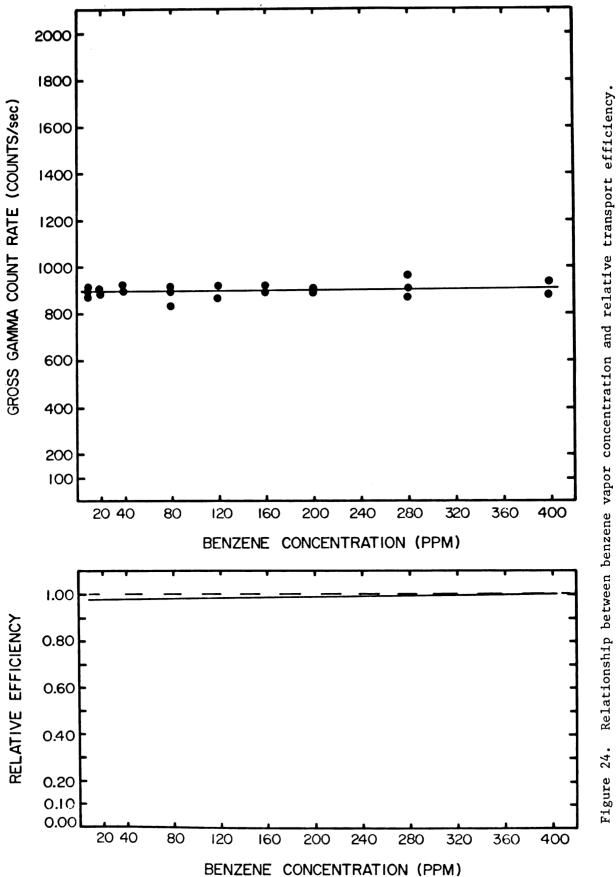


Relationship between beam current and relative transport efficiency. Figure 23.

the target must be directly proportional to beam current; therefore, it must be the efficiency with which the activity is transported through the system that is not constant. It seems most likely the drop in transport efficiency observed for low beam currents is the result of either not generating enough cluster molecules or not generating cluster molecules that are sufficiently massive. Presumably the reason for this is the drop in the number of free radicals, etc., generated because of the decreasing plasma density following the decreasing beam current. We anticipate performing an additional series of runs using a larger capillary diameter. As a result of using a larger capillary, the flow rate through the HeJRT system will be increased, thus allowing less time for suitable cluster molecules to be built up in the volume behind the target. If we are correct, we expect to see a more drastic dependence of transport efficiency on beam current.

The results from the second series of runs are shown in Figure 24. It is quite apparent that the amount of activity transported through the system is independent of the concentration of benzene between the limits shown. It is felt that the slight drop in efficiency to 98% upon going to the lowest benzene concentration may be a result of poor statistics. This is because runs in which the level of benzene in the system was more than two orders of magnitude lower still had total systems efficiencies that were quite high. It takes a couple of weeks of pumping on the HeJRT system to return the system's efficiency to the very low level observed before benzene was first added to its helium supply. Runs were also attempted in which the concentration of benzene was almost to the level of saturation, with the result of no improvement in the system's efficiency.

One of the more fundamental questions, and one of the unanswered ones,



about cluster molecules in the HeJRT system concerns the nature of the mechanism through which the nuclear recoil becomes bound to the cluster molecule. On the lowest level, it is possible to consider two mechanisms for this. One mechanism for the process is just one of entrapment, in which, as the bulk cluster material condenses out, the nuclear recoil becomes trapped during the process just because of its physical presence in the area. Here "condenses out" should not be taken literally but should be understood to be some form of nucleation or polymerization. A second mechanism for the process would be one in which the nuclear recoil becomes bound to the cluster at some time during the growth of the cluster. Here "bound" can be taken to be either reflecting a physical bond such as a result of van der Waals forces or an actual chemical bond. Section II.

o. "Plasma Chemistry" presents some evidence supporting the mechanism involving the formation of a bond between recoils and chemically specific sites in the cluster molecule.

As could be expected, considering their probable organic nature, the cluster molecules are soluble in acetone. We routinely use acetone to remove buildups of cluster molecules within the HeJRT system. However, it was not expected that we would find build up of cluster molecules to be soluble in water. There is also some evidence (see Section II. m. "Aqueous Chemistry") that there is a break-up of the cluster molecules when added to aqueous solution, with the break-up freeing the nuclear recoil occuring in quite short times.

II. g. Capillary Considerations

Our initial experiments with the HeJRT system were run using glass capillaries that were ≈ 1 meter long. With this length of capillary we were forced to run in an inconvenient location and could not sufficiently shield the detector assembly from the neutrons (and capture γ^{15}) generated in the target assembly. When we were having difficulty obtaining longer glass capillaries and were not looking forward to splicing short ones together, an attempt was made to find a substitute capillary. A stainless steel capillary was to be ordered, but in the interim it was decided to try a polyethylene capillary supported by running it in larger glass capillary. When it was found this worked well we attempted a run in which the polyethylene capillary was strung loosely between the target and detector assemblies to determine whether the capillary could suffer slight bends without losing much transport efficiency. When the HeJRT system still performed well, a series of runs was undertaken to determine how much the capillary could be bent without a serious loss in efficiency. This series of runs culminated in the tying of the capillary in a loose square knot [KoK70] in which the bends were more severe than those expected in using the HeJRT system. The result again was no significant loss in activity transported, and as a result polyethylene capillaries were chosen for our HeJRT system.

Our initial capillaries had an inside diameter of 0.022 and 0.034 in. when the total length of the system was only a few feet. Now we typically use 0.055-in. I.D. capillary that is 40-50 feet long. If in the future we are faced with difficulties in transporting very short lived products through the system, we expect to use 0.072-in. I.D. capillary. With the present diameter capillary we often use $^{28}P(t_{1/2}=270 \text{ msec})$ to study the operation of the system and have also successfully run ^{40}Sc ($t_{1/2}=182 \text{ msec}$).

(A disucssion of the transport times for the HeJRT system is included later in this section.) The capillaries are supplied in 100 foot lengths by Clay-Adams and are their "Intermedic Tubing." The 45-ft. length of the capillary allows us to set up the detector assembly in a conveniently located low background area over the cyclotron shielding wall. While we have run with capillaries longer than 100 feet, no systematic study of the operation of the system has been made as a function of capillary length. There is, of course, the limitation of increasing transport time for longer capillaries of the same diameter.

In addition to experiments in which glass and polyethylene capillaries were used, we have also run using teflon capillaries and observed the same level of performance. In the past Ron Macfarlane at Texas A & M has run using stainless steel capillaries [MaR71]. It presently appears the operation of the HeJRT system is fairly independent of the material from which the capillary is formed. Our preference for polyethylene capillary initially was based on its flexibility, but now it is just a historical carryover.

We have observed that efficient operation of the HeJRT system requires the inside bore of the capillary to be smooth and of more or less uniform cross section. Macfarlane also reports (private communication) that localized heating or physically vibrating the capillary can greatly reduce the system's transport efficiency. Another thing to be avoided is discontinuities in the capillary. At present, our system does have one such discontinuity at the point of connection of the polyethylene capillary to the short stainless steel capillary leaving the target assembly. The capillaries are joined as described in section II. c. It has proven to be a relatively simple technique and yet has not seriously affected the transport efficiency.

T. T. Sugihara's group, also at Texas A & M, has eliminated this discontinuity by eliminating the short piece of stainless steel capillary and is

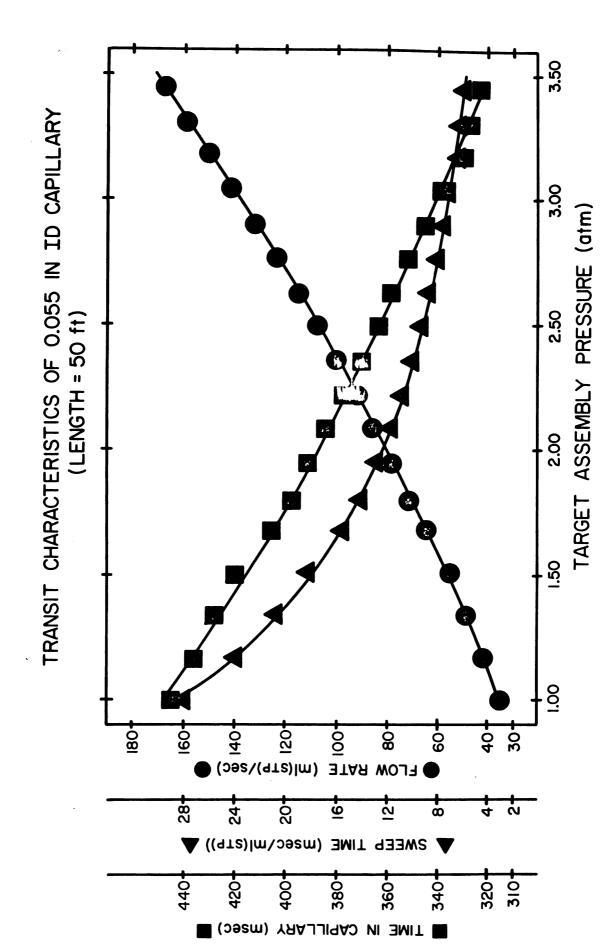
running with teflon tubing entered directly into their target assembly [SuT72].

The helium flow rates for our system using a 50 ft. 0.055 in. I.D. polyethylene capillary range from 35.7 cm³/sec (STP) to 167.8 cm³/sec (STP) when the target assembly is pressurized from 1 atm to 3.5 atms, respectively. The relationship between target assembly pressure and flow rate is summarized in Figure 25a. This figure also includes the time necessary to sweep 1 standard cm³ of helium into the capillary and an estimate of the time necessary for activities to traverse the length of the capillary. The sweep time is just the reciprocal of the flow rate. The decrease in sweep time does correspond to a legitimate decrease in the time necessary to get activities into the capillary in that the nuclear recoils will be stopped in the same number of standard cm³. The estimate of the time spent traveling through the capillary is based on an equation presented by H. Dautet, et al.

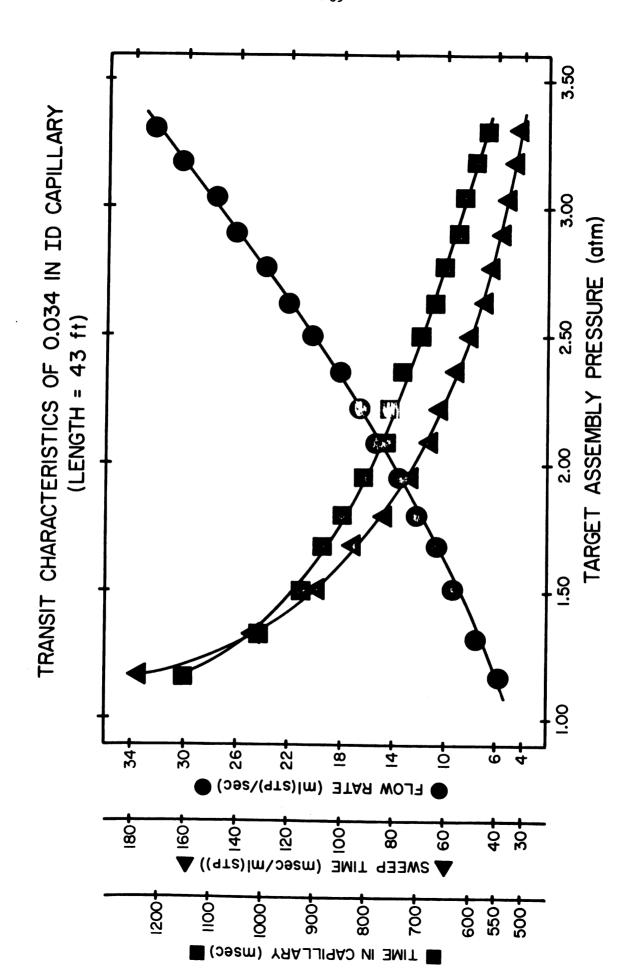
$$T = \frac{L}{a} \quad (\frac{2 + m}{3m_1} 1)$$

[DaH73], namely, where T = transit time in capillary, L = length of the capillary, a = the speed of sound in helium, and m₁ = the mach number at the entrance of the capillary. This expression assumes choked flow in the capillary (i.e. the flow reaches sonic velocity at the exit), that the flow is for an ideal gas, and that the flow is an adiabatic process. These are all reasonably good assumptions for our system. Figure 25b presents the same information for our system using a 43-ft. 0.034-in. I.D. capillary. (It should be noted the time spent in the capillary claculated from the above equation is only about one half that obtained using the graphs H. Dautet, et al., have included in their paper.)

The total transport time for a HeJRT system is just the sum of the time taken to thermalize the recoils and sweep them into the capillary



Relationship between target assembly pressure and flow rate for 0.055 in. I.D. capillary. Also included are sweep times and an estimate of times in the capillary. Figure 25a.



Relationship between target assembly pressure and flow rate for 0.034 in. I.D. capillary. Also included are sweep times and an estimate of times in the capillary. Figure 25b.

and the time spent traversing the capillary. Although there has been no direct measurement of transit time through our HeJRT system, there has been a measurement of the difference between the transit times for the 0.034- and 0.055-in. capillaries run at 1 atm target assembly pressure. This was accomplished using the 12.0-sec 23 Mg and 2.1-sec 26 Si activities produced with a 30-MeV proton Al. For two activities with different half-lives, the ratio of their activities (A/A') some time (t) after generation will be

 $A/A' = A_o/A_o' e^{-(\lambda-\lambda')t}$

where A_0/A_0' is the ratio of initial activities and λ and λ' are the decay constants. For our purposes A_0 and A_0' are functions of the beam intensity, but their ratio will be constant (with the possible exception that with large fluctuations of the current the transport mechanisms for the activities might differ, upsetting the ratio). If the same procedure is followed, allowing some different time to elapse between generation of the activities and counting, the resulting ratio of the ratios will be obtained,

$$\frac{(A/A')}{(A/A')} t_1^1 = e^{-(\lambda-\lambda')(t_1-t_2)}.$$

Here the ratios of the initial activities drops out, the decay constants are known, and the ratios of final activities can be measured. Thus, the time difference (t₁-t₂) can easily be determined. When this is done using our system, the agreement between the calculated and experimentally determined ratios was to within 7%. We expect to make a second determination of this time difference using the 70.5-sec ¹⁴0 and 0.27-sec ²⁸P activities generated from protons on a quartz target. The resulting larger difference in the decay constants will make the activity ratios more sensitive to the transport time differences. We also expect to make a direct measurement

of the transport time using a double target that will be moved through the assembly while monitoring the activities transported through the system with respect to time.

The Reynolds numbers associated with the flows near the entrance of the 45-ft capillaries range from about 40 to 250 for the 0.034-in. I.D. capillary run with target assembly pressures in the range of 1 atm to 3.5 atm and from about 300 to 1500 for the 0.055-in. I.D. capillary run with target assembly pressures in the same range. It is possible to calculate the Reynolds number at the exit of the capillary, a known Joule-Thompson coefficient, and using the detector assembly pressure (as predicted by H. Dautet et al. [DaH73] necessary to induce sonic flow at the exit of the capillary. The result of the calculations is that the Reynolds number remains essentially unchanged throughout the length of the capillary. It has generally been proven that Reynolds numbers below 2000 are associated with laminar flows [SeF70]. Accordingly, the flow through the capillary will be laminar except at any discontinuities, principally the entrance and exit of the capillary. At the entrance to the capillary there will be some distance required before the laminar boundary layer builds to the center of the capillary. The space between the boundary layer will have turbulent flow. The distance before the total flow becomes laminar is dependent on the Reynolds number of the flow and may extend several hundred diameters down the length of the capillary. When the HeJRT system is run, it is in this region where most of the activity is lost and the greatest build up of molecular clusters occurs. Presumably, this is a reflection of the flow not yet becoming completely laminar. At the exit of the capillary, as the flow suddenly expands into the larger volume and lower pressure of the detector assembly, the flow certainly becomes turbulent. However, at this point we are dealing with what could more accurately be

defined as opposed to the viscous flow associated with the higher pressures further back in the capillary, and are relying on the enormous masses of the clusters to carry them to the collecting surface. There can be activity lost in the last centimeter or two of the capillary if it is not held straight. Presumably, this is a result of the drop in pressure occurring near the exit of the capillary, with the result that there is no longer a sufficient number of interactions between the helium of the flow and the molecular clusters to cause the clusters to negotiate even a slight bend in the capillary successfully.

II. h. Total System Efficiency Determination

The overall efficiency of the helium jet transport system, including both the efficiency for the transport of activities and the efficiency for collecting these activities on paper tape has been determined for three different recoiling nuclei. The basis of the efficiency determination was a comparison of the activities generated in metal foils by conventional nuclear bombardment with the activities generated on paper tape (1" non-oiled paper computer tape) using the HeJRT system.

Copper and nickel foils were activated using the "rabbit" system described in Appendix II. The reactions of interest in the efficiency determinations were $^{65}\text{Cu}(p,3n)^{63}\text{Zn}(t_{1/2}=38.4 \text{ min})$ $^{62}\text{Ni}(p,3n)^{60}\text{Cu}$ and 60 Ni $(p,n)^{60}$ Cu $(t_{1/2}=24 \text{ min})$ and 58 Ni $(p,\alpha n)^{54}$ Co $(t_{1/2}=1.5 \text{ min})$. In each case a beam energy of 30 MeV was used, not because of cross-section considerations but to allow a comparison of present efficiency with previous runs in which the activities of interest were the lighter copper and zinc isotopes. The copper foils were activated with, as nearly as possible, constant currents for 30 sec, and the nickel foils for 60 sec. Five minutes after the end of each activation a 15-min count of the γ radiation from the foils were taken using a 4.6% (relative to a 3" x 3" NaI(T1) detector at 1.33 MeV) Ge(Li) detector at standard source geometry. Photopeaks at 669, 1332, and 410 keV were used as signatures for $^{6.9}$ Zn, $^{6.0}$ Cu, and 54m Co, respectively. In each case the peak areas were adjusted for integrated current on target and for ADC dead time. The dead-time correction was made using a pulser with a known repetition rate.

Following the runs made using the rabbit, the same activities were collected using the HeJRT system. Copper and nickel foils were placed

in the single target assembly (described in Section II. c. "Detector Assemblies.") The pressure in the target assembly was maintained at 1.0 atm using helium with an initial purity of >99.995% which was doped with approximately 250 PPM benzene vapor. The capillary was made of polyethylene, had an inside diameter of 0.055 in, and was just under 50 feet in length. The activities were collected on a stationary piece of paper mounted in the chamber pumped to <1000 µm pressure. As in the case of the rabbit runs, the targets were bombarded for 30 and 60 sec for the copper and nickel foils, respectively, with a nearly constant current of 30-MeV protons. After the end of the bombardment, the collection of the activities on the paper was continued for an additional minute to assure complete sweeping of activities from the target area. Five minutes after the end of the bombardment a 15-min count of the y radiation was taken using the same detector in the same geometry. Also, as in the case of the rabbit run, the photopeak areas were corrected for integrated current and analyzer dead time.

In both the rabbit and the HeJRT runs 0.0001-in. foils were used. However, for the efficiency determination the thickness of the target used in the HeJRT system was taken to be the maximum range of the recoils, i.e., the target thickness from which recoils were able to leave the target and enter the helium atmosphere. These maximum ranges were calculated as outlined in Section II. b. "Recoil Characteristics." The efficiencies were determined to be 24% for 63Zn, 49% for 60Cu, and 60% for 54mCo. However, it was subsequently learned that the efficiency of the HeJRT system increases as we proceed from 1 atm to 3 atm of helium pressure in the target assembly (see Section II. i. "Efficiency vs Target Assembly Pressure"). While the next section discusses this increase

using Mg and Si, the increased efficiency was confirmed for the Zn, Cu, and Co recoils. Accordingly, the efficiencies for the HeJRT system operating with 3 atm helium pressure in the target assembly are approximately 50% for Zn, 75% for Cu, and 90% for Co.

Table II. Total HeJRT System Efficiency

Efficiency			
Isotope	(1 atm)	(3 atm)	
⁶³ Zn	24%	50%	
⁶⁰ Cu	49%	75%	
54 <i>m</i> Co	60%	90%	

Even allowing for uncertainties of greater than 20% in the measured efficiencies relative to one another, it is clear that the HeJRT system exhibits varying efficiencies for different activities. In that the recoil represents such a small part (in the ppm range) of the cluster with which it is associated, it seems rather doubtful that these varying efficiencies are reflective of differing probabilities for the cluster-plus-recoil to stick to the tape. Similarly, it seems doubtful that these varying efficiencies are reflections of differing probabilities for the clusters-plus recoil to be transported through the system. Thus, as the final alternative it seems likely that these varying efficiencies are reflections of differing abilities of the recoil to form a "bond" with the cluster. [Additional evidence and a discussion of the recoil-cluster bond can be found in Sections II. f. "Cluster Molecules," II. k. "Efficiency vs Time," II. m. "Aqueous Chemistry," and II. o. "Plasma Chemistry." If

the recoil has a difficult time attaching to a cluster or if the attachment is weak possibly resulting in a separation of recoil and cluster as they move through the system, it is likely that some number of the recoils will be traveling through the capillary without being attached to a cluster. Accordingly, these unattached recoils will not be assisted through the system by the clusters and will have an efficiency corresponding to the efficiency of the HeJRT system using pure He, \$5%.

II. i. Efficiency vs Target Assembly Pressure

In the initial experiments when only non-doped helium was used (and the total HeJRT system efficiency was <5% as a result), the efficiency was essentially independent of the pressure in the target assembly. Through the pressure range from 20-in. vacuum to 4-atm there was no obvious or systematic dependence of efficiency on the target assembly pressure. However, when helium doped with small admixtures of benzene is used in the HeJRT system, the effect of target assembly pressure on the overall efficiency is obvious; see Figures 26 and 27. Each point in the figures is the average of three determinations made at that pressure.

The HeJRT system was run using the single target assembly described in Section II. c. "Detector Assemblies" using approximately 40-ft polyethylene capillaries with 0.055-in. and 0.034-in. inside diameters for Fig 26 and 27, respectively. The helium was doped with benzene to a concentration of about 20 ppm. The experiment was run using as nearly as possible 1.5 μ A of 30-MeV protons on an aluminum target foil, initiating for the most part the 27 Al $(p,2n)^{26}$ Si and the 27 Al $(p,\alpha n)^{23}$ Mg reactions. The activities were collected on paper tape moving at 0.5 in./sec past a 4.6% relative efficiency Ge(Li) detector. The activities were deposited on the tape at the edge of the detector's field of view with the capillary at a distance of 1 in. from the tape and at a 45° angle such that the tip of the capillary was out of view of the detector. The geometry was such that the activities spent 3 to 4 sec in view of the detector.

Figure 26 shows the results of runs using a 0.055-in. polyethylene capillary. Peak areas for the 820- and 439-keV transitions in 26 Si and 23 Mg, respectively, are plotted against target assembly pressures from 0 to 35 PSI gauge pressure. Peak efficiency is reached at roughly 3 atm

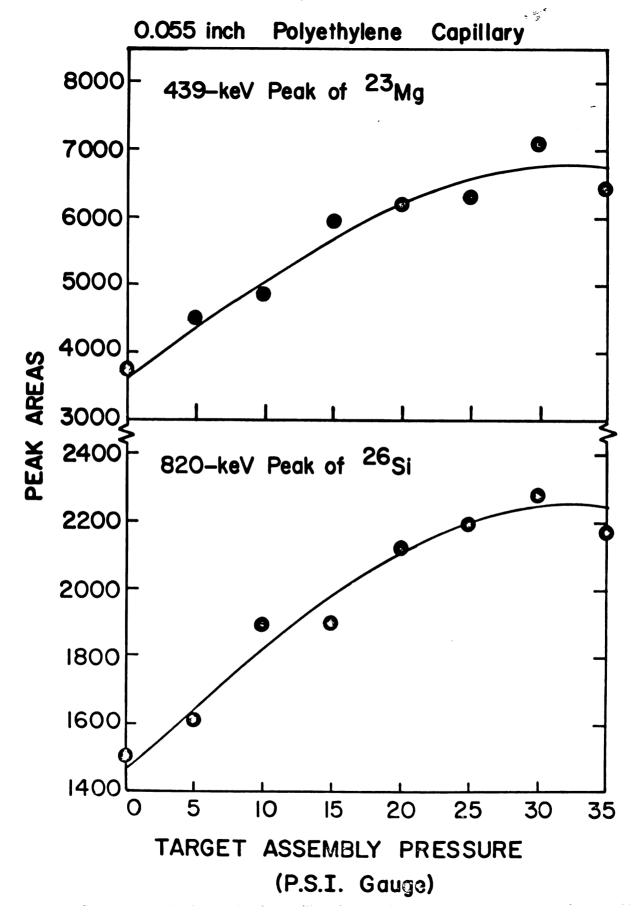


Figure 26. Peak areas for transitions in ²³Mg and ²⁶Si as a function of target assembly pressure, when using a 0.055 in. capillary.

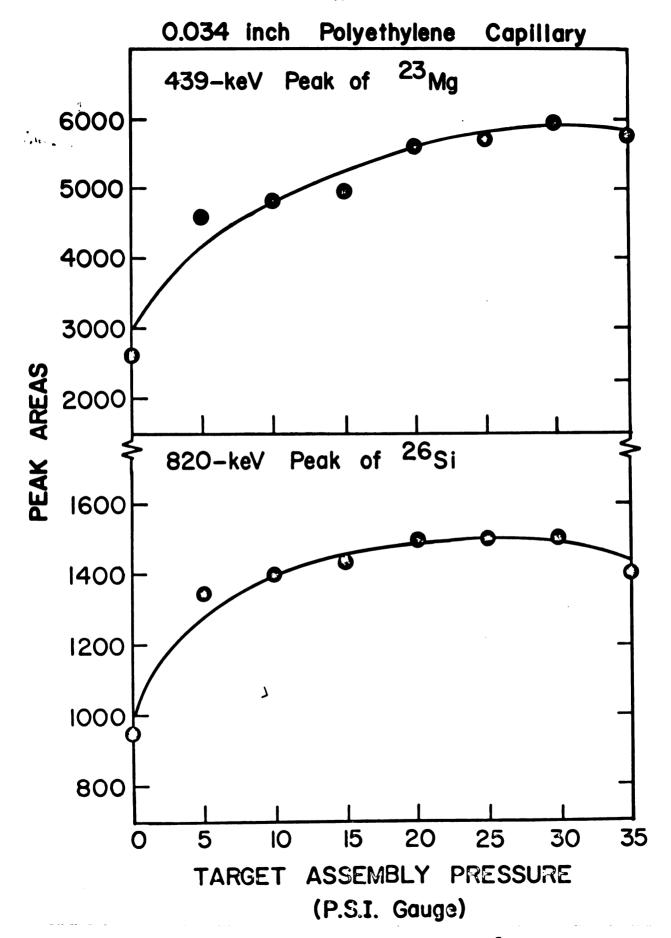


Figure 27. Peak areas for transitions in ²³Mg and ^{2C}Si as a function of target assembly pressure, when using a 0.034 in. I.D. capillary

and is about 50% greater than at 1 atm. This increase in peak areas with increasing target assembly pressures has to be considered a legitimate efficiency increase and not just the reflection of a half-life effect. [The average transit time for recoils through the HeJRT system decreases for increasing target assembly pressure, see Section II. g. "Capillary Considerations."] If the increase in peak areas with increasing target assembly pressures were a half-life effect, it would be expected that the increase for the 2.1-sec ²⁶Si activity would be much more dramatic than that for the 12.1-sec 23 Mg activity. In that the 23 Si and 23 Mg activities were made simultaneously from the same target, it seems unlikely that this peak area increase could be attributed to anything other than an increase in system efficiency. Further, in that the final cluster-plus-recoil velocity in the capillary is not affected by the target assembly pressure, in the range 0 to 35 PSI gauge pressure under the vacuum pumping conditions used (see Sections II. g. "Capillary Considerations" and II. g. iency vs Detector Assembly Pressure), it seems unlikely that the increase in system efficiency is a result of more of the activity sticking to the collecting surface. Additional evidence supporting this is presented in Section II. c. "Collecting Surface Considerations" where a comparison is made with a collecting surface with poorer sticking ability. Accordingly, the increase in system efficiency must reflect either a decrease in the number of clusters-plus-recoils lost in their flow through the capillary or an improvement in the conditions fostering the generation of clusters or fostering the attachment of recoils to cluster, possibly a result of increasing plasma density as target assembly pressure in increased.

Figure 27 shows the results of runs using a 0.034-in. I.D. polyethylene capillary. There is some disagreement between the 26 Si and 23 Mg curves as to where the maximum efficiency is reached and also as to the degree of the improvement at 3 atm over the efficiency at 1 atm target assembly pressure. The 26 Si curve reaches a maximum at roughly 2 atm and is up to about 50% over the efficiency at 1 atm, while the 23 Mg curve reaches a maximum at roughly 3 atm and is up to about 100% over the efficiency at 1 atm. It seems likely that this disagreement is a result of poor statistics. If it were the reflection of a half-life effect, the greater improvement in the efficiency would be observed in the shorter 2.1-sec 26 Si curve and not in the 12.1-sec 23 Mg curve.

There is a rather striking difference between the two sets of curves; the runs made using the smaller 0.034-in. I.D. capillary have a much more rapid increase in efficiency in the lower portion of the curves than for the run made using the 0.055-in. capillary. In the discussion of the runs made using the 0.055-in. I.D. capillary it was concluded that the increase in efficiency with increasing target assembly pressure resulted either because of a decrease in the number of clusters-plus-recoils lost in their flow through the capillary or an improvement in the conditions fostering the generation of clusters of the attachment of recoils to clusters. In that the increase in efficiency with increasing pressure is different for the two capillary diameters used, it seems unlikely that the increased efficiency results solely from an improvement in the conditions under which the clusters are formed or under which the recoil is attaching to the cluster. Additional evidence for this comes from the results reported in section II. f. "Molecular Clusters." Here the relative efficiency of the HeJRT system as a function of beam current is discussed. To the first order, plasma density behind the target will be directly proportional to both beam current and helium pressure. If the curves in figures 26 and 27 are corrected for the expected increase in system efficiency as a

result of increasing plasma density the major portion of the increase remains. Thus, the improvement in efficiency for the HeJRT system with increasing target assembly pressure must come primarily from an improvement in the flow of clusters plus recoils through the capillary. A possible explanation of this effect could lie in the reduction of the mean free path of the helium in the capillary as the pressure in the target assembly, and thus throughout the system, is raised. As the mean free path is reduced, the number of collisions occuring between the recoil-plus-cluster combination and Helium atoms is increased, which will tend to help concentrate the clusters in the center of the capillary. For a discussion of the focusing effects of laminar flow, see reference [Cow 56] and section II. f. "Molecular Clusters."

For each of the curves in Figures 26 and 27 it appears the curves are starting to turn downward. Ones first thought might be that this corresponded to the break down of laminar flow occuring at higher pressures in the target assembly. In section II. g. "Capillary Consideration" the Reynolds numbers of the flow were determined and while it was found that this could possibly be the case for the 0.055-in. capillary it most probably was not the case for the 0.034-in. capillary. Accordingly, it is felt that this effect is not a result of the breakdown in laminar flow in the capillary.

II. j. Efficiency vs Detector Assembly Pressure

In an attempt to determine the relationship between the total system efficiency of the HeJRT system and the pressure at which the detector assembly is held, a series of runs was made in which the system efficiency for collecting paper tape was monitored while the capillary to tape distance and angle were varied along with the pressure in the detector assembly. It was hoped that the drop in total system efficiency as the pressure in the detector assembly was raised could be identified as to the extent of it being a result of a drop in the efficiency for transporting activities through the capillary or a result of a drop in the efficiency for collecting activities on the collecting surface. It is expected the efficiencies associated with the generation of activities and cluster molecules and the attachment of activities to clusters would not be affected by varying the pressure in the detector assembly.

For these runs the helium was doped with 710 ppm benzene vapor and the pressure across the HeJRT system was held constant at 2 atm. The capillary used was a 0.055-in. J.O. polyethylene capillary. The tape used to collect the activities transported through the system was non-oiled paper tape (computer perforation tape) and was advanced at the rate of 0.25 in.per sec. In order to eliminate any long-term effects from the cyclotron beam current varying, ^{28}P with its short half-life of 280 msec was chosen as the activity to monitor. The ^{28}P was generated using a $^{35}-MeV$ 0.7- μ A beam of protons on a 0.05-in. quartz target to initiate a $^{28}Si(p,n)^{28}P$ reaction. A Ge(Li) detector with a 4.6% relative efficiency was used to monitor the γ count rate. The results were corrected for any small fluctuations in the beam current and were plotted against the pressure in the detector assembly (see Figure 28). The pressure in the

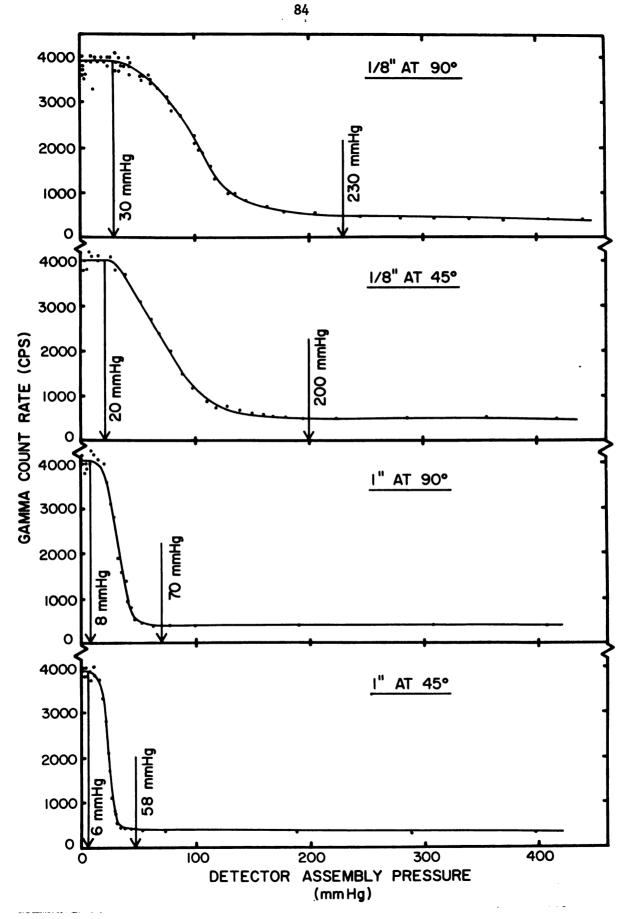


Figure 28. Curves expressing the relationship between detector assembly pressure and total system efficiency for Various to tape angles and distances.

detector assembly was varied by changing pumps and leaking air into the detector assembly.

In each of the cases, capillary to tape distance and angle, the initial system efficiency (P 1 torr) was essentially the same. [See Section II. L. "Collecting Surface Considerations" for a discussion of the initial efficiencies for capillary to tape distance of 1/8 and 1 in. and angles of 90° and 45°]. However, the pressure at which a reduction in the total system efficiency was first noticed was different for each of the four set-ups. A detector assembly pressure (P_a) of $\geqslant 30$ torr was necessary to affect the efficiency in the 1/8"-90° set-up, $P_a \ge 20$ torr for the 1/8"-45° set-up, $P_a \ge 8$ torr for the 1"-90° set-up, and P_a only ≥6 torr to affect the efficiency of the 1"-45° set-up. In each of the cases, as the pressure was further increased the observed count rates fell to a constant minimum value, which corresponded to none of the activity collecting on the tape and was just the result of decay occuring as the helium containing the activities was being pumped from the detector assembly. This was confirmed by the ovservation of an increase in the count rates when the vacuum pump was turned off (thus allowing a build up of helium containing activities in the detector chamber) followed by an appropriate reduction when the pump was turned on again.

If the observed drops in total system efficiency with increasing detector assembly pressure are the result of drops in the collecting efficiency as a consequence of collecting through a more dense atmosphere, it would be expected that the drops in efficiency would occur at lower pressures and be more severe as the capillary to tape distance was increased, allowing a greater opportunity for the beam of activities to interact with the atmosphere. Similarly, it would be expected that the drops in

efficiency would occur at lower pressures as the capillary to tape angle was made more oblique, allowing a greater opportunity for the beam of activities to be deflected from the collecting surface. Both effects are seen in the results reported in Figure 28. If the observed drops in total system efficiency with increasing detector assembly pressure were the result of drops in the transport efficiency as a consequence of changing flow considerations in the capillary, it would be expected that the efficiency would hold constant until the pressure in the detector assembly was raised beyond the point at which flow of Mach 1 could no longer be achieved, at which time the efficiency would start to drop off and continue to drop off with increasing pressure. Note, the pressure experienced at the exit of the capillary at Mach 1 is no longer achieved in the helium flow will be independent of capillary to tape distance and angle. From H. Dautet's paper [DaH73] this should occur at detector assembly pressures of ≥35 torr for our system operating as described above. While in each case the total system efficiency did seem to hold constant before starting its drop, the pressure at which the drop started and the severity of the drop was very much dependent on the capillary to tape distance and angle. It is of course necessary to consider that the pressure recorded for the detector assembly is then the pressure experienced at the exit of the capillary. However, it would be expected this error would be largest for the 1"-90° case, and this is the case for which the pressure corresponding to the initial drop in efficiency is the highest. Accordingly, it seems the primary factor acting in the drop in total system efficiency with increasing detector assembly pressure is a drop in collecting efficiency. This conclusion is reinforced upon considering the total system efficiencies of 50-75% reported in Section II. m. "Aqueous Chemistry" for collecting

activities in aqueous solution under atmospheric pressure.

From the results discussed above it is quite apparent that the requirements of the pumping system for a HeJRT system used alone are minimal. It is only necessary to maintain pressures of 20-30 torr in the low pressure end of the system without loss of efficiency. Only when the HeJRT is used to supply activities to equipment requiring low pressures is it necessary to consider large pumping capacities and helium skimming.

II. k. Efficiency vs Time

When considering the total HeJRT system efficiency vs time, it is necessary to consider two time scales. The first, measured in seconds, is the short-term efficiency building up when the cyclotron beam is first turned on. This is related to effects such as the time required to build up suitable cluster molecules. The second, measured in hours, is the long-term efficiency falling off as the system is used for long runs. This is related to effects such as cluster molecules collecting in the capillary. Occasionally it seems as if there is a third time scale, measured in minutes, over which the efficiency tends to build up after the cyclotron beam is first turned on. However, this time vs efficiency effect has not been documented. It is felt that this effect may be the result of moisture or oil leaving the target surface when it heats up from the beam striking it.

A series of runs was made to characterize the short-term efficiency build-up when the cyclotron beam is first turned on. In these runs 280-msec 28 P was the primary activity monitored. The 28 P was generated using 30-MeV protons on a 0.05-in. quartz target through the 28 Si $(p,n)^{28}$ P reaction. The helium was doped with 25 0 ppm benzene vapor and the pressure of the target assembly was maintained at 3 atm. The pressure in the detector assembly was maintained at 21 1 torr. The capillary was used 0.055-in. polyethylene. The activities were collected on paper tape which was advanced only between runs to supply a fresh surface for the next run. Also, between each run the target assembly was pumped out several times to remove cluster molecules remaining from the previous run. Each run consisted of making an x-y plot of gross γ count rate time (using a time base) as the cyclotron beam was turned on and off (see Figure 29). During the cyclotron on time the beam current was held as nearly constant as possible

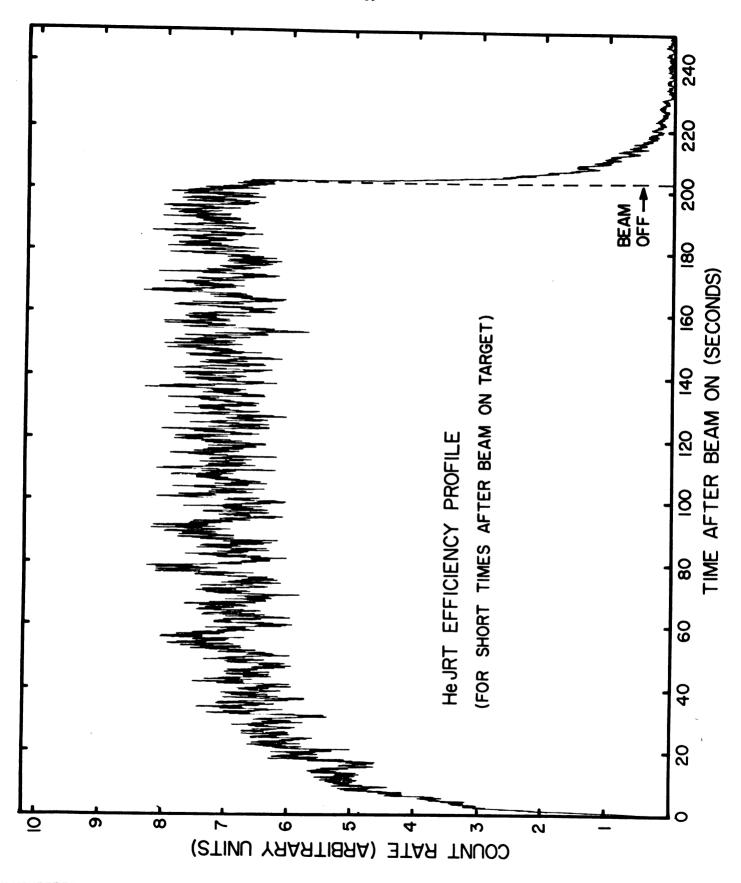


Figure 29. An example of the plots recorded as the cyclotron beam was turned on and off in an attempt to discover the short term efficiency build-up in the first moments after the beam is turned on.

usually ±3% and data from only the most constant runs were saved. The beam was turned on and off by raising and lowering a scintillator in the beam line near the cyclotron. The beam passing through the scintillator diverged and was of the wrong energy to be transported through the beam optics. This method of turning on and off the beam was chosen because it was faster than the vacuum valves in the beam line (about 0.2 sec as opposed to more than 1.0 sec for the valve). The count rate signal was taken from an ORTEC rate meter (#441) set for 10% standard deviation (shortest time constant). The output was plotted using a relatively fast Esterline Angus x-y recorder with a maximum slewing speed of 55 in./sec.

By comparing the curve recorded as the beam was turned on with the inverted curve recorded as the beam was turned off it should be possible to ovserve the build up of the total HeJRT system efficiency in the early moments after the cyclotron beam is first turned on. This should be possible because the time constants of the rate meter and the x-y recorder will be the same for increasing or decreasing count rates and the growth and decay curves for the activities generated will just be inversions of one another. Accordingly, the present difference in these two curves will correspond to the efficiency of the system. Figure 30 displays composite "beam-on" and "beam-off" curves taken from a collection of count rate curves like the one in Figure 29. Also shown in Figure 30 is the short term efficiency curve generated from the percent difference between the "beam-on" and "beam-off" curves. It can be seen that the efficiency rises very rapidly to about 70%, then rises rather slowly, taking almost a minute to reach full efficiency.

For these runs the standard target cylinder (see Section II. c.
"Target Assemblies"), which is about 4-cm long, had been replaced with one
10-cm long, such that it came to within 2 mm of the Faraday cup. This was

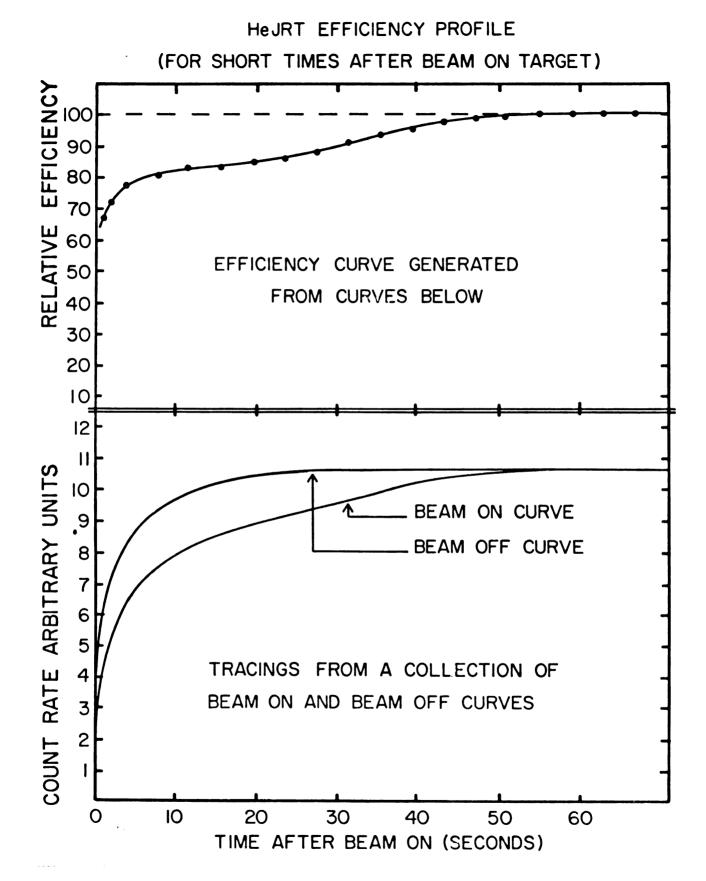


Figure 30. Composit beam-on and beam-off curves, and the relative efficiency for the HeJRT system in the first few moments after beam is first turned on.

done to insure that all molecular clusters generated in the volume between the target and the Faraday cup would immediately proceed toward entering the flow through the capillary and would not diffuse out into the bulk helium in the target assembly. This was important because if many of the clusters did enter the bulk helium supply the efficiency of the HeJRT system would not stabilize until the concentration of clusters in the bulk helium supply equilibriated. With the flow rate of 7500 standard cc-min, the rate at which the target cylinder was swept was about once every 1-1/2 sec. Accordingly, any increase in efficiency due to the generation of cluster molecules should be manifested within times of a few seconds (allowing for some mixing occuring between the helium in the cylinder and fresh helium entering the cylinder). Thus, it seems likely that the initial rapid rise in efficiency during the first seconds corresponds to the build up of the cluster molecules necessary for the efficient transport of activities through the HeJRT system.

The longer component of the efficiency rise is not so easily explainable. It could be explained if cluster molecules were diffusing out into the bulk helium supply, but this seems extremely unlikely in view of the large helium flow rate and the small separation between the target cylinder and the Faraday cup through which the clusters could diffuse. This possibility will be checked after the construction of a new target assembly is completed, one in which the helium is fed directly into the target cylinder and which has no place for clusters to diffuse to. If the longer component of the efficiency rise is still present with this new target cylinder, other possibilities such as adsorption of clusters on the cylinder walls or dead spaces occuring in the flow in the target assembly will be looked into.

As the HeJRT system is used the efficiency of its operation tends to

decrease; however, it is difficult to characterize this effect quantitatively. In early runs the drop in total system efficiency typically would manifest itself in a manner of hours of running time. Presently the drop in system efficiency does not manifest itself until many days of running time have elapsed. In fact, the capillary is now typically replaced after a week or so of running time not because of a drop in efficiency for the system but to prevent such a drop from occuring at an inconvenient time in an experiment. Thus, it is difficult to place a high efficiency time limit on the capillaries used in the system as operated today. It is, however, possible to make some empirical and/or qualitative statements concerning this efficiency drop and to present some thoughts on the subject which are not supported by hard experimental evidence.

The first concerns the nature of the efficiency drop. The efficiency will hold fairly constant, then after some time will start to drop. Then it will drop quite rapidly to about 10-20% of its initial efficiency, after which the drop is much more gradual. If the system is then rejuvinated as described below, the efficiency will return to essentially its initial value; however, as the system's use is continued the efficiency will again fall and the drop will occur after a shorter period of running than did the initial drop.

The reason for the efficiency drop is related to a build-up of material in the capillary and on the target which is usually quite visable. The effect of the build-up in the capillary presumably is to introduce additional turbulence in the helium flow and thereby to decrease transport efficiency. It seems logical that this turbulence would cause a further build-up, causing the more rapid drop in transport efficiency. The build-up in the capillary is soluble in acetone. Accordingly, by flushing the capillary

with acetone it is possible to rejuvinate the capillary. Presumably the build-up on the targets is from the same source; however, it is heated by the cyclotron beam and resembles more a carbon deposit, which is not soluble in acetone.

In early runs when benzene was first added to the helium supply to increase the efficiency of the HeJRT system, quite large amounts of benzene were used (higher than 0.1% in some cases). In an effort to reduce the build-up of material in the capillary and on the targets, the concentration of benzene in the system was gradually cut back to the 10-20 ppm used at present. While this may have helped slightly in the case of the build-up on the target it did not seem to bring about a major improvement in the case of the build-up in the capillary.

It seems the rate of decay of the system efficiency is related to air in the system. It was observed that the problem of build-up of material in the capillary was particularly bad in those runs in which the target assembly was opened frequently and those runs in which the operation of the HeJRT system using benzene in the helium supply was compared with using air plus water vapor in the helium supply. In both cases, if the pump-out of the target assembly were not complete, air would remain in the system. In general, little care was taken in these early runs to get a complete pump-out of the target assembly, relying on the flow of helium to purge the system. Since that time care has been taken to get more complete pump-outs, and the target assembly is filled with helium and pumped out 3 or 4 times before bringing the beam into the assembly. This, possibly combined with the low benzene concentrations used at present, have essentially solved the problems of build-up in the capillary and have greatly reduced the problem of build-up on the targets. Accordingly, the problem of the total transport efficiency dropping with time has been essentially eliminated.

II. 1. Collecting Surface Considerations

In the earliest runs of the HeJRT system in this laboratory the standard collecting surface was the sticky side of masking tape. For the past couple of years, since the addition of the tape transport, the standard collecting surface has become paper tape (1" non-oiled computer perforation tape, Singer P/n 200 1218 tape). The reason for the change to paper tape was for the obvious experimental simplification and has had no effect on the collection efficiency. On those occasions when cooled solid state detectors are exposed to the vacuum of the detector assembly, aluminized mylar tape is used to eliminate the problem of the small amount of moisture in the paper tape from entering the vacuum and condensing on the detector. Other groups have used such things as old computer magnetic tape (T. T. Sugihara, Texas A & M University, private communication), metal surfaces, and surfaces smeared with vacuum grease. All things considered, it does not seem to make very much difference what is used as a collecting surface when molecular clusters are used to carry activities through the system. However, a comparison of the collection efficiency of paper tape and aluminized mylar tape indicates the aluminized mylar tape to be a little less efficient. Figure 31 shows the results of the comparison made at a series of different target assembly pressures while looking at the 439-keV peak of ²³Mg. Each of the points in the figure is the average of three determinations made at that pressure. The two curves have the same essential shape, but the curve for aluminized mylar is from 9 to 12% below that for paper tape. In each case the detector assembly was pumped to below 10 torr and the capillary to tape distance and angle were 1/2 in. and 90°, respectively. At this time it is felt there is not enough known to present an explanation of the differing collection efficiencies, other

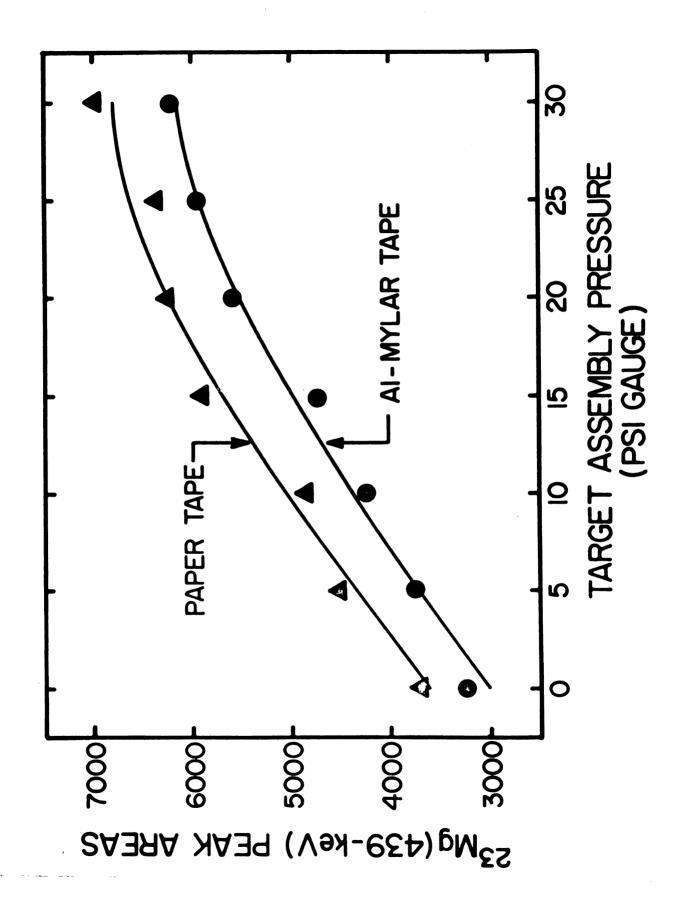


Figure 31. A comparison of the effectivness of paper tape and aluminized mylar tape as a collecting surface.

than to suggest the possibility that it is related to the rougher textured surface presented by the paper tape.

A preliminary study has been conducted to determine the effect of varying the tape to capillary distance and the angle on collection efficiency. The collection efficiency was followed by monitoring the gross γ count rate of activities produced with 30-MeV protons on aluminum. The two principal components of the activity were ²³Mg and ²⁶Si. For these determinations a 0.055-in. polyethylene capillary was used and the helium flow was doped with 10 ppm benzene vapor. The results are summarized below for paper tape.

Tape to	Capillary	Collecting
Angle	Distance	Efficiency
90°	1/8 inch	≣100%
90°	1 inch	97.5 <u>+</u> 5.%
45°	1/8 inch	98.5 <u>+</u> 5.%
45°	1 inch	97.5 <u>+</u> 5.%

Accordingly, within the limits of the uncertainty of the measurements the collecting efficiency for paper tape is unaffected by changes in capillary to tape angles up to 45° or distances up to 1 in. Since the drops in efficiency upon changing the angle and distance are so small, if they do exist, none of the in-between values were checked. The capillary to tape angle and distance of 45° and 1 in. are what is typically used in γ singles experiments in order to keep the tip of the capillary (where activities will often build up) out of the view of a collimated detector. Activities have been collected on paper tape at distances up to 6 in. with fairly good yields; however, at this distance it is necessary to take into consideration the divergence of the cluster molecules leaving the capillary. Approximately 90% of the clusters diverge with an angle of less than 3°

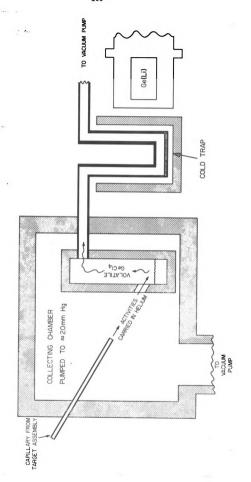
(see Section II. F. "Cluster Molecules"). As yet this study has not been extended to the aluminized mylar tape we occasionally use. However, by private communication, the members of R. D. Macfarlane's group at Texas A & M report the efficiency for collecting on mylar tape drops to about 50% on changing the capillary to tape angle from 90° to 45°

When the HeJRT system is operated using molecular clusters to increase transmission efficiency, it is necessary to consider a couple of side effects. The first is a desirable effect; when the desired product of the nuclear reaction is volatile or is naturally a gas, it is not necessary to go to any additional effort (like using a LN, cooled collecting surface) to hold the activity after transport through the system. This is evidenced by the presence of the 2311-keV line from 71-sec 14 0 in all γ spectra recorded when using an oxide target in the HeJRT system. The line is present in good yields in runs using both paper tape and aluminized mylar tape, both at room temperature. The second effect is not desirable when performing charged particle spectroscopy; the build-up of cluster molecules on the collecting surface, through which the emitted charged particles must pass will degrade the energy of the particles. The effect on β particles is small except when the build-up of clusters occurs over a long period of time as is the case for long-lived activities. However, the effect on the energy of emitted a particles is much more serious even when the build-up of clusters is only limited to a few minutes. It is hoped a heated collecting surface can be used in these cases to break up the cluster molecules as they are deposited on the collecting surface, such as R. D. Macfarlane uses in his recoil time-of-flight spectrometer [MaR73].

II. m. Aqueous Chemistry On-Line

The hope that "wet" chemistry could be performed on-line with the HeJRT system arose from the observation that the efficiency of the HeJRT system when depositing activities on paper tape did not start to fall off until the pressure in the detector chamber (box where activities transported through the system are deposited on some collecting surface and counted) was raised to above 20-30 torr (see Section II.n. 'Detector Assembly Pressure vs. Efficiency". This was important because the vapor pressure of water at 20°C is 17.5 torr. Accordingly, it would be possible to do aqueous chemistry under these conditions (collecting chamber pressure \$20 torr) and not have the solutions boiling off.

The first attempt at chemistry was an on-line attempt in the search for ⁶⁴Ge. The apparatus for this run is shown in Figure 32. The activities were generated using a ³He beam on a natural Zn foil and were transported through a polyethylene capillary to the detector chamber. The detector chamber was pumped so as to maintain a pressure ≥20 torr. The exit of the capillary was directed at an orifice in a sealed container partially filled with concentrated HCl. It was hoped that the activities attached to molecular clusters would enter the HCl container through the orifice and become trapped in the acid solution. There the Ge activities would form the volatile chloride GeCl₄ and be pumped off to a cold trap, where they could be counted. This first attempt was unsuccessful primarily because of inefficiencies remaining in the HeJRT system at that time, poor alignment between the capillary and orifice to the acid container,



Sketch of the experimental set-up for our first attempt at performing aqueous chemistry with the HeJRT system. Figure 32.

and a very small effective target thickness. The ⁶⁴Ge search was subsequently successfully carried out [RoR72] using essentially this chemistry, but a pneumatic target system [KoK73] ("rabbit") system was employed instead of the HeJRT system.

The first successful chemistry followed the discovery that not only is it possible to trap activities flowing up the capillary in aqueous solution by merely bubbling the helium flow from the capillary through the solution, but also that the yields remained essentially as good even if the "low pressure" end of the capillary and the aqueous solution were at atmospheric pressure. In a series of runs comparing the amounts of activity trapped in solution under various pressures to that collected on paper tape under ≲1 torr pressure it was observed that between 1/2 and 2/3 of the activity could be collected in the aqueous solutions. The amount of activity trapped was largely independent of the pressure over the solution (the pressure gradient across the total system was held constant at about 2 atm). The amount of activity trapped was also found to be independent of the acid concentration of the trapping solution (important if chemistry is to be performed). We also felt that much of the activity lost might have been retained by generating smaller bubbles (with correspondingly higher surface to volume ratios) to provide for more contact between the gas contained in the bubbles and the solution.

If one accepts the role of clusters to be that described in Section II.f."Cluster Molecules", then it does not necessarily follow

that if one can trap activities in solution it will be possible to perform conventional chemistry with these activities. If the thermalized recoils become a part of the cluster molecules at some point during the transport process, then it would not be possible to perform chemistry characteristic of the recoil unless the recoil is successfully freed of the cluster molecule. The reason for this is simply that the recoil is present only as a very small component (about a part per million) in the recoil-cluster combination. Accordingly if the recoil remains attached to the cluster after they are trapped in a solution one would expect the combination to follow chemistry characteristic of the cluster and not of the recoil. It is observed that cluster molecule deposits are soluble in water; however, it still does not necessarily follow that it will be possible to successfully perform chemistry with the recoils. If the recoil is deeply imbedded in the cluster molecule and if the individual cluster molecules maintain their integrity in dissolving, then the recoil would not be freed from the cluster in the dissolution process.

The first attempt at performing chemistry on activities transported by the HeJRT system and trapped in aqueous solution at atmospheric pressure was successful. This was the separation of Cu and Zn activities using ion-exchange techniques. A natural Zn target was bombarded with 30-MeV protons. The principal activities generated were (33 sec) 63 Ga and (24 min) 60 Cu, from the (p,2n) and $(p,\alpha n)$ reactions on 64 Zn. The activities were transported through the HeJRT

system and trapped in a 2N HCl solution by simply letting the helium flow from the capillary bubble through a small beaker of acid under atmospheric pressure. Activities were collected for about 25 min.

During the 25 min collecting time and a short additional time before the activities were loaded on the ion-exchange column, essentially all the 63Ga decayed to (38 min) 63Zn. The column was loaded with Dowex 1-x8 in the chloride form. The column was subsequently eluted with an additional small amount of 2N HCl, then the column and the eluant were each counted for about 10 min using a 4.6% Ge(Li) detector. The spectra recorded are shown in Figure 33. It appears the separation was rather clean in that there is no evidence of either Zn line appearing in the spectrum of the eluted sample and only a small amount of Cu was not completely eluted from the column as evidenced by the weak appearance of the 1333-keV line in the spectrum from the column.

The observation that straightforward chemistry characteristic of the recoil is successful with activities transported with the HeJRT system suggests that somehow the recoil has been freed from the recoil-cluster combination. A discussion of possible mechanisms for freeing the recoil from the cluster molecule would not be profitable at this time as more information is needed from experiments not yet performed. Also unknown at this point was the time required for the process of freeing the recoils from the clusters. This time was obviously less than the 5 to 10 minutes that elapsed between the end of the collection of activities in the experiment described above and

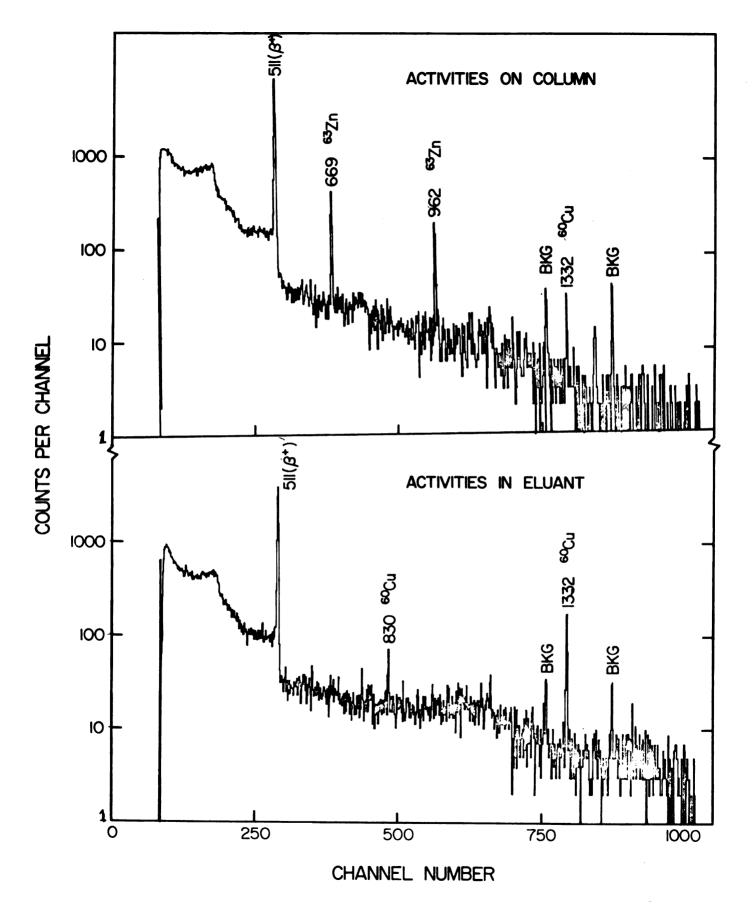


Figure 33. Spectra recorded in our first successful attempt at performing aqueous chemistry with the HeJRT system.

the passage of these activities through the ion-exchange column. If it were much longer than this it would not have been possible to have so clean a chemical separation. Zinc activities still trapped in cluster molecules would have passed through the column, resulting in Zn lines being present in the spectrum of the eluted sample.

The next attempt at performing chemistry on activities transported by the HeJRT system was an attempt at performing chemistry on-line with the HeJRT system. It was a separation of Ga from both Cu and Zn activities using ion-exchange techniques. As in the previous attempt, a natural zinc target was bombarded with 30-MeV protons, producing primarily the same (33 sec) 63Ga and (24 min) 60Cu activities. Also present was some 63 Zn from the partial decay of 63 Ga and from a (p,pn)reaction on 64Zn. However, time was not allowed in this run for the 63 Ga to decay appreciably to 63 Zn. The flow from the capillary of the HeJRT target assembly entered directly into the chemical system (see Figure 34), and was mixed with a flow of 8N HCl (with carrier) pumped from a container of acid. The mixing took place in a small chamber and was quite turbulent because of the large volume of helium flowing from the target assembly ($^{2}40$ standard cm 3 /sec). The mixture of helium and acid moved rapidly to the top of an ion-exchange column, again because of the large volume of helium flowing. Here the acid solution was allowed to enter the column while the escaping helium, presumably still carrying some activities, was pumped away. The ionexchange column was loaded with Dowex 1-x8 in the chloride form; a

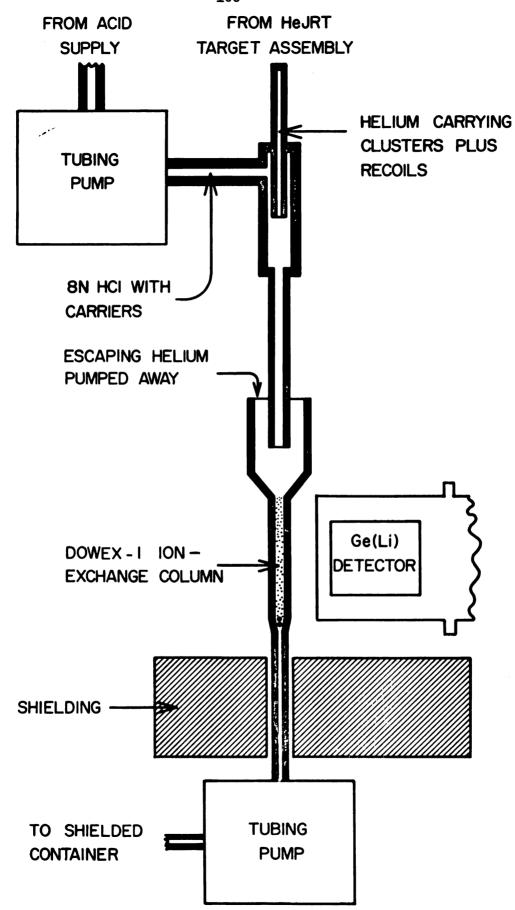


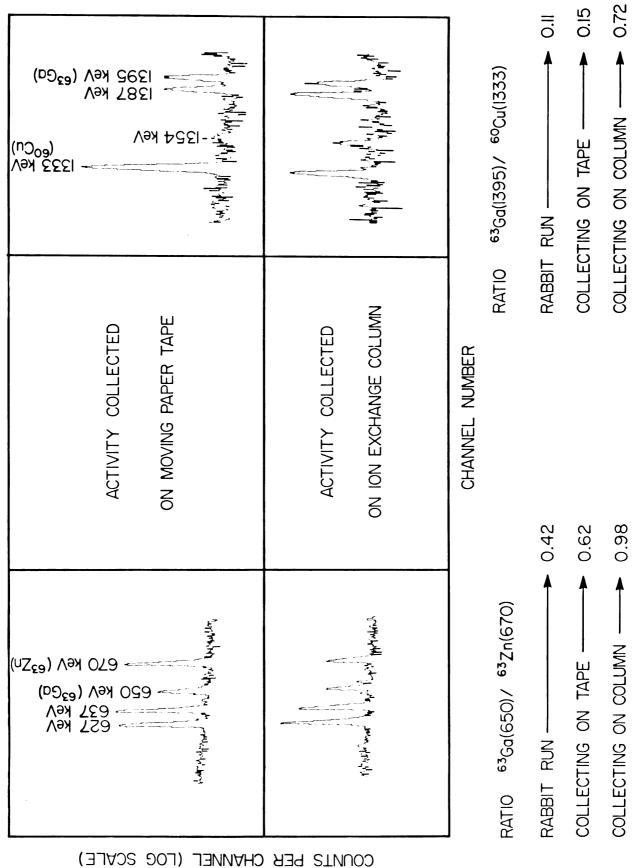
Figure 34. Sketch of the experimental set-up for on-line aqueous chemistry used in our third attempt at performing chemistry with the HeJRT system.

rather large mesh (50-100) was used to decrease the hold-up time of the column. The acid solution was drawn through the column and pumped to a shielded container, and a 4.6% Ge(Li) detector was used to record the y-ray spectra of activities on the column.

To serve as a comparison a run was made where the activities were collected on moving paper tape under vacuum. The tape speed was such that the activities on the tape spent about 1 min before the Ge(Li) detector. Two short sections of the spectra recorded in this experiment are shown in Figure 35 along with a comparison of the results. Further comparisons with a previous run made by G. C. Giesler [GiC71] using the "rabbit" system are also included in the figure. The relative intensity of the 60 Cu to the 63 Ga peaks in the chemistry run are down by a factor of 6 over those in the published rabbit run and by a factor of 5 over those in the paper tape run. The 63Zn relative to the 63Ga peaks in the chemistry run are down by a factor of more than 2 over those in the rabbit run. Further, the data acquisition rate was up by a factor of about 2 for the chemistry run over the rabbit run. The possibility that the improvement in the 63Ga to 60Cu and 63Zn ratios was just a half-life effect is eliminated by the increased presence of (2.6 min) 64 Ga and (15 min) 65 Ga peaks at 1387and 1354-keV, respectively, in the chemistry spectrum.

This experiment provides an improved upper limit of the time necessary to free recoils from molecular clusters in aqueous solution.

The time elapsing between the mixing of the helium and acid flow, and



Portions of the spectra recorded using our experimental set-up for on-line aqueous chemistry and comparison with the results from previous runs. Figure 35.

the acid solution leaving the ion-exchange column was of the order of 1 second. Accordingly, the upper limit on the time necessary to separate recoil and cluster should be set at about 1 second in this case. A check of the eluant from the column should have been made to see if any Ga activities were present; if no Ga activities were present the upper time limit of 1 second would be definite. However, from the data rate observed it is certain that at least a large fraction of the recoils had been separated from clusters in this 1 second elapsed time.

We are currently preparing to perform a series of experiments that will attempt to set a definite upper limit on the time necessary to separate recoils from clusters and also to demonstrate further the usefulness of this technique by performing separations on successively shorter-lived activities. There is some hope this series will culminate in the separation of (182 msec) 40 Sc from other products.

It is clear that much of the detail of the mechanism allowing conventional chemistry with HeJRT transported activities is not presently understood. The point of the preceding discussion is just that it is possible to do this type of chemistry with the HeJRT system. It might be further pointed out that there may be additional applications, beyond just rapid nuclear chemical separations, resulting from the observation that relatively simple "wet" chemistry, online with the HeJRT system, is possible. One additional application of this technique could be to supply chemically active radioisotopes, in times \$1 second, that are carrier and parent free, for use in studying biological or other chemical systems.

II, n. Gas Phase Separations

To date there has been no attempt to use this HeJRT system for separations involving the selective generation of gaseous products for the purpose of achieving separations of reaction products in differing physical states. There are two projects presently under consideration that would make use of this technique in this laboratory. They are the search for 54 Ni and measuring the β end points of 55 Ni and ⁶⁴Ge. It is hoped these projects can be accomplished by generating the activities as nickel carbonyl and as monogermane, by replacing the helium with carbon monoxide and hydrogen, respectively. In general, the method of separation would be to run the jet system in such a manner that its transport efficiency is very low for non-gaseous products. This is in contrast with the normal operation of the jet system, in which non-gaseous (as well as gaseous) recoils are bound to clusters to achieve high efficiencies for their transport through the system. The jet system would be run without using cluster generating impurities in the gas supplies and possibly sources of turbulence could also be placed in the capillary. Since these actions do not decrease the efficiency for transporting products normally in the gaseous state, a separation of gaseous and non-gaseous products would be achieved. If the desired activity is the only one forming a gaseous product under the conditions being used, the separation should be complete. If more than one gaseous product is formed it would be necessary to use some other property such as boiling point or decomposition point to separate the activities further after they exit the capillary. For a further discussion of this type of separation, see K. Bachmann's article in <u>Proceedings of the International Conference on Electromagnetic Isotope Separations and the Techniques of Their Applications</u> (1970), p. 126 [BMBW-FB 70-28].

II. o. Plasma Chemistry

For the purposes of this discussion plasma chemistry is taken to mean chemistry occurring between thermalized recoils and cluster molecules in the plasma in the target assembly for the purpose of achieving chemical separations. There is some evidence separations of this nature can be accomplished. If this does become a reality, it will extend the realm of ultra-fast chemistry beyond those elements that easily form gaseous products in the HeJRT system. The difficulty of collecting or trapping gaseous products would be eliminated, since virtually any surface could be used for collecting the activities. This type of chemical separation would also be fully compatible with either method of on-line mass separation (identification) discussed in this thesis.

The possibility of being able to perform plasma chemistry arises from a consideration of the mechanism through which the recoil becomes a part of the cluster molecule. It seems likely that the cluster molecules are formed as impurities present in the helium condense out of the plasma in the target assembly (where "condense out" is not clearly defined and can be taken to be polymerization, nucleation, etc; see Section II c "Cluster Molecules"). If during the process of condensation, the thermal recoil, because of its physical presence in the region of condensation, becomes trapped in the cluster molecule, then plasma chemistry will not be possible. If on the other hand, the thermal recoil becomes bound to some chemically active site on the

cluster molecule during or after the condensation process, the possibility of controlling the nature of these chemically active sites and thereby possibly achieving a separation of chemically differing recoils can be considered. That is to say, if it is possible to control the types of recoils that become attached to clusters, a separation of the recoils will be accomplished as a result of the very poor transport efficiency of the HeJRT system for those recoils not attached to clusters.

The "chemically active site" hypothesis is supported by the results of two experiments. The first supporting experiment was the series of total efficiency runs made for the HeJRT system. cies were determined for Zn, Cu, and Co recoils and were found to be 50%, 75%, and 90%, respectively (see Section II.h. "Total System Efficiency Determination" for the details of this determination). Physically these three recoils are quite similar to one another (atomic radius, polarizability, ionization potentials, etc.). Thus, it is difficult to explain the different efficiencies observed unless somehow their chemical natures are also considered, and this implies some sort of chemical bonding between recoil and clusters. The second supporting experiment was a series of runs in which the impurities fed into the helium were changed and the transport efficiencies for a pair of activities provided from the same target were monitored. In this experiment a natural aluminum target (100% ²⁷Al) was bombarded with 30-MeV protons to produce (2.1 sec) ²⁶Si and (12 sec) ²³Mg from

(p,2n) and $(p,\alpha n)$ reactions, respectively. Spectra of the products were recorded when the primary impurity in the helium was 1) benzene vapor, 2) compressed air and water vapor, and 3) when the level of impurities was very low. The concentration of benzene vapor used was roughly 0.01% to 0.1%. The concentration of compressed air used was roughly 5% and the water vapor was added by passing the helium through a gas washing bottle. Each time an impurity change was made the target assembly was pumped out and refilled two or three times with helium doped with a different impurity. However, when the main component of the impurities was changed from run to run it should be presumed that a small (and possibily significant) amount of the impurities from the previous run remained in the target assembly. This was particularly true in the runs where pure helium was used; here the transport efficiency did not drop nearly so much as it would have if no impurities had remained. The results of this experiment are shown in Figure 36. It is quite apparent that the absolute efficiencies of the HeJRT system for transporting different activities is dependent on the type of impurities in the helium. Magnesium is transported best when benzene vapor is used, while silicon is transported best when compressed air plus water vapor is used (the ratio of Si to Mg activities transported changes by nearly 40% on changing these types of impurities used to produce cluster molecules). An attempt to somehow explain away the change in efficiency for Si (by assuming the formation of a silane preferentially when one type of impurity is used) does nothing to explain away the change in efficiency for Mg. Since the activities were made at the same

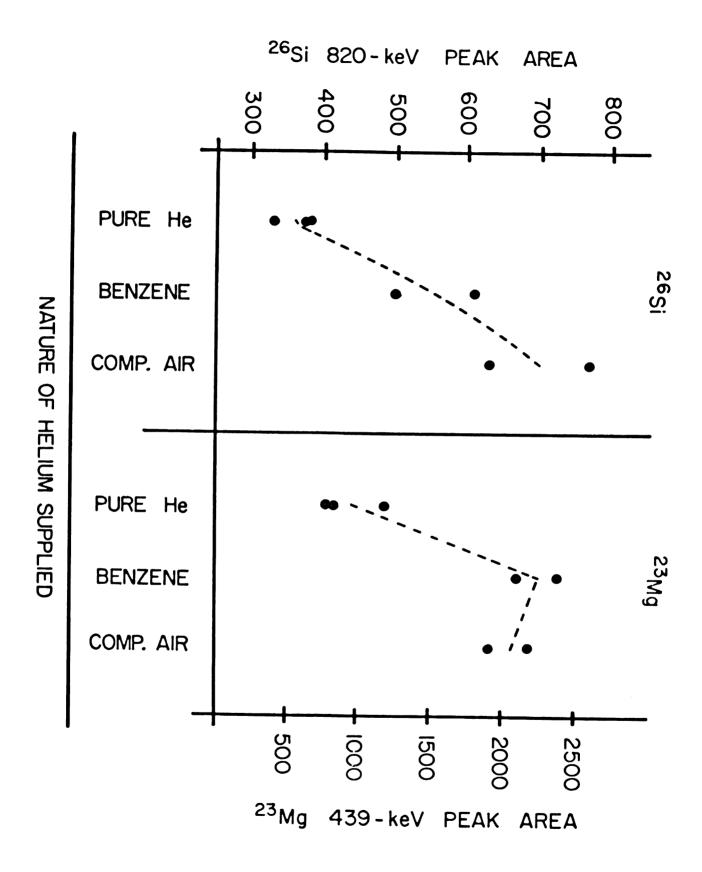


Figure 36. Results supporting the possibility that chemical separations will be possible using "plasma chemistry".

time, under the same conditions, from the same target, the efficiency changes cannot be explained away as a half-life effect or as a reflection of any changes (other than the source of cluster generating components) in the HeJRT system during the experiment.

Accordingly, from the observation that total transport efficiencies are dependent on both the chemical nature of the recoil and the source of impurities for the cluster molecule (i.e., the chemical nature of the cluster molecule), it seems likely that plasma chemistry (as defined at the start of this section) can be achieved. There remains one last consideration that may help to make clean plasma chemistry a reality. That is the possibility of generating cluster molecules off-line and feeding those molecular clusters into a system using pure helium (see Section II. f. "Cluster Molecules"). This may help because it may allow generation of more exotic molecular cluster out of components (impurities) or under conditions that would be detrimental to the successful operation of the HeJRT system.

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