

A TECHNIQUE FOR THE SPECIFICATION  
OF VARIABLES RELATING TO  
ELECTRIC POWER NETWORKS

Thesis for the Degree of Ph. D.  
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Maurice Wolla

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L. W. Van Tassle

Major professor

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Maurice Wolla

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## ABSTRACT

### A TECHNIQUE FOR THE SPECIFICATION OF VARIABLES RELATING TO ELECTRIC POWER NETWORKS

by Maurice Wolla

To effectively plan the current operation as well as the future expansion of electric power systems requires a knowledge of the operating characteristics of the existing and/or proposed systems. Analysis of a class of power system studies utilized in determining the electrical characteristics of a power system indicates that these studies are essentially problems in the analysis of electric networks. These studies differ from problems in "conventional" network analysis primarily in two aspects: (1) the size and complexity of the network under consideration, and (2) the type of initial problem specifications. The availability of digital computers has alleviated, but not eliminated, difficulties associated with the size of the network. Problems associated with the initial specification of variables are more fundamental in nature and must be considered within the framework of the network equations since it is mandatory that inconsistencies be avoided. It is logical that a re-examination of the variable specification aspect of these network studies should originate at the level of the correlating graph and associated primary system of equations since they constitute the foundation for electric network theory.

The  $\omega$ -domain graph correlates of the networks under consideration are comprised of two general types of elements: relation elements (F-elements) and no-relation elements (N-elements); the latter type is characterized by a lack of any fixed interrelation between the associated V and I variables and furthermore neither of these variables is specified initially. The resulting primary system of equations is homogeneous in form and certainly consistent. Properties of subgraphs of F-elements are subsequently utilized to define classifications of the N-elements such that either, neither, or both of their associated variables can be assigned arbitrary values with no danger of introducing inconsistencies. The investigation clearly indicates that a multiplicity of N-element classification patterns exist for a given graph and provides the basis for new and more general approaches to the analysis of electric networks-- particularly those problems in which it is desired to maintain prescribed operating conditions.

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## Chapter 1

### INTRODUCTION

#### 1. 1. Background

Planning the current operation and future expansion of a modern-day electric power system is a complex task and one of ever-increasing importance. These systems have grown from small, independent, local units at the turn of the century to the vast, interconnected "pools" of today - with still larger interconnections proposed for the future<sup>1-4</sup>. It soon became apparent that the ability to operate the small utilities successfully based primarily upon past experience was not adequate to cope with the problems associated with these rapidly expanding systems. Advances in analysis and control techniques coupled with the availability of digital and analog computers have provided the system planners of today with the opportunity to study and plan the operation of these large-scale power systems. Considerable effort has been directed toward the complete automation of system planning and operation<sup>5-9</sup>.

The components of an electric power system can be divided into three general categories: (1) the generating

stations, (2) the transmission and distribution network, and (3) the loads. The basic operating problem is to schedule the generating stations so as to supply the total load demand, plus losses within the transmission and distribution network, in a manner consistent with dependable and economical performance of the power system. The planning phase is necessary to insure that the power system has adequate generating capacity and transmitting capability to meet the constantly growing load demands.

The effective planning of the current operation and future expansion of a power system requires a knowledge of the performance characteristics of the existing and/or proposed systems. The very nature of a power system precludes any possibility of "laboratory testing" the actual system as is commonly done with many types of physical systems. Thus the system planners must devise an adequate model for the system and subsequently determine the performance characteristics of this model. The validity of the models used in such system studies is tested by correlating the performance characteristics determined from the model with those obtained from observations made on the actual system.

The investigations of this paper relate to those phases of power system studies which are primarily concerned with

the steady-state electrical characteristics of the power system. These studies utilize a single-phase network representation of the power system and in general they require a complete steady-state solution for the network, i. e. voltages, currents, real and reactive powers, power factor, etc. at various points within the network. Thus, these studies are essentially problems in network analysis. However they differ from the "conventional" problems in network analysis in a number of respects. The network to be analyzed is considerably larger and more complex than one might encounter in other areas. In addition, it has generally been the case in the past that the entire network must be considered as a unit for the purposes of analysis. In contrast many communication and control systems are often analyzed on a "piece-meal" basis since signals are channeled along desired paths by the use of uni-lateral devices and/or filtering. Thus as the size of a power system increases due to expansion and inter-connection the additional complexity itself presents a formidable problem and it magnifies the need for a better understanding of the fundamental concepts involved in the analysis of the associated network. Perhaps the most significant difference in this type of study is related to the manner in which the initial problem specifications are given.

In power system studies of the type under consideration the specifications are stated in terms of real and reactive powers and voltage magnitudes, whereas the foundations of network theory have been developed with voltages and currents as fundamental or primary variables<sup>10-11</sup>. Quantities such as real and reactive power are consequently considered as derived or secondary variables since they are defined in terms of the primary variables. Thus for any particular network element the inter-relation (complex number form) between the voltage  $V$ , current  $I$ , real power  $P$ , and reactive power  $Q$ , is given by the following relation:

$$P + j Q = VI^* \quad (1.1.1)$$

or

$$P = \text{Re} \{VI^*\} \quad (1.1.2)$$

$$Q = \text{Im} \{VI^*\} \quad (1.1.3)$$

Here one notes that on the one hand if  $V$ ,  $I$  are known, then  $P$  and  $Q$  are determined; on the other hand, however, if  $P$ ,  $Q$  are known, then neither  $V$  nor  $I$  is determined. This change in the specification of variables causes considerable difficulty in the attempt to determine a complete network solution. A specific example of this type of problem is considered in a later section.

Originally it was felt that the performance of a power system could be best predicted through the use of a miniaturized

system commonly referred to as a network analyzer. However, in recent years the digital computer has replaced the network analyzer as the primary tool for large-scale power system studies. By its very nature the digital computer is a more versatile and flexible device. Moreover, it is capable of handling not only all of the problems which can be solved on the network analyzer, but an almost endless variety of different problems as well.

## 1.2. Load or Power-Flow Studies

The load or power-flow study exemplifies the general type of problem under consideration in this investigation. A study of this type requires a complete steady-state solution for a single-phase network representation of the power system. The network is made up of generator elements, load elements, and elements corresponding to the interconnecting transmission and distribution network. The general configuration of this type of network is given in Figure 1.2.1 where the details of the transmission and distribution network are not shown. For simplicity it is also assumed that each non-reference node is incident to exactly one generator or load element.

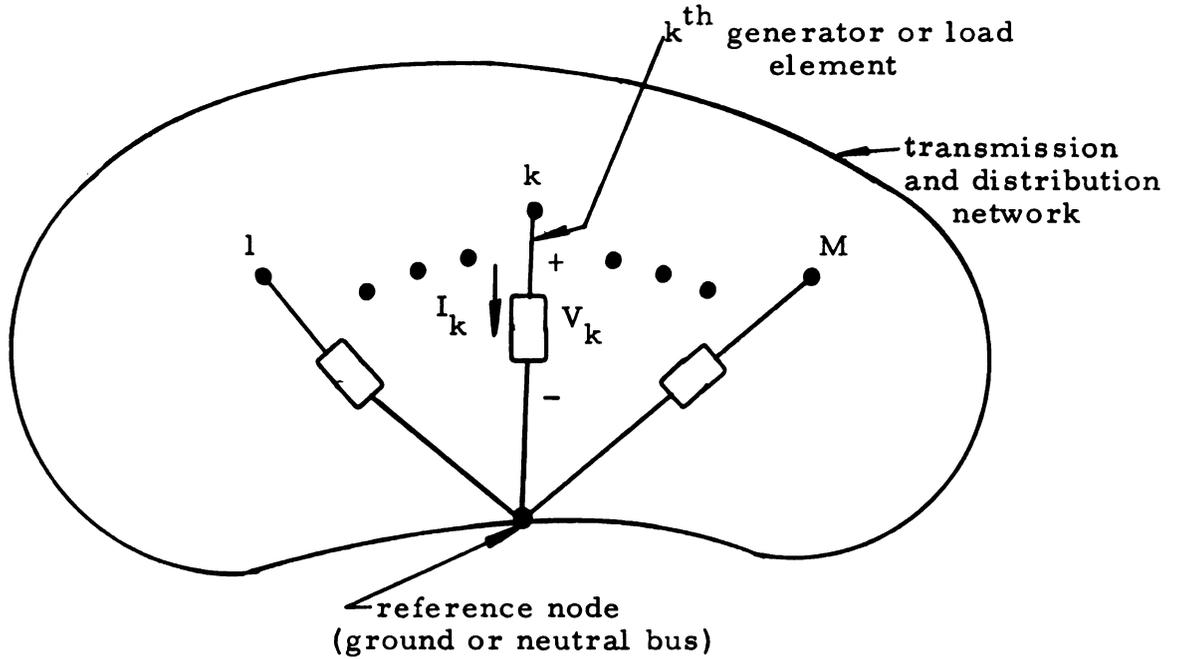


Figure 1.2.1. General Representation of a (M+1)-node Power Network Diagram.

The general nature of a load or power-flow study can be described as follows<sup>2, 12-14</sup>:

1. The complex number form of the node system of equations for the network of Figure 1.2.1

can be written as

$$I_k = - \sum_{n=1}^M Y_{kn} V_n, \quad k=1, 2, \dots, M \quad (1.2.1)$$

where

$$I_k = |I_k| e^{j\theta_k} \quad (1.2.2)$$

$$V_n = |V_n| e^{j\phi_n} \quad (1.2.3)$$

$$Y_{kn} = |Y_{kn}| e^{j\sigma_{kn}} \quad (1.2.4)$$

2. In the usual load study, three types of load and generator specifications are considered:

A. For all load elements the real and reactive power

$$P + jQ = VI^* \quad (1.2.5)$$

is specified.

B. For all generator elements except one, the real power and voltage magnitude

$$P = \text{Re} \{ VI^* \} \quad \text{and} \quad |V| \quad (1.2.6)$$

are specified.

C. For the remaining generator element, i. e. the "slack" generator, the phasor voltage

$$V = |V|e^{j\phi} \quad (1.2.7)$$

is specified.

3. The problem then, is to determine a set of  $V_k$  and  $I_k$ ,  $k=1, 2, \dots, M$ , such that the node system of equations, (1.2.1), is satisfied subject to the specifications, (1.2.5) through (1.2.7), for the appropriate generator and load elements. Once this has been done, then all voltages, currents, real and reactive powers, etc. within the transmission and distribution network can be calculated and the complete solution will have been determined.

Unfortunately the load and generator specifications cannot be used directly to obtain a solution to the node system of equations. Rather some form of iteration is used to determine a solution. One such approach proceeds in the following manner<sup>12</sup>:

1. Initial estimates are made for the  $V_k$ ,
2. The corresponding  $I_k$ 's are found from (1.2.1),
3. The appropriate quantities, (1.2.5) through (1.2.7) are calculated, compared to the specified values, and the errors are determined,
4. Suitable correction relations are used to determine new estimates for the  $V_k$ .

Steps 2 through 4 are repeated until (hopefully) the errors calculated in 3 are less than some prescribed precision index.

Another commonly used technique<sup>2, 13, 14</sup>, is to modify the node equations so as to obtain a system of simultaneous nonlinear equations expressing the real and reactive power for each generator and load element in terms of the generator and load voltages and the node admittance parameters of the transmission system. Since for  $k=1, 2, \dots, M$ :

$$P_k + jQ_k = V_k I_k^* \quad (1.2.8)$$

then, from (1.2.1)

$$P_k + jQ_k = - \sum_{n=1}^M V_k Y_{kn}^* V_n^* \quad (1.2.9)$$

Also, using (1.2.2) through (1.2.4)

$$P_k + jQ_k = - \sum_{n=1}^M |V_k| |Y_{kn}| |V_n| e^{j(\phi_k - \phi_n - \sigma_{kn})} \quad (1.2.10)$$

or

$$\begin{aligned} P_k &= - \sum_{n=1}^M |V_k| |Y_{kn}| |V_n| \cos(\phi_k - \phi_n - \sigma_{kn}) \\ Q_k &= - \sum_{n=1}^M |V_k| |Y_{kn}| |V_n| \sin(\phi_k - \phi_n - \sigma_{kn}) \end{aligned} \quad (1.2.11)$$

The initial problem specifications can now be inserted directly into any one of these last three sets of nonlinear "power equations," (1.2.9), (1.2.10), or (1.2.11). Each generator element and each load element has four associated variables in this final formulation:  $P_k$ ,  $Q_k$ ,  $|V_k|$ ,  $\phi_k$ ; for each element two of these variables are specified and the remaining two must be determined. Once again an iterative technique is used to determine a solution.

In the past the sheer size of the network and the accompanying large number of equations to be solved has been a major obstacle in load studies. However, the introduction of the digital computer, as well as specialized programs<sup>15, 16</sup>, has reduced considerably -- although certainly not eliminated -- this problem. The major difficulties in this type of study are those associated with

the iterative methods employed to determine a solution. The key considerations are those relating to existence and multiplicity of solutions, convergence, rate of convergence, the effect of initial estimates on convergence, etc. In many respects the original problem has been transformed from one in network analysis to one in numerical analysis in order to accommodate the initial problem specifications in the form given. Investigations into the problems associated with load studies, as well as other studies of this general type, have been primarily concerned with improving the iterative techniques used to obtain a solution<sup>12, 13, 17-20</sup>. As a result of these efforts computer programs, which are capable of handling large-scale power systems, are available and in use today<sup>5-8, 21</sup>.

### 1.3. Another Viewpoint

Studies of the type considered in the preceding section play a major role in predicting the current performance and analyzing the future expansion of a power system. Thus it is essential that one be able to obtain an accurate numerical solution for a particular study. Moreover, it would be of considerable benefit to a system planner if the problem formulation and associated solution processes could also be

utilized as a basis for a theoretical study of the system characteristics. Unfortunately the present problem formulation does not readily lend itself to a theoretical study of system characteristics. Rather, the resulting nonlinear equations tend to shift the emphasis to characteristics of the iterative techniques which are used to obtain a numerical solution for a particular study.

A re-examination of the basic structure of a load study, for example, indicates that this study is essentially a problem in the analysis of an electric network and that the major source of difficulty is the form in which the variables for certain elements are specified. In order to avoid nonlinearities at the outset of the problem it is necessary to reconsider the form in which the variables are specified. Since these are essentially problems in network analysis, it would seem natural to return to the basic structure of network theory and to give consideration to choosing a form for the variable specifications which is more compatible with the existing theory. Perhaps the most logical choice to consider would be that of the voltage and current variables for an element. This choice can be given initial support by noting that specifying the voltage and current variables for a network element determines the

real and reactive power variables for that element - see equations (1.1.1) through (1.1.3). Thus this choice would be closely related to the original specifications. Furthermore, an extensive body of network theory already exists, in which voltages and currents are considered as fundamental or primary variables, and elements having either their voltage or current variables specified have been considered within this theory. Therefore, consideration of elements having both voltage and current variables specified would be a logical extension of this theory. Also of importance is the fact that this approach provides an orderly and precise formulation technique and thus is well-suited for use in conjunction with the digital computer.

Within the area of network analysis little consideration has been given to elements having both voltage and current variables specified. Undoubtedly this is due to the unlikelihood of finding a correlating physical device in the laboratory. However some consideration has been given to the possibility of synthesizing "pathological" elements of this type using components such as ideal transformers, ideal gyrators, and negative resistances<sup>22, 23</sup>. Irrespective of whether or not such devices are physically realizable, the fact remains that elements of this type can be useful in theoretical studies.

The investigations of this paper are concerned with extending the class of network elements to include those for which both voltage and current variables are specified and then utilizing these elements in the analysis of electric networks.

#### 1.4. A Variable Specification Problem in Network Analysis

Any investigation into allowable patterns of element variable specifications must be based upon a study of the appropriate systems of network equations since it is imperative that inconsistencies be avoided. The primary system of network equations<sup>10, 16</sup> provides a logical starting point for such a study. This system of equations contains all of the information relative to the element voltage and current variables and ultimately it is the solution of this system of equations which is sought.

Chapter II is devoted to summarizing properties of systems of homogeneous, linear, algebraic equations with constant coefficients. These equations play a fundamental role in this investigation -- in particular those rank properties of the coefficient matrix which define partitions of the variables into dependent and independent sets. Following chapters return to a study of the electric network via the correlating oriented linear graph and

associated systems of network equations. Interrelations between subgraphs and the coefficient matrix in the network equations are exploited to interpret rank properties of the coefficient matrix in terms of interconnection patterns of the linear graph and element parameters. In this manner it is possible to determine conditions on the structure of the linear graph and the element parameters such that the graph may contain elements for which both the voltage and current variables can be arbitrarily specified. In addition one finds that still another type of element is required -- one for which neither the voltage nor the current variable is specified and further, the voltage and current variables are not interrelated in any fixed manner, as is the case for the graph elements correlating with resistors, inductors, and capacitors. Finally, consideration is given to the effect of extending the class of graph elements to include these new elements. A new approach is suggested for the analysis of large-scale electric networks by utilizing these elements in conjunction with zoning techniques.

## Chapter 2

### SYSTEMS OF HOMOGENEOUS, LINEAR, ALGEBRAIC, CONSTANT-COEFFICIENT EQUATIONS

#### 2. 1. Definitions and Fundamental Properties

For reference purposes and to define terminology it is convenient, at this point, to collect certain definitions and fundamental properties of homogeneous, linear, algebraic equations with constant coefficients. The proofs of the basic theorems may be found in most texts on matrix theory or linear algebra<sup>24-28</sup>, and are not repeated here.

In the interest of brevity, and at the same time to be complete, the following abbreviation is used:

Definition 2. 1. 1. Holac Equations.

The abbreviation holac is used to denote homogeneous, linear, algebraic, constant-coefficient.

Consider a system of  $m$  holac equations in  $n$  variables

$$\sum_{j=1}^n a_{ij} x_j = 0, \quad i=1, 2, \dots, m \quad (2. 1. 1)$$

or, in matrix form

$$aX = 0 \quad (2. 1. 2)$$

Definition 2. 1. 2. Rank of a System of Holac Equations

Let the rank of coefficient matrix,  $a$ , in (2. 1. 2) be  $r$ , then  $r$  is said to be the rank of the system (2. 1. 2).

Definition 2. 1. 3. Characteristic of a System of  
Holac Equations

Let the rank of the system (2. 1. 2) be  $r$ , then the ordered triplet of integers,  $\{m, n, r\}$  is said to be the characteristic of the system (2. 1. 2) and is written

$$aX = 0, \{m, n, r, \}$$

Definition 2. 1. 4. Linearly Dependent (Independent)  
Equations

The holac equations,  $aX = 0$ , are said to be linearly dependent (independent) if and only if the rows of the coefficient matrix,  $a$ , are linearly dependent (independent).

Definition 2. 1. 5. Equivalent Systems of Equations

Two systems of equations are said to be equivalent systems of equations if every solution of either system is also a solution of the other.

Consider a system of holac equations with characteristic

$\{m, n, r\}$  i. e.

$$aX = 0, \{m, n, r\} \quad (2. 1. 3)$$

Theorem 2. 1. 1. A necessary and sufficient condition that (2. 1. 3) have non-trivial solutions is that  $r < n$ .

Theorem 2.1.2. The equations of the system (2.1.3) are linearly dependent if and only if  $r < m$ .

Theorem 2.1.3. Every system of holac equations equivalent under elementary row operations to the system (2.1.3) may be represented in the form

$$(C a) X = 0 \quad (2.1.4)$$

where  $C$  is a non-singular matrix of order  $m$ . Conversely, if  $C$  is any non-singular matrix of order  $m$ , then (2.1.4) is equivalent to (2.1.3) under elementary row operations.

Theorem 2.1.4. Any subset of  $r$  linearly independent equations from (2.1.3) forms an equivalent system of equations.

It should be noted that the characteristic of a system of holac equations is, in essence, a description of the coefficient matrix, i. e.,  $A$  is of order  $m \times n$  and has rank  $r$ . Thus the previously stated properties of a system of holac equations are in fact properties of the coefficient matrix-- the variables in the system play a rather minor role. In general the variables have little, if any, significance with regard to the mathematical properties of a system of equations; they serve as little more than "labels" associated with the columns of the coefficient matrix.

## 2.2. The Complete Solution for a System of Holac Equations

Theorem 2.1.1 states a necessary and sufficient condition on the coefficient matrix such that (2.1.3) possesses non-trivial solutions. Although the theorem itself gives no indication of what these solutions might be, the proofs of this theorem generally exhibit a complete solution of (2.1.3). It is a well-known property of a system of holac equations with characteristic  $\{m, n, r\}$  that the complete solution can be obtained by solving the system of equations for some set of  $r$  variables in terms of the remaining  $n-r$  variables. A necessary and sufficient condition is that the  $r$  columns of the coefficient matrix corresponding to the first set of variables be linearly independent. Before stating this result formally it is convenient to introduce the following notation for a sub-matrix. Let  $\mathcal{A} = [a_{ij}]$  be a matrix of order  $m \times n$ . The sub-matrix of order  $p \times q$  formed from the array of entries located at the intersections of rows  $i_1, i_2, \dots, i_p$  and columns  $j_1, j_2, \dots, j_q$ , where  $1 \leq i_1 < i_2 < \dots < i_p \leq m$  and  $1 \leq j_1 < j_2 < \dots < j_q \leq n$  is denoted by the symbol

$$a \begin{pmatrix} i_1, i_2, \dots, i_p \\ j_1, j_2, \dots, j_q \end{pmatrix} .$$

i. e. ,

$$a \begin{pmatrix} i_1, i_2, \dots, i_p \\ j_1, j_2, \dots, j_q \end{pmatrix} = \begin{bmatrix} a_{i_1 j_1} & a_{i_1 j_2} & \dots & a_{i_1 j_q} \\ a_{i_2 j_1} & a_{i_2 j_2} & \dots & a_{i_2 j_q} \\ \dots & \dots & \dots & \dots \\ a_{i_p j_1} & a_{i_p j_2} & \dots & a_{i_p j_q} \end{bmatrix} \quad (2.2.1)$$

In some instances the set of row indices and the set of column indices are each denoted by a single symbol, say  $R$  and  $C$  respectively, then the above notation may be shortened to  $a \begin{pmatrix} R \\ C \end{pmatrix}$ .

Theorem 2.2.1. Given a system of holac equations

$$aX = 0 \quad \{m, n, r\} \quad (2.2.2)$$

Let  $x_{j_1}, x_{j_2}, \dots, x_{j_r}$ , ( $1 \leq j_1 < j_2 < \dots < j_r \leq n$ ), be any subset of  $r$  variables from  $X$ . If and only if the rank of  $a \begin{pmatrix} 1, 2, \dots, m \\ j_1, j_2, \dots, j_r \end{pmatrix}$  is  $r$ , then the complete solution for the system (2.2.2) can be obtained by solving the equations for  $x_{j_1}, x_{j_2}, \dots, x_{j_r}$  in terms of the remaining  $n-r$  variables.

Consider the system of holac equations (2.2.2). By Theorem 2.1.4, any subset of  $r$  linearly independent equations from (2.2.2) form an equivalent system of equations. Let any such subset of equations be

$$a_1 X = 0, \quad \{r, n, r\} \quad (2.2.3)$$

If  $r = n$ , then  $a_1$  is non-singular and the trivial solution is the only solution. If  $r < n$ , then by Theorem 2.1.1, the system (2.2.3) possesses non-trivial solutions and thus the original system (2.2.2) has non-trivial solutions. Since  $a_1$  has rank  $r$ , then there exists at least one set of column indices  $1 \leq j_1 < j_2 < \dots < j_r \leq n$  such that  $a_1 \begin{pmatrix} 1, 2, \dots, r \\ j_1, j_2, \dots, j_r \end{pmatrix}$  has rank  $r$ . With no loss in generality suppose that  $a_1 \begin{pmatrix} 1, 2, \dots, r \\ 1, 2, \dots, r \end{pmatrix}$  has rank  $r$ . Then (2.2.3) can be written in the form

$$\begin{bmatrix} a_{11} & a_{12} \end{bmatrix} \begin{bmatrix} \chi_1 \\ \chi_2 \end{bmatrix} = 0 \quad (2.2.4)$$

where  $a_{11}$  is  $r \times r$  and non-singular. Solving for  $\chi_1$

$$\chi_1 = -a_{11}^{-1} a_{12} \chi_2 \quad (2.2.5)$$

Therefore a complete solution for (2.2.3) and hence (2.2.2) is given by

$$\chi = \begin{bmatrix} \chi_1 \\ \chi_2 \end{bmatrix} = \begin{bmatrix} -a_{11}^{-1} a_{12} \chi_2 \\ \chi_2 \end{bmatrix} = \begin{bmatrix} -a_{11}^{-1} a_{12} \\ \mathcal{U} \end{bmatrix} \chi_2 \quad (2.2.6)$$

where  $\mathcal{U}$  is the unit matrix of order  $n-r$ .

Since (2.2.6) represents a trivial extension of (2.2.5), it is common to refer to either as representing a complete

solution for (2.2.2). A complete solution (2.2.6) of the system (2.2.2) defines an infinity of particular solutions -- one particular solution of (2.2.2) for each distinct choice for  $\mathcal{X}_2$ .

The relation (2.2.5) indicates that the  $r$  variables in  $\mathcal{X}_1$  are dependent upon the  $n-r$  variables in  $\mathcal{X}_2$ . It is common practice to designate the variables in  $\mathcal{X}_1$  as dependent variables and those in  $\mathcal{X}_2$  as independent variables. Although this is a convenient description to use, it can at times be misleading since it may lead one to view this description as a property of the variables rather than as a property of the coefficient matrix. With the appropriate interpretation it does, however, provide a useful notation. The following sequence of definitions relate to the subsequent use of this terminology in conjunction with a system of holac equations such as (2.2.2).

Definition 2.2.1.  $p$ -set of  $\mathcal{K}$

A subset of the variables in  $\mathcal{K}$ :  $x_{j_1}, x_{j_2}, \dots, x_{j_p}$ , where  $1 \leq j_1 < j_2 < \dots < j_p \leq n$ , is said to be a  $p$ -set of  $\mathcal{K}$ .

Definition 2.2.2. p-set of Dependent Variables,

## Complete Set of Dependent Variables

A p-set of  $\mathcal{X}$  is said to be a p-set of dependent variables for (2.2.2) if and only if the rank of  $a \begin{pmatrix} 1, 2, \dots, m \\ j_1, j_2, \dots, j_p \end{pmatrix}$  is p. If  $p = r$  (the rank of the system), the designation of a complete set of dependent variables for (2.2.2) is also used.

Definition 2.2.3. p-set of Independent Variables,

## Complete Set of Independent Variables

A p-set of  $\mathcal{X}$  is said to be a p-set of independent variables for (2.2.2) if and only if its complement in  $\mathcal{X}$  contains a complete set of dependent variables for (2.2.2.) The complement in  $\mathcal{X}$  of a complete set of dependent variables is also designated as the corresponding complete set of independent variables for (2.2.2).

Thus each set of  $r$  linearly independent columns of the coefficient matrix in (2.2.2) defines a partition of the  $n$  variables in  $\mathcal{X}$  into two mutually exclusive, all inclusive sets -- an  $r$ -set of dependent variables and the corresponding  $(n-r)$ -set of independent variables. Since the coefficient matrix has rank  $r$ , then there exists at least one such partition, although in general there may be more. Except for the trivial case when  $a$  is the zero matrix ( $r = 0$ ), a

complete set of dependent variables always contains at least one variable; a complete set of independent variables is empty if and only if  $n = r$ .

Consider

$$a\chi = 0, \{m, n, r\}, 0 < r \leq n. \quad (2.2.7)$$

the  $n$  variables in  $\chi$  can be partitioned into an  $r$ -set and the corresponding  $(n-r)$ -set in  $\binom{n}{r} = \frac{n!}{r!(n-r)!}$  distinct ways. Any given  $r$ -set of  $\chi$  may or may not be a complete set of dependent variables for (2.2.7). This fact results in the following designation:

Definition 2.2.4. Proper Partition

A partition of the  $n$  variables in (2.2.7) into an  $r$ -set  $\{x_{i_1}, x_{i_2}, \dots, x_{i_r}\}$  and the corresponding  $(n-r)$ -set  $\{x_{j_1}, x_{j_2}, \dots, x_{j_{n-r}}\}$  is said to be a proper partition of the variables if and only if the rank of  $a \begin{pmatrix} 1, 2, \dots, m \\ i_1, i_2, \dots, i_r \end{pmatrix}$  is  $r$ ; i. e., if and only if  $\{x_{i_1}, x_{i_2}, \dots, x_{i_r}\}$  is a complete set of dependent variables for (2.2.7).

Each proper partition of the variables in a given system of holac equations can be used to determine a complete solution. Since any one complete solution is sufficient to generate all of the particular solutions for a system of equations, it is not necessary to determine more than one proper partition of the

variables. Nevertheless, the form of the complete solution varies with the choice of proper partition and for a particular system of equations one choice may be more desirable than another.

Given a system of holac equations, such as (2.2.7), and one or more partitions of the variables into an  $r$ -set and the corresponding  $(n-r)$ -set the question of whether or not any particular partition is a proper partition of the variables can be answered by checking the rank of the appropriate sub-matrix of the coefficient matrix. All of the possible proper partitions could be determined by locating all  $m \times r$  sub-matrices which have rank  $r$ . Unfortunately the number of sub-matrices to be tested can become large for moderate sized systems of equations. For example, to determine all of the proper partitions of the variables for a system having a characteristic of  $\{10, 20, 10\}$  requires checking the rank of  $\binom{20}{10} = 184,756$  sub-matrices of order  $10 \times 10$ . This is a formidable task and would require considerable time, even on a high-speed digital computer.

It is possible, however, to use the complete solution derived from one proper partition of the variables to readily obtain information concerning other partitions. Consider

$$a\chi = 0, \quad \{r, n, r\} \quad . \quad (2.2.8)$$

Suppose that  $\det a_{1,2,\dots,r}^{(1,2,\dots,r)} \neq 0$ , then  $\{x_1, x_2, \dots, x_r\}$  is a complete set of dependent variables for (2.2.8). Solving for the  $r$  dependent variables in terms of the  $n-r$  independent variables to obtain a complete solution:

$$\begin{bmatrix} x_1 \\ x_2 \\ \cdot \\ \cdot \\ \cdot \\ x_r \end{bmatrix} = \frac{-1}{\det a_{1,2,\dots,r}^{(1,2,\dots,r)}} \begin{bmatrix} A_{11} & \dots & A_{r1} \\ A_{12} & \dots & A_{r2} \\ \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ A_{1r} & \dots & A_{rr} \end{bmatrix} \begin{bmatrix} a_{1,r+1} & \dots & a_{1n} x_{r+1} \\ a_{2,r+1} & \dots & a_{2n} x_{r+2} \\ \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ a_{r,r+1} & \dots & a_{rn} x_n \end{bmatrix} \quad (2.2.9)$$

where  $A_{ij}$  is the cofactor of  $a_{ij}$  in  $\det a_{1,2,\dots,r}^{(1,2,\dots,r)}$ , or

$$\begin{bmatrix} x_1 \\ x_2 \\ \cdot \\ \cdot \\ \cdot \\ x_r \end{bmatrix} = \begin{bmatrix} b_{11} & b_{12} & \dots & b_{1,n-r} \\ b_{21} & b_{22} & \dots & b_{2,n-r} \\ \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot \\ b_{r1} & b_{r2} & \dots & b_{r,n-r} \end{bmatrix} \begin{bmatrix} x_{r+1} \\ x_{r+2} \\ \cdot \\ \cdot \\ \cdot \\ x_n \end{bmatrix} \quad (2.2.10)$$

where

$$b_{ij} = \frac{\sum_{k=1}^r a_{k,r+j} A_{ki}}{-\det a_{1,2,\dots,r}^{(1,2,\dots,r)}}, \quad \begin{matrix} i=1, 2, \dots, r \\ j=1, 2, \dots, n-r \end{matrix}. \quad (2.2.11)$$

The numerator of  $b_{ij}$  in (2.2.11) is the determinant of a sub-matrix similar to that appearing in the denominator

except that column  $r+j$  of  $\mathcal{A}$  has replaced column  $i$ . Thus  $b_{ij} \neq 0$  ( $=0$ ) if and only if the altered sub-matrix has rank  $= r$  ( $< r$ ). Therefore, the  $r$ -set  $\{x_1, x_2, \dots, x_{i-1}, x_{i+1}, \dots, x_r, x_{r+j}\}$  is a complete set of dependent variables for (2.2.8) if and only if  $b_{ij} \neq 0$ . This result can be generalized to the following:

Theorem 2.2.2. Given

$$\mathcal{A}X = 0, \quad \{m, n, r\}.$$

Let  $\{x_{i1}, x_{i2}, \dots, x_{ir}\}$  be any complete set of dependent variables for this system of equations,  $\{x_{j1}, x_{j2}, \dots, x_{jn-r}\}$  be the corresponding complete set of independent variables, and the corresponding complete solution be

$$\begin{bmatrix} x_{i1} \\ x_{i2} \\ \cdot \\ \cdot \\ \cdot \\ x_{ir} \end{bmatrix} = \begin{bmatrix} b_{11} & b_{12} & \dots & b_{1, n-r} \\ b_{21} & b_{22} & \dots & b_{2, n-r} \\ \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot \\ b_{r1} & b_{r2} & \dots & b_{r, n-r} \end{bmatrix} \begin{bmatrix} x_{j1} \\ x_{j2} \\ \cdot \\ \cdot \\ \cdot \\ x_{jn-r} \end{bmatrix}. \quad (2.2.12)$$

The partition of the variables which results from the interchange of  $x_{is}$  and  $x_{jt}$ , ( $s=1, 2, \dots, r$ ;  $t=1, 2, \dots, n-r$ ), is a proper partition if and only if  $b_{st} \neq 0$ .

Consequently, a single complete solution such as (2.2.12) can be utilized to determine, by inspection, whether or not an additional  $r(n-r)$  partitions are proper partitions of the variables of a system of holac equations. Although Theorem 2.2.2 considers only a "singular" interchange of variables, i. e., one variable from each set, it can be used in an iterative manner to test any partition. Once a proper interchange has been found then the complete solution corresponding to the new proper partition is readily determined from the original complete solution by interchanging the two appropriate columns (with due regard to the signs of the entries) and then performing a sequence of at most  $r$  elementary row operations. A second proper interchange can be determined and the above process repeated. In this manner it is possible to determine all possible proper partitions of the variables, if desired.

### 2.3. The Complete Solution -- Another Viewpoint

In the discussion of Section 2.2 certain rank properties of the coefficient matrix in a system of holac equations with characteristic  $\{m, n, r\}$  are used to define a proper partition of the variables. A complete solution is then obtained by solving the system for the  $r$  dependent variables in terms of the  $n-r$  independent variables. Other approaches

to the problem of determining a complete solution are possible and the following discussion considers one such approach which occurs frequently in certain types of applied problems.

First, consider the sequence of steps used in Section 2.2 for determining a complete solution for the following system of holac equations:

$$a \chi = 0, \quad \{m, n, r\} \quad (2.3.1)$$

1. An equivalent system of equations consisting of any subset of  $r$  linearly independent equations is extracted from (2.3.1):

$$a_1 \chi = 0, \quad \{r, n, r\} \quad (2.3.2)$$

2. Let the first  $r$  column of  $a_1$  be linearly independent, then  $a_{11} = a_1 \begin{pmatrix} 1, 2, \dots, r \\ 1, 2, \dots, r \end{pmatrix}$  is non-singular and a complete solution for (2.3.2)

and (2.3.1) is given by

$$\chi = \begin{bmatrix} \chi_1 \\ \chi_2 \end{bmatrix} = \begin{bmatrix} -a_{11}^{-1} a_{12} \\ u \end{bmatrix} \chi_2 \quad (2.3.3)$$

Since the  $n-r$  variables in  $\chi_2$  can be arbitrarily chosen let the following  $n-r$  sets of values be successively assigned to  $\chi_2$ :

$$\begin{bmatrix} 1 \\ 0 \\ 0 \\ \cdot \\ \cdot \\ 0 \end{bmatrix}, \begin{bmatrix} 0 \\ 1 \\ 0 \\ \cdot \\ \cdot \\ 0 \end{bmatrix}, \dots, \begin{bmatrix} 0 \\ 0 \\ \cdot \\ \cdot \\ \cdot \\ 1 \end{bmatrix}$$

and the corresponding particular solutions determined

from (2.2.3). Thus each of the  $n-r$  columns of

$$\begin{bmatrix} -a_{11}^{-1} a_{12} \\ u \end{bmatrix} \text{ is a particular solution of (2.3.1);}$$

furthermore, these  $n-r$  solutions are linearly independent.

The complete solution as given in (2.3.3) may then be

interpreted as any linear combination of these  $n-r$  linearly

independent solutions. In general:

Theorem 2.3.1. If a system of holac equations has characteristic  $\{m, n, r\}$ , then every solution may be expressed as a linear combination of any  $n-r$  linearly independent solutions.

Definition 2.3.1. Fundamental System of Solutions,

Fundamental Matrix of Solutions

Let  $B_1, B_2, \dots, B_{n-r}$  be any  $n-r$  linearly independent solutions of (2.3.1), then  $\{B_1, B_2, \dots, B_{n-r}\}$  is called a fundamental system of solutions for (2.3.1) and the  $n \times (n-r)$  matrix  $B = [B_1, B_2, \dots, B_{n-r}]$  determined by

these solutions is called a fundamental matrix of solutions.

Consequently, if  $B$  is any fundamental matrix of solutions for the system  $AX = 0$ , then the columns of  $B$  are linearly independent and every linear combination of the columns of  $B$  is also a solution. From Theorem 2.3.1 it follows that a complete solution for (2.3.1) can be written in the form

$$X = BY \tag{2.3.4}$$

where  $B$  is any fundamental matrix of solutions and  $Y$  is a column matrix consisting of  $n-r$  arbitrary entries.

Frequently the entries in  $Y$  are considered as a new set of variables and (2.3.4) is subsequently considered as defining a transformation of variables. The use of the transformation of variables (2.3.4) in conjunction with the system (2.3.1) results in replacing the  $n$  variables in  $X$  by the  $n-r$  variables in  $Y$  and also reduces (2.3.1) to the matrix identity  $0=0$ .

The interrelationship between the coefficient matrix in a system of holac equations and a fundamental matrix of solutions for that system is a characteristic of a larger class of matrices defined according to:

Definition 2. 3. 2. Apolar Pair<sup>28</sup>

Let  $a, B$  have orders  $m \times n$  and  $n \times p$ , respectively. An ordered pair  $(a, B)$  of matrices is said to be an apolar pair if and only if (1)  $aB = 0$ , and (2) rank of  $a$  plus rank of  $B = n$ .

Using this concept the following result can be stated:

Theorem 2. 3. 2. Given  $aX = 0$ ,  $\{m, n, r\}$  and let  $B$  be a matrix of order  $n \times (n-r)$ . Then  $B$  is a fundamental matrix of solutions for the given system if and only if  $(a, B)$  is an apolar pair.

The existence of a suitable  $B$  is assured by the following<sup>28</sup>:

Theorem 2. 3. 3. Given any matrix  $a$  there exists another matrix  $B$  such that  $(a, B)$  is an apolar pair.

For a given coefficient matrix  $a$  the process of constructing a matrix  $B$  such that  $(a, B)$  is an apolar pair closely parallels the process of the solving the system of equations themselves and hence is not considered here. However, for certain systems of holac equations, some of which will be considered in later sections, it is possible to determine the matrix  $B$  independently of the matrix  $a$ .

#### 2.4. Interrelating the Two Viewpoints

Two approaches for obtaining a complete solution to a system of holac equations were considered in Sections 2.2 and 2.3. Since both techniques produce a complete solution for the same system of holac equations then they must be interrelated.

Consider the system of holac equations (2.3.1) and a complete solution given by (2.3.3). The particular solution,  $\chi_0$ , corresponding to any arbitrary choice,  $\chi_{20}$ , for  $\chi_2$  is, from (2.3.3):

$$\chi_0 = \begin{bmatrix} \chi_{10} \\ \chi_{20} \end{bmatrix} = \begin{bmatrix} -a_{11}^{-1} a_{12} \\ u \end{bmatrix} \chi_{20} \quad (2.4.1)$$

Also, let  $B$  be any fundamental matrix of solutions for (2.3.1). Since a complete solution is given by (2.3.4), then there must be at least one set of values  $y_0$ , such that

$$\chi_0 = B y_0 \quad (2.4.2)$$

or

$$\begin{bmatrix} \chi_{10} \\ \chi_{20} \end{bmatrix} = \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} y_0 \quad (2.4.3)$$

From (2.4.1) and (2.4.3):

$$\chi_{20} = B_2 y_0 \quad (2.4.4)$$

where  $B_2$  is a square matrix of order  $n-r$ . If  $\chi_{20} = 0$ , then from (2.4.1) it follows that  $\chi_0 = 0$ , and (2.4.2) yields  $B y_0 = 0$ . Consequently  $y_0 = 0$  since the columns of  $B$  are linearly independent. Therefore:

$$\chi_{20} = 0 \text{ implies } y_0 = 0 \quad (2.4.5)$$

On the other hand, from (2.4.4) with  $\chi_{20} = 0$ , one obtains a system of holac equations

$$B_2 y_0 = 0, \quad \{n-r, n-r, \rho\} \quad (2.4.6)$$

where  $\rho$  is the rank of  $B_2$ .

Suppose  $\rho < n-r$ . Then the system (2.4.6) has an infinity of non-trivial solutions for  $y_0$ , which contradicts (2.4.5). Since  $\rho$  cannot exceed  $n-r$ , it follows that

$\rho = n-r$  and thus  $B_2$  is non-singular. Hence for the same particular solution,  $\chi_0$ ,

$$y_0 = B_2^{-1} \chi_{20} \quad (2.4.7)$$

and there exists a one-to-one correspondence between  $\chi_{20}$  and  $y_0$ .

The preceding argument also establishes a relationship between certain sub-matrices of  $A$  and  $B$ .

Theorem 2.4.1. Given the system of holac equations

$$AX = 0, \quad \{m, n, r\}$$

and any associated fundamental matrix of solutions,  $B$ . Let  $i_1, i_2, \dots, i_r$  and  $j_1, j_2, \dots, j_{n-r}$  be sets of indices complementary with respect to the set of column indices  $1, 2, \dots, n$ ; i. e.,  $i_1, i_2, \dots, i_r$  and  $j_1, j_2, \dots, j_{n-r}$  taken together form a complete set of indices  $1, 2, \dots, n$ . Then

$A_{\substack{(1, 2, \dots, m) \\ (i_1, i_2, \dots, i_r)}}$  has rank  $r$  if and only if  $B_{\substack{(j_1, j_2, \dots, j_{n-r}) \\ (1, 2, \dots, n-r)}}$  has rank  $n-r$ .

Theorem 2.4.1 can be extended to the more general case of an apolar pair since if  $(A, B)$  form an apolar pair, then  $B$  of order  $n \times p$  is rank equivalent to  $[B_1, 0]$  where  $B_1$  is of order  $n \times (n-r)$ , has rank  $n-r$ , and by Theorem 2.3.2 is a fundamental matrix of solutions for the system of holac equations having  $A$  as a coefficient matrix. Thus:

Theorem 2.4.2. Let  $(A, B)$  be an apolar pair where  $A$  is of order  $m \times n$  and rank  $r$ ;  $B$  is a matrix of order  $n \times p$ . Let  $i_1, i_2, \dots, i_r$  and  $j_1, j_2, \dots, j_{n-r}$  be sets of indices complementary with respect to the column indices  $1, 2, \dots, n$ .

Then:

$A \begin{pmatrix} 1, 2, \dots, m \\ i_1, i_2, \dots, i_r \end{pmatrix}$  has rank  $r$  if and only if

$B \begin{pmatrix} j_1, j_2, \dots, j_{n-r} \\ 1, 2, \dots, p \end{pmatrix}$  has rank  $n-r$ .

## Chapter 3

### GENERAL PROPERTIES OF SYSTEMS OF NETWORK EQUATIONS

#### 3. 1. Introduction

Network equations are formulated in a number of different forms depending upon the type of solution that is sought. Formulation in the time-domain is most general and results in a system of ordinary differential and algebraic equations. However, for a large class of network problems, experience has shown that it is possible, and in fact, more convenient, to by-pass time-domain formulation in favor of frequency-domain or  $\omega$ -domain formulation. With this approach the network equations are wholly algebraic in form and involve complex numbers. The solutions, in terms of complex numbers, are correlated with time-domain solutions as well as observations on the physical systems. The complex number form of the network equations, resulting from formulation in the  $\omega$ -domain, is used as the basis for the investigation of this paper. Thus properties of a system of linear equations over the complex field play a fundamental role in this study.

It is possible to approach the general problem of assigning specific values to variables within a system of linear equations from two points of view. In one approach the equations are considered in a homogeneous form and rank properties of the coefficient matrix are used to define a partition of the variables into a dependent set and an independent set, i. e. , a proper partition. Once a proper partition has been determined, then the variables within the independent set are assigned arbitrary values with no danger of introducing inconsistencies. As noted in the preceding chapter, the variables themselves do not enter into the partitioning process; in fact, it is possible to obtain a complete solution from the coefficient matrix alone.

The other approach is, in some respects, the reverse of the above process. As an initial step one can assign values to a subset of the variables and subsequently examine a system of non-homogeneous equations to determine whether or not it is consistent. If it is, then it is possible to determine a complete solution; if not, then the specification pattern is altered and the process repeated. With this approach, the number of variables assigned specific values is, to a certain extent, flexible; however, great care must be exercised in the choice of both the variables which are specified and the specific

values which are assigned. The consistency conditions depend not only upon properties of the coefficient matrix, but also upon the specific values assigned to the variables. Insofar as this investigation is concerned, the first approach possesses a definite advantage over the second in that the nature of the process is such that it removes any doubt about consistency -- one is always assured of a solution. Because of this, it is possible to make definite decisions with regard to the question of which variables can be specified, based solely upon properties of the coefficient matrix. These decisions are not influenced or affected by any specific set of values which might have been assigned to a particular subset of the variables.

While systems of holac equations play a fundamental role in electric network theory, the theory of graphs<sup>29, 30</sup> also occupies a position of equal importance. The approach to network theory based upon a study of the correlating oriented linear graph<sup>10, 11, 16, 31-35</sup> has done much to add insight and precision into the formulation and solution of problems within this area. The mapping of significant subgraphs into matrices, which subsequently appear within the coefficient matrices of the network equations, allows one to interrelate properties of these subgraphs with associated properties of the equations and their solutions. In the present chapter consideration is given

to a fundamental system of network equations and some of its general properties; the following chapter is devoted to examining, in more detail, the relationships between certain subgraphs and rank properties of the coefficient matrix.

Given a particular network for analysis, it is assumed that a correlating oriented linear graph (hereafter referred to as a graph) has been established. In addition, two complex variables are associated with each element of the graph--a voltage variable,  $V$ , and a current variable,  $I$ . An extensive background of foundation material is assumed<sup>10, 11</sup>; the terminology and notation used here is essentially that found in these references.

### 3.2. Characterization of the Graph Elements

In general the graph elements used in electric network theory are classified as either relation elements (F-elements), or no-relation elements (N-elements), depending upon the presence or absence, respectively, of certain fixed mathematical equations relating the primary variables,  $V$  and  $I$ , associated with each element. Formally<sup>16</sup>:

#### Definition 3.2.1. F-element

An F-element is a graph element characterized by some fixed mathematical relation which relates  $V$  or  $I$  for

that element to  $V$  or  $I$  of the same element or any other element of the graph. The mathematical relations are characteristics of the elements themselves and are independent of the manner in which the  $F$ -elements are imbedded in the graph. The corresponding equations are called  $F$ -equations.

Commonly encountered examples of  $F$ -elements are the graph element correlates of resistors, inductors, capacitors, transformers, and the like.

Definition 3.2.2.  $N$ -element

An  $N$ -element is a graph element characterized by: (1) either, neither, or both  $V$  and  $I$  for the element are arbitrarily specified; and (2)  $V$  and  $I$  for that element are not related in any fixed manner by an equation which is characteristic of the element itself.

$N$ -elements are further classified into four different types depending upon the pattern of element variable specifications. Thus:

Definition 3.2.3.  $N_e$ -element<sup>10</sup>

An  $N$ -element for which the element variable  $V$  is arbitrarily specified is designated as an  $N_e$ -element. The specified variable  $V$  is designated by  $E$ , and the unspecified

variable I is determined by the graph incident to this  $N_e$ -element.

Definition 3.2.4.  $N_h$ -element<sup>10</sup>

An N-element for which the element variable I is arbitrarily specified is designated as  $N_h$ -element. The specified variable I is designated by H, and the unspecified variable V is determined by the graph incident to this  $N_h$ -element.

Definition 3.2.5.  $N_{eh}$ -element

An N-element for which both of the element variables, V and I, are arbitrarily specified is designated as an  $N_{eh}$ -element. The specified variables V and I are designated by E and H, respectively.

Definition 3.2.6.  $N_o$ -element

An N-element for which neither of the element variables is arbitrarily specified is designated as an  $N_o$ -element. Both of the element variables, V and I, are determined by the graph incident to this  $N_o$ -element.

Of these four types of N-elements, the  $N_e$ - and  $N_h$ -elements are "familiar" since they are the graph element correlates of regulated voltage and current sources, respectively.

Applications of  $N_{eh}$ -elements were considered briefly in Section 1.3. In spite of its apparent lack of any distinguishing characteristics (other than this very lack itself), the  $N_o$ -element has considerable utility in network analysis. The complete dependence of both of its variables upon the incident graph makes the  $N_o$ -element useful for determining certain characteristics of the incident graph per se. For example, in the following pages these elements are used as "test elements" to determine allowable locations, within a graph, for the other types of N-elements.

The form in which the F equations appear is often a deciding factor in choosing a solution technique for the network equations. For a set of  $n_F$  F-elements, the F-equations can appear in three basic form in the  $\omega$ -domain:

(1) the non-explicit F-equations:

$$\sum_{k=1}^{n_F} (f_{1ik} I_k + f_{2ik} V_k) = 0, \quad i=1, 2, \dots, n_F \quad (3.2.1)$$

or, in matrix form

$$\mathcal{I}_1 \mathcal{I}_F + \mathcal{I}_2 \mathcal{V}_F = 0 \quad (3.2.2)$$

where  $\mathcal{I}_1$  and  $\mathcal{I}_2$  are complex matrices of order  $n_F \times n_F$ , and  $\mathcal{I}_F$ ,  $\mathcal{V}_F$  are column matrices of the  $I_k$  and  $V_k$ , respectively.

(2) the I-explicit F-equations:

$$I_F - Y_F V_F = 0 \quad (3.2.3)$$

where  $Y_F$  is a complex matrix of order  $n_F \times n_F$  and is called the F-element admittance matrix;

(3) the V-explicit F-equations:

$$V_F - Z_F I_F = 0 \quad (3.2.4)$$

where  $Z_F$  is a complex matrix of order  $n_F \times n_F$  and is called the F-element impedance matrix.

Although the non-explicit form in (3.2.2) is most general, the latter two (if they exist!) are generally more desirable forms. No matter which of the three forms is considered, the F-equations are a system of  $n_F$  holac equations in  $2n_F$  variables.

### 3.3. Circuit and Seg Equations

The coefficient matrices for two fundamental systems of network equations -- Kirchhoff's voltage and current equations -- are established by mapping certain classes of subgraphs into matrices. As a result of mapping all circuits of a graph  $G$  into a matrix one obtains a complete circuit matrix for  $G$ ; the associated system of holac equations is called a complete system of circuit equations for  $G$ :

$$B_a v_e = 0 \quad (3.3.1)$$

where  $B_a$  is a complete circuit matrix for  $G$ , and  $v_e$  is a column matrix of the element  $V$ 's.

Mapping all segs of  $G$  into a matrix results in a complete seg matrix for  $G$ ; the associated system of holac equations -- a generalization of Kirchhoff's current equations -- is called a complete system of seg equations:

$$S_a I_e = 0 \quad (3.3.2)$$

where  $S_a$  is a complete seg matrix for  $G$ , and  $I_e$  is a column matrix of the element  $I$ 's.

The rank of  $B_a$  is  $e-v+1$ , and that of  $S_a$  is  $v-1$ , for an  $e$ -element,  $v$ -vertex connected graph  $G$ . Thus, from Theorem 2.1.4: any subset of  $e-v+1$  linearly independent equations from a complete system of circuit equations constitutes an equivalent system of equations; any subset of  $v-1$  linearly independent equations from a complete system of seg equations constitutes an equivalent system of equations. Hence it is neither necessary nor desirable to consider a complete system of circuit or seg equations in order to study their properties. Rather, one need consider only a basis system of circuit equations:

$$B v_e = 0, \quad \{e-v+1, e, e-v+1\} \quad (3.3.3)$$

and, a basis system of seg equations:

$$\mathcal{L}\mathcal{L}_e = 0, \quad \{v-1, e, v-1\} \quad (3.3.4)$$

where

Definition 3.3.1. Basis circuit matrix  $\mathcal{B}$

Any  $(e-v+1)$ -row,  $e$ -column,  $(e-v+1)$ -rank sub-matrix of a complete circuit matrix  $\mathcal{B}_a$  is designated as a basis circuit matrix  $\mathcal{B}$ ;

Definition 3.3.2. Basis seg matrix  $\mathcal{L}$

Any  $(v-1)$ -row,  $e$ -column,  $(v-1)$ -rank sub-matrix of a complete seg matrix  $\mathcal{L}_a$  is designated as a basis seg matrix  $\mathcal{L}$ .

In Section 2.2 rank properties of the coefficient matrix in a system of holac equations are used to define a proper partition of the variables. This proper partition is subsequently used to determine a complete solution for the system. The following Theorems provide a foundation on which to interrelate certain interconnection patterns of the elements of a graph and certain rank properties of the coefficient matrices which appear in basis systems of circuit and seg equations:

Theorem 3.3.1. Let  $G_s$  be an  $m$ -element subgraph of a connected graph  $G$ ,  $1 \leq m \leq e-v+1$ ; and

let  $B = [B_1 B_2]$  be any basis circuit matrix for  $G$ , where the columns of  $B_1$  correspond to the elements of  $G_s$ . Then the columns of  $B_1$  are linearly independent if and only if  $G_s$  contains no seg of  $G$ .

Theorem 3.3.2. A subgraph  $G_s$ , of a connected graph  $G$ , is a subgraph of some cotree if and only if  $G_s$  contains no seg of  $G$ .

Theorem 3.3.3. Let  $G_s$  be an  $m$ -element subgraph of a connected graph  $G$ ,  $1 \leq m \leq v-1$ ; and let  $S = [S_1 S_2]$  be any basis seg matrix for  $G$ , where the columns of  $S_1$  correspond to the elements of  $G_s$ . Then the columns of  $S_1$  are linearly independent if and only if  $G_s$  contains no circuits.

Theorem 3.3.4. A subgraph  $G_s$ , of a connected graph  $G$ , is a subgraph of some tree of  $G$  if and only if  $G_s$  contains no circuits.

Theorem 3.3.5. Let  $G$  be a connected graph. If  $G_1$  and  $G_2$  are any two subgraphs of  $G$  such that:  
 i)  $G_1$  and  $G_2$  have no elements in common, ii)  $G_1$  contains no circuits, and iii)  $G_2$  contains no seg of  $G$ ; then there

exists some tree  $T$  of  $G$  such that  $G_1$  is a subgraph of  $T$  and  $G_2$  is a subgraph of the complement, in  $G$ , of  $T$ .

Another approach to determining a complete solution for a system of holac equations is considered in Section 2.3. The approach there is based upon the concept of a fundamental matrix of solutions. Again the graph and certain of its associated matrices provide an effective means to obtain a fundamental matrix of solutions. The following theorem provides the needed relationships:

**Theorem 3.3.6.** Let  $G$  be a connected graph, and let  $B_a$  and  $S_a$  be, respectively, a complete circuit matrix and a complete seg matrix for  $G$ . If the columns of  $B_a$  and  $S_a$  are ordered the same with respect to the elements of  $G$ , then

$$S_a B_a' = 0 \quad \text{and} \quad B_a S_a' = 0. \quad (3.3.5)$$

Since

$$\text{rank of } B_a + \text{rank } S_a = (e-v+1) + (v-1) = e \quad (3.3.6)$$

then, from definition 2.3.2, one concludes that  $(S_a, B_a')$  and  $(B_a, S_a')$  are apolar pairs. Furthermore, if  $S_a$  and/or  $B_a$  are replaced by any basis seg matrix  $S$  and any basis circuit matrix  $B$ , respectively, then similar

conclusions follow. Thus: the transpose of any basis circuit matrix  $B$  is a fundamental matrix of solutions for both a complete system and any basis system of seg equations; the transpose of any basis seg matrix  $S$  is a fundamental matrix of solutions for both a complete system and any basis system of circuit equations. Therefore, from Theorem 2.3.2,

$$V_e = S' W_1, \quad (3.3.7)$$

where  $S$  is any basis seg matrix for  $G$ , and  $W_1$  is an arbitrary  $(v-1)$ -rowed column matrix, is a complete solution for (3.3.1) and (3.3.3);

$$I_e = B' W_2, \quad (3.3.8)$$

where  $B$  is any basis circuit matrix for  $G$ , and  $W_2$  is an arbitrary  $(e-v+1)$ -rowed column matrix,

is a complete solution for (3.3.2) and (3.3.4).

### 3.4. Primary Systems of Equations

Collectively, the circuit, seg, and F-equations contain all the information relative to the primary variables,  $V$  and  $I$ , associated with the elements of a graph. Due to the fundamental nature of these equations it is useful to have a single designation for this collection of equations. Accordingly:

Definition 3.4.1. Primary system of equations

The combination of any basis system of seg equations, any basis system of circuit equations, and the F-equations associated with a graph is designated as a primary system of equations for the graph.

A primary system of equations is also classified as non-explicit, I-explicit, or V-explicit depending upon the form of the F-equations which appear within the system.

Ultimately, it is a solution for a primary system of equations that is sought, although this does not imply that one must solve these equations as they stand. It is more often the case that certain secondary or derived systems of equations, such as the mesh, branch, and node equations, are utilized to obtain numerical solutions since they generally involve fewer simultaneous equations to solve. However, these secondary systems are established from the primary system as a base.

Consider a non-explicit primary system of equations for a connected graph  $G$  containing  $e$  elements,  $v$  vertices, and  $n$  N-elements:

$$\begin{array}{c}
 v-1 \\
 e-v+1 \\
 e-n
 \end{array}
 \begin{array}{c}
 n \\
 e-n \\
 n \\
 e-n
 \end{array}
 \begin{array}{c}
 \mathcal{L}_N \\
 \mathcal{L}_F \\
 0 \\
 0 \\
 \mathcal{B}_N \\
 \mathcal{B}_F \\
 0 \\
 0 \\
 \mathcal{I}_1 \\
 \mathcal{I}_2
 \end{array}
 \begin{array}{c}
 \mathcal{L}_N \\
 \mathcal{L}_F \\
 \mathcal{V}_N \\
 \mathcal{V}_F
 \end{array}
 = 0$$

(3.4.1)

where the N and F subscripts refer to the N-elements and the F-elements, respectively.

If, at the outset, the N-elements are all  $N_0$ -elements, then there are no specified variables in (3.4.1), and this is a system of  $2e-n$  holac equations in  $2e$  variables. Suppose that the rank of this system is also  $2e-n$ , as is the case with the  $\omega$ -domain graph correlates of many classes of electric networks. If  $n > 0$ , then (3.4.1) possesses non-trivial solutions and complete sets of independent variables consist of some subsets of  $n$  of the element variables. Thus, the number of variables which can be assigned arbitrary values is equal to the number of N-elements in the graph. Consideration of the various combinations of the element variables which could occur within a complete set of independent variables indicates that if V, I, or V and I for an  $N_0$ -element appear within this set then it is possible to replace the

$N_o$ -element by an  $N_e$ -,  $N_h$ -, or  $N_{eh}$ -element, respectively, with no danger of introducing inconsistencies. In this sense the  $N_o$ -element is used as a "test element" to check whether or not certain patterns of N-elements can be present within a given graph. Furthermore, the number of independent variables is fixed at  $n$  regardless of the type of N-elements present; thus, if both variables for one N-element occur in an independent set then both variables for some other N-element must occur in the dependent set. In a similar manner, if an F-element variable occurs in an independent set then both variables for some N-element must occur within the dependent set.

### 3. 5. I-Explicit Primary Systems Associated with Power Networks

The present section is devoted to a consideration of the  $\omega$ -domain graph correlates of electric power networks of the type discussed in Sections 1. 1 and 1. 2. These graphs contain three general types of elements; namely: elements correlating with generators, loads, and the components which comprise the transmission and distribution network. The elements associated with the generators are N-elements, while those associated with the transmission and distribution network are F-elements. Unfortunately the elements

corresponding to the loads cannot, in general, be categorized in a clear-cut manner. One is inclined to consider these elements as F-elements and characterize them, in the  $\omega$ -domain, by a complex admittance or impedance. However, more often than not, the load admittance or impedance is either not known or, at best, only partially specified at the outset of a problem. Consequently, these elements do not readily fit into the F-element classification. The specifications for the load elements are often stated in terms of specified variables such as real and reactive powers; thus they do not immediately fit into the N-element classification, which involves  $V$  and/or  $I$  specifications. However, based upon the discussion of Section 1.3, the N-element classification seems more appropriate as a general rule. If the load admittance is given, then, as shown next, it is possible to use either classification -- F-element or N-element.

Consider an I-explicit primary system for a connected graph of  $e$  elements and  $v$  vertices. Let the graph contain  $n$   $N_0$ -elements, and further, suppose that the system of equations has characteristic  $\{2e-n, 2e, 2e-n\}$  :

$$\begin{matrix}
 v-1 \\
 e-v+1 \\
 e-n
 \end{matrix}
 \begin{bmatrix}
 n & e-n & n & e-n \\
 \mathcal{L}_N & \mathcal{L}_F & 0 & 0 \\
 0 & 0 & \mathcal{B}_N & \mathcal{B}_F \\
 0 & \mathcal{U}_F & 0 & -\mathcal{Y}_F
 \end{bmatrix}
 \begin{bmatrix}
 \mathcal{L}_N \\
 \mathcal{L}_F \\
 \mathcal{V}_N \\
 \mathcal{V}_F
 \end{bmatrix}
 = 0
 \tag{3.5.1}$$

where  $\mathcal{Y}_F$  is a non-singular diagonal matrix with complex entries.

This system of equations is presented in more detail below in order to consider the most general distribution of element variables within the dependent and independent sets of a proper partition:

$$\begin{matrix}
 v-1 \\
 e-v+1 \\
 n_{F1} \\
 n_{F2} \\
 n_{F3}
 \end{matrix}
 \begin{bmatrix}
 n_1 & n_2 & n_3 & n_4 & n_{F1} & n_{F2} & n_{F3} & n_1 & n_2 & n_3 & n_4 & n_{F1} & n_{F2} & n_{F3} \\
 \mathcal{L}_{N1} & \mathcal{L}_{N2} & \mathcal{L}_{N3} & \mathcal{L}_{N4} & \mathcal{L}_{F1} & \mathcal{L}_{F2} & \mathcal{L}_{F3} & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & \mathcal{B}_{N1} & \mathcal{B}_{N2} & \mathcal{B}_{N3} & \mathcal{B}_{N4} & \mathcal{B}_{F1} & \mathcal{B}_{F2} & \mathcal{B}_{F3} \\
 0 & 0 & 0 & 0 & \mathcal{U}_{F1} & 0 & 0 & 0 & 0 & 0 & 0 & -\mathcal{Y}_{F1} & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & \mathcal{U}_{F2} & 0 & 0 & 0 & 0 & 0 & 0 & -\mathcal{Y}_{F2} & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & \mathcal{U}_{F3} & 0 & 0 & 0 & 0 & 0 & 0 & -\mathcal{Y}_{F3}
 \end{bmatrix}
 \begin{bmatrix}
 \mathcal{L}_{N1} \\
 \mathcal{L}_{N2} \\
 \mathcal{L}_{N3} \\
 \mathcal{L}_{N4} \\
 \mathcal{L}_{F1} \\
 \mathcal{L}_{F2} \\
 \mathcal{L}_{F3} \\
 \mathcal{V}_{N1} \\
 \mathcal{V}_{N2} \\
 \mathcal{V}_{N3} \\
 \mathcal{V}_{N4} \\
 \mathcal{V}_{F1} \\
 \mathcal{V}_{F2} \\
 \mathcal{V}_{F3}
 \end{bmatrix}
 = 0$$

where  $n_1 + n_2 + n_3 + n_4 = n$ , and  $n_{F1} + n_{F2} + n_{F3} = e-n$ .

Rearranging the columns to indicate the desired distribution of element variables

$$\begin{bmatrix}
 S_{N1} & S_{N2} & 0 & 0 & S_{F1} & 0 & S_{F2} & 0 \\
 0 & 0 & B_{N1} & B_{N3} & 0 & B_{F1} & 0 & B_{F3} \\
 0 & 0 & 0 & 0 & u_{F1} & y_{F1} & 0 & 0 \\
 \hline
 0 & 0 & 0 & 0 & 0 & 0 & u_{F2} & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & -y_{F3}
 \end{bmatrix}
 \begin{bmatrix}
 I_{N1} \\
 I_{N2} \\
 v_{N1} \\
 v_{N3} \\
 I_{F1} \\
 v_{F1} \\
 \hline
 I_{F2} \\
 v_{F3}
 \end{bmatrix}$$

$$= - \begin{bmatrix}
 S_{N3} & S_{N4} & S_{F3} & 0 & 0 & 0 \\
 0 & 0 & 0 & B_{N2} & B_{N4} & B_{F2} \\
 0 & 0 & 0 & 0 & 0 & 0 \\
 \hline
 0 & 0 & 0 & 0 & 0 & -y_{F2} \\
 0 & 0 & u_{F3} & 0 & 0 & 0
 \end{bmatrix}
 \begin{bmatrix}
 I_{N3} \\
 I_{N4} \\
 I_{F3} \\
 v_{N2} \\
 v_{N4} \\
 v_{F2}
 \end{bmatrix}$$

(3.5.3)

If and only if the coefficient matrix on the left-hand side of (3.5.3) is non-singular, then the above partition of the variables is a proper partition into a complete dependent set

$$\{ I_{N1}, V_{N1}, I_{N2}, V_{N3}, I_{F1}, V_{F1}, I_{F2}, V_{F3} \} \quad (3.5.4)$$

and the corresponding complete independent set

$$\{ V_{N2}, I_{N3}, I_{N4}, V_{N4}, V_{F2}, I_{F3} \} . \quad (3.5.5)$$

Suppose that this is the case. Then it is necessary that

$$n_1 = n_4 + n_{F2} + n_{F3} ; \quad (3.5.6)$$

That is, the number of N-elements having both variables in the dependent set is equal to the number of N-elements having both variables in the independent set plus the number of F-elements having one variable, either V or I, in the independent set. It is noted that it is not possible to have an F-element of the type considered here with both variables in the independent set. However, specification of either variable for this type of F-element immediately determines the other variable. Thus specifying one variable for an F-element has the same effect as specifying both variables -- only one of which is arbitrarily chosen. In fact an F-element having one variable in the independent set can also be handled as an N-element with both variables in the independent set -- provided that one assigns values to these variables in a prescribed manner. Consider the coefficient matrix on the left-hand side of (3.5.3.):

$$\left[ \begin{array}{cccc|cc} S_{N1} & S_{N2} & 0 & 0 & S_{F1} & 0 & S_{F2} & 0 \\ 0 & 0 & B_{N1} & B_{N3} & 0 & B_{F1} & 0 & B_{F3} \\ 0 & 0 & 0 & 0 & u_{F1} & -y_{F1} & 0 & 0 \\ \hline 0 & 0 & 0 & 0 & 0 & 0 & u_{F2} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & -y_{F3} \end{array} \right]$$

$$= \begin{bmatrix} m_{11} & m_{12} \\ 0 & m_{22} \end{bmatrix} = \mathcal{M}$$

(3.5.7)

Since, by hypothesis, the matrix  $\mathcal{M}$  is non-singular then  $m_{11}$  and  $m_{22}$  are non-singular. In fact, due to the nature of  $m_{22}$ , one has that  $\mathcal{M}$  is non-singular if and only if  $m_{11}$  is non-singular. Suppose that the last two sets of  $n_{F2} + n_{F3}$  F-equations in (3.5.2) or (3.5.3) are deleted; however, the corresponding graph elements are not deleted -- so the seg and circuit matrices remain unaltered. The only change is that these elements are now classified as N-elements. Thus both the number of equations in the system and the rank of the system are diminished by  $n_{F2} + n_{F3}$ , but the number of variables remains unchanged. Consequently the number of variables in a complete dependent (independent) set is decreased (increased) by  $n_{F2} + n_{F3}$ . If this altered system of equations is now rearranged to include the  $n_{F2}$  variables

in  $\mathcal{L}_{F2}$  and the  $n_{F3}$  variables in  $\mathcal{V}_{F3}$  in a new set of (potential) independent variables then one obtains (retaining the notation of (3.5.2) ):

$$\begin{array}{c}
 v-1 \\
 e-v+1 \\
 n_{F1}
 \end{array}
 \begin{bmatrix}
 \overset{n_1}{\mathcal{L}_{N1}} & \overset{n_2}{\mathcal{L}_{N2}} & 0 & 0 & \overset{n_{F1}}{\mathcal{L}_{F1}} & 0 \\
 0 & 0 & \mathcal{L}_{N1} & \mathcal{L}_{N3} & 0 & \mathcal{L}_{F1} \\
 0 & 0 & 0 & 0 & \mathcal{U}_{F1} & -\mathcal{Y}_{F1}
 \end{bmatrix}
 \begin{bmatrix}
 \mathcal{L}_{N1} \\
 \mathcal{L}_{N2} \\
 \mathcal{V}_{N1} \\
 \mathcal{V}_{N3} \\
 \mathcal{L}_{F1} \\
 \mathcal{V}_{F1}
 \end{bmatrix}$$
  

$$= - \begin{bmatrix}
 \overset{n_3}{\mathcal{L}_{N3}} & \overset{n_4}{\mathcal{L}_{N4}} & \overset{n_{F2}}{\mathcal{L}_{F2}} & \overset{n_{F3}}{\mathcal{L}_{F3}} & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & \mathcal{L}_{N2} & \mathcal{L}_{N4} & \mathcal{L}_{F2} & \mathcal{L}_{F3} \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0
 \end{bmatrix}
 \begin{bmatrix}
 \mathcal{L}_{N3} \\
 \mathcal{L}_{N4} \\
 \mathcal{L}_{F2} \\
 \mathcal{L}_{F3} \\
 \mathcal{V}_{N2} \\
 \mathcal{V}_{N4} \\
 \mathcal{V}_{F2} \\
 \mathcal{V}_{F3}
 \end{bmatrix}$$

(3.5.8)

The coefficient matrix on the left-hand side of (3.5.8) is precisely  $\mathcal{M}_{11}$  from (3.5.7) and thus has the proper order and rank if and only if the coefficient matrix  $\mathcal{M}$  on the left-hand side of (3.5.3) has the proper order and rank.

Since, by hypothesis,  $\mathcal{M}$  has the proper order and rank then

$$\{I_{N1}, \nu_{N1}, I_{N2}, \nu_{N3}, I_{F1}, \nu_{F1}\} \quad (3.5.9)$$

is a complete set of dependent variables for (3.5.8) and

$$\{\nu_{N2}, I_{N3}, I_{N4}, \nu_{N4}, I_{F2}, \nu_{F2}, I_{F3}, \nu_{F3}\} \quad (3.5.10)$$

is the corresponding complete set of independent variables.

Although the systems of equations (3.5.2) and (3.5.8) are neither identical nor equivalent systems of equations they are closely related. Every solution of (3.5.2) is also a solution of (3.5.8) but the converse is not true. However, every solution of (3.5.8) for which the variables  $I_{F2}$ ,  $\nu_{F2}$ ,  $I_{F3}$ ,  $\nu_{F3}$  are chosen so that

$$I_{F2} = \nu_{F2} \nu_{F2} \quad \text{and} \quad I_{F3} = \nu_{F3} \nu_{F3} \quad (3.5.11)$$

is also a solution of (3.5.2).

The transition from (3.5.2) to (3.5.8) was accomplished by deleting certain F-equations from the primary system of equations; in effect changing the character of the elements involved from F-elements to N-elements, but otherwise leaving the graph unaltered. It is then possible to assign values to the variables associated with these N-elements so as to maintain

any desired relationship between them. The admittance coefficients for the "transformed" F-elements no longer appear within the system of equations; thus it is possible to effectively handle situations where these coefficients are not completely known, or are variable, without introducing unknown or changing quantities into the coefficient matrix.

A distinctive feature of a "per-phase" representation of a power network is the presence of a common node or "ground bus". In particular, within the graph correlate, the N- and F-elements corresponding to the generators and loads are incident to a common vertex--the "reference" vertex. With no loss in generality it is assumed that each non-reference vertex of the graph is incident to exactly one N-element and that all N-elements are also incident to the reference vertex. For the case of a non-generator, non-load vertex, or a load vertex for which the admittance coefficient of the incident load element is known, then the incident N-element can be specified as an  $N_h$ -element for which  $H \equiv 0$ , i. e., an open-circuit, or possibly an  $N_{eh}$ -element for which  $H \equiv 0$  and  $E$  is an arbitrarily specified complex number. With this assumption the graphs under consideration consist of the union of a  $v$ -vertex connected graph of F-elements and a Lagrangian tree of  $v-1$  N-elements---see figure 3.5.1.

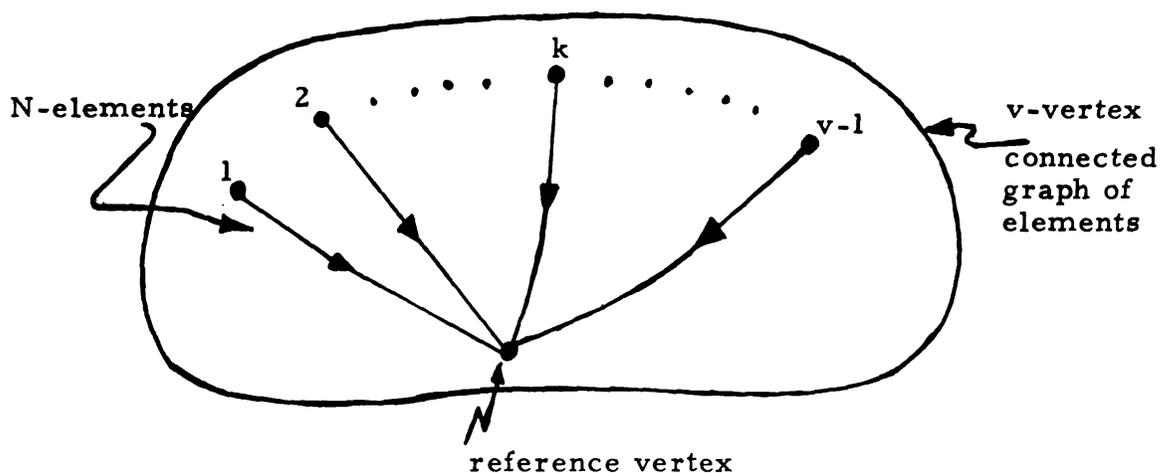


Figure 3.5.1. Graph Correlate of a Power Network.

In the formulation of a primary system of equations for the graph correlate of a network one has, in general, a variety of basis seg matrices from which to choose<sup>10</sup>; in the following sections an incidence-seg matrix  $a$  is used exclusively. There is no loss in generality in this choice, and one has an advantage in that a basis incidence-seg matrix is formed with relative ease from data which is readily available. Furthermore, this matrix is well-suited for formation by a digital computer.<sup>15,16</sup>

Consider an  $\mathcal{L}$ -explicit primary system of equations for the  $v$ -vertex graph of Figure 3.5.1--where  $n=v-1$  is the number of N-elements,  $n_F$  is the number of F-elements, the F-element admittance matrix  $y_F$  is a complex diagonal matrix, and the subscripts N, F refer to the N-element and F-element subgraphs respectively:

$$\begin{array}{c} n \\ n_F \\ n_F \end{array} \begin{bmatrix} u_F & a_F & 0 & 0 \\ 0 & 0 & b_N & u_F \\ 0 & u_F & 0 & -y_F \end{bmatrix} \begin{bmatrix} l_N \\ l_F \\ r_N \\ r_F \end{bmatrix} = 0, \{ 2n_F+n, 2(n_F+n), 2n_F+n \} . \quad (3.5.12)$$

From (3.3.5)

$$b_N a' = [b_N \ u_F][u_N \ a_F]' = b_N + a'_F = 0 \quad (3.5.13)$$

or

$$b_N = -a'_F . \quad (3.5.14)$$

Using the above relation to eliminate  $b_N$  from (3.5.12):

$$\begin{bmatrix} u_N & a_F & 0 & 0 \\ 0 & 0 & -a'_F & u_F \\ 0 & u_F & 0 & -y_F \end{bmatrix} \begin{bmatrix} l_N \\ l_F \\ r_N \\ r_F \end{bmatrix} = 0, \{ 2n_F+n, 2(n_F+n), 2n_F+n \} . \quad (3.5.15)$$

Upon premultiplying the coefficient matrix in (3.5.15) by the following non-singular matrix

$$\begin{bmatrix} 0 & y_F & u_F \\ 0 & u_F & 0 \\ u_N & -a_F y_F & -a_F \end{bmatrix} \quad (3.5.16)$$

one obtains, after a slight rearrangement of the variables, the following equivalent system of equations:

$$\begin{bmatrix} u_F & 0 & 0 & -y_F a'_F \\ 0 & u_F & 0 & -a'_F \\ 0 & 0 & u_N & a_F y_F a'_F \end{bmatrix} \begin{bmatrix} I_F \\ v_F \\ I_N \\ v_N \end{bmatrix} = 0, \{2n_F+n, 2(n_F+n), 2n_F+n\}. \quad (3.5.17)$$

Thus every solution of (3.5.17) is a solution of (3.5.12) and conversely.

Consider now the last set of  $n$  equations in (3.5.17):

$$[u_N \ y] \begin{bmatrix} I_N \\ v_N \end{bmatrix} = 0, \{n, 2n, n\} \quad (3.5.18)$$

where  $y = a_F y_F a'_F$ .

First, one notes that each solution of (3.5.17) certainly determines exactly one corresponding solution of (3.5.18); second, each solution of (3.5.18) determines exactly one corresponding solution of (3.5.17):

$$\begin{bmatrix} I_F \\ v_F \\ I_N \\ v_N \end{bmatrix} = \begin{bmatrix} 0 & y_F a'_F \\ 0 & a'_F \\ u_N & 0 \\ 0 & u_N \end{bmatrix} \begin{bmatrix} I_N \\ v_N \end{bmatrix}. \quad (3.5.19)$$

The systems of equations (3.5.17) and (3.5.18) are, in a sense, equivalent systems of equations since each solution of either determines exactly one corresponding solution of the other. Since one of the primary concerns in this investigation is to study the

properties of solutions of (3.5.12) in terms of the variables associated with the N-elements, then it is appropriate to examine the solutions of (3.5.18).

In order to consider the most general partition of the variables in (3.5.18) it is necessary to subdivide the set of N-elements into four subsets. Since each N-element is incident to exactly one non-reference vertex then the vertices of the graph are subdivided into five subsets--the reference vertex alone and four additional subsets, each corresponding to a distinct N-element subset. This necessitates a more detailed partitioning for the incidence-seg matrix:

$$a = \begin{bmatrix} u_{N1} & 0 & 0 & 0 & a_{F1} \\ 0 & u_{N2} & 0 & 0 & a_{F2} \\ 0 & 0 & u_{N3} & 0 & a_{F3} \\ 0 & 0 & 0 & u_{N4} & a_{F4} \end{bmatrix} \quad (3.5.20)$$

and the corresponding changes in (3.5.18):

$$\begin{matrix} & \begin{matrix} n_1 & n_2 & n_3 & n_4 & n_1 & n_2 & n_3 & n_4 \end{matrix} \\ \begin{matrix} n_1 \\ n_2 \\ n_3 \\ n_4 \end{matrix} & \begin{bmatrix} u_{N1} & 0 & 0 & 0 & y_{11} & y_{12} & y_{13} & y_{14} \\ 0 & u_{N2} & 0 & 0 & y_{21} & y_{22} & y_{23} & y_{24} \\ 0 & 0 & u_{N3} & 0 & y_{31} & y_{32} & y_{33} & y_{34} \\ 0 & 0 & 0 & u_{N4} & y_{41} & y_{42} & y_{43} & y_{44} \end{bmatrix} \end{matrix} \begin{bmatrix} l_{N1} \\ l_{N2} \\ l_{N3} \\ l_{N4} \\ \gamma_{N1} \\ \gamma_{N2} \\ \gamma_{N3} \\ \gamma_{N4} \end{bmatrix} = 0 \quad (3.5.21)$$

where  $n = v - 1 = \sum_{k=1}^4 n_k$  and  $n_k \geq 0$ ,

$$y_{ij} = a_{Fi} y_F a'_{Fj}, \quad i, j = 1, 2, 3, 4$$

Rearranging (3.5.21) to indicate the most general partition of the variables:

$$\begin{matrix} n_1 \\ n_2 \\ n_3 \\ n_4 \end{matrix} \begin{bmatrix} n_1 & n_2 & n_1 & n_3 \\ u_{N1} & 0 & y_{11} & y_{13} \\ 0 & u_{N2} & y_{21} & y_{23} \\ 0 & 0 & y_{31} & y_{33} \\ 0 & 0 & y_{41} & y_{43} \end{bmatrix} \begin{bmatrix} I_{N1} \\ I_{N2} \\ V_{N1} \\ V_{N3} \end{bmatrix} = - \begin{bmatrix} n_3 & n_4 & n_2 & n_4 \\ 0 & 0 & y_{12} & y_{14} \\ 0 & 0 & y_{22} & y_{24} \\ u_{N3} & 0 & y_{32} & y_{34} \\ 0 & u_{N4} & y_{42} & y_{44} \end{bmatrix} \begin{bmatrix} I_{N3} \\ I_{N4} \\ V_{N2} \\ V_{N4} \end{bmatrix}$$

(3.5.22)

From Definition 2.2.4 it follows that the above partition is a proper partition of the variables in (3.5.18) if and only if

$$n_1 = n_4 \quad (3.5.23)$$

and

$$\det \begin{bmatrix} y_{31} & y_{33} \\ y_{41} & y_{43} \end{bmatrix} \neq 0. \quad (3.5.24)$$

If this is the case, then a complete set of dependent variables consists of the  $n$  variables:

$$\{I_{N1}, I_{N2}, V_{N1}, V_{N3}\} \quad (3.5.25)$$

and the corresponding complete set of independent variables consists of the  $n$  variables:

$$\{I_{N3}, I_{N4}, \mathcal{V}_{N2}, \mathcal{V}_{N4}\}. \quad (3.5.26)$$

At this point the characterization of the  $N$ -elements can be specified with no danger of introducing inconsistencies; i. e., the graph can be considered to contain  $n_1$   $N_o$ -elements,  $n_2$   $N_e$ -elements,  $n_3$   $N_h$ -elements, and  $n_4$   $N_{eh}$ -elements.

As noted earlier, the condition  $n_1 = n_4$  requires that for each  $N_{eh}$ -element in the graph there must also be a distinct  $N_o$ -element. Moreover, there is a stronger and more useful interrelation between the  $N_{eh}$ -elements and the  $N_o$ -elements in a graph. Since  $\mathcal{Y}$  in (3.5.18) is a symmetric matrix, then in (3.5.21):

$$\mathcal{Y}_{ij} = \mathcal{Y}_{ji} \quad i, j = 1, 2, 3, 4. \quad (3.5.27)$$

Hence,

$$\det \begin{bmatrix} \mathcal{Y}_{31} & \mathcal{Y}_{33} \\ \mathcal{Y}_{41} & \mathcal{Y}_{43} \end{bmatrix} = \det \begin{bmatrix} \mathcal{Y}_{13} & \mathcal{Y}_{14} \\ \mathcal{Y}_{33} & \mathcal{Y}_{34} \end{bmatrix}. \quad (3.5.28)$$

However the necessary and sufficient conditions for

$$\{I_{N2}, I_{N4}, \mathcal{V}_{N3}, \mathcal{V}_{N4}\} \quad (3.5.29)$$

to be a complete set of dependent variables for (3.5.21) are that  $n_1 = n_4$  and that the second determinant in (3.5.28) be non-zero. Therefore, the set of variables in (3.2.25) is a complete set of

dependent variables for (3.5.21) if and only if the set of variables in (3.5.29) is also. Consequently, within a given allowable classification of the N-elements of a graph into the  $N_o$ -,  $N_e$ -,  $N_h$ -, and  $N_{eh}$ -classes, it is possible to interchange the  $N_o$ - and  $N_{eh}$ -classifications.

It is worthwhile to note once again that although the preceding discussion is concerned with the variables within a system of equations, it is the coefficient matrix which actually contains the necessary information and properties. In the next chapter these properties of the coefficient matrix are "reflected" back into corresponding properties of the graph.

## Chapter 4

### MAXIMUM TERM RANK SUBMATRICES OF $\mathcal{Y}$ AND CORRESPONDING F-ELEMENT SUBGRAPHS

#### 4.1. Introduction

In the preceding chapters rank properties of the coefficient matrix are used to define a proper partition of the variables within a system of holac equations. In Section 3.5 this definition is applied to a general partition of the variables within a system of holac equations associated with the graph correlate of an electric network:

$$[u_N \ y] \begin{bmatrix} \mathcal{I}_N \\ \mathcal{V}_N \end{bmatrix} = 0, \quad \{n, 2n, n\} \quad (4.1.1)$$

where

$$y = a_F y_F a_F' \quad (4.1.2)$$

Of the resulting necessary and sufficient conditions for the partition of (3.5.22) to be a proper partition, the first, (3.5.23), insures that the appropriate submatrices have the proper orders, while the second condition, (3.5.24), requires that a certain minor from  $\det \mathcal{Y}$  does not vanish. In a particular case this minor can be evaluated and the corresponding partition checked. Although this procedure provides a definite test, it gives little insight into the reasons why a particular partition either passed or failed the test.

Now  $Y$ , and hence all properties of  $Y$ , are dependent solely upon the subgraph of F-elements and the associated F-element admittance coefficients; in (4.1.2),  $A_F$  can be construed as a basis incidence-seg matrix of order  $(v-1)$  by  $n_F$  for the connected  $v$ -vertex,  $n_F$ -element subgraph of F-elements, and  $Y_F$  is the diagonal matrix of the F-element admittance coefficients. The partitioning of the N-element variables, as in (3.5.22), identifies the corresponding minor from  $\det Y$  which must be tested, but this is the extent of the effect of the N-elements in the partitioning and testing process. The following sections of this chapter are devoted to examining the composition of the matrix  $Y$  in (4.1.2) in order to establish interrelations between subgraphs of F-elements and non-vanishing minors of  $\det Y$ .

In general the expansion of a minor involves a summation of terms; thus a minor can vanish for one of two reasons--each term in the summation is zero, or the non-zero terms are such that their summation is zero. If the minor does not vanish then the summation of necessity contains non-vanishing terms. As shown later, the presence or absence of non-vanishing terms in the expansion of a minor of  $\det Y$  is directly related to the existence or non-existence, respectively, of certain subgraphs of F-elements. In anticipation of this result the following terminology is introduced:<sup>30</sup>

Definition 4.1.1. Term Rank of a Matrix

The term rank of a matrix is the order of the greatest minor containing a non-vanishing term in its expansion.

The following theorems can be utilized to check the term rank of a matrix:<sup>30</sup>

Theorem 4.1.1. The expansion of the determinant of a square matrix  $M$  of order  $r$  contains non-vanishing terms if and only if any  $k$  rows of  $M$  include non-vanishing entries  $m_{ij}$  from at least  $k$  columns,  $k = 1, 2, \dots, r$ .

Theorem 4.1.2. The term rank of a square matrix of order  $r$  is less than  $r$  if and only if there exists a zero submatrix of order  $m$  by  $n$  with  $m + n > r$ .

If a square matrix of order  $r$  has term rank  $r$  then its determinant may be non-zero for some sets of values for the entries or possibly for all sets of non-zero values for the entries. If the term rank is less than  $r$ , then the determinant vanishes for all sets of values for the entries.

Consider a minor of order  $r$  from  $\det Y$ . In either case-- direct evaluation of the minor, or determination of the rank of the corresponding submatrix using Theorem 4.1.1 or Theorem 4.1.2 it is necessary to form the matrix  $Y$ , or at least the appropriate submatrix, in order to test it; as the size and complexity of the graph increases the formation of the matrix itself becomes a significant problem. Furthermore this process provides no explicit information about the properties of the graph itself in relation to the partitioning problem although the graph of  $F$ -elements determines the properties of  $Y$ .

#### 4.2. The Binet-Cauchy Formula

A generalization of the Binet-Cauchy formula<sup>25</sup> provides a technique to establish an interrelation between subgraphs of  $F$ -elements and non-vanishing minors of  $\det \mathcal{Y}$ :

Let  $a, B$  be matrices of order  $r$  by  $n$  and  $n$  by  $q$  respectively, and let  $C = aB$ . Consider an arbitrary minor of order  $m$  from  $\det C$ :

$$\det C \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} \quad (4.2.1)$$

where

$$m \leq \min(r, q)$$

$$1 \leq i_1 < i_2 < \dots < i_m \leq r$$

$$1 \leq j_1 < j_2 < \dots < j_m \leq q.$$

Then, if  $1 \leq m \leq n$ :

$$\det C \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} = \sum_{1 \leq k_1 < k_2 < \dots < k_m \leq n} \det a \begin{pmatrix} i_1, i_2, \dots, i_m \\ k_1, k_2, \dots, k_m \end{pmatrix} \det B \begin{pmatrix} k_1, k_2, \dots, k_m \\ j_1, j_2, \dots, j_m \end{pmatrix} \quad (4.2.2)$$

or, if  $m > n$ :

$$\det C \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} = 0. \quad (4.2.3)$$

Now, let

$$D = Y_F A'_F \quad (4.2.4)$$

and consider any minor of order  $m$ ,  $1 \leq m \leq v-1$ , from  $\det Y$  where  $Y$  is given in (4.1.2). Applying the Binet-Cauchey formula, (4.2.2), twice:

$$\det Y \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} = \sum_{1 \leq k_1 < k_2 < \dots < k_m \leq n_F} \det A'_F \begin{pmatrix} i_1, i_2, \dots, i_m \\ k_1, k_2, \dots, k_m \end{pmatrix} \det D \begin{pmatrix} k_1, k_2, \dots, k_m \\ j_1, j_2, \dots, j_m \end{pmatrix} \quad (4.2.5)$$

and

$$\det D \begin{pmatrix} k_1, k_2, \dots, k_m \\ j_1, j_2, \dots, j_m \end{pmatrix} = \sum_{1 \leq \ell_1 < \ell_2 < \dots < \ell_m \leq n_F} \det Y_F \begin{pmatrix} k_1, k_2, \dots, k_m \\ \ell_1, \ell_2, \dots, \ell_m \end{pmatrix} \det A'_F \begin{pmatrix} \ell_1, \ell_2, \dots, \ell_m \\ j_1, j_2, \dots, j_m \end{pmatrix} \quad (4.2.6)$$

Since  $Y_F$  is a nonsingular, diagonal matrix then the only non-vanishing minors are principal minors; thus the summation in (4.2.6) contains at most one non-vanishing term--corresponding to the case when  $\ell_1 = k_1, \ell_2 = k_2, \dots, \ell_m = k_m$ . Further

$$\det Y_F \begin{pmatrix} k_1, k_2, \dots, k_m \\ k_1, k_2, \dots, k_m \end{pmatrix} = Y_{k_1} Y_{k_2} \dots Y_{k_m} \quad (4.2.7)$$

and

$$\det a'_F \begin{pmatrix} k_1, k_2, \dots, k_m \\ j_1, j_2, \dots, j_m \end{pmatrix} = \det a_F \begin{pmatrix} j_1, j_2, \dots, j_m \\ k_1, k_2, \dots, k_m \end{pmatrix} . \quad (4.2.8)$$

Combining the last four relations:

$$\det y \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} = \sum_{1 \leq k_1 < k_2 < \dots < k_m \leq n_F} Y_{k_1} Y_{k_2} \dots Y_{k_m} \det a_F \begin{pmatrix} i_1, i_2, \dots, i_m \\ k_1, k_2, \dots, k_m \end{pmatrix} \det a_F \begin{pmatrix} j_1, j_2, \dots, j_m \\ k_1, k_2, \dots, k_m \end{pmatrix} . \quad (4.2.9)$$

Examination of (4.2.9) indicates that the summation contains a total of

$$\binom{n_F}{m} = \frac{n_F!}{m! (n_F - m)!} \quad (4.2.10)$$

terms, and that each term is composed of two types of factors. The first factor is a product of  $n$  of the F-element admittance coefficients; for the type of F-elements considered, each admittance coefficient is finite and non-zero, hence this factor is always finite and non-zero. In addition, this factor involves a distinct set of  $m$  F-elements, i. e., no two terms in the summation involve the same set of  $m$  F-elements. It is also noted that this factor depends solely upon the admittance coefficients and is independent of the manner in which the F-elements are interconnected. The second factor in each term

is the product of two minors from the incidence-seg matrix and has a value of +1, -1, or zero since the value of any minor of an incidence-seg matrix is +1, -1, or 0.<sup>11</sup> This factor, in contrast with the first type, depends solely upon the manner in which the F-elements are interconnected and is independent of the F-element admittance coefficients. Thus connection patterns of F-elements determine whether or not the summation in (4.2.9) contains non-vanishing terms:

Theorem 4.2.1. The  $m$  by  $m$  submatrix,  $1 \leq m \leq v-1$ ,

$$y \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} \quad (4.2.11)$$

in (4.2.9) has term rank  $m$  if and only if there exists at least one  $m$ -element subgraph of F-elements such that

$$a_F \begin{pmatrix} i_1, i_2, \dots, i_m \\ k_1, k_2, \dots, k_m \end{pmatrix} \quad \text{and} \quad a_F \begin{pmatrix} j_1, j_2, \dots, j_m \\ k_1, k_2, \dots, k_m \end{pmatrix} \quad (4.2.12)$$

are both nonsingular.

#### 4.3. Nonsingular Submatrices of the Complete Incidence-seg Matrix and Corresponding Subgraphs

Consider a graph  $G_0$  which is connected, i. e. a part, and consists of  $e_0$  elements and  $v_0$  vertices. An incidence-seg matrix for  $G_0$  is formed by mapping the element-vertex incidence pattern of the graph into a matrix. The complete incidence-seg

matrix  $A_a$  for  $G_0$  is a matrix of order  $v_0$  by  $e_0$  where the typical entry  $a_{ij}$  is defined as follows:<sup>10</sup>

$$a_{ij} = \begin{cases} +1, & \text{if element } e_j \text{ is incident to vertex } v_i \text{ and oriented} \\ & \text{away from this vertex;} \\ -1, & \text{if element } e_j \text{ is incident to vertex } v_i \text{ and oriented} \\ & \text{toward this vertex;} \\ 0, & \text{if element } e_j \text{ is not incident to vertex } v_i. \end{cases}$$

Under this mapping each row of  $A_a$  corresponds to a distinct vertex of  $G_0$  and each column of  $A_a$  corresponds to a distinct element of  $G_0$ . Since the vertex and element numbers are arbitrary it is assumed that the vertex and element numbers correspond to the row and column indices, respectively of  $A_a$ .

Let:

$V_0$  denote the set of all vertices of  $G_0$ ,

$E_0$  denote the set of all elements of  $G_0$ ,

$V_m$  denote a proper subset of  $V_0$  consisting of  $m$  distinct vertices,

$E_m$  denote a proper subset of  $E_0$  consisting of  $m$  distinct elements, and

$V(E_m)$  denote the set of vertices incident to the elements in  $E_m$ .

Corresponding to any  $m$  by  $m$  submatrix of  $A_a$  is a set of  $m$  distinct vertices and a set of  $m$  distinct elements of  $G_0$ . This correspondence is denoted by the following notation:

$$A_a \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} = A_a \begin{pmatrix} V_m \\ E_m \end{pmatrix} \quad (4.3.1)$$

where

$$V_m = \{v_{i1}, v_{i2}, \dots, v_{im}\}$$

$$E_m = \{e_{j1}, e_{j2}, \dots, e_{jm}\} .$$

Also associated with this submatrix is a second vertex set; namely,  $V(E_m)$ .

The following two theorems characterize sets of linearly independent rows and columns of  $a_a$ :

Theorem 4.3.1. If  $V_m$  is any subset of  $m$  distinct vertices of  $G_o$ ,  $1 \leq m \leq v_o - 1$ , then the  $m$  by  $e_o$  submatrix

$$a_a \begin{pmatrix} V_m \\ E_o \end{pmatrix} \quad (4.3.2)$$

has rank  $m$ .

Theorem 4.3.2. Let  $E_m$  be any  $m$ -element subgraph of  $G_o$ ,  $1 \leq m \leq v_o - 1$ . The  $v_o$  by  $m$  submatrix

$$a_a \begin{pmatrix} V_o \\ E_m \end{pmatrix} \quad (4.3.3)$$

has rank  $m$  if and only if  $E_m$  contains no circuits.

Consider an arbitrary  $m$  by  $m$  submatrix of  $a_a$ ,  $1 \leq m \leq v_o - 1$ :

$$a_a \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} = a_a \begin{pmatrix} V_m \\ E_m \end{pmatrix} \quad (4.3.4)$$

where

$$V_m = \{v_{i1}, v_{i2}, \dots, v_{im}\} \quad (4.3.5)$$

$$E_m = \{e_{j1}, e_{j2}, \dots, e_{jm}\} . \quad (4.3.6)$$

Theorems 4.3.1 and 4.3.2 provide necessary conditions for the submatrix (4.3.4) to be nonsingular. Theorem 4.3.1 is certainly satisfied; if the subgraph  $E_m$  contains no circuits then the submatrix, (4.3.3), of order  $v_0$  by  $m$  has rank  $m$ . Therefore there exists at least one  $m \times m$  submatrix of (4.3.3) which is nonsingular. However this nonsingular submatrix may or may not be the one in (4.3.4). The following theorem gives necessary and sufficient conditions, in terms of the subgraph  $E_m$  and the vertex set  $V_m$ , such that the submatrix (4.3.4) is nonsingular:

Theorem 4.3.3. If and only if: (1)  $E_m$  contains no circuits, and (2) each part of  $E_m$  contains exactly one vertex  $v^* \in V(E_m)$  such  $v^* \notin V_m$ , then the submatrix (4.3.4) is nonsingular.

**Proof:** Let  $E_m$  and  $V_m$  be given, where the subgraph  $E_m$  consists of  $m$  elements,  $p$  parts, and the vertex set  $V(E_m)$  contains  $x$  vertices. Let the  $i$ -th part of  $E_m$  contain  $m_i$  elements and  $x_i$  vertices, where

$$m_1 + m_2 + \dots + m_p = m \quad (4.3.7)$$

$$x_1 + x_2 + \dots + x_p = x \quad (4.3.8)$$

since a part and its complement have no elements or no vertices in common. (a) Sufficient. Let  $E_m$  contain no circuits and each part of  $E_m$  contain exactly one vertex  $v^* \in V(E_m)$  such that  $v^* \notin V_m$ . Because  $E_m$  contains no circuits, then each part of  $E_m$  contains no circuits and:

$$m_i - x_i + 1 = 0 \quad i = 1, 2, \dots, p \quad (4.3.9)$$

or

$$x_i = m_i + 1 \quad i = 1, 2, \dots, p. \quad (4.3.10)$$

Each part of  $E_m$  contains exactly one vertex  $v^* \notin V_m$ , thus each part contains exactly  $m_i$  vertices from  $V_m$ . From (4.3.7) it follows that  $V_m$  is a proper subset of  $V(E_m)$ . Construct an incidence-seg matrix  $a_i$  of order  $m_i$  by  $m_i$  for the  $i$ -th part of  $E_m$ ; the omitted row corresponding to that vertex of part  $i$  which is not a member of  $V_m$ . Since each part is a tree then the rank of  $a_i$  is  $m_i$ . By proper ordering of the elements and vertices, an incidence-seg matrix,  $a^*$ , for  $E_m$  can be written as a block diagonal matrix:

$$a^* = \begin{matrix} & m_1 & \dots & m_i & \dots & m_p \\ \begin{matrix} m_1 \\ \vdots \\ m_i \\ \vdots \\ m_p \end{matrix} & \left[ \begin{array}{cccc} a_1 & \dots & 0 & \dots & 0 \\ \vdots & & \vdots & & \vdots \\ 0 & \dots & a_i & \dots & 0 \\ \vdots & & \vdots & & \vdots \\ 0 & \dots & 0 & \dots & a_p \end{array} \right] & \cdot & \end{matrix} \quad (4.3.11)$$

Hence,  $a^*$  is an  $m \times m$  matrix and has rank  $m$ . The  $m$  rows of  $a^*$  correspond to the vertices in  $V_m$ , the  $m$  columns of  $a^*$

correspond to the  $m$ -elements in  $E_m$ , and

$$a_a \begin{pmatrix} V_m \\ E_m \end{pmatrix} = P_1 a^* P_2 \quad (4.3.12)$$

where  $P_1, P_2$  are conformable permutation matrices and thus nonsingular. Therefore,  $a_a \begin{pmatrix} V_m \\ E_m \end{pmatrix}$  is nonsingular. (b) Necessary. Let  $a_a \begin{pmatrix} V_m \\ E_m \end{pmatrix}$  be nonsingular. Since a nonsingular matrix contains no zero rows or columns, then every vertex in  $V_m$  is incident to at least one element of  $E_m$  and each element of  $E_m$  is incident to at least one vertex from  $V_m$ . Thus  $V_m$  is a subset of  $V(E_m)$ . Further, the columns of this submatrix are linearly independent, thus  $E_m$  contains no circuits and

$$x = m + p. \quad (4.3.13)$$

Therefore  $V_m$  is a proper subset of  $V(E_m)$ , and  $V(E_m)$  must contain exactly  $p$  distinct vertices which are not members of  $V_m$ . There exist permutation matrices  $P_3$  and  $P_4$  such that

$$P_3 a_a \begin{pmatrix} V_m \\ E_m \end{pmatrix} P_4 = \begin{bmatrix} a_1 & \dots & 0 & \dots & 0 \\ \vdots & & \vdots & & \vdots \\ 0 & \dots & a_i & \dots & 0 \\ \vdots & & \vdots & & \vdots \\ 0 & \dots & 0 & \dots & a_p \end{bmatrix}$$

$$(4.3.14)$$

where the  $m_i$  columns of  $a_i$  correspond to the elements of  $E_m$  in part  $i$  and the rows of  $a_i$  correspond to the vertices of  $V_m$  in part  $i$  -- note that at this time the number of rows in  $a_i$  is not

known to be  $m_i$ . Suppose that all of the  $m_i+1$  vertices of part  $i$  are members of  $V_m$ . Then  $A_i$  is a complete incidence-seg matrix for part  $i$  and thus the rows of  $A_i$  are linearly dependent. Therefore the rows of  $A_a \begin{pmatrix} V_m \\ E_m \end{pmatrix}$  are linearly dependent and the matrix is singular. As  $A_a \begin{pmatrix} V_m \\ E_m \end{pmatrix}$  is nonsingular then each part of  $E_m$  must contain at least one vertex which is not a member of  $V_m$ . But  $V(E_m)$  contains exactly  $p$  vertices which are not members of  $V_m$ ; since each of the  $p$  parts must contain at least one, then each part of  $E_m$  must contain exactly one vertex which is not a member of  $V_m$ . q. e. d.

Subgraphs which contain no circuits, such as  $E_m$  in Theorem 4.3.3, are closely related to another class of subgraphs which are defined as follows:<sup>32</sup>

Definition 4.3.1. k-tree

A  $k$ -tree,  $T_k$ , of a  $v_0$ -vertex part  $G_0$  is a subgraph of  $G_0$  which contains  $k$  parts, all  $v_0$  vertices of  $G_0$ , and no circuits. (Note: in this definition one must allow the possibility that a part may consist of an isolated vertex.)

Theorem 4.3.4.<sup>32</sup> Let  $G_0$  be a part with  $v_0$  vertices, then:

- (1) A  $k$ -tree of  $G_0$  contains  $v_0-k$  elements,  $1 \leq k \leq v_0$ ;
- (2) A subgraph of  $G_0$  which contains  $v_0$  vertices,  $v_0-k$  elements, and no circuits is a  $k$ -tree of  $G_0$ .

Thus, if  $V(E_m) = V_0$  then  $E_m$  is a  $(v_0-m)$ -tree of  $G_0$ ; if  $V(E_m)$

is a proper subset of  $V_0$ , then  $E_m$  differs from a  $(v_0 - m)$ -tree by a set of isolated vertices--namely those vertices of  $V_0$  which are not contained in  $V(E_m)$ .

Definition 4.3.2. Basis for a k-tree

The subgraph of a k-tree  $T_k$  consisting of the  $v_0 - k$  elements is designated as the basis for that k-tree and denoted by  $T_k(E_{v_0 - k})$ .

Theorem 4.3.5. Let  $G_0$  be a part containing  $v_0$  vertices then any subgraph of  $G_0$  containing  $v_0 - k$  elements,  $1 \leq k \leq v_0$ , and no circuits is the basis for some k-tree of  $G_0$ .

In order to characterize the subgraphs of Theorem 4.3.3, which correspond to nonsingular submatrices of the complete incidence-seg matrix, one additional concept is required:

Definition 4.3.3. k-tree pair

Let  $G_0$  be a part containing  $v_0$  vertices, and  $V_{v_0 - k}$  and  $E_{v_0 - k}$  be any subset of  $v_0 - k$  distinct vertices and  $v_0 - k$  distinct elements of  $G_0$ , respectively.  $\{V_{v_0 - k}, E_{v_0 - k}\}$  is said to be a k-tree pair if and only if  $E_{v_0 - k}$  is the basis for some k-tree  $T_k$ , and each part of  $T_k(E_{v_0 - k})$  contains exactly one vertex  $v^*$  such that  $v^*$  is not a member of  $V_{v_0 - k}$ .

Therefore Theorem 4.3.3 can be restated as follows:

Theorem 4.3.6.

$a_a \begin{pmatrix} V_m \\ E_m \end{pmatrix}$  is nonsingular if and only if  $\{V_m, E_m\}$  is a  $(v_o - m)$ -tree pair.

For a given  $e_o$ -element,  $v_o$ -vertex part  $G_o$  it is of interest to determine the number of  $(v_o - m)$ -tree pairs that exist for either a fixed set of  $m$  vertices of  $G_o$  or a fixed set of  $m$  elements of  $G_o$ , where  $1 \leq m \leq v_o - 1$ .

Theorem 4.3.7. Let  $V_m$  be any fixed set of  $m$  distinct vertices of  $G_o$ ,  $1 \leq m \leq v_o - 1$ , and let  $n_E$  be the number of distinct sets of  $m$  elements of  $G_o$ ,  $E_{m_i}$ , for which  $\{V_m, E_{m_i}\}$  is a  $(v_o - m)$ -tree pair, then

$$n_E = \det \left\{ a_a \begin{pmatrix} V_m \\ E_o \end{pmatrix} a'_a \begin{pmatrix} E_o \\ V_m \end{pmatrix} \right\}. \quad (4.3.15)$$

Proof: Using the Binet-Cauchy formula:

$$\det \left\{ a_a \begin{pmatrix} V_m \\ E_o \end{pmatrix} a'_a \begin{pmatrix} E_o \\ V_m \end{pmatrix} \right\} = \sum_{E_{m_i}} \det a_a \begin{pmatrix} V_m \\ E_{m_i} \end{pmatrix} \det a'_a \begin{pmatrix} E_{m_i} \\ V_m \end{pmatrix} \quad (4.3.16)$$

$$= \sum_{E_{m_i}} \left\{ \det a_a \begin{pmatrix} V_m \\ E_{m_i} \end{pmatrix} \right\}^2 \quad (4.3.17)$$

where  $E_{m_i}$  ranges over all distinct  $m$ -element combinations of the

$e_0$  elements of  $G_0$ . The determinant in (4.3.17) has the value +1, or -1, if and only if  $\{V_m, E_{m_i}\}$  is a  $(v_0 - m)$ -tree pair and hence the result follows. The following theorem is proved in a similar manner:

Theorem 4.3.8. Let  $E_m$  be any fixed set of  $m$  elements of  $G_0$ ,  $1 \leq m \leq v_0 - 1$ , and let  $n_V$  be the number of distinct sets of  $m$  distinct vertices of  $G_0$ ,  $V_{m_i}$ , for which  $\{V_{m_i}, E_m\}$  is a  $(v_0 - m)$ -tree pair, then

$$n_V = \det \left\{ a_a' \begin{pmatrix} E_m \\ V_0 \end{pmatrix} a_a \begin{pmatrix} V_0 \\ E_m \end{pmatrix} \right\}. \quad (4.3.18)$$

As a direct consequence of theorem 4.3.2:

Corollary 4.3.9. The number  $n_V$  in Theorem 4.3.8 is zero if and only if  $E_m$  contains a circuit.

#### 4.4. Maximum Term Rank Submatrices of $\mathcal{Y}$ and Corresponding Subgraphs

Necessary and sufficient conditions for an arbitrary  $m$  by  $m$  submatrix of  $\mathcal{Y}$  to have term rank  $m$  are stated in Theorem 4.2.1 in terms of nonsingular submatrices of an incidence-seg matrix. If this theorem is combined with Theorem 4.3.6 these conditions can be stated in terms of properties of subgraphs.

Let  $G_0$  be a part containing  $n_F$  F-elements and  $v_0$  vertices; consider an arbitrary  $m$  by  $m$  submatrix,  $1 \leq m \leq v_0 - 1$ , from the matrix  $\mathcal{Y}$  in (4.1.2):

$$\mathcal{Y} \begin{pmatrix} i_1, i_2, \dots, i_m \\ j_1, j_2, \dots, j_m \end{pmatrix} \quad (4.4.1)$$

The relation (4.2.9) establishes a correspondence between the row and column indices in (4.4.1) and two sets of row indices from the incidence-seg matrix; thus one can associate two sets of  $m$  distinct vertices from  $G_0$  with the submatrix in (4.4.1):

$$V_{m_i} = \{ v_{i1}, v_{i2}, \dots, v_{im} \} \quad (4.4.2)$$

and

$$V_{m_j} = \{ v_{j1}, v_{j2}, \dots, v_{jm} \} . \quad (4.4.3)$$

Theorem 4.4.1. The  $m$  by  $m$  submatrix

$$\mathcal{Y} \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix} \quad (4.4.4)$$

in (4.4.1) has term rank  $m$  if and only if there exists at least one  $m$ -element subgraph  $E_m$  of  $G_0$  such that  $\{ V_{m_i}, E_m \}$  and  $\{ V_{m_j}, E_m \}$  are both  $(v_0 - m)$ -tree pairs for  $G_0$ .

Corollary 4.4.2. The  $m$  by  $m$  submatrix  $\mathcal{Y} \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix}$  has term rank  $m$  if and only if  $\mathcal{Y} \begin{pmatrix} V_{m_j} \\ V_{m_i} \end{pmatrix}$  has term rank  $m$ .

Although Theorem 4.4.1 relates term rank to properties of subgraphs it is instructive to examine the stated conditions in more detail in order to extract additional information characterizing the type of subgraph  $E_m$  meeting these requirements.

The basis incidence-seg matrix  $A_F$  in (4.1.2) is derived from the complete incidence-seg matrix  $A_a$  by deleting the row corresponding to the reference vertex  $r_o$ ; thus  $r_o$  is never contained in either  $V_{m_i}$  or  $V_{m_j}$ . Therefore, for a given  $V_{m_i}$  and  $V_{m_j}$ , the vertex set of  $G_o$ :

$$V_o = \{v_1, v_2, \dots, v_{v_o-1}, r_o\}, \quad (4.4.5)$$

is partitioned into these proper subsets:  $V_{m_i}$ ,  $V_{m_j}$ , and the subset consisting of all vertices of  $V_o$  which are not contained in either  $V_{m_i}$  or  $V_{m_j}$ . The latter subset always contains at least one member--the reference vertex  $r_o$ . Although  $V_{m_i}$  contains  $m$  distinct vertices, as does  $V_{m_j}$ , it is possible for the composition of these two sets to vary from that of identical sets to that of disjoint sets.

If the vertex sets  $V_{m_i}$  and  $V_{m_j}$  are identical, then it is necessary and sufficient that there exists an  $m$ -element subgraph  $E_m$  such that  $\{V_{m_i}, E_m\}$  is a  $(v_o-m)$ -tree pair:  $E_m$  must contain no circuits and each part of  $E_m$  must contain exactly one vertex which is not contained in  $V_{m_i}$ . For a given graph  $G_o$ , and a given vertex set  $V_{m_i}$ , these conditions can be applied and it can be determined whether or not one or more allowable subgraphs exist. Alternately, one could utilize (4.3.15) to determine  $n_E$ , the number of  $m$ -element subgraphs such that  $\{V_{m_i}, E_m\}$  is a  $(v_o-m)$ -tree pair. Hence the term rank of  $\mathcal{Y}\left(\begin{smallmatrix} V_{m_i} \\ V_{m_i} \end{smallmatrix}\right)$  is  $m$  if and only if  $n_E \neq 0$ .

If the vertex sets  $V_{m_i}$  and  $V_{m_j}$  are not identical, then  $G_o$  must be searched for allowable  $m$ -element subgraphs such that both  $\{V_{m_i}, E_m\}$  and  $\{V_{m_j}, E_m\}$  are  $(v_o - m)$ -tree pairs. Unfortunately no formula has been found from which to calculate the number of distinct  $m$ -element subgraphs that satisfy both of these conditions. A determinant:

$$\det \left\{ a_a \begin{pmatrix} V_{m_i} \\ E_o \end{pmatrix} \quad a'_a \begin{pmatrix} E_o \\ V_{m_j} \end{pmatrix} \right\}, \quad (4.4.6)$$

similar to that used in (4.3.15), can be formed and evaluated. Application of the Binet-Cauchy formula indicates that the non-zero terms in the expansion,  $+1$  or  $-1$ , do correspond to allowable subgraphs; however, the heterogeneous pattern of signs which may occur allow one to conclude in general that if there are  $t$  non-vanishing terms in the expansion, then the value of the determinant might range from  $+t$  to  $-t$  and including zero. If the value of the determinant in (4.4.6) is  $n$ , then there are at least  $|n|$  distinct  $m$ -element subgraphs  $E_{m_k}$  such that  $\{V_{m_i}, E_{m_k}\}$  and  $\{V_{m_j}, E_{m_k}\}$  are both  $(v_o - m)$ -tree pairs. Therefore  $n \neq 0$  is sufficient for the term rank of  $y \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix}$  to be  $m$ , but it is not necessary.

Consider the type of subgraph  $E_m$  for which both  $\{V_{m_i}, E_m\}$  and  $\{V_{m_j}, E_m\}$  are  $(v_o - m)$ -tree pairs when  $V_{m_i}$  and  $V_{m_j}$  are not identical. In addition to containing no circuits, each part of  $E_m$  must contain exactly one vertex which is not contained in  $V_{m_i}$  and exactly one vertex which is not contained in  $V_{m_j}$ . If  $V_{m_i}$  and

$V_{m_j}$  are disjoint then, since each part of  $E_m$  contains at least two vertices, each part must contain exactly two vertices--one from  $V_{m_i}$  and one from  $V_{m_j}$ . The  $m$ -element subgraph  $E_m$  must consist of  $m$  parts; each part is a single element incident to one vertex from  $V_{m_i}$  and one vertex from  $V_{m_j}$ . Thus, if  $V_{m_i}$  and  $V_{m_j}$  are disjoint, the  $m$ -element,  $m$ -part subgraph can be viewed as matching the vertices of  $V_{m_i}$  onto the vertices of  $V_{m_j}$  in a one-to-one manner. Therefore, when  $V_{m_i}$  and  $V_{m_j}$  are disjoint,  $y \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix}$  has term rank  $m$  if and only if at least one such matching subgraph exists in  $G_0$ .

Suppose the vertex sets  $V_{m_i}$  and  $V_{m_j}$  are neither identical nor disjoint. Then the vertex set  $V_0$  in (4.4.5) is partitioned into four mutually exclusive, all inclusive, non-empty subsets:  $S_1$ ,  $S_2$ ,  $S_3$ , and  $S_4$ --see Figure 4.4.1.

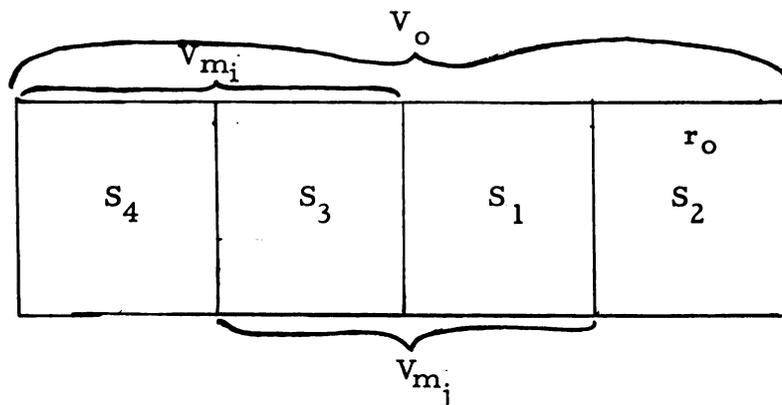


Figure 4.4.1. Vertex Partition.

Consider a subgraph  $E_m$  which contains no circuits; let  $P_i$  be any part of  $E_m$  and  $V(P_i)$  be the set of vertices in  $P_i$ . If  $\{V_{m_i}, E_m\}$  is a  $(v_0 - m)$ -tree pair then there is exactly one vertex  $a \in V(P_i)$  such that  $a \notin V_{m_i}$ ; therefore

$$a \in S_1 \quad \text{or} \quad a \in S_2, \quad (4.4.7)$$

and for any vertex  $c \in V(P_i)$ ,  $c \neq a$ , then  $c \in V_{m_i}$ :

$$c \in S_3 \quad \text{or} \quad c \in S_4. \quad (4.4.8)$$

If  $\{V_{m_j}, E_m\}$  is a  $(v_0 - m)$ -tree pair then there is exactly one vertex  $b \in V(P_i)$  such that  $b \notin V_{m_j}$ ; therefore

$$b \in S_2 \quad \text{or} \quad b \in S_4, \quad (4.4.9)$$

and for any vertex  $c \in V(P_i)$ ,  $c \neq b$ , then  $c \in V_{m_j}$ :

$$c \in S_1 \quad \text{or} \quad c \in S_3. \quad (4.4.10)$$

These conditions must all be satisfied if  $E_m$  is to be an allowable subgraph. Note that  $a$  and  $b$  are particular vertices from  $V(P_i)$  and that  $c$  is any vertex of  $V(P_i)$ ,  $c \neq a$ ,  $c \neq b$ ; therefore: if  $a = b$ , then

$$a \in S_2 \quad \text{and} \quad c \in S_3; \quad (4.4.11)$$

if  $a \neq b$ , then

$$a \in S_1 \quad \text{and} \quad b \in S_4 \quad \text{and} \quad c \in S_3. \quad (4.4.12)$$

In the case where  $V_{m_i}$  and  $V_{m_j}$  are neither identical nor disjoint and both  $\{V_{m_i}, E_m\}$ ,  $\{V_{m_j}, E_m\}$  are  $(v_0 - m)$ -tree pairs then  $E_m$  must contain  $m$  elements and no circuits;  $V(E_m)$

must contain all of the vertices of  $V_{m_i}$ ,  $V_{m_j}$ --and perhaps other vertices; each part  $P_i$  of  $E_m$  must also satisfy either one of the following criteria:

Criterion A:  $P_i$  must contain exactly one vertex which is not contained in either  $V_{m_i}$  or  $V_{m_j}$ , and all remaining vertices of  $P_i$  must be contained in both  $V_{m_i}$  and  $V_{m_j}$ ;

Criterion B:  $P_i$  must contain exactly one vertex which is contained in  $V_{m_i}$  but not contained in  $V_{m_j}$  and exactly one vertex which is contained in  $V_{m_j}$  but not contained in  $V_{m_i}$ ; all remaining vertices of  $P_i$  must be contained in both  $V_{m_i}$  and  $V_{m_j}$ .

Further, if the number of vertices in  $S_4$ , and hence  $S_1$ , is  $x_1$ , then  $E_m$  must contain at least  $x_1$  parts.

The subgraphs of Figure 4.4.2 illustrate, for the case  $m = 2$ , all possible types of two element subgraphs  $E_{2k}$  such that both  $\{V_{2i}, E_{2k}\}$  and  $\{V_{2j}, E_{2k}\}$  are  $(v_0 - 2)$ -tree pairs. The unlabeled vertices in the Figure can be any other vertices of the graph. For subgraphs (a) - (d):  $V_{2i} = V_{2j} = \{v_1, v_2\}$ ; (e) - (h):  $V_{2i} = \{v_1, v_2\}$ ,  $V_{2j} = \{v_2, v_3\}$ ; (i) and (j):  $V_{2i} = \{v_1, v_2\}$ ,  $V_{2j} = \{v_3, v_4\}$ . Consequently, for a connected graph  $G_0$  containing at least four vertices:  $\gamma \begin{pmatrix} 1, 2 \\ 2, 3 \end{pmatrix}$  has term rank two if and only if  $G_0$  contains at least one of the subgraphs (e) - (h) of Figure 4.4.2.

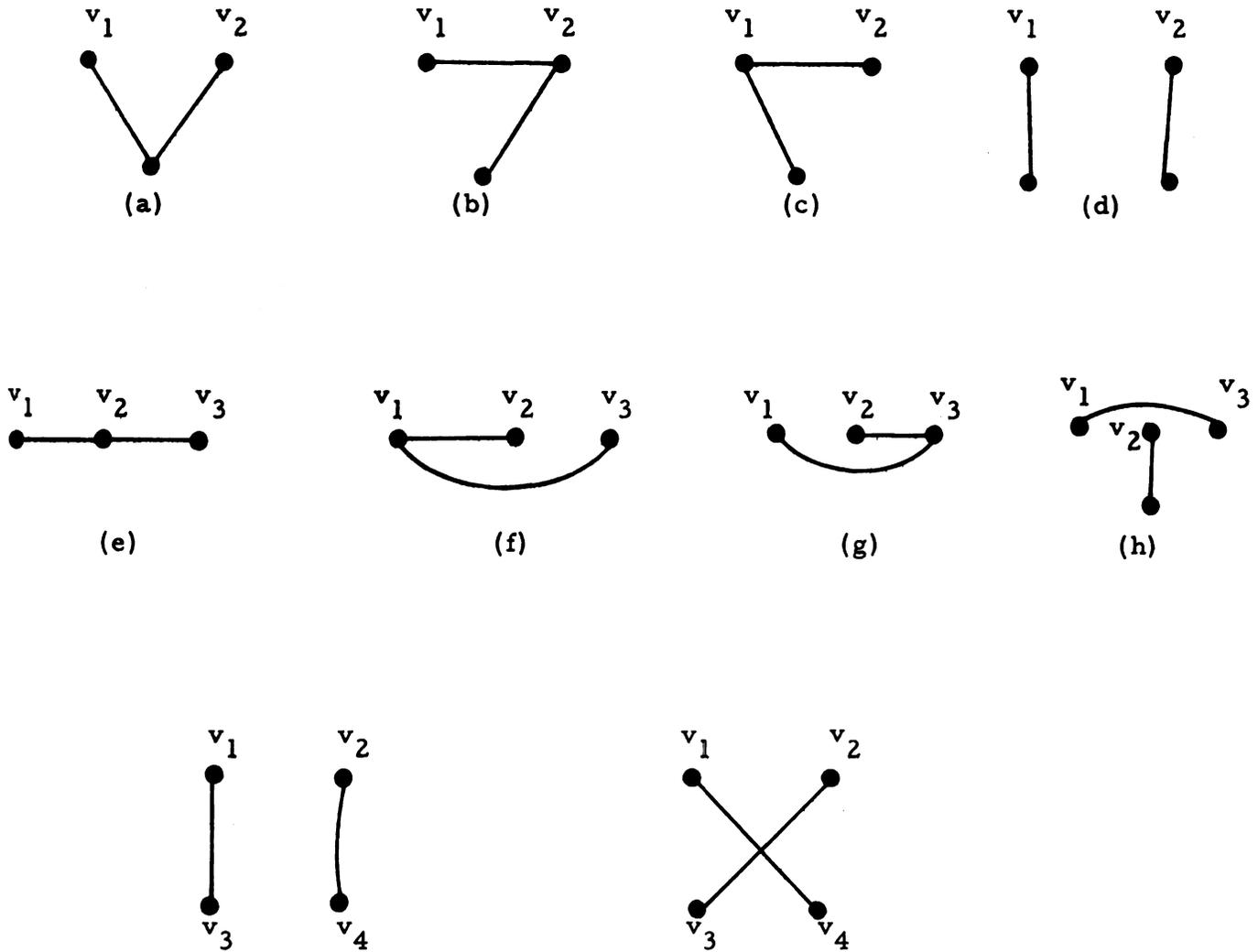


Figure 4.4.2. Allowable Subgraphs,  $m = 2$ .

Assuming that at least one allowable  $E_m$  has been found for a given  $V_{m_i}$  and  $V_{m_j}$  then, using criterion A and B in conjunction with an examination of the allocation of the vertices from  $V_{m_i}$ ,  $V_{m_j}$  within the parts of  $E_m$ , it is possible to determine whether or not certain vertices can be interchanged between  $V_{m_i}$ ,  $V_{m_j}$  and still maintain the  $(v_0-m)$ -tree pair property for  $E_m$ . If, for example, in determining the term rank of  $y \begin{pmatrix} 1, 2 \\ 2, 3 \end{pmatrix}$  one finds at least subgraph (e) of Figure 4.4.2 within  $G_0$ , then all of the following submatrices also have term rank two:

$$y \begin{pmatrix} 1, 2 \\ 2, 3 \end{pmatrix}, y \begin{pmatrix} 2, 3 \\ 1, 2 \end{pmatrix}, y \begin{pmatrix} 1, 3 \\ 2, 3 \end{pmatrix},$$

$$y \begin{pmatrix} 2, 3 \\ 1, 3 \end{pmatrix}, y \begin{pmatrix} 1, 2 \\ 1, 3 \end{pmatrix}, y \begin{pmatrix} 1, 3 \\ 1, 2 \end{pmatrix}. \quad (4.4.13)$$

If, on the other hand, examination of  $G_0$  indicates that the only allowable subgraph contained in  $G_0$  has the form (h) of Figure 4.4.2, then only the first two submatrices in (4.4.13) have term rank two; the term rank of the last four submatrices is less than two.

The existence or non-existence of at least one allowable subgraph  $E_m$  for a given pair of vertex sets  $V_{m_i}$  and  $V_{m_j}$  can be checked by direct inspection of the graph. If the graph contains a large number of vertices and elements then this can become a time consuming process. Various algorithms have been devised

and programmed to utilize a digital computer to search for numerous types of subgraphs--trees, k-trees, circuits, paths, etc. --within a given graph.<sup>36-40</sup> Programs of this type could be modified, or new programs devised, to implement a testing process. Consequently, this aspect is not considered further in this investigation.

In the event that all allowable subgraphs have been found-- as might well be the case when a computer search program is used--then (4.2.9) can be used to evaluate the minor of  $Y$  without the necessity of actually forming the matrix  $Y$ . On the assumption that  $Y \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix}$  has term rank  $m$ , then two cases arise: (1) if  $V_{m_i}$  and  $V_{m_j}$  are identical; i. e. a principal minor of  $Y$ , then the non-vanishing minors of the incidence-seg matrix in (4.2.9) have the same sign within each term and (4.2.9) becomes:

$$\det Y \begin{pmatrix} V_{m_i} \\ V_{m_i} \end{pmatrix} = \sum_{E_{m_k}} Y(E_{m_k}) \quad (4.4.14)$$

where  $Y(E_{m_k})$  is the product of the F-element admittance coefficients for the elements of  $E_{m_k}$  and the summation ranges over all  $E_{m_k}$  such that  $\{V_{m_i}, E_{m_k}\}$  is a  $(v_0 - m)$ -tree pair; (2) If  $V_{m_i}$  and  $V_{m_j}$  are not identical then the evaluation of the minor is complicated by the fact that the non-vanishing minors of the incidence-seg matrix in (4.2.9) can have either sign within a given term. A formula for the signs of the non-vanishing terms has been derived and the result is given below.

Let

$$V_{m_i} = \{ v_{i1}, v_{i2}, \dots, v_{im} \} \quad (4.4.15)$$

and

$$V_{m_j} = \{ v_{j1}, v_{j2}, \dots, v_{jm} \} \quad (4.4.16)$$

where

$$1 \leq i_1 < i_2 < \dots < i_m \leq v_o - 1$$

$$1 \leq j_1 < j_2 < \dots < j_m \leq v_o - 1$$

Since  $V_{m_i}$  and  $V_{m_j}$  are not identical, then the subsets  $S_1$  and  $S_4$  in Figure 4.4.1 are not empty. Let the number of vertices in  $S_1$ , and hence in  $S_4$ , be  $x$ , and

$$S_4 = \{ v_{i\alpha_1}, v_{i\alpha_2}, \dots, v_{i\alpha_x} \} \quad (4.4.17)$$

$$S_1 = \{ v_{j\beta_1}, v_{j\beta_2}, \dots, v_{j\beta_x} \} \quad (4.4.18)$$

where  $\alpha_i$  and  $\beta_i$  are the positional indices of these vertices within  $V_{m_i}$  and  $V_{m_j}$  respectively and

$$\alpha_1 < \alpha_2 < \dots < \alpha_x,$$

$$\beta_1 < \beta_2 < \dots < \beta_x.$$

Criterion B implies that any allowable  $E_m$  must contain at least  $x$  parts and further, each part containing a single vertex from  $S_4$  must also contain a single vertex from  $S_1$ . Thus this part matches a vertex from  $S_4$  to a corresponding vertex from  $S_1$ . If  $\mu_k$

is the number of inversions needed to rearrange the vertices in  $S_1$  so that they appear in the same order as their corresponding matched vertices in  $S_4$ , then for an allowable  $E_{m_k}$

$$\det a_F \begin{pmatrix} V_{m_i} \\ E_{m_k} \end{pmatrix} \det a_F \begin{pmatrix} V_{m_j} \\ E_{m_k} \end{pmatrix} = (-1)^{x+\sum \alpha_i + \sum \beta_i} (-1)^{\mu_k} \quad (4.4.19)$$

Since only  $\mu_k$  depends upon  $E_{m_k}$ , then (4.2.9) becomes

$$\det y \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix} = (-1)^{x+\sum \alpha_i + \sum \beta_i} \sum_{E_{m_k}} (-1)^{\mu_k} Y(E_{m_k}) \quad (4.4.20)$$

where the summation ranges over all  $E_{m_k}$  such that  $\{V_{m_i}, E_{m_k}\}$  and  $\{V_{m_j}, E_{m_k}\}$  are both  $(v_0-m)$ -tree pairs.

#### 4.5. From Subgraphs to Maximum Term Rank Submatrices

The preceding discussion has assumed that the vertex sets  $V_{m_i}$  and  $V_{m_j}$  were specified initially and thus it became necessary to examine the graph  $G_0$  to determine whether or not it contained at least one subgraph  $E_{m_k}$  which satisfied both  $(v_0-m)$ -tree pair conditions. However, if any subgraph  $E_m$ , containing no circuits, is selected from  $G_0$  then it is a simple matter to list all the vertex sets  $V_{m_i}$  such that  $\{V_{m_i}, E_m\}$  is a  $(v_0-m)$ -tree pair.

Associated with any two of these vertex sets is an  $m$  by  $m$  submatrix from

$$y_a = a_a y_F a'_a \quad (4.5.1)$$

and this submatrix must have term rank  $m$ . Note that the complete

incidence-seg matrix is used in (4.5.1) to allow for the possibility that the subgraph contains the reference vertex  $r_0$ . These results are applicable to the  $\mathcal{Y}$  matrix in (4.1.2) if the vertex sets containing the reference vertex are deleted from the list.

First, consider another approach to calculating the number  $n_v$  defined in Theorem 4.3.8:

Theorem 4.5.1. Let  $G_0$  be a part of  $v_0$  vertices and  $E_m$  any  $m$ -element subgraph which contains no circuits. If  $E_m$  contains  $p$  parts and the  $k$ -th part contains  $x_k$  elements then the vertex set  $V(E_m)$  can be decomposed into

$$n_v = \prod_{k=1}^p (x_k + 1) \quad (4.5.2)$$

distinct subsets  $V_{m_i}$  of  $m$  distinct vertices such that  $\{V_{m_i}, E_m\}$  is a  $(v_0 - m)$ -tree pair,  $i = 1, 2, \dots, n_v$ .

Proof: Since  $E_m$  contains no circuits, then  $V(E_m)$  contains  $m+p$  vertices and each part of  $E_m$  contains  $x_k+1$  vertices. Let  $V_{m_i}$  be any  $m$  vertex subset formed by deleting  $p$  vertices from  $V(E_m)$ , one vertex from each part. This can be done in any one of  $n_v = \prod_{k=1}^p (x_k+1)$  different ways. Now,  $E_m$  contains no circuits and each part of  $E_m$  contains exactly one vertex which is not a member of  $V_{m_i}$ . Therefore  $\{V_{m_i}, E_m\}$  is a  $(v_0 - m)$ -tree pair for  $G_0$ .

Consequently, if  $G_0$  is a graph of  $F$ -elements such that the  $F$ -element admittance matrix,  $y_F$ , is diagonal and nonsingular, and  $V_{m_i}, V_{m_j}$  are any two of the vertex sets of Theorem 4.5.1 then

$$y_a \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix}$$

has term rank  $m$ . Furthermore, noting that

$$y_a \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix}$$

has term rank  $m$  if and only if

$$y_a \begin{pmatrix} V_{m_j} \\ V_{m_i} \end{pmatrix}$$

has term rank  $m$ , and accounting for the fact that  $V_{m_i}$  and  $V_{m_j}$  can be identical, there are a total of

$$2 \binom{n_v}{2} + n_v = n_v^2 \quad (4.5.3)$$

different  $m$  by  $m$  submatrices of  $y_a$  associated with a single circuitless subgraph  $E_m$ , and each of these submatrices has term rank  $m$ .

## Chapter 5

### COMPLETE SOLUTIONS FOR THE PRIMARY SYSTEM OF EQUATIONS

#### 5.1. Subgraphs and Feasible Proper Partitions

The preceding chapter provides a basis for interrelating proper partitions of the variables within a system of holac equations associated with the graph correlate of an electric network and classes of subgraphs of that graph. A given partition of the variables is a proper partition if and only if a related submatrix has the proper dimensions and rank; this submatrix, in turn, has the proper term rank if and only if there exists within the graph at least one member of a particular class of subgraphs. An  $m$  by  $m$  submatrix has rank  $m$  only if its term rank is  $m$ ; consequently the existence of a particular subgraph constitutes a necessary condition for the corresponding partition to be a proper partition of the variables. It is not in general a sufficient condition as certain subsets of values for the F-element admittance coefficients, in conjunction with certain interconnection patterns of the F-elements, can result in the rank of the submatrix being less than its term rank. In certain types of problems this characteristic is desirable--for example: balanced bridges and resonant networks, while in other types it may or may not be desirable. In recognition of these two possibilities a partition of the variables is said to be a feasible proper partition if and only if the related submatrix has the proper dimensions and term rank.

As previously noted a complete solution for a system of holac equations can be determined in many forms--for example, any proper partition of the variables determines a corresponding complete solution. Although any complete solution implies all particular solutions it is often the case that certain forms of a complete solution are more desirable than others. The approach considered here allows one to investigate the feasibility of a variety of forms of a complete solution without the necessity of actually formulating the primary system of equations. The only complete solutions which are considered explicitly here are those obtained directly from proper partitions of the variables.

The key issue in such an investigation is to determine whether or not a given partition of the variables is a feasible proper partition. If it is, then a continuation of the investigation indicates whether or not it is also a proper partition. The vertex subsets,  $S_1$ ,  $S_2$ ,  $S_3$ , and  $S_4$  introduced in the preceding chapter play a central role in these investigations. Each non-reference vertex of the graph is incident to exactly one N-element, thus a one-to-one correspondence is established between the  $v_0 - 1$  N-elements and the  $v_0 - 1$  non-reference vertices of the graph. Recall that

$$Vm_i = S_3 \cup S_4, \quad (5.1.1)$$

$$Vm_j = S_1 \cup S_3, \quad (5.1.2)$$

and that the set  $S_2$  contains all other vertices of the graph--

including the reference vertex  $r_0$ . Permitting  $S_1$  and  $S_4$ , or  $S_3$ , to be empty allows one to consider within the same framework the possibilities of  $V_{m_i}$  and  $V_{m_j}$  being identical, disjoint, or neither. Consider the system of holac equations in (3.5.21); the set

$$\{I_{N1}, I_{N2}, \mathcal{V}_{N1}, \mathcal{V}_{N3}\} \quad (5.1.3)$$

is a complete set of dependent variables and

$$\{I_{N3}, I_{N4}, \mathcal{V}_{N2}, \mathcal{V}_{N4}\} \quad (5.1.4)$$

is the corresponding complete set of independent variables for this system of holac equations if and only if

$$n_1 = n_4 \quad (5.1.5)$$

and

$$\det y \begin{pmatrix} V_{m_i} \\ V_{m_j} \end{pmatrix} = \det \begin{bmatrix} y_{31} & y_{33} \\ y_{41} & y_{43} \end{bmatrix} \neq 0. \quad (5.1.6)$$

Examination of the relationships among the allocation of the N-element variables within (5.1.3) and (5.1.4), the row and column indices of the submatrix whose determinant appears in (5.1.6), and the vertex sets  $S_1$  through  $S_4$  yields the following conclusions:

- (1) Each of the  $n_1$  N-elements incident to the  $n_1$  vertices of  $S_1$  has both associated element variables within the dependent set (5.1.3). These N-elements are classified as  $N_0$ -elements;

- (2) Each of the  $n_2$  N-elements incident to the  $n_2$  vertices of  $S_2$  (other than  $r_0$ ) has its associated voltage variable within the independent set (5.1.4) and current variables within the dependent set (5.1.3). These N-elements are classified as  $N_e$ -elements;
- (3) Each of the  $n_3$  N-elements incident to the  $n_3$  vertices of  $S_3$  has its associated current variable within the independent set (5.1.4) and voltage variable within the dependent set (5.1.3). These N-elements are classified as  $N_h$ -elements;
- (4) Each of the  $n_4$  N-elements incident to the  $n_4$  vertices of  $S_4$  has both of its associated variables within the independent set (5.1.4). These N-elements are classified as  $N_{eh}$ -elements.

Thus a partition of the variables, such that  $n_1 = n_4$ , identifies the vertex sets  $S_1$  through  $S_4$  and conversely. This information, in conjunction with the developments of the preceding chapter, allows one to investigate certain properties of a complete solution for the primary system of equations in terms of properties of the graph without the need for explicit formulations of the equations.

The classification of the N-elements as  $N_o$ -,  $N_e$ -,  $N_h$ -, or  $N_{eh}$ -elements is determined by properties of the system of holac equations and the graph--not by consideration of the correlating electric network. This allows one considerable freedom in the classification of the N-elements since there are often many

different proper partitions of the variables for a given system of holac equations. This represents a departure from the usual practice in electric network theory where the inclusion of  $N_e$ - and  $N_h$ -elements has been generally based upon the presence of regulated voltage and current sources within the correlating electric network. Furthermore, this classification was seldom altered. The general absence of any device in the physical network having terminal characteristics which correlate with the characteristics of  $N_o$ - and  $N_{eh}$ -elements has undoubtedly been a major reason for the general lack of consideration given to these classes of N-elements.

## 5.2. Particular Solutions and Specification of Variables

Once a desired proper partition of the variables has been determined and the corresponding complete solution for a system of holac equations has been obtained then the variables within the independent set can be assigned arbitrary values with no danger of introducing inconsistencies. Each such set of values determines a particular solution and all particular solutions can be generated in this manner. Often it is desired to select from the multiplicity of particular solutions that solution, or solutions, which best satisfy some prescribed criteria. These criteria may be stated directly in terms of the variables within the system of holac equations and/or in terms of other secondary or derived quantities related to these variables. The form in which these criteria are stated is often a deciding factor in the choice of partitions to be checked.

The primary variables in the systems of holac equations considered in this investigation are the voltage and current variables associated with each element in the graph correlate of an electric network:

$$V_k = |V_k| e^{j\phi_k} = V_{k1} + j V_{k2}, \quad (5.2.1)$$

and

$$I_k = |I_k| e^{j\theta_k} = I_{k1} + j I_{k2} \quad (5.2.2)$$

for element  $k$ . The real power and reactive power variables for certain elements comprise one set of secondary variables commonly encountered in electric power network problems.

Again for element  $k$ :

$$P_k + j Q_k = V_k I_k^* = |V_k| e^{j\phi_k} |I_k| e^{-j\theta_k} \quad (5.2.3)$$

$$= |V_k| |I_k| e^{j\sigma_k} \quad (5.2.4)$$

where

$P_k$  is the real power,

$Q_k$  is the reactive power, and

$\sigma_k$  is the power factor angle.

Earlier developments have shown that a complete solution for a primary system of equations can be obtained in terms of certain subsets of the voltage and current variables associated with the  $N$ -elements in the graph. Thus particular solutions are obtained by assigning specific values to these variables in terms of magnitudes and angles, or in terms of real parts and imaginary

parts. If one or more of the variables within the independent set is not assigned a specific value or is only specified in part--for example, the magnitude is specified but not the angle--then a family of particular solutions is obtained. These particular solutions contain one or more parameters which can be varied in an attempt to satisfy additional conditions which might have been placed upon the particular solution. Consequently, for a particular proper partition, the  $N$ -element falling into the  $N_e$ -, or  $N_h$ -element classification can have at most two parameters, while those in the  $N_{eh}$ -element classification can have at most four parameters. By the appropriate specification of the voltage and current variables for an  $N_{eh}$ -element it is possible to maintain any desired interrelation between these variables--for example, specifying the magnitudes of the voltage and current variables and the power factor angle fixes both the real and reactive power for that element yet neither the element voltage nor the element current is completely specified.

One further property of a system of holac equations is examined at this point. Consider a fixed system of holac equations; assume that at least two proper partitions of the variables exist and that the corresponding complete solution for the system has been determined for each proper partition. If the variables within the independent set of one of these proper partitions are assigned specific values then a particular solution is obtained. Now if the variables within the independent set of any other proper partition are subsequently assigned the values that they assumed in this

first solution then the resulting particular solution is identical with the first one obtained. In terms of the N-element classification defined earlier this means that if a desired particular solution is obtained with a certain pattern of  $N_o$ -,  $N_e$ -,  $N_h$ -, and  $N_{eh}$ -elements then this pattern can be altered into any other allowable pattern and it is possible to maintain the same particular solution. For example, established criteria for the consistent location of regulated voltage and current sources within a physical network coincide with the conditions such that the correlating N-elements in the graph can be classified as  $N_e$ - and  $N_h$ -elements respectively.<sup>10, 11, 41</sup> However, within the framework of the correlating graph and primary system of equations, one is not in general restricted to this particular N-element classification. Thus if the appropriate conditions are satisfied these particular N-elements can be considered as either  $N_e$ - or  $N_h$ -elements, as well as  $N_o$ - and  $N_{eh}$ -elements. Consequently the use of the  $N_o$ - and  $N_{eh}$ -element classifications in an analysis problem need not be based upon the existence of any correlating physical device.

### 5.3. Applications in the Analysis of Electric Power Networks

Although the results of the preceding investigation are applicable to a larger class of network problems they are particularly well-suited for use in the analysis of electric power networks. As discussed in Chapter 1, specifying variables plays an important role in many phases of electric power network analysis. The techniques developed in this investigation permit

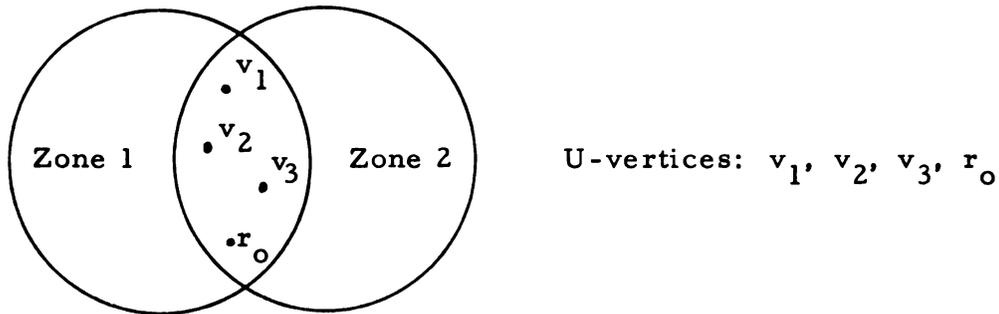


one to exercise considerably more freedom in the choice of specified variables than was possible before. At the same time one is assured that the chosen variables can be assigned arbitrary values with no danger of introducing inconsistencies into the system of network equations. These techniques are based upon properties of the primary system of equations yet the investigation can be completed without the necessity of actually formulating the equations. The required properties are stated directly in terms of the graph and thus allow one to interrelate properties of the graph and properties of solutions to the primary system of equations.

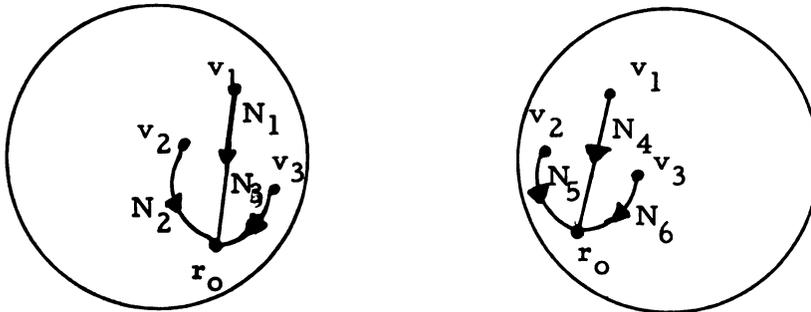
Theoretically the results of this investigation can be applied to any finite graph of the type considered; however there are practical limitations on the number of vertices and elements that can be accommodated in an effective manner. Certainly the use of a digital computer with a large storage capacity permits one to consider problems associated with larger and larger networks. However this capability, in itself, is not a panacea for all the problems in the analysis of electric networks. There are situations when it is desirable to "localize" the problem and yet not completely dissociate it from its relative place within a larger problem. The results of this investigation, coupled with a zoning concept described in the literature<sup>15, 16</sup> provide the means for a new approach to the analysis of large-scale electric networks.

In the zoning approach<sup>16</sup> a large graph is decomposed into a number of subgraphs or zones such that (a) each subgraph is connected and (b) any two subgraphs are element disjoint but have certain vertices

called U-vertices, in common. For the class of graphs considered in this discussion it is assumed that the reference vertex is a U-vertex for each zone and that each zone contains at least one other U-vertex distinct from the reference vertex. Once the original graph has been zoned in this manner the zones are then separated and an "external" set of N-elements is added to each zone; these N-elements are incident to the U-vertices only and each non-reference U-vertex in a zone is incident to exactly one of these added N-elements. In addition all external N-elements in a given zone are incident to the reference vertex (which is also a U-vertex for that zone). Figures 5.3.1 illustrates this for the case of two zones.



(a) Identification of zone and U-vertices.



(b) Graph after zoning and adding external N-elements.

Figure 5.3.1. Illustration of Zoning Technique.

It can be shown<sup>16</sup> that if the primary system of equations for the zoned graph, Figure 5.3.1(b), is augmented with the following sets of auxiliary equations:

$$\begin{bmatrix} V_{N1} \\ V_{N2} \\ V_{N3} \end{bmatrix} = \begin{bmatrix} V_{N4} \\ V_{N5} \\ V_{N6} \end{bmatrix} \quad \text{and} \quad \begin{bmatrix} I_{N1} \\ I_{N2} \\ I_{N3} \end{bmatrix} = - \begin{bmatrix} I_{N4} \\ I_{N5} \\ I_{N6} \end{bmatrix}, \quad (5.3.1)$$

then each solution of this augmented primary system of equations determines exactly one solution for the primary system of equations for the original graph, Figure 5.3.1(a), and conversely. Thus the augmented primary system of equations for the zoned graph and the primary system for the original graph are essentially equivalent systems of equations.

The zoned graph consists of a number of separate graphs, or zones, and for each zone a primary system of equations can be formulated and solved. If, in addition, the auxiliary equations, such as (5.3.1), are satisfied then a solution of the primary system of equations for the original graph is obtained. This suggests a new approach to the analysis of large complex networks. If zones are so chosen that each of the external N-elements can be classified as  $N_{eh}$ -elements then, since both  $V$  and  $I$  for these N-elements can be arbitrarily specified, one is assured that the auxiliary equations can be satisfied. Once this has been established each zone can be analyzed independently--yet the composite of the zone

solutions determines a corresponding solution for the original un-zoned graph.

This technique provides considerable flexibility in the analysis of electric networks. For the purpose of illustration consider the two zone case of Figure 5.3.1 and assume that the original graph has been zoned so that elements  $N_1$ ,  $N_2$ , and  $N_3$  can be classified as  $N_{eh}$ -elements for zone 1 and that elements  $N_4$ ,  $N_5$ , and  $N_6$  can be classified as  $N_{eh}$ -elements for zone 2. Suppose that one has a particular solution for the primary system of equations associated with the original unzoned graph. Using standard techniques<sup>34</sup> the  $V$  and  $I$  variables associated with the external  $N$ -elements are calculated so that the corresponding solution is maintained in the zoned graph. Actually the entire solution for the original graph is not needed--only that portion of the solution required to calculate the  $V$ ,  $I$  variables for these  $N$ -elements is necessary. Note that this data could be obtained from measurements made in the actual network. Now consider zone 1 and its associated primary system of equations. Any solution of this primary system for which the  $V$  and  $I$  variables associated with elements  $N_1$ ,  $N_2$ , and  $N_3$  remain invariant can be combined with the existing solution for zone 2 to obtain a new solution for the primary system for the original graph. One is assured that the  $V$  and  $I$  variables for  $N_1$ ,  $N_2$ , and  $N_3$  can be maintained at the desired values since they can be classified as  $N_{eh}$ -elements. In this manner the

solution for zone 1 can be varied and yet the solution for zone 2 remains invariant. Changes in the solution have been localized or confined to zone 1. When this is applied to a multi-zone problem the concept represents not only a reduction in the complexity of the problem to be analyzed but also permits one to investigate the possibilities of localizing, within prescribed zones, changes in the operating characteristics.

One further application is considered at this time. Again consider a zoned graph. The fact that the external  $N$ -elements for a zone can be classified as  $N_{eh}$ -elements implies that there exists within the zone an equal number of  $N_o$ -elements; furthermore the  $N_o$ - and  $N_{eh}$ -element classifications can always be interchanged. Thus it is possible to obtain a particular solution for the primary system associated with this zone utilizing the maximum number of specified conditions within the zone. This solution determines the  $V$ ,  $I$  variables associated with the  $N_o$ -elements incident to the  $U$ -vertices of that zone. Then the auxiliary equations, such as (5.3.1), are used to transfer this condition to the  $N_{eh}$ -elements in the adjacent zones; in this process the effects of the first zone upon the adjacent zones is completely determined in terms of the  $V$  and  $I$  variables associated with the external  $N$ -elements. Depending upon the  $F$ -element subgraph with a particular zone it is also possible to interchange the  $N_o$ -,  $N_{eh}$ -element classifications for subsets of the  $N$ -elements and thus it is possible to reflect changes in the solution into selected zones.

#### 5.4. Example

A portion of an actual electric power system--the Denver area of the Public Service Company of Colorado--is examined in this section to illustrate the preceding developments and at the same time to establish the feasibility of the zoning techniques discussed in Section 5.3. A network representation of this system contains 33 nodes plus the ground bus, 39 transmission line sections--each represented by the conventional pi equivalent, 6 generators, and 24 loads. A simplified interconnection diagram representing the transmission network is shown in Figure 5.4.1 and detailed nodal diagrams of the individual zones are shown in Figures 5.4.3 through 5.4.7.

The zones in this example were chosen in a somewhat arbitrary manner to illustrate the technique; in general the initial choice of zones would depend upon particular characteristics of the system under investigation. Factors which would influence the choice include geographical distribution of the system, service or load areas, locations of interconnections with adjacent systems, etc. Once the zones have been defined it is necessary to determine whether or not the external N-elements can be classified as  $N_{eh}$ -elements. For each zone in this example the external N-elements can be classified as  $N_{eh}$ -elements, i. e. both of the V and I variables associated with each of these N-elements can be allocated to the independent set of some proper partition of the variables within the primary system of equations for that zone.

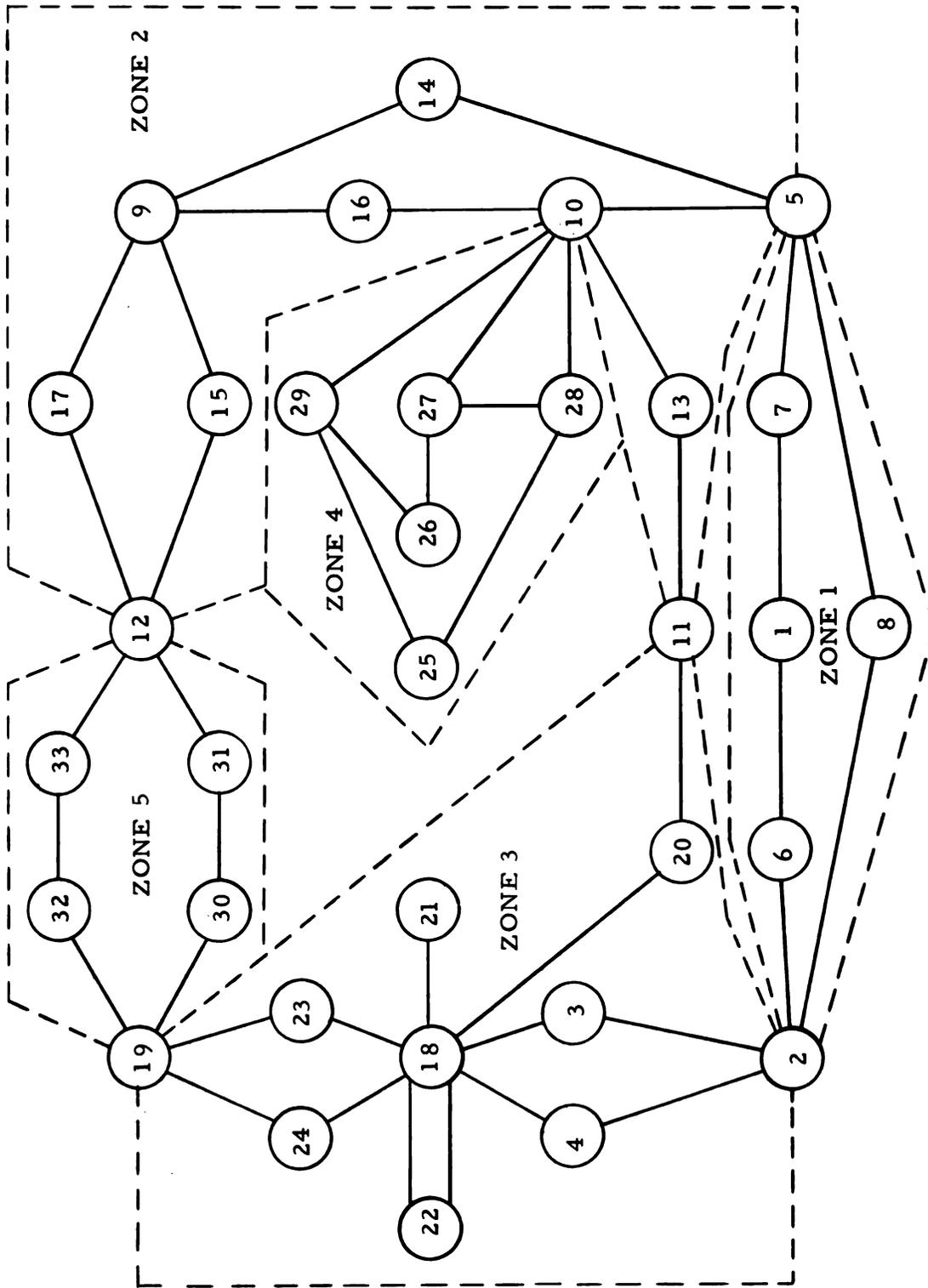


Figure 5.4.1. Interconnection Diagram for Transmission Network.

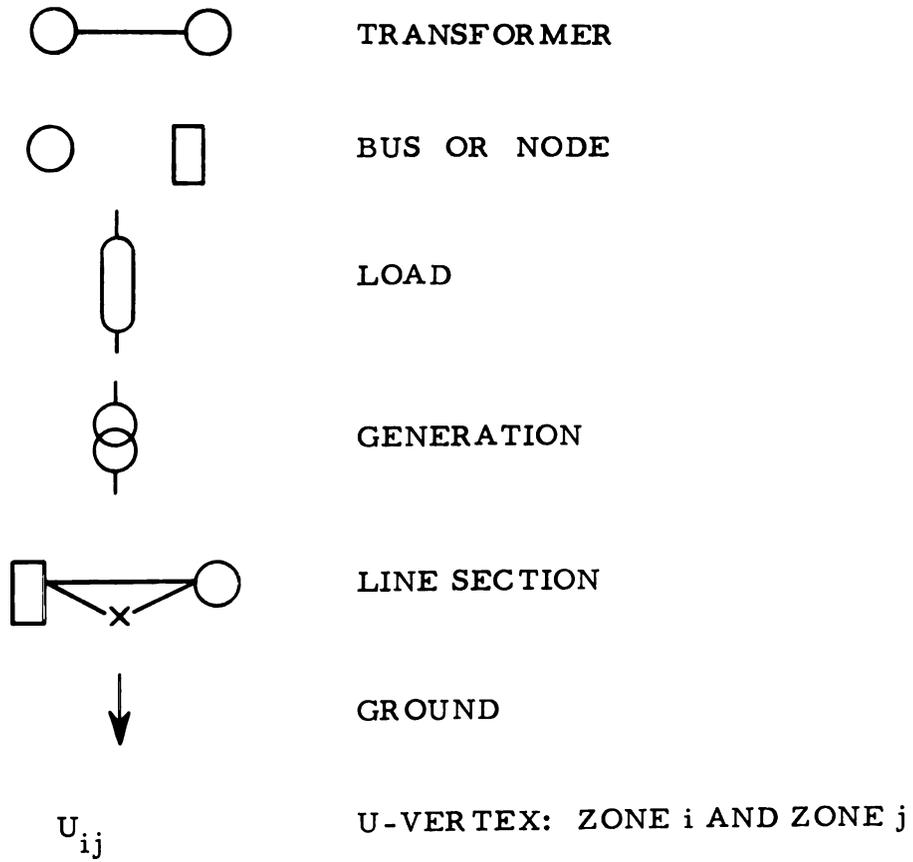


Figure 5.4.2. Key to Symbols.

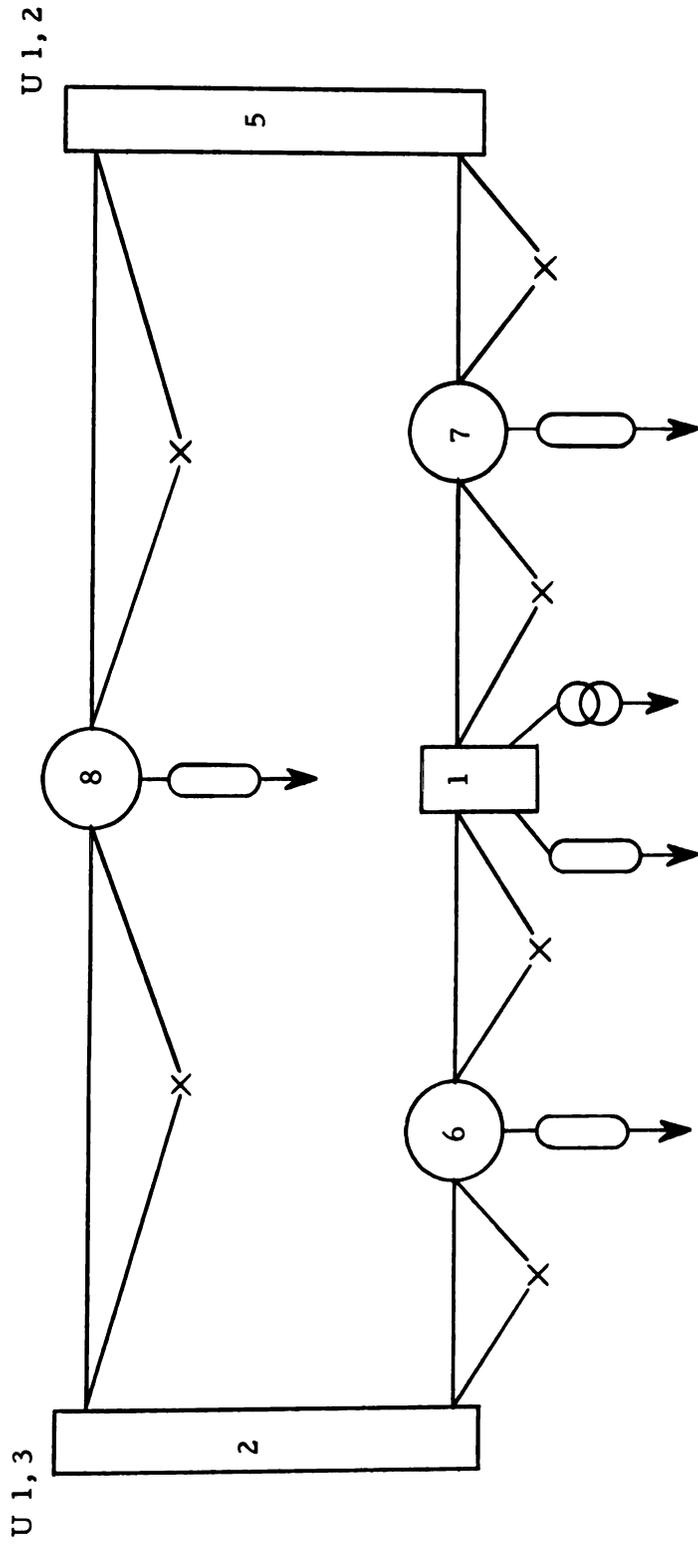


Figure 5.4.3. Nodal Diagram - Zone 1.

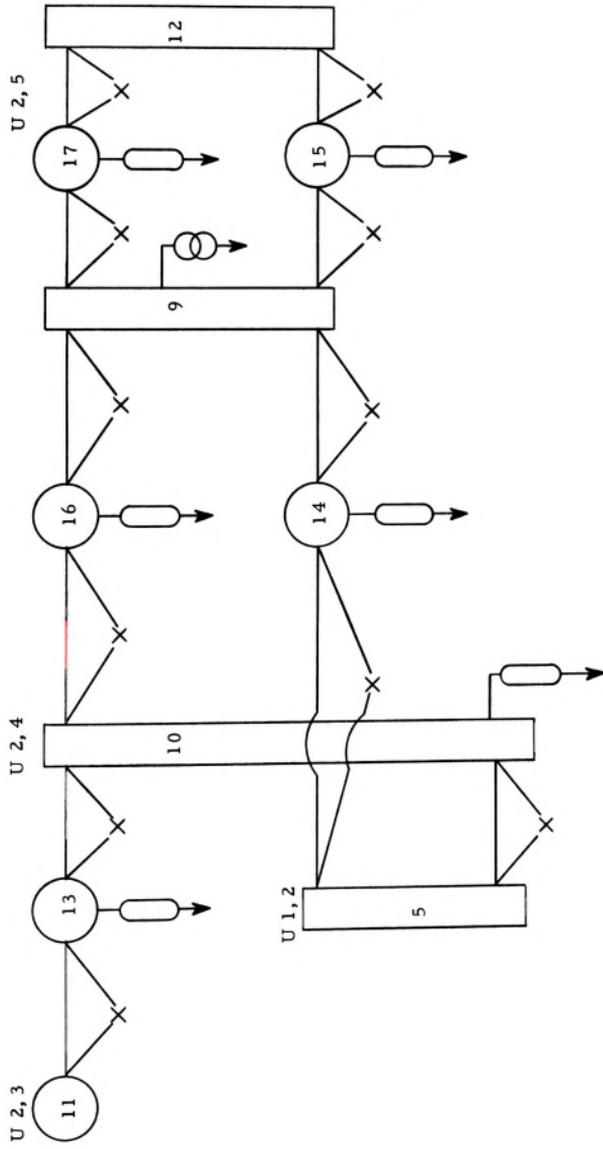


Figure 5.4.4. Nodal Diagram - Zone 2.

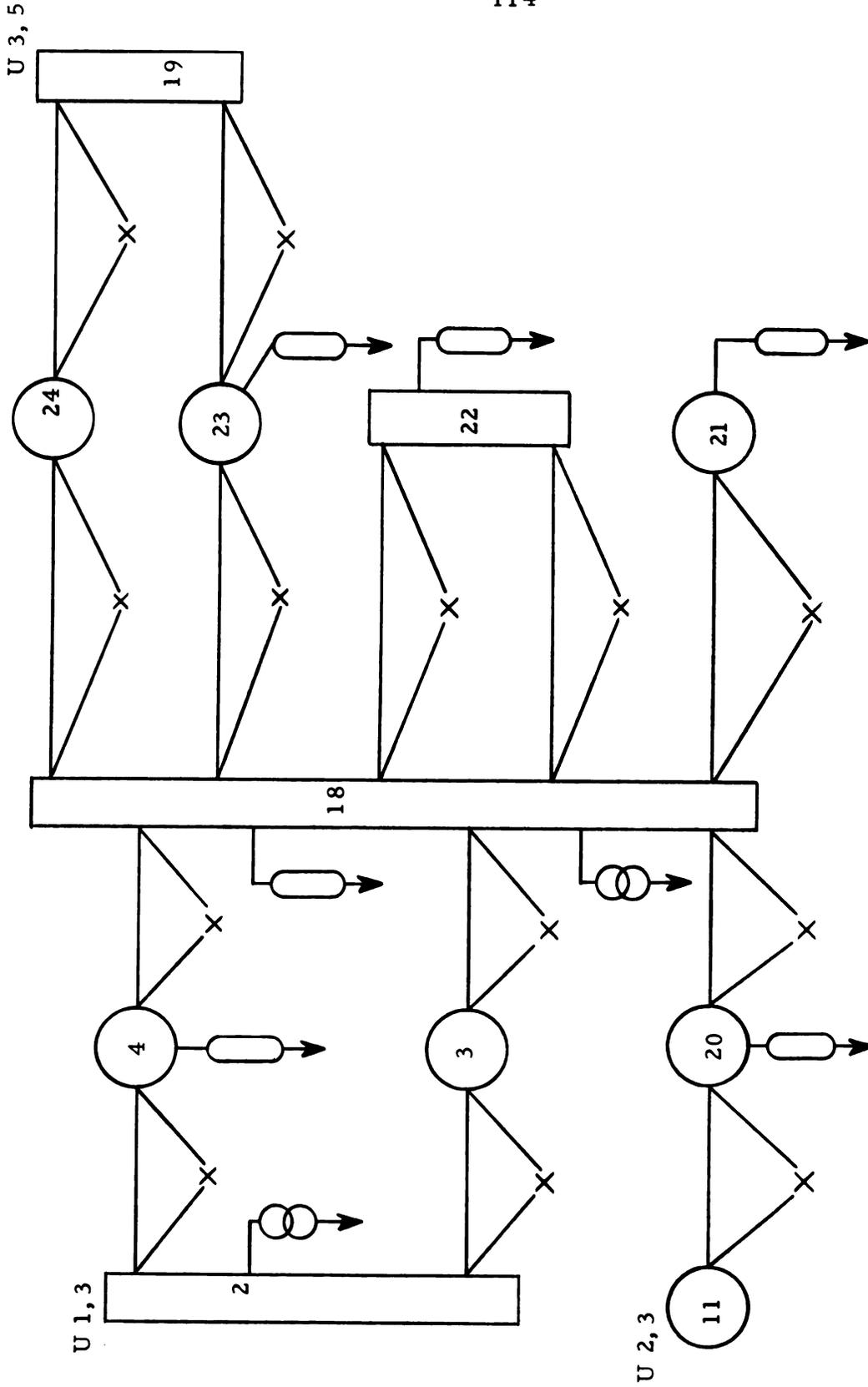


Figure 5.4.5. Nodal Diagram - Zone 3.

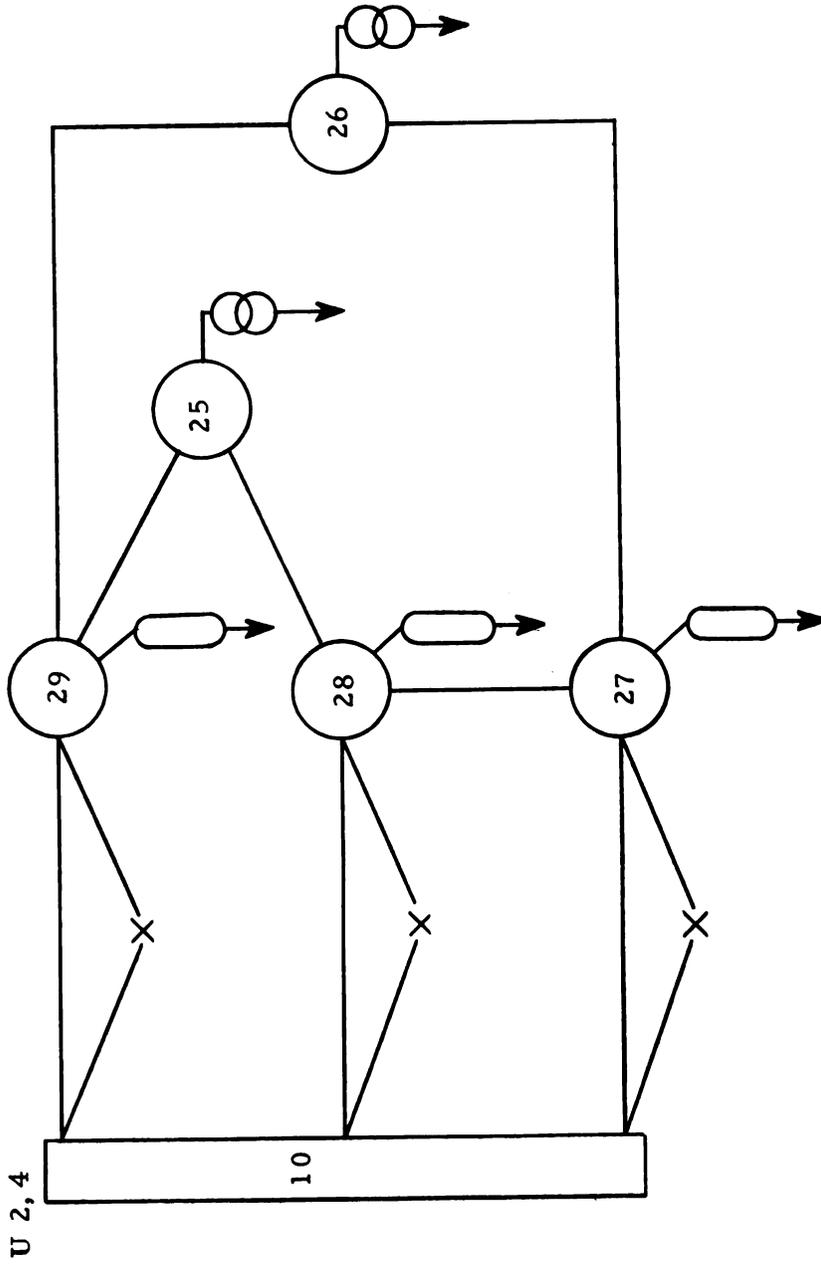


Figure 5.4.6. Nodal Diagram - Zone 4.

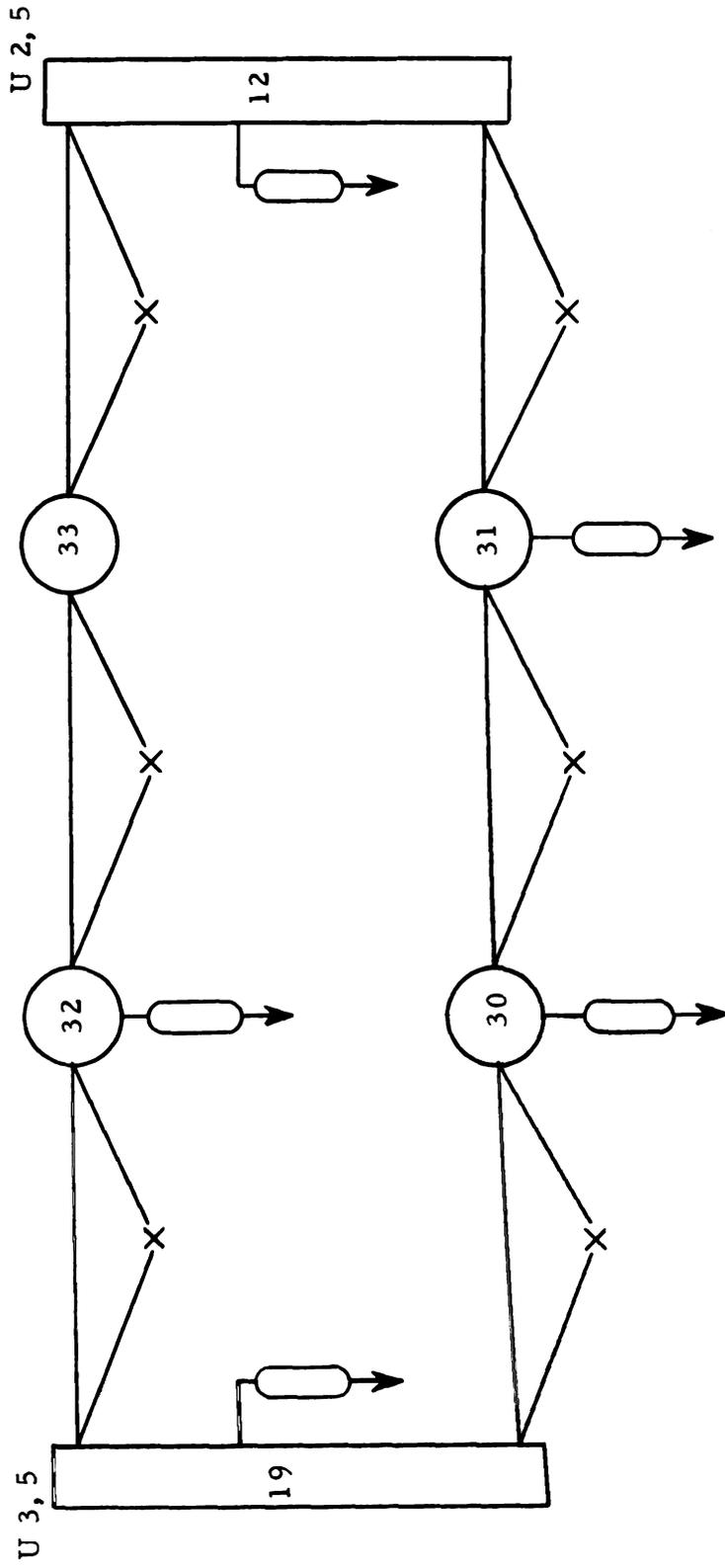


Figure 5.4.7. Nodal Diagram - Zone 5.

This fact establishes the feasibility of the zoning approach discussed in Section 5.3.

Consider the subgraph corresponding to any zone and the set of external N-elements for that zone. The graph elements corresponding to the transmission network are considered as F-elements and the graph elements corresponding to the generators are considered as N-elements. If the load admittance coefficients are not known then the corresponding graph elements are considered as N-elements; if a load admittance coefficient is known then the graph element can be handled as an F-element or as an N-element as discussed in Section 3.5. In this example it is assumed that all graph elements corresponding to loads are treated as N-elements. In addition any non-reference vertex which is not a U-vertex, or is not incident to a generator or load element, is considered to be incident to an N-element--see Section 3.5. When these steps have been completed it is possible that certain non-reference vertices are incident to more than one N-element; this is the case when a given node is incident to both a generator and a load, or when a U-vertex is incident to a generator and/or load. Any such parallel connection of N-elements is now replaced by a single N-element. There is no loss in generality in doing this since  $V$  for the equivalent N-element is the same as  $V$  for each of the parallel N-elements and  $I$  for the equivalent N-element is the sum of the  $I$ 's for each of the parallel N-elements. Once this equivalent  $I$  has been determined then any choice of values for the  $I$ 's of the

parallel N-elements which yields this sum is satisfactory. (Note that if one of the external N-elements parallels another N-element and is subsequently replaced by a single N-element then it is necessary to determine the  $I$  associated with the external N-element before the auxiliary equations discussed in Section 5.3 are used). At this point a  $v_0$ -vertex zone contains a total of  $v_0 - 1$  N-elements; each non-reference vertex is incident to exactly one N-element and all N-elements are incident to the reference vertex.

As discussed in Section 5.1 any partition of the  $2(v_0 - 1)$  variables associated with this set of N-elements into two disjoint sets of  $v_0 - 1$  variables each, i. e. a trial classification of the N-elements, defines the distribution of the vertices of the zone into the sets  $S_1, S_2, S_3,$  and  $S_4$  which, in turn, define the two vertex sets  $Vm_i$  and  $Vm_j$ . If the graph contains at least one m-element subgraph of F-elements  $E_m$  such that both  $\{Vm_i, E_m\}$  and  $\{Vm_j, E_m\}$  are  $(v_0 - m)$ -tree pairs then this partition is a feasible proper partition and the corresponding N-element classification is called a feasible classification. For any feasible proper partition the investigation is continued until all such subgraphs have been determined, then (4.4.20) can be utilized to determine whether or not this feasible proper partition is also a proper partition of the variables.

To illustrate this technique consider zone 2 as shown in Figure 5.4.4. The graph for this zone contains 10 vertices in

addition to the reference vertex. The F-element subgraph consists of the elements corresponding to the line sections since the generator and all loads are represented by N-elements. Note that the single N-element incident to vertex 10 in the zone graph represents the parallel connection of an N-element corresponding to the load and the external N-element added to this zone by virtue of the fact that this vertex is also a U-vertex. Let the N-elements be identified by referring to the vertex to which the element is incident. The zone graph is now investigated to determine whether or not  $N_5$ ,  $N_{10}$ ,  $N_{11}$ , and  $N_{12}$  can be classified as  $N_{eh}$ -elements. Since a complete set of independent variables for this zone contains 10 variables this choice does not completely determine a trial classification pattern. To complete the trial classification of the N-elements let  $N_5$ ,  $N_9$ ,  $N_{10}$ ,  $N_{11}$ , and  $N_{12}$  be considered as potential  $N_{eh}$ -elements; thus  $N_{13}$ ,  $N_{14}$ ,  $N_{15}$ ,  $N_{16}$ , and  $N_{17}$  must be considered as potential  $N_o$ -elements. The corresponding vertex sets are

$$V_{5i} = S_4 = \{ 5, 9, 10, 11, 12 \} \quad (5.4.1)$$

and

$$V_{5j} = S_1 = \{ 13, 14, 15, 16, 17 \} \quad (5.4.2)$$

The vertex sets  $V_{5i}$  and  $V_{5j}$  are disjoint hence any subgraph of F-elements which satisfies the 6-tree pair condition for both vertex sets must consist of 5 elements which match  $V_{5i}$  onto  $V_{5j}$  in a one-to-one manner. Any such set of 5 F-elements must

be included in the subgraph shown in Figure 5.4.8. Inspection of this subgraph indicates the existence of exactly two 5-element subgraphs having the desired characteristic. These subgraphs are shown in Figure 5.4.9.

The existence of either subgraph insures that the partition of variables under consideration is a feasible proper partition. Further it is known that the expansion of  $\det y \begin{pmatrix} V_{5i} \\ V_{5j} \end{pmatrix}$  for this zone graph contains exactly two non-zero terms.

Using (4.4.20) to evaluate this determinant:

$$\det y \begin{pmatrix} V_{5i} \\ V_{5j} \end{pmatrix} = - \{ -Y_1 Y_3 Y_7 Y_8 Y_{10} + Y_1 Y_5 Y_7 Y_8 Y_9 \} \quad (5.4.3)$$

$$= Y_1 Y_7 Y_8 (Y_5 Y_9 - Y_3 Y_{10}). \quad (5.4.4)$$

For the particular system under investigation

$$Y_3 = Y_5 \quad \text{and} \quad Y_9 = Y_{10}, \quad (5.4.5)$$

and although  $y \begin{pmatrix} V_{5i} \\ V_{5j} \end{pmatrix}$  has term rank 5, the actual rank is less than 5. Therefore this particular partition of the variables is not a proper partition of the variables and the trial classification of the N-elements is not acceptable.

Since the original requirement was only that elements  $N_5$ ,  $N_{10}$ ,  $N_{11}$ , and  $N_{12}$  be classified as  $N_{eh}$ -elements it is possible that another classification of the N-elements will work. Consider the following trial classification-- $N_{eh}$ :  $N_5$ ,  $N_{10}$ ,  $N_{11}$ ,  $N_{12}$ ;  $N_e$ :  $N_9$ ,  $N_{17}$ ;  $N_o$ :  $N_{13}$ ,  $N_{14}$ ,  $N_{15}$ ,  $N_{16}$ . The corresponding vertex

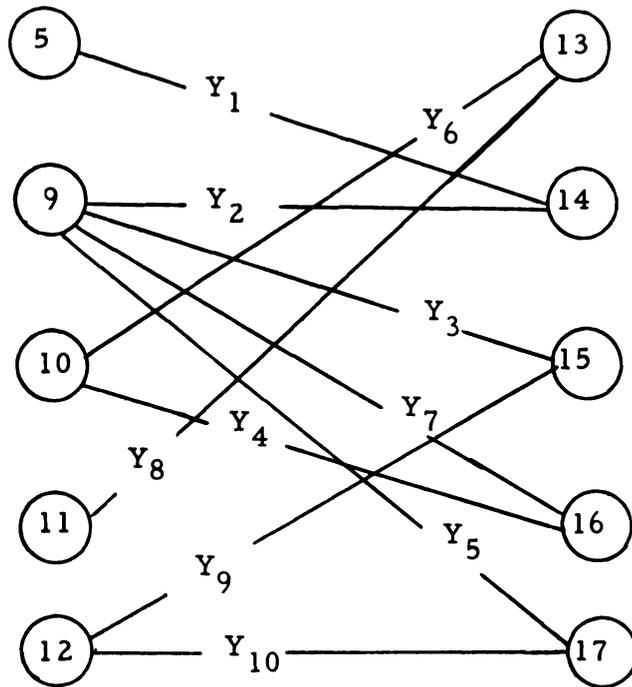


Figure 5.4.8. F-Element Subgraph

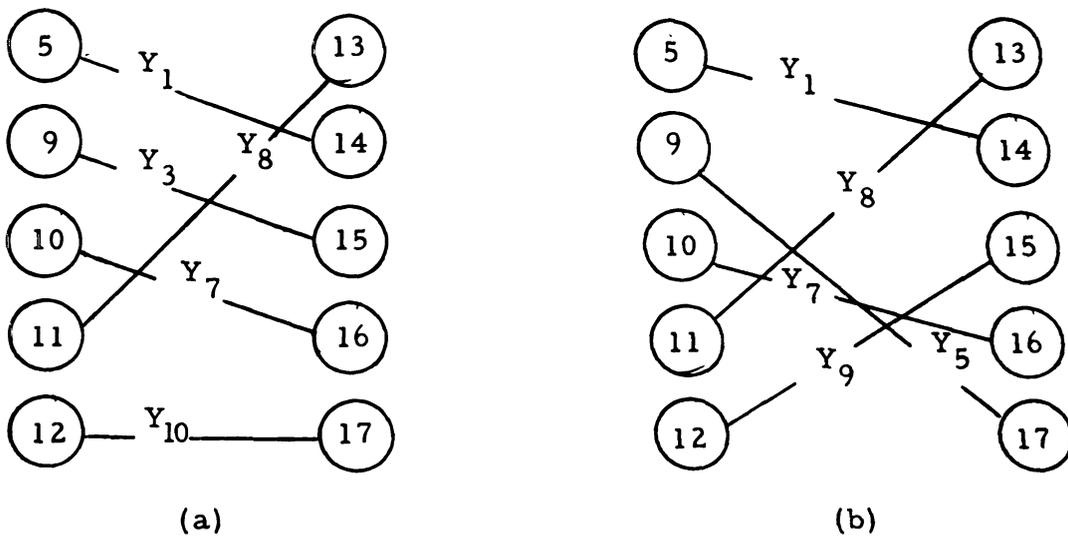


Figure 5.4.9. Subgraphs which Satisfy the 6-Tree Pair Criteria.

sets are:

$$V_{4j} = S_1 = \{13, 14, 15, 16\}, \quad (5.4.6)$$

$$S_2 = \{9, 17, r_o\}, \quad (5.4.7)$$

$$V_{4i} = S_4 = \{5, 10, 11, 12\}. \quad (5.4.8)$$

Again, since  $V_{4i}$  and  $V_{4j}$  are disjoint, any 4-element subgraph  $E_{4k}$  such that  $\{V_{4i}, E_{4k}\}$  and  $\{V_{4j}, E_{4k}\}$  are both 7-tree pairs must match  $V_{4i}$  onto  $V_{4j}$  in a one-to-one manner and thus be contained in the F-element subgraph of Figure 5.4.8. Exactly one such subgraph exists and is shown in Figure 5.4.10. The F-element admittance coefficients are non-zero and  $\det Y \begin{pmatrix} V_{4i} \\ V_{4j} \end{pmatrix}$  contains only one non-vanishing term in its expansion--therefore both the term rank and the rank are 4 and the partition under consideration is a proper partition of the variables for this zone.

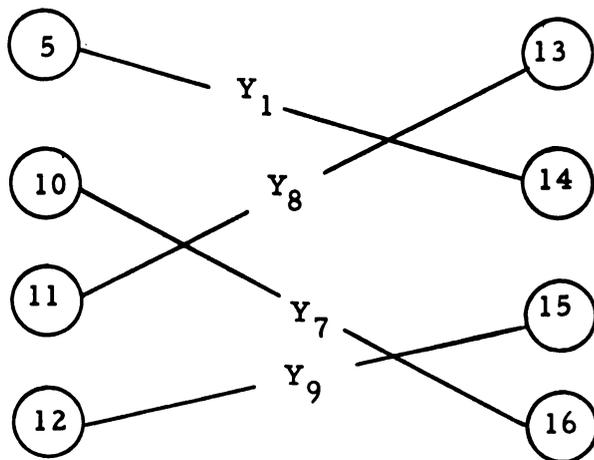


Figure 5.4.10. Subgraph which Satisfies the 7-tree Pair Criteria.

This result establishes that it is possible to classify elements  $N_5$ ,  $N_{10}$ ,  $N_{11}$ , and  $N_{12}$  for zone 2 as  $N_{eh}$ -elements. Other proper partitions for this zone also yield the same conclusion. In general the type of problem under consideration dictates which proper partition or partitions are apt to be more useful in a particular situation.

The preceding example illustrates the approach which proceeds from a given partition of the variables to a search for suitable subgraphs. As indicated in Section 4.5 this process can be revised in the sense that starting from a given circuitless subgraph it is possible to determine a considerable number of feasible proper partitions. This method is more direct than the first and at the same time gives a better indication of the interrelation between the interconnection patterns of the F-elements and corresponding feasible proper partitions. Of course for certain sets of values for the F-element admittance coefficients it is possible for a feasible proper partition to fail to qualify as a proper partition. To verify whether or not this is the case it becomes necessary to examine the graph and search for additional allowable subgraphs.

To illustrate this second approach consider zone 4--see Figure 5.4.6. The zone graph contains 6 N-elements and a complete solution for the primary system of equations is obtained in terms of certain subsets of 6 N-element variables. The fact that 6 variables can be selected from a set of 12 variables in

any one of 924 different combinations gives at least some indication that there is potentially considerable flexibility in the choice of a set of independent variables for the primary system of equations for this zone. Consider the simple 3-element subgraph of F-elements from zone 4 as shown in Figure 5.4.11.

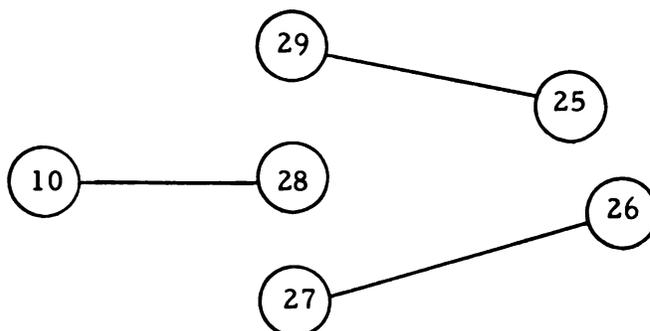


Figure 5.4.11. F-Element Subgraph from Zone 4.

There are eight distinct sets of three vertices for which the given subgraph satisfies the 3-tree pair criteria:

$$\{ 10, 25, 26 \} , \{ 10, 25, 27 \} , \{ 10, 26, 29 \} , \{ 10, 27, 29 \} , \\ \{ 25, 26, 28 \} , \{ 25, 27, 28 \} , \{ 26, 28, 29 \} , \{ 27, 28, 29 \} .$$

(5.4.9)

The reference vertex is not contained in any of those vertex sets so there are then 64 different ways of choosing  $V_{3i}$  and  $V_{3j}$  from this list of vertex sets and corresponding to each choice one obtains a feasible proper partition of the variables! These results are given in Tabulation 5.4.1 in terms of feasible N-element classifications.

## TABULATION 5.4.1.

A PARTIAL LISTING OF  
FEASIBLE N-ELEMENT CLASSIFICATIONS FOR ZONE FOUR

	VERTEX SETS		N-ELEMENT CLASSIFICATION			
	$V_{3i}$	$V_{3j}$	$N_o$	$N_e$	$N_h$	$N_{eh}$
1	10, 25, 26	10, 25, 26	--	27, 28, 29	10, 25, 26	--
2		10, 25, 27	27	28, 29	10, 25	26
3		10, 26, 29	29	27, 28	10, 26	25
4		10, 27, 29	27, 29	28	10	25, 26
5		25, 26, 28	28	27, 29	25, 26	10
6		25, 27, 28	27, 28	29	25	10, 26
7		26, 28, 29	28, 29	27	26	10, 25
8		27, 28, 29	27, 28, 29	--	--	10, 25, 26
9	10, 25, 27	10, 25, 27	--	26, 28, 29	10, 25, 27	--
10		10, 26, 29	26, 29	28	10	25, 27
11		10, 27, 29	29	26, 28	10, 27	25
12		25, 26, 28	26, 28	29	25	10, 27
13		25, 27, 28	28	26, 29	25, 27	10
14		26, 28, 29	26, 28, 29	--	--	10, 25, 27
15		27, 28, 29	28, 29	26	27	10, 25
16	10, 26, 29	10, 26, 29	--	25, 27, 28	10, 26, 29	--
17		10, 27, 29	27	25, 28	10, 29	26
18		25, 26, 28	25, 28	27	26	10, 29
19		25, 27, 28	25, 27, 28	--	--	10, 26, 29
20		26, 28, 29	28	25, 27	26, 29	10
21		27, 28, 29	27, 28	25	29	10, 26
22	10, 27, 29	10, 27, 29	--	25, 26, 28	10, 27, 29	--
23		25, 26, 28	25, 26, 28	--	--	10, 27, 29
24		25, 27, 28	25, 28	26	27	10, 29
25		26, 28, 29	26, 28	25	29	10, 27
26		27, 28, 29	28	25, 26	27, 29	10
27	25, 26, 28	25, 26, 28	--	10, 27, 29	25, 26, 28	--
28		25, 27, 28	27	10, 29	25, 28	26
29		26, 28, 29	29	10, 27	26, 28	25
30		27, 28, 29	27, 29	10	28	25, 26
31	25, 27, 28	25, 27, 28	--	10, 26, 29	25, 27, 28	--
32		26, 28, 29	26, 29	10	28	25, 27
33		27, 28, 29	29	10, 26	27, 28	25
34	26, 28, 29	26, 28, 29	--	10, 25, 27	26, 28, 29	--
35		27, 28, 29	27	10, 25	28, 29	26
36	27, 28, 29	27, 28, 29	--	10, 25, 26	27, 28, 29	--

Since the  $N_o$ - and  $N_{eh}$ -element classifications are always interchangeable only 36 different classifications are shown.

It should be noted that once it is established that a given partition of the variables is a feasible proper partition then only specific interrelations among the admittance coefficients of the F-elements contained in the allowable subgraphs can result in this partition failing to qualify as a proper partition. Consequently there is a good possibility that most feasible partitions are also proper partitions. For example, within the partial listing of Tabulation 5.4.1 there are 16 feasible proper partitions in which  $N_{10}$  (the external N-element for this zone) is classified as an  $N_{eh}$ -element. In each case the partition is also a proper partition of the variables. Furthermore each of these proper partitions determines an additional proper partition by interchanging the  $N_o$ - and  $N_{eh}$ -element classifications. Hence of the 64 feasible proper partitions determined by the simple subgraph of Figure 5.4.10 at least 32 are also proper partitions of the variables. Consequently it is possible to select from a multiplicity of proper partitions those which are best suited for the particular study under consideration.

## Chapter 6

### SUMMARY AND SUGGESTIONS FOR FURTHER RESEARCH

#### 6.1. Summary

To effectively plan the current operation as well as the future expansion of electric power systems requires a knowledge of the operating characteristics of the existing and/or proposed systems. Analysis of a class of power system studies utilized in determining the electrical characteristics of a power system indicates that these studies are essentially problems in the analysis of electric networks. These studies differ from problems in "conventional" network analysis primarily in two aspects: (1) the size and complexity of the network under consideration, and (2) the type of initial problem specification. The availability of digital computers has alleviated, but not eliminated, difficulties associated with the size of the network. Problems associated with the initial specification of variables are more fundamental in nature and must be considered within the framework of the network equations since it is mandatory that inconsistencies are avoided. It is logical that a re-examination of the variable specification aspect of these network studies should originate at the level of the correlating graph and associated primary system of equations since they constitute the foundation for electric network theory.

The  $\omega$ -domain graph correlates of the network under consideration are comprised of two general types of elements: relation elements (F-elements) and no-relation elements (N-elements); the latter type is characterized by a lack of any fixed interrelation between the associated V and I variables and furthermore neither of these variables is specified initially. The resulting primary system of equations is homogeneous in form and certainly consistent. Properties of subgraphs of F-elements are subsequently utilized to define classifications of the N-elements such that either, neither, or both of their associated variables can be assigned arbitrary values with no danger of introducing inconsistencies. The investigation clearly indicates that a multiplicity of N-element classification patterns exist for a given graph and provides the basis for new and more general approaches to the analysis of electric networks--particularly those problems in which it is desired to maintain prescribed operating conditions.

## 6.2. Suggestions for Further Research

The most apparent area for further study, and the one in which current work is directed, is the application of these techniques to problems associated with specific power systems. As noted in the examples of Chapter 5 there exist a multiplicity of proper partitions, or N-element classification patterns, even in simple examples and in general the criteria for the selection of one or more of these allowable patterns is dictated by the system under consideration. A similar argument holds for the choice of zones

within a particular system. Another important concept is implicit in these studies and this regards instrumentation. It is conceivable that studies of this nature will indicate a need for new concepts and/or techniques in instrumentation if optimal operating conditions are to be maintained as the system size increases.

Other areas of suggested research include consideration of graphs containing more general configurations of N-elements and extension of the class of N-elements to include, for example, "coupling" between N-elements. Last, but not least, is the need for continuing investigations into the general properties of the primary system of network equations.

## BIBLIOGRAPHY

1. Ewald, E., and Anglund, D. W., "Regional Integration of Electric Power Systems," *IEEE Spectrum*, Vol. 1, No. 4, April 1964, pp. 96-101.
2. Stevenson, W. D., Elements of Power Systems Analysis, second edition, McGraw-Hill Book Company, Inc., New York, 1962.
3. Swidler, J.C., "National Power Survey and the Public Interest," *Proc. American Power Conference*, Vol. XXV, 1963, pp. 17-24.
4. Swidler, J. C., "The Electric Power Industry in the Decades Ahead," *Proc. American Power Conference*, Vol. XXVI, 1964, pp. 34-42.
5. Concordia, C., and Maginniss, F. J., "Developments in the Automation of System Planning During 1960," *Proc. American Power Conference*, Vol. XXIII, 1961, pp. 820-830.
6. Dillard, J. K., and Sels, H. K., "System Planning--Past, Present, and Future," *Proc. American Power Conference*, Vol. XXIV, 1962, pp. 928-938.
7. Fiedler, H. J., and Kirchmayer, L. K., "Digital Computer Control of System Operation," *Proc. American Power Conference*, Vol. XXV, 1963, pp. 868-878.
8. Ender, R. C., and Galloway, C. D., "Progress in Total System Planning--Generation, Transmission and Distribution," *Proc. American Power Conference*, Vol. XXV, 1963, pp. 812-822.
9. Friedlander, G. D., "Computer-controlled Power Systems," *IEEE Spectrum*, Vol. 2, No. 4, April 1965, pp. 60-81; and Vol. 2, No. 5, May 1965, pp. 72-91.
10. Reed, M. B., Foundation for Electric Network Theory, Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 1961.
11. Seshu, S., and Reed, M. B., Linear Graphs and Electrical Networks, Addison-Wesley Publishing Company, Inc., Reading, Massachusetts, 1961.

12. Hale, H. W., and Goodrich, R. W., "Digital Computation of Power Flow--Some New Aspects," AIEE Transactions, Vol. 78, pt. III, October 1959, pp. 919-924.
13. Van Ness, J. E., and Griffin, J. H., "Elimination Methods for Load-Flow Studies," AIEE Transactions, Vol. 80, pt. III, June 1961, pp. 299-304.
14. Zabrosky, J. and Rittenhouse, J. W., Electric Power Transmission, Ronald Press Co., New York, 1954.
15. Reed, M. B., Reed, G. B., McKinley, J. L., Polk, H. K., Hugo, R. V., and Martin, W. J., "A Digital Approach to Power-System Engineering-I, -II, -III, -IV," AIEE Transactions, Vol. 80, pt. III, June 1961, pp. 198-225.
16. Reed, M. B., and Reed, G. B., A Network Reduction-Restoration (Equivalence) Theory, Michigan State University Press, East Lansing, Michigan, 1964.
17. Ward, J. B., and Hale, H. W., "Digital Computer Solution of Power Flow Problems," AIEE Transactions, Vol. 75, pt. III, June 1956, pp. 398-404.
18. Brown, R. J., and Tinney, W. F., "Digital Solutions for Large Power Networks," AIEE Transactions, Vol. 76, pt. III, June 1957, pp. 347-355.
19. Glimm, A. F., and Stagg, G. S., "Automatic Calculation of Load Flows," AIEE Transactions, Vol. 76, pt. III, October 1947, pp. 817-828.
20. Van Ness, J. E., "Iteration Methods for Digital Load Flow Studies," AIEE Transactions, Vol. 78, pt. III, August 1959, pp. 583-588.
21. Dyrkacz, M. S., and Maginniss, F. J., "A New Automatic Program for Load-Flow Studies on the IBM 704," AIEE Transactions, Vol. 78, pt. III, April 1959, pp. 52-62.
22. Carlin, H. J., and Youla, D. C., "Network Synthesis with Negative Resistors," Proc. IRE, Vol. 49, May 1961, pp. 907-920.
23. Carlin, H. J., "Singular Network Elements," IEEE Trans. on Circuit Theory, Vol. CT-11, March 1964, pp. 67-72.
24. Birkhoff, G., and Mac Lane, S., A Survey of Modern Algebra, revised edition, The MacMillan Company, New York, 1953.

25. Gantmacher, F. R., The Theory of Matrices, Vol. I, Chelsea Publishing Company, New York, 1959.
26. Hohn, F. E., Elementary Matrix Algebra, The MacMillan Company, New York, 1958.
27. Mirsky, L., An Introduction to Linear Algebra, Clarendon Press, Oxford, England, 1955.
28. Thrall, R. M., and Tornheim, L., Vector Spaces and Matrices, John Wiley and Sons, Inc., New York, 1957.
29. Berge, Claude, The Theory of Graphs and Its Applications, John Wiley and Sons, Inc., New York, 1962.
30. Ore, Oystein, Theory of Graphs, American Mathematical Society Colloquium Publications, Vol. XXXVIII, Providence, Rhode Island, 1962.
31. Guilleman, E. A., Introductory Circuit Theory, John Wiley and Sons, Inc., New York, 1953.
32. Kim, W. H., and Chien, R. T., Topological Analysis and Synthesis of Communication Networks, Columbia University Press, New York, 1962.
33. Reed, M. B., and Seshu, S., "On Topology and Network Theory," Proc. U. of Ill. Symposium on Circuit Analysis, May 1955, pp. 2.1-2.16.
34. Seshu, S., and Balabanian, N., Linear Network Analysis, John Wiley and Sons, Inc., 1959.
35. Weinberg, Louis, Network Analysis and Synthesis, McGraw-Hill Book Company, New York, 1962.
36. Fujisawa, T., "On a Problem of Network Topology," IRE Trans. on Circuit Theory, Vol. CT-6, September 1959, pp. 261-266.
37. Maxwell, L. M., and Reed, G. B., "Subgraph Identification--Segs, Circuits, and Paths," Proceedings Eighth Midwest Symposium on Circuit Theory, June 1965, Colorado State University.
38. Mayeda, W., and Seshu, S., "Generation of Trees without Duplication," IEEE Trans. on Circuit Theory, Vol. CT-12, June 1965, pp. 181-184.

39. Minty, G. J., A Simple Algorithm for Listing all the Trees of a Graph," IEEE Trans. on Circuit Theory, Vol. CT-12, March 1965, p. 120.
40. Piekarski, M., "Listing of All Possible Trees of a Linear Graph," IEEE Trans. on Circuit Theory, Vol. CT-12, March 1965, pp. 124-125.
41. Reed, G. B., and Reed, M. B., "Patterns of Driving Elements such as Appear in Tube and Transistor Networks," Proc. 2nd. Midwest Symposium on Circuit Theory, Michigan State University, December 1956, pp. 3.1-3.16.

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