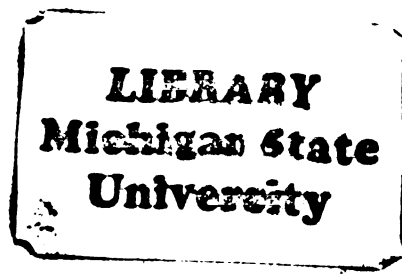




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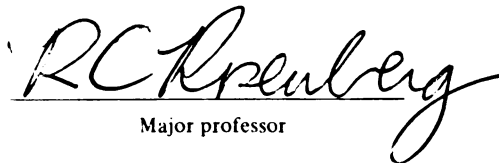
Sensitivity Calculations for Bond Graph
Models of Linear Resistive Systems

presented by

David Richard Reed

has been accepted towards fulfillment
of the requirements for

Master's degree in Mechanical
Engineering


Major professor

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**SENSITIVITY CALCULATIONS FOR BOND GRAPH
MODELS OF LINEAR RESISTIVE SYSTEMS**

By

David Richard Reed

A THESIS

**Submitted to
Michigan State University
in partial fulfillment of the requirements
for the degree of**

MASTER OF SCIENCE

Department of Mechanical Engineering

1984

ABSTRACT

SENSITIVITY CALCULATIONS FOR BOND GRAPH MODELS OF LINEAR RESISTIVE SYSTEMS

By

David Richard Reed

Knowledge of the sensitivities of system response variables to a set of design parameters can be very useful in designing engineering systems. This thesis presents a method for calculating output sensitivities for linear resistive engineering systems modeled by bond graphs. A software module, written to interface with an existing bond graph processor, provides linear resistive system solutions and output sensitivities. The sensitivities are used to predict new solutions that result from parameter variations.

ACKNOWLEDGMENTS

I would like to thank my major professor, Dr. Ronald Rosenberg. His guidance, knowledge, and friendship have made this research possible.

I would also like to thank DuPont and Chevron for providing fellowship support during my graduate study at Michigan State University.

Finally, for her continuous love and support, I would like to thank my best friend and wife, Tamra.

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Chapter 1

INTRODUCTION

Modern design of engineering systems often involves computer analysis of a mathematical model. Knowledge of the sensitivities of system response variables to a set of design parameters can greatly enhance the design process. The problem considered in this thesis is how to calculate the sensitivities of system outputs to resistive parameters for linear resistive engineering systems modeled by bond graphs [1]. Emphasis is placed upon efficient computation. Many practical system models fall into this class of systems.

In general, output sensitivities can be obtained by stepping the parameters over a range of values and calculating the associated changes in output. Although this may be acceptable for small systems with only a few parameters, the computational burden increases significantly for larger systems. Numerous complete system solutions would be necessary to find the sensitivity of a set of outputs to each parameter.

An alternative method for calculating output sensitivities for linear electrical resistive networks was given by Frank [2] and developed more fully by Calahan [3]. The method is based on a general network theorem by Tellegen and makes use of an adjoint network

(sensitivity model) approach. The adjoint network solution and the original network solution are used to calculate precisely output sensitivities without recourse to an analytic expression.

Adapting this adjoint system approach to bond graph models provided an efficient method for calculating output sensitivities. A computer software module called STATIC was written to interface with ENPORT-5 [4], an interactive bond graph processor for linear dynamic systems. The combined program will solve linear resistive systems with constant inputs, calculate output sensitivities, and use the sensitivities to predict new solutions due to one-port resistance parameter variations.

Chapter 2 describes the implementation and operation of STATIC and presents some examples. Chapter 3 illustrates a sample run through the STATIC module. Chapter 4 considers in detail the sensitivity calculation method and how it applies to bond graphs. Chapter 5 provides a summary of results and some suggestions for future work.

Chapter 2

THE STATIC MODULE

The STATIC module, when interfaced with ENPORT-5, allows solution of linear resistive systems modeled by bond graphs. Such systems contain no C or I elements. The ENPORT-5 program processes the bond graph through equation formulation. Program control is then transferred to the STATIC module for solution. The inputs are set and the outputs are computed. The effort and flow on each resistive port (R-port) is also available. Next the sensitivity of each system output to each one-port resistive parameter (R-parameter) may be calculated. Finally a prediction of new system outputs due to changes in one or more R-parameters may be made. The prediction makes use of the calculated output sensitivities to generate a linear approximation to the new solution.

2.1 Implementation and Operation

The calculation of sensitivities by the adjoint system method requires the computation of R-port flows for both the original system and the adjoint system (see Chapter 4). The structure of both systems is identical and is defined by the original model. ENPORT-5 will process the model to the following junction structure equations.

$$D_i = S_{33} * D_o + S_{34} * U \quad (2.1)$$

$$V = S_{43} * D_o + S_{44} * U \quad (2.2)$$

$$D_o = L * D_i. \quad (2.3)$$

D_i , D_o , U , and V are vectors defined in Figure 1 and S_{33} , S_{34} , S_{43} , S_{44} , and L are matrices [5]. Equation (2.3) is substituted into (2.1) and the dissipation field (R-field) input D_i is solved for as a function of U . The resulting equation is

$$D_i = (I - S_{33} * L)^{-1} * S_{34} * U. \quad (2.4)$$

The R-field output is computed using equation (2.3). The R-port efforts and flows are contained in D_i and D_o and are extracted using causality information. The junction structure output V is then computed using equation (2.2).

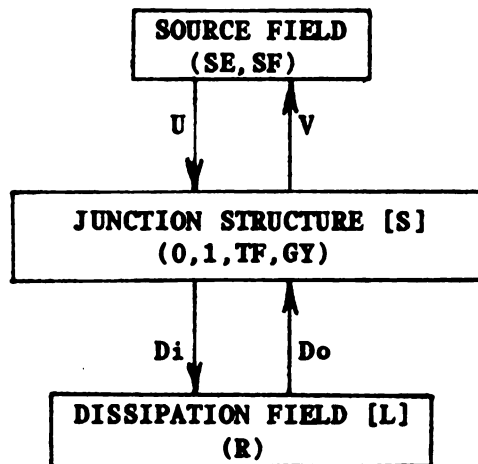


Figure 1. Structure of a Linear Resistive System

To calculate sensitivities, the adjoint system must now be solved. Since the structure is identical to the original system, equations (2.4) and (2.3) can be used with an adjoint input vector. All inputs are set to zero except the input corresponding to the desired output, which is

set to magnitude 1. The adjoint R-field vectors are computed and the adjoint R-port flows are extracted. The sensitivity of the desired system output to each one-port R-parameter is then calculated as the negative product of the R-port flows from the original and adjoint systems. Chapter 4 develops the the adjoint sensitivity method in some detail.

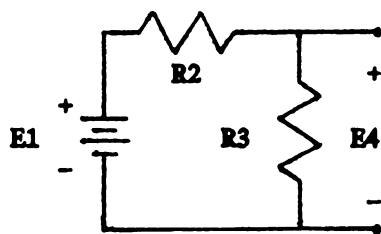
A prediction of a new solution can be made once the original solution, the output sensitivities, and a user-defined delta-R vector of changes are known. The following equation is used.

$$V(k, \text{predicted}) = V(k) + \sum ((dV(k)/dR_i) \cdot dR_i)$$

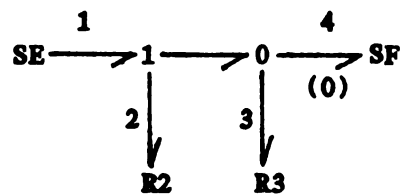
where $dV(k)/dR_i$ is the sensitivity of output $V(k)$ to parameter R_i and dR_i is the change in resistance for parameter R_i . A dR value may be set for each one-port R-parameter and the above summation is taken over all i , where $i = 1$ to r , the number of one-port resistors.

2.2 Example 1 - Voltage Divider Circuit

Consider the linear resistive circuit of Figure 2 and its bond graph.



Circuit Diagram



Bond Graph

Figure 2. Voltage Divider Circuit

Note that the zero flow source on port 4 of the bond graph represents the open circuit voltage output E4. The units are volts, amperes, and ohms. The inputs are $E(1) = 10$, $F(4) = 0$. The R-parameters are $R2 = 25$, $R3 = 75$. The bond graph was described to ENPORT-5 and processed. The STATIC module computed the system solution and calculated the sensitivities. The computer generated results are:

SYSTEM INPUTS...

$E(1) = 1.0000E+01$
 $F(4) = 0.0000E-01$

SYSTEM OUTPUTS...

$F(1) = 1.0000E-01$
 $E(4) = 7.5000E+00$

R ELEMENTS...

$E(2) = 2.5000E+00$ $F(2) = 1.0000E-01$
 $E(3) = 7.5000E+00$ $F(3) = 1.0000E-01$

SENSITIVITIES...

$dF(1)/d(R2) = -1.0000E-03$
 $dF(1)/d(R3) = -1.0000E-03$
 $dE(4)/d(R2) = -7.5000E-02$
 $dE(4)/d(R3) = 2.5000E-02$

For comparison, the analytical solution of the voltage divider circuit is:

OUTPUTS

$F(1) = E(1)/(R2 + R3) = 0.1$
 $E(4) = E(1)*R3/(R2 + R3) = 7.5$

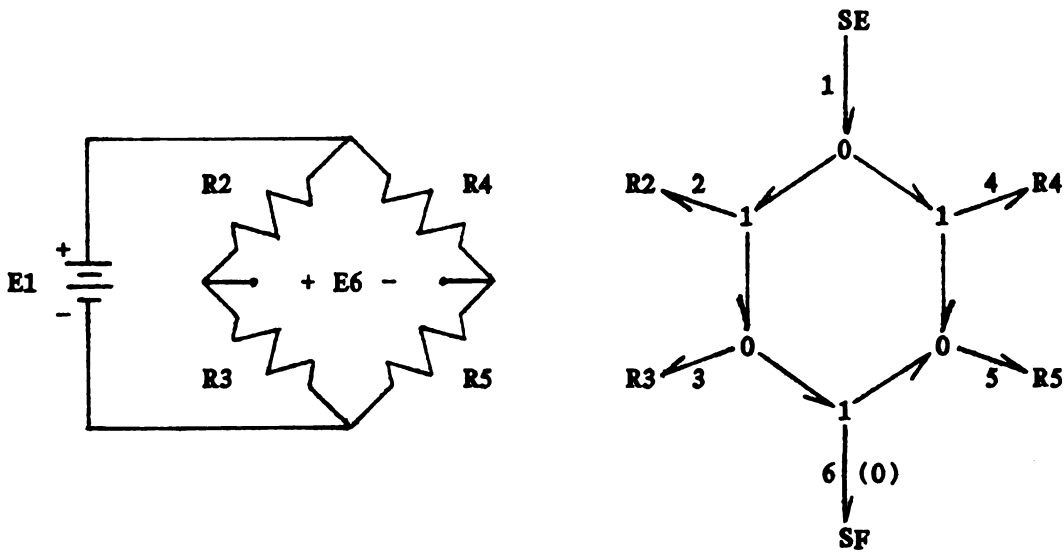
SENSITIVITIES

$dF(1)/dR2 = -E(1)/(R2 + R3)^2 = -0.001$
 $dF(1)/dR3 = -E(1)/(R2 + R3)^2 = -0.001$
 $dE(4)/dR2 = -E(1)*R3/(R2 + R3)^2 = -0.075$
 $dE(4)/dR3 = E(1)*R2/(R2 + R3)^2 = 0.025$

The computer generated results match the analytical results.

2.3 Example 2 - Wheatstone Bridge Circuit

Consider the linear resistive circuit of Figure 3 and its bond graph. The inputs are $E(1) = 6$, $F(6) = 0$. The R-parameters are $R2 = 20$, $R3 = 100$, $R4 = 200$, $R5 = 40$. The bond graph was described to ENPORT-5 and processed.



Circuit Diagram

Bond Graph

Figure 3. Wheatstone Bridge Circuit

The STATIC module computed the system solution and calculated the sensitivities. The computer generated solution is:

SYSTEM INPUTS...		SYSTEM OUTPUTS...	
$E(1) =$	$6.0000E+00$	$F(1) =$	$7.5000E-02$
$F(6) =$	$0.0000E-01$	$E(6) =$	$4.0000E+00$
R ELEMENTS...			
$E(2) =$	$1.0000E+00$	$F(2) =$	$5.0000E-02$
$E(3) =$	$5.0000E+00$	$F(3) =$	$5.0000E-02$
$E(4) =$	$5.0000E+00$	$F(4) =$	$2.5000E-02$
$E(5) =$	$1.0000E+00$	$F(5) =$	$2.5000E-02$

SENSITIVITIES...

$dF(1)/d(R2) = -4.1667E-04$
 $dF(1)/d(R3) = -4.1667E-04$
 $dF(1)/d(R4) = -1.0417E-04$
 $dF(1)/d(R5) = -1.0417E-04$

$dE(6)/d(R2) = -4.1667E-02$
 $dE(6)/d(R3) = 8.3333E-03$
 $dE(6)/d(R4) = 4.1667E-03$
 $dE(6)/d(R5) = -2.0833E-02$

Suppose that the nominal value given for R4 was uncertain. Let the original value be reduced by 10%. New outputs can be predicted by the STATIC module. First the dR vector is set by entering -20 (a 10% reduction) for dR4. Next the new solution is predicted. The computer results are:

THE dR VECTOR...

$d(R2) = 0.0000E-01$
 $d(R3) = 0.0000E-01$
 $d(R4) = -2.0000E+01$
 $d(R5) = 0.0000E-01$

LINEAR PREDICTION OF SYSTEM SOLUTION...

SYSTEM INPUTS...

$E(1) = 6.0000E+00$
 $F(6) = 0.0000E-01$

SYSTEM OUTPUTS...

$F(1) = 7.7083E-02$
 $E(6) = 3.9167E+00$

For comparison, the system was re-solved completely with $R4 = 180$. The results are:

SYSTEM INPUTS...

$E(1) = 6.0000E+00$
 $F(6) = 0.0000E-01$

SYSTEM OUTPUTS...

$F(1) = 7.7273E-02$
 $E(6) = 3.9091E+00$

The predicted solution nearly matches the actual solution but required fewer calculations and much less time to get. The percent error between the actual solution and the predicted solution is 0.25% for F(1) and 0.20% for E(6).

Chapter 3

STATIC MODULE SAMPLE RUN

This chapter illustrates a sample run through the STATIC module. Consider the bond graph model of Figure 4.

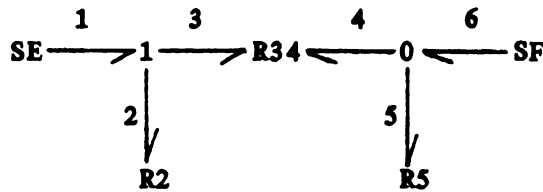


Figure 4. Sample Run System Model

The system parameters and defining constitutive equations are given below.

PARAMETERS

$$R2 = 250$$

$$R34 = \begin{bmatrix} 350 & 200 \\ 200 & 200 \end{bmatrix}$$

$$R5 = 200$$

CONSTITUTIVE EQUATIONS

$$E(2) = 250 * F(2)$$

$$E(3) = 350 * F(3) + 200 * F(4)$$

$$E(4) = 200 * F(3) + 200 * F(4)$$

$$E(5) = 200 * F(5)$$

The following processing steps were performed in ENPORT-5.

- (1) Input the bond graph
- (2) Assign power directions
- (3) Assign causality
- (4) Set parameters
- (5) Formulate the system equations

Program control was then transferred to the STATIC module for solution.

The next few pages show the transcript of the sample run through the STATIC module.

STATIC SOLVER OPTIONS

```

-----
L: LIST INPUT VALUES
M: MODIFY/SET INPUT VALUES
G: GET THE SYSTEM SOLUTION
D: DISPLAY SYSTEM SOLUTION
C: CALCULATE SENSITIVITIES
S: SHOW THE SENSITIVITIES
P: PREDICT NEW SYSTEM SOLUTION
H: HELP
X: EXIT STATIC SOLVER (=DEFAULT)
-----

```

ENTER OPTION (X):M

SET INPUTS...

ENTER E(1) (0.0000E-01):10

ENTER F(6) (0.0000E-01):

STATIC SOLVER OPTIONS (L,M,G,D,C,S,P,H,X,<FULL>):G

COMPUTATION COMPLETED.

STATIC SOLVER OPTIONS (L,M,G,D,C,S,P,H,X,<FULL>):D

SYSTEM INPUTS...

SYSTEM OUTPUTS...

E(1) = 1.0000E+01

F(1) = 2.0000E-02

F(6) = 0.0000E-01

E(6) = 2.0000E+00

DISPLAY EFFORTS AND FLOWS ON R-PORTS? (Y):

R ELEMENTS...

E(2) = 5.0000E+00

F(2) = 2.0000E-02

E(3) = 5.0000E+00

F(3) = 2.0000E-02

E(4) = 2.0000E+00

F(4) = -1.0000E-02

E(5) = 2.0000E+00

F(5) = 1.0000E-02

STATIC SOLVER OPTIONS (L,M,G,D,C,S,P,H,X,<FULL>):C

CALCULATION COMPLETED.

STATIC SOLVER OPTIONS (L,M,G,D,C,S,P,H,X,<FULL>):S

SENSITIVITIES...

$dF(1)/d(R2) = -4.0000E-05$

$dF(1)/d(R5) = -1.0000E-05$

$dE(6)/d(R2) = -4.0000E-03$

$dE(6)/d(R5) = 4.0000E-03$

SENSITIVITIES ASSOCIATED WITH MULTI-PORT R'S ARE NOT AVAILABLE.

STATIC SOLVER OPTIONS (L,M,G,D,C,S,P,H,X,<FULL>):P

PREDICTOR OPTIONS

 L: LIST THE dR VECTOR
 M: MODIFY THE dR VECTOR
 S: SET ALL dR VALUES
 G: GET THE PREDICTED SYSTEM SOLUTION
 D: DISPLAY PREDICTED SYSTEM SOLUTION
 H: HELP
 X: EXIT PREDICTOR (=DEFAULT)

ENTER OPTION (X):S

ENTER d(R2) (0.0000E-01):20

ENTER d(R5) (0.0000E-01):-20

PREDICTOR OPTIONS (L,M,S,G,D,H,X,<FULL>):G

COMPUTATION COMPLETED.

PREDICTOR OPTIONS (L,M,S,G,D,H,X,<FULL>):D

LINEAR PREDICTION OF SYSTEM SOLUTION...

SYSTEM INPUTS...

SYSTEM OUTPUTS...

E(1) = 1.0000E+01

F(1) = 1.9400E-02

F(6) = 0.0000E-01

E(4) = 1.8400E+00

PREDICTOR OPTIONS (L,M,S,G,D,H,X,<FULL>):X

STATIC SOLVER OPTIONS (L,M,G,D,C,S,P,H,X,<FULL>):X

PROCEED? (Y):

At this point, program control was returned to ENPORT-5 and the sample run was ended.

Chapter 4

SENSITIVITY CALCULATION METHOD

The basis of the adjoint system method for calculating sensitivities is a general network theorem by Tellegen [6]. In bond graph terms, the theorem may be developed as follows.

Consider two bond graph models N and \bar{N} which have the identical junction structure but possibly different types of field elements. The field elements are C, I, R, SE, and SF. Let $(E(k), F(k))$ and $(\bar{E}(k), \bar{F}(k))$ be the (effort, flow) on corresponding external ports (i.e., field ports of the junction structure) of N and \bar{N} . Further, let the corresponding power directions be the same. If n is the number of external ports on each junction structure, then Tellegen's theorem states that

$$\sum E(k) * \bar{F}(k) = 0 \quad \text{and} \quad \sum F(k) * \bar{E}(k) = 0, \text{ for } k = 1 \text{ to } n. \quad (4.1)$$

Now let the efforts and flows in N change by amounts $dE(k)$ and $dF(k)$. Tellegen's theorem must still be satisfied, so that

$$\sum (E(k) + dE(k)) * \bar{F}(k) = 0 \quad \text{and} \quad \sum (F(k) + dF(k)) * \bar{E}(k) = 0 \quad (4.2)$$

which requires

$$\sum dE(k) * \bar{F}(k) = 0 \quad \text{and} \quad \sum dF(k) * \bar{E}(k) = 0. \quad (4.3)$$

Equations (4.3) can be combined and written as

$$\sum (dE(k) * \bar{F}(k) - dF(k) * \bar{E}(k)) = 0. \quad (4.4)$$

Equation (4.4) provides the key to sensitivity calculations. If the

elements of \bar{N} are chosen correctly, each term of (4.4) can be forced to zero except the terms from the output port and the varied parameter port. A sensitivity can be directly calculated from the non-zero terms.

As an example, consider the linear resistive system of Figure 5. The inputs are $E(1) = \text{constant}$, $F(4) = \text{zero}$. Assume the desired output is $E(4)$ and the R-parameter to be varied is $R2$. The Tellegen sum (equation (4.4)) for each external port will be evaluated and the elements of \bar{N} will be determined.

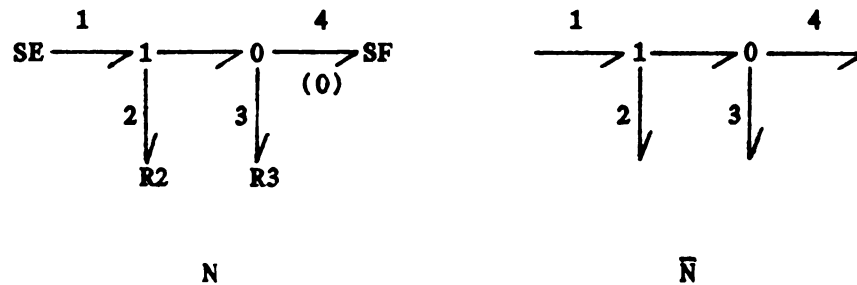


Figure 5. Linear Resistive System

For port 1 ($k = 1$), $dE(1) = 0$ because $E(1) = \text{constant}$. If $\bar{E}(1)$ is set to zero (implying a zero effort source on port 1 of \bar{N}), the Tellegen sum for port 1 becomes

$$(dE(1) \cdot \bar{F}(1) - dF(1) \cdot \bar{E}(1)) = 0.$$

For port 2 ($k = 2$), $dR2 \neq 0$, so $dE(2) = R2 \cdot dF(2) + F(2) \cdot dR2$. If $R2$ is duplicated in \bar{N} , cancellation results and the Tellegen sum for port 2 becomes

$$(dE(2) \cdot \bar{F}(2) - dF(2) \cdot \bar{E}(2)) = F(2) \cdot \bar{F}(2) \cdot dR2.$$

For port 3 ($k = 3$), $dR_3 = 0$, so $dE(3) = R_3 \cdot dF(3)$. If R_3 is duplicated in \bar{N} , cancellation results and the Tellegen sum for port 3 becomes

$$(dE(3) \cdot \bar{F}(3) - dF(3) \cdot \bar{E}(3)) = 0.$$

For port 4 ($k = 4$), $dF(4) = 0$ because $F(4) = \text{constant}$. If $\bar{F}(4)$ is set to 1 (implying a flow source on port 4 of \bar{N}), the Tellegen sum for port 4 becomes

$$(dE(4) \cdot \bar{F}(4) - dF(4) \cdot \bar{E}(4)) = dE(4) \cdot (1).$$

Summing the terms of equation (4.4) for ports 1 through 4 results in

$$0 + F(2) \cdot \bar{F}(2) \cdot dR_2 + 0 + dE(4) = 0.$$

Solving for the sensitivity,

$$dE(4)/dR_2 = -F(2) \cdot \bar{F}(2).$$

Similarly, if R_2 is held constant and R_3 is varied,

$$dE(4)/dR_3 = -F(3) \cdot \bar{F}(3).$$

Thus, for a linear resistive system with constant inputs, the sensitivity of an output to each one-port R-parameter can be calculated after solving for the R-port flows of N and \bar{N} . \bar{N} is called the adjoint system.

In general, to construct the adjoint system for a linear resistive model, the following procedure is used. Note that the original bond graph model must contain a source corresponding to each desired output.

(1) All R-elements in N are duplicated in \bar{N} (including multi-port R-elements) and retain the identical resistance parameters. (2) All independent sources in N are duplicated in \bar{N} . The inputs are set to zero in \bar{N} . (3) If the output under consideration is an effort, then the flow for that port (which is an input) is set to 1 in \bar{N} . (4) If the

output under consideration is a flow, then the effort for that port (which is an input) is set to -1 in N .

Thus, for a linear resistive model with one-port or multi-port resistors and independent effort or flow sources, the adjoint system \bar{N} is nearly identical to the original system N . The only change is a different input vector U . Therefore, only a single reduction of the junction structure is necessary in order to solve both the original and adjoint systems.

For computer solution, the junction structure is reduced and D_i and D_o are computed given U using equations (2.4) and (2.3). The R-port flows are extracted from D_i , D_o . Next, the adjoint input vector \bar{U} corresponding to the output under consideration is substituted and \bar{D}_i and \bar{D}_o are computed. The adjoint flows are extracted and the output sensitivities are calculated.

Chapter 5

SUMMARY

A sensitivity calculation method for network models based on an adjoint network was adapted and applied to bond graph models. This adjoint system method allows calculation of the sensitivities of system outputs to one-port resistive parameters for linear resistive systems with constant inputs. A software module, STATIC, was written to interface with ENPORT-5, a bond graph processor for linear dynamic systems. The STATIC module computes static system solutions, calculates output sensitivities and predicts new solutions due to variations in one or more resistive parameters.

5.1 Conclusion

For linear resistive bond graph models, the adjoint system approach provides an efficient method for computer calculation of sensitivities. Only one junction structure reduction is necessary to solve the original system and the one or more adjoint systems needed to calculate the sensitivities of system outputs to resistive parameters.

5.2 Future Work

Some suggestions for future work are:

- (1) Develop a sensitivity calculation method for C-fields and I-fields. C-field problems have application in static deflection of compliant systems.
- (2) Develop a sensitivity calculation method for linear dynamic systems modeled by bond graphs. Possible considerations are state variable sensitivity, eigenvalue sensitivity, and frequency response sensitivity.
- (3) Make use of sensitivities in optimizing system parameters.
- (4) Develop an efficient sensitivity calculation method for nonlinear systems.

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LIST OF REFERENCES

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APPENDICES

APPENDIX A

STATIC MODULE SUBROUTINES

The following is a list of subroutines in STATIC with a brief description of each.

STCALC calculates the sensitivity of each output to each one-port R-parameter.

STCOMP computes the effort and flow on each external bond.

STDRVR drives the STATIC module.

STINPT lists or modifies/sets the inputs.

STPRED predicts a new solution using the sensitivities and a user defined delta-R vector.

STRDUC reduces the junction structure matrices.

STSENS prints the sensitivities to the terminal screen.

STSGET gets the S_{ij} sub-arrays from the S matrix.

STSOLN prints the system solution to the terminal screen.

The following is a calling tree for the subroutines in STATIC.

```

DRIVER (ENPORT)
  STDRVR
    GOON1
    STRDUC
      CSMPY2
      CSADD2
      INPRD2
      STSGET
    PROMPT1
    GETWD1
    STINPT
      PROMPT1
      GETRL1
      NCHARS3
    STCOMP
      CSMPY2
    STSOLN
      NCHARS3
      PROMPT1
      YORN1
    STCALC
      CSMPY2
    STSENS
      NCHARS3
    STPREO
      PROMPT1
      GETWD1
      NCHARS3
      GETRL1
      CSMPY2
      CSADD2
    RHFILE4
    PROCED1

```

- ¹ Subroutine contained in IOUTIL (ENPORT)
- ² Subroutine contained in CSUTIL (ENPORT)
- ³ Function contained in IOUTIL (ENPORT)
- ⁴ Subroutine contained in UFILER (ENPORT)

APPENDIX B

STATIC MODULE DATA BASE

Many of the variables and arrays used in STATIC subroutines are shared with ENPORT-5 through common files. A list of the shared common files and the variables used from each is given below.

COMMON FILE	VARIABLES USED
SYGBBK	IELLST, NBIMX, IBMX, NPTR, IELNAM, IBNAM, NEL, NBD
CAUSBK	ICMX
CLASBK	NFL, NFS
RDUCBK	S, IPS, LS, T, IPT, LENT, WK, IWK, LENWK, FL, IPFL, LENFL, W2, IW2, LENW2
SOLNBK	MAXU, U
UTILBK	IERRF

In addition to the shared common files, the STATIC module also uses a local common file called STATBK. A listing of each STATIC common file is given in Appendix C.

APPENDIX C

STATIC MODULE SOURCE CODE

The common files and subroutines in this appendix appear in the following sequence:

- | | |
|-----------|------------|
| 1. SYBGBK | 9. STRDUC |
| 2. CAUSBK | 10. STSGET |
| 3. CLASBK | 11. STINPT |
| 4. RDUCBK | 12. STCOMP |
| 5. SOLNBK | 13. STSOLN |
| 6. UTILBK | 14. STCALC |
| 7. STATBK | 15. STSENS |
| 8. STDRVR | 16. STPRED |

The next several pages contain the source code for the STATIC module.


```

CCLASBK*****C
C
C--- CLASBK  SUPPORTS CLASS, DATA FOR BOND TYPE CLASSIFICATION C
C          BY FIELD. C
C C
C--- IBEQ    BOND EQUIVALENT LIST, MAPS INTEGER NAME INTO C
C          WORKING POSITION IN FIELD VECTOR. C
C  IBT      BOND TYPE LIST, DEFINES BOTH FIELD TYPE AND CAUSALITY. C
C          SEE CLASS FOR DETAILS OF FIELD TYPES. C
C  NBEX     NUMBER EXTERNAL (FIELD) BONDS C
C  NBIN     NUMBER INTERNAL (JUNCTION) BONDS C
C  NFI      NUMBER INDEPENDENT STORAGE BONDS (STATE) C
C  NFD      NUMBER DEPENDENT STORAGE BONDS C
C  NFL      NUMBER DISSIPATION (R) BONDS C
C  NFS      NUMBER SOURCE BONDS C
C  NFT      NUMBER TWO-PORT (TF,GY) BONDS C
C  NFJ      NUMBER OF (0,1) BONDS (SAME AS NBIN NOW) C
C
C--- REQUIRES THE PRIOR USE OF SYGBK FOR PARAMETERS C
C
C      COMMON /CLASBK/ IBEQ(MNBD),IBT(MNBD),NBEX,NFI,NFD,NFL,NFS,
C      +              NBIN,NFT,NFJ
C
CENDCLASBK*****C
C
CRDUCBK*****C
C
C--- RDUCBK : COMMON FOR REDUCE AND CSUTIL OPERATIONS C
C
C--- VARIABLES:
C   S      IS THE JUNCTION STRUCTURE ARRAY
C   T      IS USED AS A WORKSPACE
C   WK     IS A WORKSPACE ARRAY
C   FL     IS THE DISSIPATION FIELD MATRIX
C   FS     IS THE STORAGE FIELD MATRIX
C   TP     IS THE TF,GY MODULUS FIELD MATRIX
C   W2     IS A WORKSPACE ARRAY
C   A      IS THE SYSTEM 'A' MATRIX
C   B      IS THE SYSTEM 'B' MATRIX
C   E      IS THE SYSTEM 'E' MATRIX (DEPENDENT C,I)
C   LS     IS THE JS MATRIX BREAK POINT ARRAY
C
C--- NOTE. SPARSE ARRAY STORAGE: S(I) CONTAINS THE SDATA,
C          IPS(I) GIVES THE K POSITION (RUNNING ROW INDEX),
C          AND LENS IS TOTAL NUMBER OF NONZERO ITEMS IN S.
C          OTHER SPARSE ARRAYS ARE SIMILAR.
C

```

C--- PARAMETER DECLARATIONS:

C

```

PARAMETER (MAXS=400)
PARAMETER (MAXT=MAXS)
PARAMETER (MAXWK=2*MAXS/3)
PARAMETER (MAXFL=100)
PARAMETER (MAXFS=100)
PARAMETER (MAXTP=100)
PARAMETER (MAXW2=MAXWK)
PARAMETER (MAXA=250)
PARAMETER (MAXB=100)
PARAMETER (MAXE=100)
PARAMETER (MAXC=100)
PARAMETER (MAXD=50)

```

C

C--- COMMON DECLARATIONS:

C

```

COMMON /BK8/ S(MAXS),IPS(MAXS),LENS,LS(16),
+           T(MAXT),IPT(MAXT),LENT,
+           WK(MAXWK),IWK(MAXWK),LENWK
COMMON /BK9/ FL(MAXFL),IPFL(MAXFL),LENFL,
+           FS(MAXFS),IPFS(MAXFS),LENFS,
+           TP(MAXTP),IPTP(MAXTP),LENTP,
+           W2(MAXW2),IW2(MAXW2),LENW2
COMMON /BK10/ A(MAXA),IPA(MAXA),LENA,
+            B(MAXB),IPB(MAXB),LENB,
+            E(MAXE),IPE(MAXE),LENE

```

C

CENDRUCBK*****C

C

CSOLNBK*****C

C

C--- SOLNBK SUPPORTS SOLUTION PHASE WITH CONTROL DATA

C

C--- VARIABLES:

```

C      AMX      IS THE A MATRIX IN FULL STORAGE MODE
C      BMX      IS THE B MATRIX IN FSM
C      NX       IS THE NUMBER OF STATE VBLS
C      NU       IS THE NUMBER OF INPUTS
C      XIN      IS THE INITIAL CONDITION VECTOR
C      X        IS THE STATE VECTOR AT TIME T
C      U        IS THE INPUT VECTOR AT TIME T
C      DX       IS THE X-DOT VECTOR AT TIME T
C      TIN      IS THE INITIAL TIME
C      TFIN     IS THE FINAL TIME
C      NSAV     IS THE NUMBER OF STAGES TO STORE RESULTS (TOTAL)
C      DTSTR    IS THE DT STORAGE INTERVAL
C      RES      IS THE RESULTS ARRAY
C      XSAVL    IS LOGICAL SAVE LIST FOR X VARIABLES
C      USAVL    IS LOGICAL SAVE LIST FOR U VBLS
C      DSAVL    IS LOGICAL SAVE LIST FOR DX/DT VBLS
C      NREQ     IS NUMBER OF REQUESTS TO BE SAVED
C

```

```

PARAMETER (MAXX=15)
PARAMETER (MAXU=10)
PARAMETER (MAXXUD=15)
PARAMETER (MAXRES=501)

C
LOGICAL XSAVL(MAXX),USAVL(MAXU),DSAVL(MAXX)
INTEGER NREQ

C
COMMON /ABMXBK/ AMX(MAXX,MAXX),BMX(MAXX,MAXU)
COMMON /XVBLBK/ NX,XIN(MAXX),X(MAXX),DX(MAXX)
COMMON /UVBLBK/ NU,U(MAXU)
COMMON /TCTLBK/ TIN,TFIN,NSAV,DTSTR
COMMON /RSLTBK/ RES(MAXRES,MAXXUD)
COMMON /SAVEBK/XSAVL,USAVL,DSAVL,NREQ

C
CENDSOLNBK*****C
C
CUTILBK*****C
C
C--- UTILBK  GENERAL SUPPORT FUNCTIONS
C
C--- VARIABLES:
C      IERRF  ERROR RETURN VALUE
C      ABNEW  .TRUE. IF A,B ARE NEW TO SOLVIT
C      DUMPFG  SYSTEM LEVEL FLAG FOR DUMPING COMMON
C      ITERM  SPECIFIES KIND OF TERMINAL THE USER HAS
C      DYNFLG  IF TRUE WE HAVE A DYNAMIC SYSTEM
C      STTFLG  IF TRUE WE HAVE A STATIC SYSTEM
C
LOGICAL ABNEW,DUMPFG,DYNFLG,STTFLG
C
COMMON /UTILBK/IERRF,ABNEW,DUMPFG,ITERM,DYNFLG,STTFL
C
CENDUTILBK*****C
C

```

```

CSTATBK*****C
C
C--- STATBK - LOCAL COMMON FOR THE ENPORT STATIC MODULE
C
C--- THIS COMMON REQUIRES THE PRIOR USE OF $INSERT SOLNBK.
C
C--- VARIABLES
C
C    MLTPRT - TRUE IF MULTI-PORT R IS PRESENT
C    POWRIN - TRUE FOR POWER INTO SYSTEM (MAXU*1)
C
C    MAXR   - MAXIMUM R-PORTS ALLOWED
C    MAXU   - MAXIMUM SOURCES ALLOWED (FROM SOLNBK)
C    INLST  - LIST OF NODES OF ONE-PORT R'S
C    IRLST  - LIST OF BONDS ON R'S W/CAUSALITY
C    ISLST  - LIST OF BONDS ON SOURCES W/CAUSALITY
C    IPDU   - POINTER FOR DI,DO,U,V VECTORS
C
C    DI     - R-FIELD INPUT VECTOR (Di)
C    DO     - R-FIELD OUTPUT VECTOR (Do)
C    EFRT   - EFFORT VECTOR (SORTED FROM Di AND Do)
C    FLOW   - FLOW VECTOR (SORTED FROM Di AND Do)
C    S4     - STORAGE FOR S44 MATRIX
C    SN     - SENSITIVITY ARRAY d(Vi)/d(Rj)
C    DR     - DELTA-R VECTOR
C    U      - SYSTEM INPUT VECTOR (FROM SOLNBK)
C    V      - SYSTEM OUTPUT VECTOR
C
C    NOTE:  MAXR MUST BE GREATER THAN MAXU.
C
C    PARAMETER (MAXR=25)
C    PARAMETER (MAXRU=MAXR*MAXU)
C    PARAMETER (MAXUU=MAXU*MAXU)
C
C    LOGICAL MLTPRT,POWRIN(MAXU)
C
C    COMMON /STATB1/ MLTPRT,POWRIN
C    COMMON /STATB2/ INLST(MAXR),IRLST(MAXR),ISLST(MAXU)
C    COMMON /STATB3/ DI(MAXR),DO(MAXR),EFRT(MAXR),FLOW(MAXR),
+                   DR(MAXR),IPDU(MAXR),V(MAXU)
C    COMMON /STATB4/ S4(MAXUU),IPS4(MAXUU),LENS4,
+                   SN(MAXRU),IPSN(MAXRU),LENSN
C
CENDSTATBK*****C

```

```
C      ENPORT STATIC MODULE
C
CSTDRVR >>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>><C
C
C      SUBROUTINE STDRVR(PROCFG)
C
C--- PROGRAMMER: D.R.REED (SPRING 1984)
C
C--- STDRVR DRIVES ENPORT'S STATIC MODULE.
C
C--- DECLARATIONS
C
$INSERT SYGBK
$INSERT CLASBK
$INSERT SOLNBK
$INSERT UTILBK
$INSERT STATBK
C
C      LOGICAL PROCFG,FULL,NEWLIN,ENDLIN,SENSIT,
+          SETFLG,SOLFLG,SENFLG
C      CHARACTER*1 ANS
C      CHARACTER*32 FNAME
C      CHARACTER*70 STRING
C
C***STDRVR*****C
C
C--- CHECK NUMBER OF R'S AND U'S
C      IF (NFL.GT.MAXR) THEN
C          ANS='R'
C          WRITE(*,9000)ANS,MAXR,ANS
C          CALL GOON
C          PROCFG=.FALSE.
C          RETURN
C      ENDIF
9000 FORMAT(/' *** TOO MANY',A1,'''S, MAXIMUM IS ',I3,
+         ' NO FURTHER ACTION POSSIBLE.',
+         /' *** WE SUGGEST INCREASING MAX',A1,',')
C      IF (NFS.GT.MAXU) THEN
C          ANS='U'
C          WRITE(*,9000)ANS,MAXU,ANS
C          CALL GOON
C          PROCFG=.FALSE.
C          RETURN
C      ENDIF
C
C--- INITIALIZE
C      DO 10 I=1,MAXU
10    U(I)=0.0
C      DO 20 I=1,MAXR
20    DR(I)=0.0
C      SOLFLG=.FALSE.
C      SENFLG=.FALSE.
C      IERRF=0
C      CALL STRDUC(SENSIT)
```

```

      IF (IERRF.NE.0) THEN
        WRITE(*,9001) IERRF
9001   FORMAT(/' *** ERROR NUMBER ',I6,' FOUND.',
+         /5X,'NO FURTHER PROCESSING POSSIBLE.')
        CALL GOON
        PROCFG=.FALSE.
        RETURN
      ENDIF

C
C--- PRINT STATIC SOLVER OPTIONS
      FULL=.TRUE.
100   CONTINUE
      IF (FULL) THEN
        WRITE(*,1000)
1000  FORMAT(/'  STATIC SOLVER OPTIONS'
+         /'  -----'
+         /'  L: LIST INPUT VALUES'
+         /'  M: MODIFY/SET INPUT VALUES'
+         /'  G: GET THE SYSTEM SOLUTION'
+         /'  D: DISPLAY SYSTEM SOLUTION'
+         /'  C: CALCULATE SENSITIVITIES'
+         /'  S: SHOW THE SENSITIVITIES'
+         /'  P: PREDICT NEW SYSTEM SOLUTION'
+         /'  H: HELP'
+         /'  X: EXIT STATIC SOLVER (=DEFAULT)'
+         /'  -----')
        STRING='  ENTER OPTION (X):'
      ELSE
        WRITE(*,'(1X)')
        STRING='  STATIC SOLVER OPTIONS (L,M,G,D,C,S,P,H,X,<FULL>):'
      ENDIF

C
C--- REQUEST AND GET SELECTED OPTION
      CALL PROMPT(STRING)
      NEWLIN=.TRUE.
      ANS='#'
      CALL GETWD(ANS,NEWLIN,ENDLIN)

C
C--- PROCESS SELECTED OPTION
      IF (ANS.EQ. '#') THEN
        IF (FULL) THEN
          ANS='X'
        ELSE
          FULL=.TRUE.
          GO TO 100
        ENDIF
      ENDIF

C
      IF (ANS.EQ. 'L') THEN
        SETFLG=.FALSE.
        CALL STINPT(SETFLG)
      ELSEIF (ANS.EQ. 'M') THEN
        SETFLG=.TRUE.
        CALL STINPT(SETFLG)

```

```

ELSEIF (ANS.EQ.'G') THEN
  IERRF=0
  CALL STCOMP(SOLFLG)
  IF (IERRF.NE.0) THEN
    WRITE(*,9001) IERRF
  ENDIF
ELSEIF (ANS.EQ.'D') THEN
  IF (SOLFLG) THEN
    CALL STSOLN
  ELSE
    WRITE(*,9010)
9010    FORMAT('/' YOU MUST GET THE SYSTEM SOLUTION',
+          '/' BEFORE DISPLAYING IT.')
  ENDIF
ELSEIF (ANS.EQ.'C') THEN
  IF (SENSIT) THEN
    IF (SOLFLG) THEN
      IERRF=0
      CALL STCALC(SENFLG)
      IF (IERRF.NE.0) THEN
        WRITE(*,9001)IERRF
      ENDIF
    ELSE
      WRITE(*,9020)
9020    FORMAT('/' YOU MUST GET THE SYSTEM SOLUTION',
+          '/' BEFORE CALULATING SENSITIVIES.')
    ENDIF
  ELSE
    WRITE(*,9015)
9015    FORMAT('/' SENSITIVITIES ARE NOT AVAILABLE',
+          '/' DUE TO BOND ACTIVATION.')
  ENDIF
ELSEIF (ANS.EQ.'S') THEN
  IF (SENFLG) THEN
    CALL STSENS
  ELSE
    WRITE(*,9030)
9030    FORMAT('/' YOU MUST CALCULATE THE SENSITIVITIES',
+          '/' BEFORE SHOWING THEM.')
  ENDIF
ELSEIF (ANS.EQ.'P') THEN
  IF (SENFLG) THEN
    CALL STPRED
  ELSE
    WRITE(*,9040)
9040    FORMAT('/' YOU MUST CALCULATE THE SENSITIVITIES',
+          '/' BEFORE PREDICTING A NEW SOLUTION.')
  ENDIF
ELSEIF (ANS.EQ.'H') THEN
  FNAME='PUBLIC>E5.2>HELP.STATIC'
  CALL RHFILE(FNAME)
ELSEIF (ANS.EQ.'X') THEN
  CALL PROCED(PROCFG)
  RETURN

```



```

                IF ((ICMX(J1).EQ.6).OR.(ICMX(J1).EQ.5) THEN
                    IRLST(NR)= -IRLST(NR)
                ENDIF
                NR=NR+1
20          CONTINUE
                ELSEIF ((IELLST(I).EQ.4).OR.(IELLST(I).EQ.5)) THEN
C---- SOURCE ELEMENT
                    J=NPTR(I)
                    K=NBIMX(J)
                    IF (IBMX(K,1).EQ.I) THEN
                        POWRIN(NS)=.TRUE.
                    ELSE
                        POWRIN(NS)=.FALSE.
                    ENDIF
                    IF (IELLST(I).EQ.4) K=-K
                    ISLST(NS)= K
                    NS=NS+1
                ENDIF
30          CONTINUE
C
C---- CHECK FOR ACTIVATED BONDS
                SENSIT=.TRUE.
                DO 40 I=1,2*NBD
                    IF ((ICMX(I).EQ.2).OR.(ICMX(I).EQ.5)) THEN
                        SENSIT=.FALSE.
                    ENDIF
40          CONTINUE
C
C---- REDUCE THE JUNCTION STRUCTURE EQUATIONS
C
C---- SET UP AND COMPUTE {(INV(I-S33*L))*S34}
C
C---- PUT IDENTITY MATRIX (NFLxNFL) INTO T/IPT/LENT
                DO 50 NR=1,NFL
                    T(NR)=1.0
50          IPT(NR)=(NR-1)*NFL+NR
                LENT=NFL
C
C---- MULTIPLY S33*L AND PUT -(S33*L) INTO W2/IW2/LENW2
                CALL CSMPY(NFL,NFL,LS(11),IPS,S,
                    +      NFL,LENFL,IPFL,FL)
                IF (IERRF.NE.0) RETURN
                DO 60 I=1,LENWK
                    W2(I)=-WK(I)
60          IW2(I)=IWK(I)
                LENW2=LENWK
C
C---- COMPUTE (I-S33*L) AND PUT INTO W2/IW2/LENW2
                CALL CSADD(LENT,IPT,T,LENW2,IW2,W2)
                IF (IERRF.NE.0) RETURN
                DO 70 I=1,LENWK
                    W2(I)=WK(I)
70          IW2(I)=IWK(I)
                LENW2=LENWK

```



```

        DI(NR)=0.0
        DO(NR)=0.0
        EFRT(NR)=0.0
        FLOW(NR)=0.0
10     IPDU(NR)=NR
C
C--- COMPUTE Di = INV(I-S33*L)*S34*U
        J=1
        CALL CSMPY(NFL,NFS,LENT,IPT,T,
+               J,NFS,IPDU,U)
        IF (IERRF.NE.0) RETURN
        DO 20 I=1,LENWK
20     DI(IWK(I))=WK(I)
C
C--- COMPUTE Do=L*Di
        CALL CSMPY(NFL,NFL,LENFL,IPFL,FL,
+               J,NFL,IPDU,DI)
        IF (IERRF.NE.0) RETURN
        DO 30 I=1,LENWK
30     DO(IWK(I))=WK(I)
C
C--- COMPUTE S43*Do AND PUT INTO EFRT (TEMPORARILY)
        CALL CSMPY(NFS,NFL,LENW2,IW2,W2,
+               J,NFL,IPDU,DO)
        IF (IERRF.NE.0) RETURN
        DO 40 I=1,LENWK
40     EFRT(IWK(I))=WK(I)
C
C--- COMPUTE S44*U AND PUT INTO FLOW (TEMPORARILY)
        CALL CSMPY(NFS,NFS,LENS4,IPS4,S4,
+               J,NFS,IPDU,U)
        IF (IERRF.NE.0) RETURN
        DO 50 I=1,LENWK
50     FLOW(IWK(I))=WK(I)
C
C--- COMPUTE V=S43*Do+S44*U
        DO 60 NS=1,NFS
60     V(NS)=EFRT(NS)+FLOW(NS)
C
C--- SORT Di AND Do VECTORS INTO EFRT AND FLOW VECTORS
C
        DO 70 NR=1,NFL
        IF (IRLST(NR).GT.0) THEN
            EFRT(NR)=DI(NR)
            FLOW(NR)=DO(NR)
        ELSE
            EFRT(NR)=DO(NR)
            FLOW(NR)=DI(NR)
        ENDIF
70     CONTINUE
C
C--- NORMAL RETURN
        SOLFLG=.TRUE.
        WRITE(*,1000)

```



```

        ELSE
            UADJ(NS)= 1.0
        ENDIF
    ELSE
C---- EFFORT SOURCE
        IF (POWRIN(NS)) THEN
            UADJ(NS)= 1.0
        ELSE
            UADJ(NS)=-1.0
        ENDIF
    ENDIF

C
C---- ZERO Di AND Do
        DO 20 NR=1,MAXR
            DI(NR)=0.0
20      DO(NR)=0.0
C
C---- COMPUTE Di = INV(I-S33*L)*S34*UADJ
        J=1
        CALL CSMPY(NFL,NFS,LENT,IPT,T,
+              J,NFS,IPDU,UADJ)
        IF (IERRF.NE.0) RETURN
        DO 30 I=1,LENWK
30      DI(IWK(I))=WK(I)
C
C---- COMPUTE Do=L*Di
        CALL CSMPY(NFL,NFL,LENFL,IPFL,FL,
+              J,NFL,IPDU,DI)
        IF (IERRF.NE.0) RETURN
        DO 40 I=1,LENWK
40      DO(IWK(I))=WK(I)
C
C---- SORT DI AND DO, RETAIN ADJOINT FLOW ONLY
        DO 50 NR=1,NFL
            IF (IRLST(NR).GT.0) THEN
                FADJ=DO(NR)
            ELSE
                FADJ=DI(NR)
            ENDIF
C
C---- STORE SENSITIVITIES
        SN((NS-1)*NFL+NR)=-1.0*FLOW(NR)*FADJ
        IPSN((NS-1)*NFL+NR)=(NS-1)*NFL+NR
50      CONTINUE
C
C---- RESET ADJOINT INPUT VECTOR
        UADJ(NS)=0.0
100     CONTINUE
        LENS=NFS*NFL
C
C---- NORMAL RETURN
        SENFLG=.TRUE.
        WRITE(*,1000)
1000    FORMAT('/' CALCULATION COMPLETED.')
```



```
CSTPRED >>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>><<<<<<<<<<<<<<<<<<<<<<<<<<<<C
C                                     C
C      SUBROUTINE STPRED                                     C
C                                     C
C--- PROGRAMMER:   D.R.REED (SPRING 1984)                   C
C                                     C
C--- STPRED PREDICTS STATIC SYSTEM SOLUTIONS USING THE CALCULATED C
C      SENSITIVITIES AND A USER SUPPLIED DELTA-R VECTOR.    C
C                                     C
C--- DECLARATIONS                                          C
C                                     C
$INSERT SYBGBK
$INSERT CLASBK
$INSERT RDUCKB
$INSERT SOLNBK
$INSERT UTILBK
$INSERT STATBK
C                                     C
      LOGICAL FULL,NEWLIN,ENDLIN,PREFLG
      CHARACTER*1 ANS,IType,OType
      CHARACTER*6 INODE
      CHARACTER*8 IBOND
      CHARACTER*70 STRING
      REAL DV(MAXU)
C                                     C
C***STPRED*****C
C                                     C
C--- INITIALIZE
      FULL=.TRUE.
      RLO=-1.0E+10
      RHI= 1.0E+10
      NEWLIN=.TRUE.
      DO 1 NS=1,MAXU
1       DV(NS)=0.0
      PREFLG=.FALSE.
C--- BE SURE THERE ARE ONE-PORT R ELEMENTS TO VARY
      DO 10 NR=1,NFL
10      IF (INLST(NR).NE.0) GO TO 100
C--- OOPS, NO ONE-PORT R'S TO VARY, RETURN TO SIDVR
      WRITE(*,9000)
9000    FORMAT('/' NO ONE-PORT R PARAMETERS TO VARY.')
      IF (MLTPRT) WRITE(*,9010)
9010    FORMAT(' VARYING OF MULTIPORT R''S IS NOT AVAILABLE.')
      RETURN
C
C--- PRINT PREDICTOR OPTIONS
100     CONTINUE
        IF (FULL) THEN
          WRITE(*,1000)
1000    FORMAT('/' PREDICTOR OPTIONS'
+           /' -----'
+           /' L: LIST THE dR VECTOR'
+           /' M: MODIFY THE dR VECTOR'
+           /' S: SET ALL dR VALUES'
```

```

+          /'  G: GET THE PREDICTED SYSTEM SOLUTION'
+          /'  D: DISPLAY PREDICTED SYSTEM SOLUTION'
+          /'  H: HELP'
+          /'  X: EXIT PREDICTOR (=DEFAULT)'
+          /'  -----')
      STRING='  ENTER OPTION (X):'
      ELSE
        WRITE(*,'(1X)')
        STRING=' PREDICTOR OPTIONS (L,M,S,G,D,H,X,<FULL>):'
      ENDIF

C
C--- REQUEST AND GET SELECTED OPTION
      CALL PROMPT(STRING)
      NEWLIN=.TRUE.
      ANS=' '
      CALL GETWD(ANS,NEWLIN,ENDLIN)

C
C--- PROCESS SELECTED OPTION
      IF (ANS.EQ.' ') THEN
        IF (FULL) THEN
          ANS='X'
        ELSE
          FULL=.TRUE.
          GO TO 100
        ENDIF
      ENDIF

C
      IF (ANS.EQ.'L') THEN
        WRITE(*,1010)
1010    FORMAT(/'      THE dR VECTOR...'/)
        O 110 NR=,NFL
          IF (INLST(NR).EQ.0) GO TO 110
          INODE=IELNAM(INLST(NR))
          WRITE(*,1020)INODE(1:NCHARS(INODE)),DR(NR)
1020    FORMAT(' d(',A,') = ',1PE11.4)
110    CONTINUE

C
      ELSEIF (ANS.EQ.'M') THEN
C--- GET R NODE NAME
120    INODE='QUIT'
        WRITE(*,'(1X)')
        STRING=' ENTER R NODE NAME (<RETURN> TO QUIT):'
        CALL PROMPT(STRING)
        CALL GETWD(INODE,NEWLIN,ENDLIN)
C--- PROCESS NODE NAME
        IF (INODE.NE.'QUIT') THEN
          DO 130 NR=1,NFL
            IF (INLST(NR).EQ.0) GO TO 130
            IF (INODE.EQ.IELNAM(INLST(NR))) GO TO 140
130    CONTINUE
          WRITE(*,9020)
9020    FORMAT(/' *** BAD NODE NAME - TRY AGAIN')
          GO TO 120
C--- GOOD NODE NAME, NOW GET dR

```

```

140      RVAL=DR(NR)
      WRITE(STRING,1030)INODE(1:NCHARS(INODE)),RVAL
1030     FORMAT(' ENTER d(' ,A,') (' ,1PE11.4,') :')
      CALL PROMPT(STRING)
      CALL GETRL(RVAL,RLO,RHI,NEWLIN,ENDLIN)
      DR(NR)=RVAL
      GO TO 120
    ENDIF
  C
    ELSEIF (ANS.EQ.'S') THEN
      WRITE(*,'(1X)')
      DO 150 NR=1,NFL
        IF (INLST(NR).NE.0) THEN
          INODE=IELNAM(INLST(NR))
          RVAL=DR(NR)
          WRITE(STRING,1030)INODE(1:NCHARS(INODE)),RVAL
          CALL PROMPT(STRING)
          CALL GETRL(RVAL,RLO,RHI,NEWLIN,ENDLIN)
          DR(NR)=RVAL
        ENDIF
150      CONTINUE
    C
      ELSEIF (ANS.EQ.'G') THEN
C--- GET PREDICTION
      DO 160 NS=1,MAXU
160      DV(NS)=0.0
      J=1
      IERRF=0
      CALL CSMPY(NFS,NFL,LENSN,IPSN,SN,
+           J,NFL,IPDU,DR)
      IF (IERRF.NE.0) THEN
        WRITE(*,9030) IERRF
1030      FORMAT('/ *** ERROR NUMBER ',I6,' FOUND.',
+           ' NO FURTHER ACTION POSSIBLE.')
      RETURN
    ENDIF
      DO 170 I=1,LENWK
170      DV(IWK(I))=WK(I)
      CALL CSADD(NFS,IPDU,DV,NFS,IPDU,V)
      IF (IERRF.NE.0) THEN
        WRITE(*,9030) IERRF
      RETURN
    ENDIF
      DO 180 I=1,LENWK
180      DV(IWK(I))=WK(I)
      PREFLG=.TRUE.
      WRITE(*,1050)
1050     FORMAT('/ COMPUTATION COMPLETED.')
    C
      ELSEIF (ANS.EQ.'D') THEN
C--- DISPLAY PREDICTION
      IF (PREFLG) THEN
        WRITE(*,1060)
1060      FORMAT('/6X,' LINEAR PREDICTION OF SYSTEM SOLUTION...'/

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+      /,4X,'SYSTEM INPUTS...',T28,4X,'SYSTEM OUTPUTS...')
DO 190 NS=1,NFS
  IBOND=IBNAM(ABS(ISLST(NS)))
  IF (ISLST(NS).GT.0) THEN
    ITYPE='F'
    OTYPE='E'
  ELSE
    ITYPE='E'
    OTYPE='F'
  ENDIF
  WRITE(*,1070)ITYPE,IBOND(1:NCHARS(IBOND)),U(NS),
+      OTYPE,IBOND(1:NCHARS(IBOND)),DV(NS)
1070  FORMAT(1X,A1,'(',A,') = ',1PE11.4,
+      T28,1X,A1,'(',A,') = ',1PE11.4)
190  CONTINUE
  ELSE
    WRITE(*,9040)
9040  FORMAT(/' YOU MUST GET THE PREDICTION',
+      /' BEFORE DISPLAYING IT.')
  ENDIF
C
  ELSEIF (ANS.EQ.'H') THEN
    WRITE(*,1080)
1080  FORMAT(/' THE dR VECTOR CONTAINS dR FOR EACH ONE-PORT R.',
+      /' EACH ENTRY IN THE dR VECTOR EQUALS THE CHANGE',
+      /' IN R FOR THE ASSOCIATED ONE-PORT R ELEMENT.')
C
  ELSEIF (ANS.EQ.'X') THEN
    RETURN
  ELSE
    WRITE(*,*)' *** THIS IS NOT A VALID OPTION.'
  ENDIF
  FULL=.FALSE.
  GO TO 100
END
C
CENDSTPRED
C
CENDSTATIC
C

```