



8175

196-59

JUL 08 '83

66B-216

APR 19 '87

136 A 116

MAY 08 '89

400 A 070

OVERDUE FINES:

25¢ per day per item

RETURNING LIBRARY MATERIALS:

Place in book return to remove  
charge from circulation records

10 K058

338

OCT 13 '99

A COMPARISON OF DAIRY WASTE HANDLING SYSTEMS  
AND COMPONENTS THROUGH THE USE OF AN  
INTERACTIVE COMPUTER PROGRAM

By

Winston George Ingalls

A DISSERTATION

Submitted to  
Michigan State University  
in partial fulfillment of the requirements  
for the degree of

DOCTOR OF PHILOSOPHY

Department of Dairy Science

1980

## ABSTRACT

### A COMPARISON OF DAIRY WASTE HANDLING SYSTEMS AND COMPONENTS THROUGH THE USE OF AN INTERACTIVE COMPUTER PROGRAM

By

Winston George Ingalls

Twenty-five dairymen averaging 120 milking cows were interviewed to gain information on the type of waste handling equipment routinely used and the labor requirements of various waste handling tasks. In addition, 60 equipment manufacturers were canvassed for cost and performance data of waste handling equipment. The data from the two studies were utilized to describe each task according to initial cost, ownership costs, energy use and cost, labor use and cost, value of retained nutrients and net annual costs. The complete waste handling process was divided into eight sections and each section contained several options. An interactive computer program was subsequently designed to allow construction of all feasible systems for 100 to 300 cow dairy herds. Handling dairy wastes as a liquid provided the greatest number of feasible systems, but storage costs were generally much higher than with solids. Opportunities for saving labor exist primarily at the alley cleaning and movement to storage phases. In general, no single system emerged as always the best; rather, it depended on the owners' personal needs.

0114478

## ACKNOWLEDGMENTS

The author wishes to express his gratitude to his wife Ann for her patience and support during the course of the Ph.D. program.

Sincere appreciation is also extended to Doctors Lassiter and Hafs, who served as chairmen of the Dairy Science Department during the course of the thesis work and provided financial assistance for the program. Also I would like to recognize the assistance of my committee members, Dr. John Speicher of Dairy Science, Dr. Ted Loudon of Agricultural Engineering, Dr. Larry Connor of Agricultural Economics, and Dr. Maurice Vitosh of the Soil Science Department.

Finally, a very special note of thanks is extended to Dr. Roger Neitzel and Dr. Lee Shull who helped in a great many ways to make this effort a success.



## TABLE OF CONTENTS

	Page
LIST OF TABLES . . . . .	vi
LIST OF FIGURES . . . . .	viii
INTRODUCTION . . . . .	1
REVIEW OF LITERATURE . . . . .	3
Historical Perspective of Animal Waste Handling Systems and Research . . . . .	3
Agricultural Trends and Rural Population Profiles . . . . .	6
Pollution Control Legislation and the Livestock Industry . . . . .	9
Point Source Pollution . . . . .	9
Non-Point Source Pollution . . . . .	11
Nutrient Losses Associated With Waste Handling Systems . . . . .	13
Nutrient Content of Dairy Waste . . . . .	13
Nitrogen Losses . . . . .	13
Phosphorus and Potassium Losses . . . . .	14
Economic Impact of Controlling Agricultural Pollution . . . . .	15
Agriculture's Contribution to Water and Air Pollution . . . . .	15
Economic Impact of Controlling Feedlot Runoff . . . . .	16
Overall Impact of Non-Point Source Pollution Regulation . . . . .	17
Livestock Waste Handling System Selection and Comparison . . . . .	20
Waste Handling Routines . . . . .	20
Selection of Components for a Complete Waste Handling System . . . . .	22
Selection of a "Best" Waste Handling System . . . . .	24
RESEARCH OBJECTIVES . . . . .	29

	Page
RESEARCH METHODS AND PROCEDURES. . . . .	30
Labor and Bedding Requirements of Waste Handling Systems . . . . .	31
Farm Study of Labor and Bedding Needs of Waste Handling Systems. . . . .	31
Location of Farms . . . . .	32
Questionnaire and Arranging for Interview . . . . .	32
On Farm Interview . . . . .	33
Equipment Cost and Performance Survey . . . . .	35
Computer Program Development for Comparison of Waste Handling Systems . . . . .	37
Construction and Implementation of Interactive Program . . . . .	43
Variable Names and Descriptive Equations. . . . .	43
Creation of All Possible Systems. . . . .	49
RESULTS AND DISCUSSION . . . . .	52
Farm Survey and Equipment Survey Information . . . . .	52
General Discussion. . . . .	52
Bedding Material. . . . .	54
Bedding of Freestalls . . . . .	55
Time and Labor to Rebed Stalls. . . . .	57
Alley Cleaning Systems. . . . .	61
Automatic Alley Scrapers For Confinement Housing. . .	65
Movement of Waste Material to Various Storage Units . . . . .	69
Impellor Pump For Emptying Liquid Storage Units . . .	76
Impellor Pump and Irrigation Pump for Emptying Liquid Storage Units. . . . .	77
Solids Storage Unloading Equipment. . . . .	80
Movement of Waste Materials From Storage to the Field . . . . .	82
Irrigation Equipment for Waste Handling . . . . .	84
Comparison of Systems Available for 100 Cow Herds. . . .	88
Comparison Method 1 . . . . .	88
Comparison of Waste Handling Systems for 100 Cows on the Basis of Storage Type. . . . .	98
Nutrient Retaining Ability of Systems. . . . .	100
Comparison of Commonly Used Waste Handling Systems . . .	103
Initial Cost. . . . .	104
Energy and Labor Needs. . . . .	104
CONCLUSIONS AND RECOMMENDATIONS. . . . .	108
SUMMARY. . . . .	111

	Page
BIBLIOGRAPHY . . . . .	113
APPENDIX A: SURVEY QUESTIONNAIRE FORMS. . . . .	121
APPENDIX B: COMPUTER PROGRAMS FOR DETERMINING COSTS, ENERGY DEMANDS AND LABOR DEMANDS FOR VARIOUS WASTE HANDLING SYSTEMS. . . . .	129
APPENDIX C: COMPARISON OF 58 COMMONLY USED WASTE HANDLING SYSTEMS FOR 100-300 COW HERDS . . . . .	165

## LIST OF TABLES

Table	Page
1 Comparison of manure nutrient values from Roberts (1884) and MWPS-18 (1975). . . . .	4
2 Phases of dairy waste handling systems. . . . .	37
3 System phases and available options . . . . .	39
4 Feasible option combinations. . . . .	41
5 Variable names and descriptions . . . . .	44
6 Sample run of interactive program . . . . .	47
7 Output from computer run for typical system . . . . .	50
8 General description of 25 participating farms . . . . .	53
9 Frequency of bedding stalls with different bedding material . . . . .	56
10 Replacement interval for bedding (weeks). . . . .	57
11A Time and men required to add sand bedding . . . . .	58
11B Time and men required to add straw or sawdust twice monthly to stalls. . . . .	58
12A Time and men required to bed stalls with chopped straw or sawdust using a skidsteer loader. . . . .	59
12B Time and men required to bed stalls with chopped straw or sawdust using a front end loader. . . . .	60
13 Tractor scraping of confinement barn alleys . . . . .	62
14 Cost and energy usage of scraping tractors. . . . .	65
15 Cost figures for alley scraper components . . . . .	68

Table	Page
16A Manure transfer equipment for solid waste material (cross conveyor and stacker). . . . .	74
16B Manure transfer systems using piston pump or compressed air unit . . . . .	75
17 Cost of various storages designed for 100 cows and 180 day storage . . . . .	77
18 Cost, agitating capacity and pumping capacity of impeller pumps. . . . .	79
19 Cost of irrigation pumps . . . . .	79
20 Time to load 275 bushel solids spreader with skidsteer or front end loader . . . . .	81
21 Spreader capacities and unloading times for liquid tanker. . . . .	83
22 Comparison of stationary big gun sprinkler and the traveling gun system for irrigating liquid wastes . . .	87
23 Cost, labor and energy needs of floor cleaning options . .	90
24 Comparison of storage units for 100 cow herd size. . . . .	92
25 Storage filling options. . . . .	93
26 Storage unit emptying options. . . . .	94
27 Equipment used to move dairy wastes to the field . . . . .	96
28 Summary of waste systems according to storage types. . . .	99

## LIST OF FIGURES

Figure	Page
1A Solid blade scraper . . . . .	67
1B Folding blade scraper . . . . .	67
2 Piston pump and PVC pipe. . . . .	71

## INTRODUCTION

The enactment of the 1972 Federal Water Pollution Control Act and the subsequent development of supporting regulations created the impetus for economists, engineers, etc., to research the effects of compliance with such rules on all segments of the Nation's industry. This act specifically identified agriculture as a contributor of pollutants to the waterways of the Nation, from both point and non-point sources. Particulate matter, organic matter, bacteria as well as nitrogen, phosphorus and potassium compounds have all been discussed as emanating from agriculture.

The total agricultural community, from farmer to academician, has entered into the controversy regarding pollution control regulations on several fronts. One effort has been to involve agriculture supporters, those knowledgeable in modern agriculture practices, on committees which review proposals and develop plans of action for pollution control. Another major undertaking involved accumulation of reliable data from agriculture pursuant to the pollution problem. The Environmental Protection Agency and state agencies were given the task of formulating effective and reasonable pollution control standards. Finally it was the role of the agricultural academic community to use various objective analysis techniques to assess the impact of potential rules and regulations on production agriculture.

For livestock operations, such considerations as no spreading of manure on frozen or snow-covered ground, immediate soil incorporation and mandatory six months manure storage have been examined. Most studies were macro in nature, designed to assess total industry impact rather than specific farm effect.

In conjunction with the uncertainty of future pollution control regulations, many Michigan dairymen have been expanding to benefit from the scale effect of a larger operation. Expansion has involved new, larger facilities and/or additions to existing facilities. Many dairymen currently are in a position whereby consideration of all existing and potential rules dealing with pollution control must be examined to avoid future confrontations. For most, expansion via new construction allows incorporation of many desired features because all options are available with the only restrictions being those which are self-imposed. Many options exist for waste handling on dairy farms. Producers generally choose a system based on such factors as initial cost, labor demands, convenience, nutrient retaining ability, etc. It was in this framework that this project was initiated. The primary objective was to construct an interactive computer program which allows a dairyman flexibility to design and compare feasible systems for waste handling.



## REVIEW OF LITERATURE

### Historical Perspective of Animal Waste Handling Systems and Research

Material reviewed in this section has been published within the past 100 years. Obviously, reports on this subject were published prior to 1878; however, it was felt that most of the documented research relevant to this project occurred within this period and consequently only this material was reviewed. Also, publications of this era were examined to gain a general impression of research techniques and waste handling systems rather than specific methodologies.

A somewhat surprising and significant finding in the literature of this period was that not much has changed in 100 years relevant to manure nutrient content and the fate of such nutrients under various conditions. Scientists of then were aware of the nitrogen (N), phosphorus (P), and potassium (K) needs of plants. Chemical analysis of manures yielded N, P and K values comparable to present-day estimates. Table 1, comparing manure nutrient values from Roberts (1884) and MWPS-18 (1975), best illustrates this.

The material in Roberts' sample contained much bedding and would resemble manure from a bedded pack in a loafing barn and is quite similar to the MWPS-18 sample, which is solid manure with bedding. Despite 92 years of reexamination and improvement in

Table 1.--Comparison of manure nutrient values from Roberts (1884) and MWPS-18 (1975).

	Roberts (1884)	MWPS-18 (1975)
Moisture	72.95%	79.00%
Nitrogen	0.78%	0.45%
Phosphorus	0.40%	0.20%
Potassium	0.84%	0.50%

laboratory techniques, the figures published by Roberts (1884) remain reasonable estimates for dairy waste with bedding. In addition, Roberts (1884) established a value of the manure based on the concentration of the three major components. He applied values of 17¢/lb. of nitrogen, 7¢/lb. of phosphoric acid, and 4.25¢/lb. of potash, which resulted in a price of \$3.61 per ton of stable manure. These appear high compared with present-day prices. Vitosh (1975) valued cattle waste at \$5-10 per ton based on the N, P and K content.

Roberts (1891) published data on daily manure production per cow and the nutrient content of both liquid and solid fractions was analyzed separately. He found urine to have a high nitrogen content, which prompted his recommendation that the liquid portion of cattle waste be conserved to retain the nitrogen of the waste material. In his 1891 report to the Cornell University Experiment Station, the comment was included that he found it difficult to persuade farmers to change their waste handling methods. Most

farmers were unwilling to protect manure from the elements to maximize nutrient retention.

Sempers (1893) described farmyard manure as containing all the constituents of plant food. He cited manure as causing some disintegration of soils, having a warming effect on cold, clayey soils, and helping retain soil moisture and ammonia compounds. Sempers (1893), among others of this period, felt that faulty fermentation and leaching action of storms on unprotected manure caused great nutrient losses and rendered it practically useless as a fertilizer.

Fermentation was considered the most important process in proper management of farmyard wastes. Both anaerobic and aerobic processes were known to exist, and rotted manure was considered to contain more soluble organic matter than fresh manure. Caution was often taken to avoid "fire-fanging" of manure since it was believed this lessened its value. This process referred to the tremendous heat generated by piles of horse manure. Sempers (1893) suggested that to produce the highest quality manure it had to be kept under cover, with no drainage allowed and kept sufficiently high in moisture to reduce ammonia volatilization.

In 1913, Wheeler published a book entitled Manures and Fertilizers. He cited experiments conducted at Rothamstead Experiment Station in England as early as 1843, in which manure was used as a fertilizer source. Much of this early work dealt with plant nitrogen needs and how effectively manure met this need. Wheeler

(1913) wrote that practical utilization of manures involved hauling and rapid soil incorporation to conserve maximum nitrogen. He suggested also that manure should not be spread on frozen or ice-covered slopes due to potential runoff problems and loss of nutrients. Reference was made also to the timeliness problem of handling wastes; if manure was not applied as produced, a farmer might handicap himself in the spring by having to haul manure when planting should be scheduled. This could then lead to a series of delays and losses throughout the course of the year.

Over the past 80 to 100 years, most of the concerns cited by the aforementioned authors have not changed. Increased population and larger and more concentrated livestock industries, however, have focused substantially more attention on pollution control and recovery of animal waste nutrients as plant fertilizers.

#### Agricultural Trends and Rural Population Profiles

In order to understand the nature and scope of present agricultural waste management problems, some insight into the changes occurring in agriculture in general and dairying in particular must be gained. An appreciation must also come to exist of the constant reorganization of the makeup of the rural population in Michigan and other states.

The Michigan State University Agricultural Experiment Station and the Cooperative Extension Service in 1972 published a report entitled "The Michigan Dairy Industry of 1985." The intent

was to project the status of the Michigan dairy industry in 1985.

Some of the following predictions were made by authors contributing to the report:

1. The number of active dairymen in Michigan has been declining for the past 20 years, and it is expected that by 1985 only 3500-4500 Grade A dairymen will be selling milk.
2. The number of milk cows in 1985 will range from 320,000-400,000.
3. Herd sizes will dramatically increase. More than 25 percent of all dairies will have greater than 100 cows and 50 percent of all milk cows or more will be located on dairies with greater than 100 cows.
4. Man equivalents per farm will decrease to 2.5 by 1985, even though milk output per man will have dramatically increased.
5. Feed sources will consist of increased amounts of corn silage and grain mixes and less hay.
6. A great increase will occur in total confinement housing systems. It is estimated that by 1985, 35 percent of all herds and 55 percent of all cows will be in covered facilities.

Another point of concern for Michigan dairymen was illustrated by Hoglund et al. (1972) in an Agricultural Economics Report on waste management practices and systems for Michigan dairy farms. Their results indicated that 50 to 60 percent of all dairymen surveyed for their report had non-farm neighbors living within one-half mile of their barn area, and even a higher percentage had non-farm neighbors living within one-half mile of fields where manure might be spread.

In this same questionnaire, another potential problem reported by dairymen was their nearness to bodies of water. Thirty to 44 percent of dairymen with different types of housing and manure handling systems were within one-half mile of a lake or stream and 33 to 56 percent of these same dairymen indicated that one or more of the fields where they hauled manure was within a half mile of a stream or lake. In cases where land application of manure is close to navigable waterways, consideration must be given to proper procedures to avoid pollution.

Participating dairymen were asked, "Are you concerned about laws and regulations that might be passed or pressures from neighbors concerning manure odors or noise factors or water pollution? If so, how?" Sixty-five to 70 percent of all dairymen replied affirmatively, and the reasons varied from fear that the cost of complying with such regulations would be high to fear that non-farm neighbors would have no tolerance for animal odors. Another major concern was the uncertainty of what future environmental regulations might be promulgated by Federal and state agencies.

In general terms, Michigan dairymen will be milking greater numbers of cows per farm, the per-farm labor needs will increase as well as crop acreage, and more dairy farms will have non-farm neighbors near them. This set of projected conditions means increased potential for pollution by dairymen and their opportunities for confrontations with non-farm residents intolerant of odors, etc., will rise. This may force adoption of different waste handling methods to meet this problem.

Pollution Control Legislation and  
the Livestock Industry

Point Source Pollution

The demand for a cleanup of the Nation's water and air has been ongoing for decades. Such demands became even greater during the 1960's and eventually resulted in Congressional enactment of the 1972 Federal Water Pollution Control Act (F.W.P.C.A.). The stated objective of this legislation is to restore and maintain the chemical, physical and biological integrity of the Nation's waters. The agency charged with the responsibility of achieving these objectives is the Environmental Protection Agency (EPA).

On May 22, 1973, the EPA published in the Federal register its initial version of the policies and procedures for the National Pollutant Discharge Elimination System (NPDES) for agriculture. The significant factor for livestock owners was the specific identification of livestock operations as potential point sources of pollution which must either be contained or eliminated. The NPDES established a permit program which applied to specific point sources of pollution and considered only those operations which met certain criteria as outlined by EPA.

The level of pollution control, the timetable for achieving such standards and the control technology to be applied were stated in the following sections of the Federal Water Pollution Control Act:

Section 301.(b) (1) (A)  
not later than July 1, 1977 effluent limitations for  
point sources, other than publicly owned treatment

works will require the application of the best practicable control technology currently available as defined by the administration.

Section 301 (b) (2) (A)

not later than July 1, 1983 effluent limitations for categories and classes of point sources shall require application of the best available technology economically achievable for such category or class.

The point sources to be considered were as follows (Fed. Reg., Nov. 20, 1975):

- a. Man made drainage ditches, flushing systems or other such devices where measurable waste results and is discharged into water.
- b. Natural runoff from confined livestock operations if the following animal concentrations are exceeded: 1000 beef cattle, 700 dairy cows, 200,000 broiler chickens, 180,000 laying hens, 55,000 turkeys, 4500 slaughter hogs, 35,000 feeder pigs, 12,000 sheep or lambs, and 145,000 ducks.
- c. Any feedlot operations which result in direct discharge of wastes into a stream which traverses the feedlot regardless of number of animals involved.

Any animal feeding operation falling into one of the previous categories was required to apply for and obtain a permit.

The permit application, if accepted, would specify allowable amounts and constituents to be discharged and a schedule for achieving compliance. On March 18, 1976, in the Federal Register, EPA published some minor revisions to the permit program. Humenik (1976) has summarized the current permit requirements and has stated it as follows:

- 1. Permits are required for feedlots with 700 mature dairy cows that discharge pollutants.
- 2. Permits are required for feeding operations with less than 700 but more than 200 dairy cows only if



discharges of pollutants occur (a) through a man made conveyance or (b) directly into navigable waters which pass through the confined area.

3. Feedlots with less than 200 dairy cows are not subject to the permit requirements unless there is an on-site inspection and the owner or operator is notified in writing that such an application is required.

The enforcement of this program has been given to the states in most cases. In Michigan jurisdiction over this area rests with the Water Resources Commission, which is responsible for reviewing and issuing permit applications. Due to the nature of the livestock industry in Michigan, few permit requests have been submitted, and in those cases where a permit application has been made, the Commission has suggested elimination of the pollution via holding basins, etc., rather than issue a permit to discharge (personal communication).

#### Non-Point Source Pollution

Livestock operators have the potential to be point source polluters via feedlot runoff, milk house drains, drainage from waste storage facilities, etc. The EPA, however, recognized the major sources of agricultural pollution to be non-point source in nature (Federal Register, November 20, 1975). The F.W.P.C.A. (Section 208) also recognized non-point pollution to be a major problem both for agriculture and non-agricultural areas. Section 208 (a) (2) specifically assigned to the Governor of each state the responsibility of designating representative organizations to assess non-point pollution problems in various state areas and make

recommendations for abatement. With regard to agriculture, such designated groups have the following responsibilities:

Section 208.(b) (2) (F)

such a group shall consider a process to (i) identify if appropriate, agriculturally and silviculturally related non-point sources of pollution including runoff from manure disposal areas and from land used for livestock and crop production and (ii) set forth procedures and methods (including land use requirements) to control to extent feasible such sources.

At the state level, the Michigan Legislature (1970) passed the Environmental Protection Act. This act allows the Attorney General, any citizen, corporation, organization, governmental unit, or any other legal entity the right to bring action in the circuit courts of the state against any other citizen--entity for declaratory and equitable relief for the purpose of protecting the air, water and other natural resources of the state from pollution, impairment or destruction.

The implications of this bill are far reaching and somewhat indeterminate. Under this legislation one case (Clinton County Circuit Court File No. 844 [1971] was brought to court. In this case the farmer won, but many more challenges are likely to be seen in the future.

It is within the framework of ever-increasing rules and regulations pertaining to agriculture that tomorrow's dairymen must exist.

## Nutrient Losses Associated With Waste Handling Systems

### Nutrient Content of Dairy Waste

Loehr (1974), Midwest Plan Service-18 (1975) and Walsh et al. (1975), in addition to many others, have published representative figures on the nutrient content of animal waste. Caution must be exercised when dealing with such figures due to the variety of conditions under which they were generated, and on what basis they were reported. Some reports cite values for the minor elements, but practically all concentrate on nitrogen (N), phosphorus ( $P_2O_5$ ), and potassium ( $K_2O$ ). The reports previously noted indicate that dairy cattle manure (feces and urine combined) as it is excreted contains approximately 10.3 pounds N, 2.4 pounds  $P_2O_5$ , and 9.8 pounds  $K_2O$  on a per ton basis. Recently with higher priced commercial fertilizer, energy shortages and legislative mandates to control water and air pollution, more attention has been focused on the quantity of nutrients generated by animal industries and the ultimate fate of such nutrients.

### Nitrogen Losses

Nitrogen loss from waste systems generally is of greatest concern due to its mobility, pollutant potential and value as a crop nutrient. Fogg (1974) described N losses from various systems ranging from 15 to 85 percent, and Vanderholm (1975) cited comparable figures. Vanderholm (1975) also indicated that 50 percent of the nitrogen in fresh dairy manure is in the ammonia form, which is

highly volatile and rapidly lost under many circumstances. Heck (1936) described large nitrogen losses during the interval between hauling and spreading and soil incorporation. Nearly 75 percent of the ammonia nitrogen was lost in seven days post spreading if not incorporated into the soil. Lauer et al. (1976) reported similar ammonia losses from surface applied waste. Total ammonia loss ranged from 61 to 99 percent over a 5 to 25 day time period.

Another route of loss for nitrogen is via surface runoff. Young and Mutchler (1976) reported up to 20 percent of the manure nitrogen applied to alfalfa plots appeared in spring runoff. Loehr (1974) and the 1975 Agricultural Waste Management Field Manual of the Soil Conservation Service also include discussions on nitrogen loss from runoff in addition to losses via nitrate leaching.

#### Phosphorus and Potassium Losses

Phosphorus occurs primarily in soil as water insoluble compounds of aluminum, iron or calcium. In most cases these metals appear as free metals on clay particles and this helps explain the strong adsorption of phosphorus to soil particles (Loehr, 1974). Apart from feedlot and field runoff, agricultural practices which effectively control soil erosion should not contribute substantial amounts of phosphorus to streams and lakes. Potassium is not generally considered to be a problem in water pollution.

Therefore, in dealing with pollution from livestock operations, reduction of nitrogen losses assumes the highest priority due to its mobility in soil and water. The control of phosphorus

and potassium is no less important, but due to their stability in storage units and in the soil, they present less of a control problem.

### Economic Impact of Controlling Agricultural Pollution

#### Agriculture's Contribution to Water and Air Pollution

Some monitoring of pollutant runoff from manure covered fields and open feedlots or corrals has taken place in recent years. Such research has had two major goals. First, there needed to be established a data base for future pollution control guidelines, and second, such data could be used in answering the questions relevant to effective systems for storing and handling manure to reduce pollution and maximize nutrient retention for crops.

Reports on this subject are to be found in the 1969, 1972, and 1974 Proceedings of the Cornell Agricultural Waste Management Conferences and the Proceedings of the 1st, 2nd, and 3rd International Symposia on Livestock Wastes. R. C. Loehr (1974) deals extensively with this matter in his book, Agricultural Waste Management. Some of the most frequently used journals for publishing research pertinent to waste disposal and nutrient movement are:

- a. Journal of Environmental Quality
- b. Transactions of the American Society of Agricultural Engineers
- c. Water Resources Research
- d. Environmental Science and Technology

It is beyond the scope of this thesis to detail nutrient movement in soils, nutrient transformation or crop utilization of applied nutrients. A previous section on nutrient content of manure

and nutrient losses has briefly outlined these topics. Suffice it to say that it is an actively researched area with a rapidly growing body of literature.

#### Economic Impact of Controlling Feedlot Runoff

Enactment of the Federal Water Pollution Control Act (1972) caused all segments of the livestock industry to assess the economic impact of both point source and non-point source pollution control. Buxton and Ziegler (1974) estimated that if all U.S. dairymen were to control runoff from a 10 year maximum, 24 hour storm the total industry investment would approach \$780 million. This added investment would hit hardest the dairymen with 20 or less cows. They felt overall industry efficiency might improve, however, due to some smaller farms quitting the business or expanding and adopting more efficient techniques. The technology suggested by Buxton and Ziegler (1974) was designed primarily for larger herds. There may be control systems such as grass filtration areas, etc., which would suit the smaller producer and not prove to be financially overburdening.

Johnson and Davis (1974) analyzed the effect of pollution control regulations on the U.S. feed-beef industry. They focused on the 18 major beef states producing 95 percent of the U.S. beef. They determined that approximately 49,000 beefmen would have to make improvements totalling \$133 million.

A similar economic impact study for the swine industry suggested that 86,000 producers would be forced to invest to some

degree in new pollution control technology (Van Arsdall, 1974). The ultimate effect on consumer prices, however, appeared to be minimal because of improved efficiency as a result of new waste handling technology.

#### Overall Impact of Non-Point Source Pollution Regulation

Murphy (1974) noted that a comprehensive non-point source control program was inevitable. Section 208.(b) (2) (F) of the 1972 F.W.P.C.A. specifically applied to agriculture and it specified that agriculture non-point sources of pollution shall be identified and control measures recommended. Non-point source pollution control is mandated now, but the question is: how will it be implemented and what impact will implementation have on the dairy industry?

Buxton and Ziegler (1975) examined non-point source control measures in effect or under consideration by several states. They reported the following general categories of guidelines:

1. Restrictions on application rates of waste per acre. Such restrictions usually limit the amount of nitrogen, manure tonnage or number of animals per acre.
2. Restrictions on spreading manure on land adjacent to water or residences or on land exceeding a certain slope.
3. Restrictions on spreading on frozen or snow-covered ground.

Several studies have been conducted to determine the effect on livestock producers of certain point source and non-point source pollution control measures. Good (1972), using linear programming

techniques and synthesized representative dairy farms, measured the impact of applying the following controls:

1. Mandatory retention and disposal of surface runoff at the production site.
2. No winter spreading of wastes on the land.
3. Mandatory subsurface disposal of wastes.

The effect was measured in terms of labor requirements, costs of production and returns to the operator's labor and management. The absolute costs of various equipment were also included. Synthesized dairies were organized around specific herd sizes, housing systems and waste handling systems. Good (1972) found that compliance with the above control policies necessitated additional capital investment in waste handling equipment and increased the costs of milk production in all cases. Cold covered housing units incurred the least increase in total costs, while stanchion barns and open lot systems experienced the most increase. Cold covered, 160 cow operations had only a 5 percent reduction in returns to operator's labor, but stanchion operators with 40 cows suffered a 37 percent reduction. Therefore, the size factor was considered a potential cause of smaller operators either leaving the dairy business or expanding. Such regulation would in effect favor larger operations.

Using beef feedlots as the model and pollution abatement policies similar to Good's (1972), Forster (1974) indicated compliance would cause some reduced beef production and increased production costs. Economies of size were again noted with operations feeding greater than 100 head experiencing less added costs per head



than those feeding lesser numbers. For all feedlots, adoption of the rules would tend to increase asset fixity due to investment in durables. Effect on consumers was considered to be very limited, with the main impact being a reduction in beef surpluses. Small feedlot cutbacks might be offset by larger feedlot increases. Forster (1974) concluded that the main implications of imposing such rules would be highly uncertain and unidentified benefits.

Another approach used to assess runoff control costs was presented by Schaffer et al. (1974). Their working model consisted of a small watershed in New York State. They developed predictive equations for estimating losses of nitrogen, phosphorus and soil. Once the losses were calculated, an economic analysis was done to determine the costs of farmers of reducing these losses by specific amounts. Results indicated significant costs to farmers if nutrient and soil losses were to be reduced by any substantial percentage.

One of the more obvious conclusions resulting from the various economic impact studies is that small farm units will suffer more costs per cow than larger units. This may force smaller units to either terminate their business or expand to take advantage of economies of size. Economies of size exist with all other farm systems, so there is a constant pressure to expand.

Stoll (1974) analyzed problems associated with expansion of Michigan dairy farms. Of the 47 herds studied, the problems cited in order of importance were: animal health, labor, heat detection and manure handling. Expanded farms experienced some production

losses, increased culling, 13.1 percent increased veterinary usage during early expansion, and 8 percent increased calf losses during years one and two of expansion. Reproductive problems also increased significantly. Finally, nearly 68 percent of all expansions experienced cash flow problems lasting approximately two years with 10 percent of those being considered serious.

It appears that the assumptions used in many economic analyses are so rigid that there is no way to include changes in managerial effectiveness which may accompany many of the expansion projects. This is difficult to quantify, but it may explain some of the trends noted by Stoll (1974) and should be brought to the attention of the farmer who is considering expansion.

To summarize the economic impact of controlling agricultural pollution, certain conclusions can be drawn. First, more extensive pollution control measures are inevitable and agriculture must be prepared to comply. Second, waste handling is only one of many farm activities and is certainly not considered a revenue generating unit. Therefore, waste handling techniques will have to be selected which interfere minimally with other farm enterprises. This means multidisciplinary thinking is needed to develop the best total system.

### Livestock Waste Handling System Selection and Comparison

#### Waste Handling Routines

The EPA guidelines and permit program prompted three main questions from livestock producers:

- a. What are the standards to be met?
- b. What systems are available to meet these standards?
- c. How much will compliance cost?

Environmental Protection Agency guidelines were finalized by 1976, but even prior to that most farmers were aware of the standards relevant to point sources. Regarding non-point sources, however, the specific requirements to be followed have still not been fully formulated or published. Much speculation still exists about the specific nature of these controls.

Many authors have characterized the waste handling routine on livestock farms. Ogilvie et al. (1975) described the process as involving the following four basic steps: (1) collection of manure; (2) transfer to storage; (3) storage; and (4) transfer to land. Cluever and Lubinus (1977) and the Soil Conservation Service (1975) both presented on-farm waste handling routines very similar to Ogilvie et al. (1975). Each author described how, within each phase of the operation, a variety of equipment is available. The job then becomes one of choosing the various components of the complete system to produce a workable unit which is compatible with the farmer's capital and labor restrictions.

Several authors have examined viable components and systems and calculated their initial costs, operating costs, and labor needs. Johnson et al. (1972) reviewed many feasible systems on this basis. They examined herd size, barn styles, etc., in various geographic regions of the nation. Runoff problems varied greatly; open lots have greater compliance problems than other systems. Most dairies would have to invest in additional storage capacity if field

spreading is to be done at times of the year when runoff would be minimal, i.e., before spring planting and immediately post harvest.

Graves (1975), in an update of an earlier report by Berge (1971), evaluated waste systems available for 50 and 100 cow herds. He described a daily haul system as having the lowest initial investment and a stacking system for solids had the lowest total annual cost. Below building tank systems cost the most, but the cost of the floor was not included. Slotted floor units were considered to be less expensive than below building tank systems. This was due mainly to no expenditures for alley cleaning equipment. On a total annual cost basis stacking cost the least while tanks or silo systems were the most expensive. The high annual costs of ownership associated with liquid systems more than offset the labor savings.

Hoglund (1976) developed investment costs, annual costs, labor needs, tractor power and electrical energy requirements for several waste management options designed for 40 to 200 cow herds. In all cases below building storage proved to be the most expensive.

#### Selection of Components for a Complete Waste Handling System

Within each phase of a waste system many different components are capable of fulfilling the job requirements. The main differences among components are their labor needs, energy consumption or initial cost. The technique of selecting components and building a system has been discussed by various authors. The objective is usually to assemble a system for the least initial cost, least annual costs or least labor.

When evaluating time to do a particular job, techniques such as PERT (Program Evaluation and Review Technique) or SPNA (Shortest Path Network Analysis) have application. Hanratty (1975) outlined PERT and its mode of application. Use of this technique allows computation of the earliest completion time of a project by selection of components which use the least time.

Ogilvie et al. (1975), using SPNA, determined least cost swine and dairy waste handling systems. They figured the fixed, variable and labor costs for 100 potentially usable components and on this basis calculated a least cost network. Economies of size were also noted for the system studied. The high fixed costs of liquid systems made total costs less favorable for larger herds, but variable costs of liquid units ranged from 50 to 70 percent of the variable costs of all other systems over all herd sizes considered.

Safley (1974), using what he termed "network analysis," conducted a study similar to that of Ogilvie et al. (1975). His program allowed a large number of components to be interchanged and the initial and annual costs were calculated for each complete system as well as the labor requirements. With this method, oxidation ditch systems and covered manure storage proved the most expensive to build and operate, while daily haul and outdoor stacks were the cheapest.

Safley and Price (1976) added to the network analysis by incorporating a factor for manure nutrient value into the various systems. This fertilizer value was then subtracted from the operating costs to give a value for "net system cost per year." By

using this method any system which had the capacity to retain nutrients would be favored. Systems with daily haul or outdoor stacks still ranked high due to their low initial investment, while liquid systems with injection had the highest fertilizer value. Based on the network analysis Safley (1977) had one very sound conclusion. He stated that there is no one "best" system for all farms and that the decision for system choice depends on a combination of factors such as net annual costs, personal preference, odor control and management requirements.

#### Selection of a "Best" Waste Handling System

Despite Safley's (1977) statement that there is no one "best" system, several authors have attempted to define one (Pherson, 1974; Forster, 1974; Good, 1972). Their analysis techniques have used simulation or linear programming and, in certain cases, the two have been used in combination. In such situations "best" is generally reserved for that system which either minimizes costs or labor associated with waste handling or allows maximization of farm profits. When the criteria for systems comparisons are costs, labor needs or energy requirements, the programs work well. However, when the criteria for selection become more abstract (i.e., water quality, air quality or aesthetics), such techniques are less feasible.

Whereas the literature cited in the previous section did not concern itself with labor or capital restrictions, several

optimizing routines have been devised which do. Amir and Ogilvie (1977), working with swine waste systems, constructed a model to choose the best combination of components to minimize annual operating costs.

Their results showed different systems were optimum for different herd sizes but in all cases a fully slotted floor with underfloor tanks, pump and tanker was the second best choice. No inverse relationship was found between capital invested and the required manpower.

Safley et al. (1977) extended their previously cited work by devising an optimization routine for dairy manure handling systems based on linear programming techniques. The model was for a specific herd size and designed to examine a complete year. The object of the model was to minimize the cost of manure handling. Those factors which were constrained were labor, energy, herd size, land available and fertilizer value of manure. Solution of their model indicated a daily haul system had the lowest annual operating costs.

Mote and Taiganides (1975) simulated a swine farm and devised subroutines for each component that influenced the disposal of wastes. The following subroutines were included:

1. Waste production rate for a specific swine population
2. Waste storage
3. Soil trafficability
4. Field application of waste

The program called for field application when the storage unit reached a preestablished level, but before hauling commenced, soil conditions, crop growth and previous waste application had to

be checked. If for any reason the waste could not be hauled, the excess was considered overflow and assigned a cost.

Two problems were noted. Large storage units which were allowed to completely fill up tended to need emptying when soil trafficability was poor or crop development prohibited spreading. The second problem was the need for cropping programs which included some land available for waste application. Cropping programs with all corn proved to be the worst in this regard for swine operations. Although not an optimization program, this model did consider all phases of the farm operation and their interaction.

As was indicated previously, enterprise interdependence is an important consideration in systems design. Not only is the total labor required critical, but more importantly, when is it required? With waste handling, the goal is to build a system which permits the farmer to minimize labor competition with other jobs both on a daily and seasonal basis.

Pherson (1974) recognized this situation when he examined ways of defining the optimal beef farmer response to Minnesota environmental regulations. He dealt with both direct and indirect costs associated with compliance and, using a whole farm analysis approach, attempted to maximize profits. Indirect costs were crop yield reduction due to late planting or harvesting because of the necessity of having to dispose of animal wastes at critical times. Pherson (1974) used linear programming to maximize profits when options were available on housing styles, cropping plans, feeding



calves or yearlings, and waste handling techniques. Linear program modelling allowed the development of a year-round schedule for all activities including planting schedules, and the waste system was then matched to best fit other farm operations.

Results indicated a slotted floor, liquid system generated the greatest returns to labor and the solid waste systems ranked second. Pherson suggested the following reasons for this ranking:

1. Slotted floors seemed to have a faster cattle turnover rate.
2. No bedding is necessary.
3. Earlier planting and harvesting was possible due to more rapid waste handling.

This approach considered interactions among various farm operations and timeliness of these operations as important factors. A premium was placed on systems which allowed cattlemen to get onto cropland early in the spring and devote time to cropping. Similarly, waste systems which detracted minimally from harvesting routines were rated higher. Other systems were recognized to be so inflexible that competition resulted between them and other farm routines. Such systems were penalized by suffering increased indirect costs. The method used by Pherson (1974) combines elements of maximizing returns and constructing compatible enterprises on a whole farm basis.

To summarize a review of the literature, it is clear that federal and state pollution regulations, proximity to navigable waterways and non-farm rural residents, farm expansion and system convenience are major factors that will need to be considered in evaluating existing and future waste handling systems. Safley (1974)

concluded that no "best" system exists for the dairy industry. Furthermore, each unit must be constructed in a manner to accommodate the personal preferences of individual dairymen. The criteria by which dairy farmers select a system are numerous. However, it appears the following list encompasses most of these factors: (a) total initial cost; (b) daily labor requirements; (c) peak labor demands; and, when they occur, (d) energy demands; (e) maintenance needs; and (f) nutrient conserving ability of the system. The main problem confronting dairymen is not having an organized method to incorporate selected evaluation criteria so that comparisons of several complete units can be made with little or no previous knowledge about actual systems.

## RESEARCH OBJECTIVES

It has been previously noted that the number of total possible waste handling systems available to dairymen is large. The best way for an operator to appraise a system he is considering is to locate a functioning unit and spend time discussing it with the owners and observing the individual components during operation. Unfortunately, time often does not allow this and, when it does, only a few systems might be observed. With these considerations in mind, the main objectives of this research were as follows:

1. Identify components available for each phase of waste handling systems.
2. Collect up-to-date price and performance information for waste handling equipment.
3. Gather labor data for equipment usable at each phase of the waste handling process.
4. Develop or adapt a methodology which would allow large numbers of feasible systems to be assembled and analyzed on the basis of initial cost, energy and labor needs, nutrient conserving ability, annual total costs and net annual costs.
5. Evaluate and compare systems and individual components over various herd sizes.

## RESEARCH METHODS AND PROCEDURES

The ability to synthesize large numbers of functional waste handling systems from individual components and subsequently compare them depends on two factors. The first is a data base which accurately represents individual components, thus allowing construction of representative systems. Secondly, due to the large number of systems that potentially exist, the high speed computational ability of present-day computers must be utilized or otherwise time becomes a limiting factor when attempting to assemble and compare systems.

For the systems which shall be described later, data collection was needed for the following categories of factors:

- a. Cost figures for equipment, labor, energy and bedding
- b. Labor demands of various waste handling jobs
- c. Energy needs of each task
- d. Depreciation, interest, repair and insurance rates
- e. Bedding requirements
- f. Volumes and nutrient content of waste
- g. Performance data for various equipment.

There exist in the literature large amounts of data pertaining to the previous list. Unfortunately, much of it is insufficiently documented or detailed to be of use to this project.

Those studies which did report data with a detailed discussion of

their collection methods and system design were utilized only when the present study failed to provide such information.

#### Labor and Bedding Requirements of Waste Handling Systems

Labor data for specific waste handling tasks are limited and often subject to interpretation due to inadequate descriptions of the methods used for data collection. MacLachlan (1966) and Safley (1974) have both published well documented labor statistics for various waste handling tasks. MWPS-11 (1972) has also published labor requirements for various irrigation methods when used for handling animal wastes. These three reports comprise the bulk of usable labor data pertaining to handling of animal wastes.

In order to establish a sizable data base on labor needs of waste handling components, a survey was conducted on 35 Michigan dairy farms with 100 or more milking cows. This lower limit in herd size was chosen due to the large number of dairy herd expansions which culminate with that number of milking cows. A second reason was that most expansion projects involve construction of new facilities capable of housing increased cattle numbers. Expansion minded dairymen usually attempt to examine feasible alternatives and during this planning stage the only restrictions are those which are self-imposed.

#### Farm Study of Labor and Bedding Needs of Waste Handling Systems

The main study involved 32 dairymen in Clinton County, located 20 to 30 miles north of the Michigan State University campus.

Farmers were selected through the recommendations of the Clinton County Extension agents who were familiar with the county dairymen. The only selection criterion was that dairymen have approximately 100 or more milking cows. The waste handling systems in use were expected to represent a majority of the system components and systems most frequently observed for such herd sizes. With 32 farms on the study, sufficient numbers of each system component were anticipated for the most commonly used equipment to allow statistical comparisons.

#### Location of Farms

The dairymen identified by the county agents were located in each of the various townships within the county. In order to facilitate the process of identifying each farm, where it was located, and adjacency to other dairymen, a county platt book was purchased and each dairyman's location was identified and marked.

#### Questionnaire and Arranging for Interview

Prior to actually identifying specific farms, a questionnaire was prepared for use at each farm. It was designed to gather most of the relevant information about each dairyman's waste handling technique. The questions as they appeared in the questionnaire are listed in Appendix Table A.1. This material was not sent directly to the dairymen; rather, it was prefaced by a letter of introduction explaining what the project involved and who was conducting it. Subsequent to the preface letter, each farmer was telephoned and the intent of the project was again explained and a farm visit

request was made. If the farmer was unwilling to participate for whatever reason, he was not coerced into it; rather, he was thanked for his time and it was suggested that the results of the study might eventually be of some assistance to him.

It was expected that a two or three hour block of time would be required for each farm visit, so at best three visits per day would be the maximum. Prior to calling to arrange for an interview, the farm locations within each township were noted. This allowed dairymen in the same vicinity to be scheduled for interviews on the same day and thus reduced the miles driven between interviews. All interviews were to be conducted in July and August, and this meant a schedule which had to avoid conflicts with haying, wheat harvest and vacations.

The time gap between the telephone call and farm visit was important due to the tendency of farmers to forget appointments. Within two days of the phone call they still anticipated the visit, but by day four their reaction was much less positive, nearly surprise in some cases. When a dairyman expected the interviewer's arrival, he was generally prepared to give his time freely, but when he was a bit unprepared, it usually required some diplomacy to get him into the proper mood to cooperate and participate fully.

#### On Farm Interview

The previously described telephone contact established a day and a specific time for the interview. First interviews of the day were generally scheduled for 8:30 or 9 a.m. Most dairymen had

finished milking, eaten breakfast and were cleaning up by this time. Initially a second morning visit was attempted, but farmers enjoy talking and so usually only one morning interview was completed. A second visit was scheduled with another farm at 1 p.m. and, if possible, a third was arranged for 3 p.m. Many dairymen start milking about 3:30 p.m., so this time slot was not always used. A self-imposed factor in the interview procedure was punctuality. Being punctual did not force alterations in the farmer's schedule, established a degree of confidence and allowed for a more organized interview. Farm operators are extremely busy and plagued by many unexpected interruptions, so an interviewer should not further complicate a dairyman's schedule.

The farm interview was intended to be conducted directly with the individuals involved with waste handling. In many cases this was a son, partner or hired man. In such cases, both the owner and assistant were involved in the interview. In no instance was an interview conducted without first talking to the owner. Most owners also needed reassuring at the outset that all information was to be kept confidential and we only wanted data pertaining to their waste handling system.

The farm visit was not to gather time-motion data on various waste handling chores. Rather, the laborer was quizzed regarding how much labor and time each job required and what equipment was used for each job. It was felt that each worker routinely did the same job over a period of months or years and consequently was able to provide sufficiently accurate data for each event. In many



cases farmers would elaborate on an answer and such comments were included if pertinent.

Initially 32 farms were available, but due to rejections and farms that had too few cows, the final number of usable herds was 25. The raw data were summarized and are presented in the results and discussion section.

#### Equipment Cost and Performance Survey

In order to price complete waste handling systems, individual component prices were necessary. New equipment prices are subject to wide ranges depending on equipment size, options selected and terms of sale. For this work prices reflect factory prices on new equipment, sized and equipped in a comparable manner to that which was described by dairymen in the farm survey. As an example, the farm survey indicated most dairymen with solids handling systems used a 280 bushel capacity solids spreader equipped with tandem wheels and a hydraulic end gate. Consequently, performance and price information was solicited for this spreader.

Each January, Dairy Herd Management magazine publishes an extensive list of manufacturers and dealers of farm equipment according to type of use. Using this listing, approximately 60 firms which sell waste handling equipment were identified. Following company identification, a general cover letter was prepared to accompany the requests for information. The contents specified why such information was needed and what use would be made of information provided. In addition, it was made clear in the letter

that specific company names would not be endorsed or used in the study but that all cooperating firms would be acknowledged. This letter is presented in Appendix Table A.2.

Accompanying the letter to each firm was a standardized list of the various types of equipment for which cost and performance figures were required. When this list was sent to specific firms, those pieces of equipment manufactured by that company were checked on the list and this indicated to the letter recipients what information was being requested (Appendix Table A.3).

As the equipment information was supplied by various companies, it was summarized according to category of use on the basis of cost and, in the case of powered equipment, on the basis of fuel consumption, i.e., garden tractors, skidsteer loaders, etc.

Another extensive source of information on tractors and some other equipment was the Official Guide Tractors and Farm Equipment (1977). It is issued quarterly and contains cost figures on new and used equipment as well as fuel consumption and horsepower ratings of both later and earlier model tractors. Solids spreaders were also listed in this guide. This source provided data for fuel consumption and initial price of the various sized tractors used in the systems.

These two sources provided most of the equipment specifications. Various local dealers were also contacted, but in most cases they had no interest in the project and consequently were usually reluctant to provide even minimal information. There were

some very cooperative dealers also, but many were either too busy or too suspicious to provide necessary data.

Computer Program Development for  
Comparison of Waste Handling  
Systems

Ogilvie et al. (1975) outlined the process of handling animal wastes on the farm. Their concepts of this procedure involved up to seven distinct steps. Within each step there are several possible options. If a farmer were to build a new system, he would need to select from among various options for each phase of the system. The decision would be based on few or no restrictions if a completely new facility is constructed, or it might include existing equipment combined with new options to create a new unit. Table 2 presents the various phases of a complete waste handling system for dairy which were utilized in this project. Each phase also has a designated section number.

Table 2.--Phases of dairy waste handling systems.

Waste Handling Phases	Section Number
1. Stall type	01
2. Bedding material and method of distribution to stalls	02
3. Floor style	03
4. Floor cleaning procedure	04
5. Movement to storage	05
6. Storage	06
7. Storage agitation and emptying	07
8. Movement to field and land application	08

Phases 1 and 2 are not considered by most authors. However, it was felt they are important here because they are involved in decision making and a decision influences subsequent option selection; thus, they were included. An example of their importance is illustrated by assuming sand is the desired bedding material. Sand's lack of absorbancy makes it a poor choice for concrete stalls and it is incompatible with liquid systems.

Following the selection of the waste handling phases, consideration was next given to available options within each phase. Table 3 lists all options for liquid and solids systems. This list formed a table of option titles which were stored as a permanent file at the MSU computer center under the permanent file name, WITITLES.

The second aspect of the decision model involved development of a table which listed only feasible option combinations from adjoining phases and eliminated impossible pairings regardless of reason. Elimination of a solids spreader from a liquids system using an impellor pump for storage emptying is an example.

The starting point for this task commenced with the assignment of a number (Section Number) to each waste handling phase and to each option (Option Number) with each phase (Table 3). As can be seen, a two digit number was assigned to designate individual phases of the system and they were numbered as follows: Stall Type (01), Bedding and Method of Distribution (02), Floor Style (03), Alley Cleaning Systems (04), Movement to Storage (05), Storage (06),

Table 3.--System phases and available options.

Waste Handling Phase	Section Number	Available Options	Option Number
Stall Type	01	Clay	01
		Concrete	02
Bedding Material and Distribution Method	02	Sawdust (SKS)*	01
		Sawdust (FEL)**	02
		Chopped Straw (SKS)	03
		Chopped Straw (FEL)	04
		Sand (SKS)	05
		Sand (FEL)	06
		Rubber Mats, Shavings (SKS)	07
		Rubber Mats, Shavings (FEL)	08
		Rubber Mats, Chopped Straw (SKS)	09
		Rubber Mats, Chopped Straw (FEL)	10
Floor Style	03	Solid	01
		Slatted	02
Floor Cleaning	04	Automatic Alley Scraper	01
		Skidsteer Loader	02
		Garden Tractor	03
		Utility Tractor & Blade	04
		Flushing	05
		None	06
Movement to Storage	05	Cross Conveyor & Short Elevator	01
		Cross Conveyor & Stacker	02
		Piston Pump & PVC Pipe	03
		Cross Conveyor, Piston Pump, PVC	04
		Cross Conveyor, Compressed Air Unit, PVC	05
		Concrete Ramp	06
		None	07
		Concrete Flume	08
		None (Slatted Floor)	09
Storage	06	Cement Silo	01
		Steel Silo	02
		Earth Basin (Solids) & Liquids Basin	03
		Earth Basin Liquids	04
		Paved Slurry Basic	05
		Concrete Pit Under Slats	06
		Concrete Tank Under Barn	07
		None	08
		Settling Basin & Lagoon	09

Table 3.--Continued.

Waste Handling Phase	Section Number	Available Options	Option Number
Agitation and Emptying	07	Impellor Pump	01
		Front End Loader	02
		Skidsteer Loader	03
		Self-Loading Spreader	04
		None	05
		Impellor & Irrigation Pumps	06
Movement to Field and Land Application	08	Self-Loading Spreader	01
		Tanker (3200 gal.)	02
		Tanker & 4-Row Injectors	03
		Solids Spreader	04
		Aluminum Pipe & Stationary Big Gun Sprinkler	05
		Aluminum Pipe, Flexible Hose Traveling Gun Sprinkler	06

\*SKS = skidsteer

\*\*FEL = Front End Loader

Agitation and Storage Unloading (07), and Movement to Field and Land Application (08).

Each option within a phase of the system was then numbered with a two digit number, 01 being Option 1 in each phase. For example, Alley Cleaning Systems (04) has six options numbered 01 to 06, and Movement to Storage (05) has options numbered 01 to 09. This procedure was followed for all eight system phases.

The next step involved creation of all feasible option-option combinations beginning with Phase 01, Option 01, and Phase 02, Option 01, and continuing through Phase 07, Option 06 and Phase

08, Option 06. By doing this, all feasible stall/bedding, bedding/floor, floor/cleaning method, cleaning method/move to storage, move to storage/storage, storage/storage emptying, and storage emptying/movement to field combination--were assembled. Table 4 is an example of the option-option combinations. These actual examples represent 12 of the 103 total combinations.

Table 4.--Feasible option combinations.

	Section Number	Previous Option	New Option	Actual Code of New Option
1	01	01	01	01
2	01	01	02	02
3	02	01	01	10
4	02	01	02	11
5	02	01	03	12
6	02	01	04	13
7	02	01	05	14
8	02	01	06	15
9	02	02	01	10
10	02	02	02	11
11	02	02	03	12
12	02	02	04	13

For an explanation of how the option combinations are listed, an examination of lines 1, 2, 3 and 9 from Table 4 is necessary. In lines 1 and 2, section number 01 refers to stall type as listed in Table 2. Since stall type selection represents the initial decision, there is no previous option, but 01 is entered in this slot as a filler. The new option code, 01, designates the first option within stall type and in this case refers to clay stalls. Line 2 is identical except that new option 02 is used, which represents concrete stalls. The actual code of the new option refers to the permanent numerical code given each option and is reported in Table 3. In the case of the first two lines, the new option numerical code and the actual code of the option are identical because of stalls being the starting point of system description.

Line 3 presents the first option combination between two phases, stall type and bedding type. Previous option 01 refers to clay stalls from line 1 and new option 01 designates the first compatible bedding source (sawdust [skidsteer]), which has as its actual code the numerical designation, 10. All feasible clay stall, bedding type combinations are subsequently defined in a similar manner. Line 9 reflects a switch to a new stall type. It is still in section number 02, but concrete stalls (02) now become the previous option. The first compatible new option (01) again refers to sawdust bedding with a skidsteer, and in Table 4 this is coded 10. This process was repeated until all concrete stall, bedding



combinations were established. It then advanced to section 03, floor style, and all compatible floor styles and bedding combinations were listed. The establishment of combinations was completed when the last emptying of storage, movement to field pairing had been constructed. All option combinations were stored for future use under the permanent file name, WICODES.

#### Construction and Implementation of Interactive Program

Prior discussion described various phases and options available for waste handling systems. In this section, the equations used to describe individual options and complete systems shall be discussed. In the research objectives section, a list was formulated which represented the majority of factors used by dairymen in selecting a manure management scheme. Based on that list, a series of equations was developed for each option which defined initial cost, or DIRT I costs, energy usage and cost, labor requirements and cost, bedding needs, annual costs for operating and total annual costs, the nutritive value of the waste material and net annual costs. The complete series of equations appears in Appendix Table B.1.

#### Variable Names and Descriptive Equations

Each factor used to describe some aspect of a particular option was assigned a variable name which in most cases was mnemonic. Table 5 lists several variable names together with a description.

Table 5.--Variable names and descriptions.

Variable Name	Description
CSLABOR	Labor costs per hour
STDIRTR	Stall DIRT rate
STWCSTD	Daily straw costs
UTOPCSY	Utility tractor operating costs/year
EBSDIGC	Cost/cubic yard to dig an earthen basin

Variable names were limited to seven digits, and if they referred to an integer number they commenced with the letters, I, J, K, L, M, or N as is the rule for standard Fortran language.

Many of the variable names describe some aspect of an option that is constant, i.e., amount of urine and feces produced per cow per day. Although there is some variation in this factor, it is often assumed to be fixed. Other variable names define rates of production or usage. Two examples from the slotted floor section of Appendix B illustrate this:

(a) SLOTCFT = 2.25

(b) SLFDEPR = 0.05

The first example defines the cost of a square foot of slatted floor at \$2.25, and item (b) describes the per annum depreciation rate as 5 percent. For each of the approximately 1400 variable names there is an accompanying comment statement describing each one. The variable name, SLOTCFT, described above is preceded in the program

by a statement which reads: cost of slotted floor alley (\$/sq. ft.). The values associated with each fixed variable were derived primarily from data gathered in the two studies described earlier. In some instances literature values were used when the survey data failed to provide them.

The second type of equation describes values derived from calculations involving multiple variables. In all cases such equations and the associated variable name define a total for cost, labor, etc., relative to a specific herd size. An example from Appendix Table B.1 is:

$$\text{VOLMSTW} = \text{TVMANDY} + \text{WSMHTFT} + \text{VOLSTDY}$$

In this case, VOLMSTW describes the total daily volume of manure, milk, house waste and straw entering the manure storage unit. The variable name TVMANDY refers to the total daily volume of urine and feces, WSMHTFT designates the total daily volume of milkhouse wastes entering the storage unit, and VOLSTDY specifies the daily volume of straw.

With the completion of all the variable names used to describe the options, all the necessary components to build a complete waste handling system were available. The final essential element was a computer program which could assemble various systems in their entirety and describe them in designated terms. It was decided that the technique allowing the greatest flexibility and opportunity to personalize the systems was an interactive model which could be

operated by an operator with a minimal amount of computer training. With this approach as a goal and the expert technical assistance of Dr. Roger Neitzel, the effort to develop such a program commenced.

The language chosen was Fortran. It was compatible with the CDC 6500 computer available at MSU and posed no problems in terms of writing the program. All inputs and outputs were dimensioned at the beginning of the program. Section titles and option titles from the WITITLES and file, and feasible options from the WICODES permanent file, were all read in according to the appropriate format. At this point with the interactive model, a user of this program receives a printed statement from the computer which specifies the program's capabilities. Table 6 is an example of the type of interaction that occurs between user and computer during operation of the program.

It can be seen in Table 6 how a decision at each phase forces the program to advance to the subsequent section and present compatible options. Option selection is made by typing in the appropriate three-digit code for the desired choice. Following this step the computer asks if you wish to use the option selected. If the reply is affirmative, it proceeds to the next section. If the response is negative, all options for that section will again be presented and the user can make an alternate choice.

Following the last decision in section 8, the operator is asked to indicate via a three-digit number how many cows the system is to accommodate. Finally, a choice of barn styles is allowed; either a two alley, four alley or a custom built facility can be

Table 6.--Sample run of interactive program.

---

This program calculates the cost associated with a particular waste management system.

There are eight sections of criteria needed to complete this task. The sections are as follows:

- 1 Stall type
- 2 Bedding type
- 3 Floor type
- 4 Alley cleaning systems
- 5 Movement to storage
- 6 Storage systems
- 7 Emptying and agitating equipment
- 8 Field transport and application

For each section there are several options. When prompted with an asterisk, type in the code for the option desired in I3 format, IE 002. For all possible options from this point on-type 000.

Section 1      Stall Type

<u>Code</u>	<u>Option</u>
1	Clay stalls
2	Cement stalls

You wish to use clay stalls.  
Type Y for Yes, N for No

Is that correct?

Section 2      Bedding Type

<u>Code</u>	<u>Option</u>
10	Sawdust (Skidsteer)
11	Sawdust (Front End Loader)
12	Chopped Straw (Skidsteer)
13	Chopped Straw (Front End Loader)
14	Sand (Skidsteer)
15	Sand (Front End Loader)

You wish to use Sawdust (Skidsteer).  
Type Y for Yes, N for No.

Is that correct?

Section 3      Floor Type

<u>Code</u>	<u>Option</u>
20	Solid floor
21	Slatted floor

You wish to use solid floor.  
Type Y for Yes, N for No.

Is that correct?

Table 6.--Continued.

---

<u>Section 4</u>	<u>Alley Cleaning Systems</u>	
<u>Code</u>	<u>Option</u>	
30	Auto alley scraper	
31	Skidsteer	
32	Garden tractor	
33	Utility tractor	
34	Flushing	
You wish to use auto alley scraper.		Is that correct?
Type Y for Yes, N for No.		

<u>Section 5</u>	<u>Movement to Storage</u>	
<u>Code</u>	<u>Option</u>	
40	Cross conveyor and short elev	
41	Cross conveyor and stacker	
43	Cross conveyor ram and PVC	
44	Cross conveyor and air unit	
46	None	
You wish to use cross conveyor and stacker.		Is that correct?
Type Y for Yes, N for No.		

<u>Section 6</u>	<u>Storage Systems</u>	
<u>Code</u>	<u>Option</u>	
62	Earth basin solids and liquids B	
You wish to use earth basin solids and liquids B.		Is that correct?
Type Y for Yes, N for No.		

<u>Section 7</u>	<u>Emptying and Agitating Equipment</u>	
<u>Code</u>	<u>Option</u>	
81	Front end loader	
82	Skidsteer loader	
You wish to use skidsteer ladder.		Is that correct?
Type Y for Yes, N for No.		

<u>Section 8</u>	<u>Field Transport and Application</u>	
<u>Code</u>	<u>Option</u>	
103	Solids spreader	
You wish to use solids spreader.		Is that correct?
Type Y for Yes, N for No.		

---

utilized. Once the barn style has been designated, the user's input is complete and the program makes the appropriate calculations relative to costs, labor, energy, etc. In fact, calculations are not made for specific systems; rather, all calculations are made for a designated herd size and the calculated values are entered into appropriate arrays. Subsequent to this the operator receives a listing of the system options he previously selected. Finally, the appropriate figures for the system selected are taken from their array locations and printed out with explanatory headings, etc. A typical output from the program is demonstrated in Table 7.

After the complete system is listed as in Table 7, the program automatically readies itself for another possible run. All values which were calculated are zeroed out and the files containing WITITLES and WICODES are rewound to the beginning. Following this the operator is asked if he wants to analyze another system. An affirmative response starts the series of questions described in Table 6. If the response is negative, the interaction ends and the user is able to log out.

#### Creation of All Possible Systems

In addition to the need for an interactive computer model to create selected waste systems, it was also necessary to develop all possible systems for various herd sizes. This would then permit comparisons on the basis of labor, energy costs, etc. An operator prerogative was included in the program for this purpose. Following the presentation of the two stall choices, if the three-digit code

Table 7.--Output from computer run for typical system.

The following options have been selected for system number 1

<u>Section</u>	<u>Component</u>	<u>Option</u>
1	Stall type	Clay stalls
2	Bedding type	Sawdust (Skidsteer)
3	Floor type	Solid floor
4	Alley cleaning systems	Auto alley scraper
5	Movement to storage	Cross conveyor and stacker
6	Storage systems	Earth basin solids and liquids B
7	Emptying and agitating equipment	Skidsteer loader
8	Field transport and application	Solids spreader

Network analysis output for dairy waste handling systems.  
Outputs are based on the number of cows in the herd: 100

<u>System Components</u>	<u>Initial Costs</u>	<u>Annual Cost of Ownership PCT(DIRTI)</u>	<u>Annual DIRTI Totals</u>
Stall type	1080.00	.14	242.55
Bedding material	90.03	0.00	345.60
Floor style	9625.00	.14	1299.38
Alley cleaning system	5042.00	.26	1326.05
Movement to storage	3241.50	.28	917.34
Storage system	14440.74	.15	2093.91
Unloading of storage	10500.00	0.00	193.45
Movement to field and application	5000.00	.25	1250.00
Total System Costs	49019.24	1.21	7668.27

	<u>Yrly Mhrs of Labor Used (Comp-Event)</u>	<u>Yearly Labor Costs</u>	<u>Units of Energy Used Per Year (Comp-Event)</u>
Stall Type	0.00	0.00	0.00
Bedding material	43.20	151.20	120.95
Floor style	0.00	0.00	0.00
Alley cleaning system	17.16	60.06	16118.40
Movement to storage	29.20	102.20	503.70
Storage system	0.00	0.00	0.00
Unloading of storage	24.18	84.63	67.71
Movement to field and application	87.54	306.39	418.56
Total System Costs	201.23	704.48	



Table 7.--Continued.

	Yearly Energy Costs (Comp-Event)	Yearly Bedding Used	Yearly Bedding Costs	Annual Costs (Comp-Event)
Stall type	0.00	0.00	0.00	242.55
Bedding material	70.16	78.84	1576.80	2143.76
Floor style	0.00	0.00	0.00	1299.38
Alley cleaning system	805.00	0.00	0.00	2191.11
Movement to storage	25.19	0.00	0.00	1044.73
Storage system	0.00	0.00	0.00	2093.91
Unloading of storage	39.27	0.00	0.00	317.35
Movement to field and application	217.65	0.00	0.00	2430.57
Total System Costs	1157.26	78.84	1576.80	11763.35
Yearly value of manure				5004.15
Net System Cost				6759.20
Do you want an analysis of another system?				

000 was entered in place of either 001 or 002, all feasible systems would be constructed and non-feasible combinations deleted. Due to the large number of possible systems, the output was stored on tape for further reference with each system being coded for later identification.

## RESULTS AND DISCUSSION

The results of this project shall be discussed in two general sections. The first section will deal with the farm survey and the cost and performance data acquired from the manufacturers of waste handling equipment. From the farm survey the discussion will center on type of equipment, type of storage and labor requirements of various waste handling tasks. The second section will deal with the initial cost, labor and energy requirements, nutrient conserving ability and net annual cost of the many systems which were generated by the computer program.

### Farm Survey and Equipment Survey Information

#### General Discussion

Approximately 25 of the original 32 farms selected for the survey supplied usable data for the project. Farms were deleted for a variety of reasons, including (a) too few cows; (b) owners who did not agree to participate; and (c) inability to make contact with the farm operator or establish a mutually acceptable interview time. Table 8 summarizes the general characteristics of the 25 farms used. Herd size averaged 120 cows and ranged from 70 to 160 milking cows. This satisfied the initial requirement of a 100 cow average herd size. The daily labor force of three full-time men

Table 8.--General description of 25 participating farms.

---

Average number of cows	120 $\pm$ 39
Average daily labor force (full time)	3 $\pm$ .84
Confinement housing	8
Open lot with freestalls	17
Clay stalls	66%
Cement stalls	34%
Sawdust bedding	61%
Straw bedding	23%
Sand	16%
Storage--3 months or more	9
Liquid storage	3
Solids storage	6
Average hauling distance (miles)	.33 $\pm$ .20

---

usually included the owner, a son or relative and a full-time hired man or two. In several cases the work force consisted solely of family members. Farmers tend to avoid hired labor if possible, so full-time employees are kept to a minimum. It appeared that most farmers delegate the waste handling chores to sons or the hired man and opted to use their seniority to do other tasks.

Eight of the 25 facilities visited were confinement barns and only one of the eight was a warm enclosed building. All total confinement units had been built within the past seven years, while all facilities with outside lots were older. Most older barns had

four or five 40 to 50 foot alleys which were perpendicular to the barn length and each alley was flanked by freestalls. New barns had two or four alleys which ran parallel to the barn length, the full length of the building. The new confinement facilities have no need for multiple access to an outside lot, so parallel alleys are more logical.

Clay or dirt bottomed stalls were favored by two-thirds of the dairymen and concrete base stalls were used by the others. Many farmers with clay stalls inquired about concrete stalls. Most were concerned that they would be too cold in the winter or they would cause cow discomfort. The main complaint from clay stall owners was the necessity to occasionally fix holes in the stall bottom caused by cows digging out dirt with their feet. This job was usually done twice yearly and involved about 15 minutes per stall to add fresh material and level out the dirt base.

#### Bedding Material

Sawdust (61 percent), straw (34 percent), and sand (16 percent) were the bedding materials used. Sawdust and shavings are still quite plentiful and inexpensive. Some operators only pay hauling costs and the material is free. If purchased, the price is \$20 to \$30 per ton delivered compared to \$50 to \$75 per ton for straw and \$3.00 to \$4.00 per cubic yard of sand. Sawdust is preferred due to ease of handling, price, and compatibility with both liquid and solid systems. Straw was used mainly in a chopped form with a few daily haul situations using long-stemmed baled straw.

Many dairymen grow oats or wheat and provide their own bedding material for the cost of processing and storage. Chopping the straw makes it pack better, provides more surface area for moisture absorption, it stays in the stalls better and is compatible with pumps used for moving manure slurries.

Sand was used on six farms. Those using it felt the cows stayed clean and its availability and cost also favored its use. The sand generally came from the immediate vicinity of the farm, and the cost of acquisition amounted to digging and hauling costs. Dairymen not using it questioned its ability to keep cattle clean and dry and its coldness in winter weather. Sand bedding was observed to have two limitations. With liquid systems it is very abrasive on pumps, causing accelerated wear, and in storage units it settles out to form a non-pumpable layer on the bottom. The second limitation was with a flushing unit. As cows drag sand out of the stalls it builds up in two or three days in sufficient quantities to divert the flow of water and lessen the efficiency of flush cleaning. This necessitates scraping the alleys with a tractor and blade two or three times weekly to remove the impediment to water flow.

#### Bedding of Freestalls

The movement of bedding material to stalls and into each stall is accomplished with a skidsteer loader or a utility tractor equipped with a front mounted bucket. These units generally do double duty by also cleaning the alleys. During the farm survey,

dairymen were asked how frequently the stalls were rebedded, what equipment was used, how many people were involved, and how much time was required. Three observations were not included due to uniqueness. One added baled straw daily by hand, a second replaced the sawdust bedding every six months, while the third dairyman used an unloader trailer normally used for fence line feeding. It took him 20 minutes weekly to bed 220 stalls. Due to lack of data on this bedding method, it was not used as an option, but due to its labor-saving potential it should eventually be included. Table 9 summarizes the 22 observations on frequency of adding bedding. Sawdust was the most commonly used bedding material. In Table 10 the average interval between addition of fresh material is shown for the three bedding types.

Table 9.--Frequency of bedding stalls with different bedding material.

Bedding Replacement Intervals (Weeks)	No. Observations/Bedding Material			Total
	Sand	Sawdust	Straw	
0.5	-	-	1	1
1.0	1	3	3	7
1.5	-	1	-	1
2.0	2	2	1	5
3.0	-	-	-	0
4.0	<u>1</u>	<u>6</u>	<u>1</u>	<u>8</u>
	4	12	6	22

Table 10.--Replacement interval for bedding (weeks).

	Bedding Type			All Types
	Sand	Sawdust	Straw	
Replacement Interval (Weeks)	2.3 ± 1.3	2.7 ± 1.4	1.6 ± 1.3	2.3 ± 1.4

Straw is replaced more often than either sand or shavings or sawdust. Two explanations for this are possible. First, straw, even when chopped, is more easily pushed out of stall bottoms by cows than either sand or sawdust. Second, straw is generally stored on the farm near the barns, which allows easy access to it. Usually a one-year supply is readily available. Both sand and sawdust are generally procured from a more distant source in quantities sufficient to bed all stalls once and when again needed this procedure is repeated. This inconvenience often deters dairymen from bedding stalls more often, especially if other jobs are pressing.

#### Time and Labor to Rebed Stalls

According to Table 10, bedding material is routinely added to stalls about every two weeks on the average. The time and manpower required are shown in Tables 11-A and 11-B.

Due to only four observations with sand bedding, no major conclusions can be drawn. It appears that use of a skidsteer loader and two men is an efficient combination. Those dairymen using sand bedding and skidsteer loaders all indicated the maneuverability of the skidsteer allowed the sand to be dumped directly into the stalls.

Table 11.A.--Time and men required to add sand bedding.

Farm Number	Loader Used	Hours to Add Sand to All Stalls	Number of Stalls	Number of Men
1	Front End loader	6.00	85	1
2	Skidsteer	0.75	120	2
3	Skidsteer	1.00	110	2
4	Skidsteer	<u>1.00</u>	<u>105</u>	<u>2</u>
		$\bar{X} = 2.2 \pm 2.5$	$\bar{X} = 105 \pm 14.7$	$\bar{X} = 1.75 \pm 0.5$

Table 11.B.--Time and men required to add straw or sawdust twice monthly to stalls.

Farm Number	Loader Used	Time to Rebed Stalls Twice Monthly (Hrs)	Number of Stalls	Men Involved
1	FEL*	0.75	110	3
2	FEL	1.50	65	1
3	FEL	4.00	180	1
4	FEL	5.00	90	1
5	FEL	1.00	110	4
6	SKS**	1.00	100	1
7	FEL	1.50	80	3
8	FEL	2.50	90	1
9	SKS	1.00	85	2
10	FEL	1.50	80	3
11	SKS	0.50	110	2
12	SKS	2.00	115	2
13	FEL	1.00	75	2
14	SKS	4.00	90	2
15	SKS	1.00	115	2
16	FEL	<u>3.00</u>	<u>145</u>	<u>1</u>
		$\bar{X}=1.95 \pm 1.36$	$\bar{X}=102.5 \pm 28.58$	$\bar{X}=1.94 \pm .93$

\*FEL = Front end loader; \*\*SKS = Skidsteer



This greatly reduced hand labor involved with spreading the heavy sand. The front end loader, being physically larger and less maneuverable, does not allow the sand to be optimally placed, resulting in a good deal of hand labor. The use of one man with a front end loader for sand bedding appears to be slow and inefficient.

Chopped straw and sawdust were combined in Table 11.B due to their similar bulkiness and handling characteristics. Two men may be involved in the task, but one man doing it alone is also common. However, the total time involved with one man is usually somewhat higher. With two men doing the bedding, the average time for 102 stalls is nearly two hours using either a skidsteer or front end loader. The data of Table 11.B are expressed according to type of loader used in Tables 12.A and 12.B.

Table 12.A.--Time and men required to bed stalls with chopped straw or sawdust using a skidsteer loader.

Hours Required to Bed Stalls	Number of Stalls	Men Involved	Man-Hours Per Stall
1.0	100	1	.01
1.0	85	2	.02
0.5	110	2	.01
2.0	115	2	.03
4.0	90	2	.09
1.0	115	2	.02

Table 12.B.--Time and men required to bed stalls with chopped straw or sawdust using a front end loader.

Hours Required to Bed Stalls	Number of Stalls	Men Involved	Man-Hours Per Stall
0.75	110	3	.02
1.50	65	1	.02
4.00	180	1	.02
5.00	90	1	.06
1.00	110	4	.04
1.50	80	3	.06
2.50	90	1	.03
1.50	80	3	.06
1.00	75	2	.03
<u>3.00</u>	<u>145</u>	<u>1</u>	<u>.02</u>
2.18	102.5	2.0	0.04

It appears that use of a skidsteer slightly reduces the time required to bed freestalls, but both systems average two men when rebedding. Leveling and distributing the sawdust or straw is not a strenuous task, thus leaving the laborer with small amounts of idle time between bucket loads. This open time is not sufficient, however, to allow anything else to be accomplished due to its limited duration.

When the bedding time was computed on a monthly basis as time per stall, the average was .04 hours/stall/month using two people or .08 manhours/stall/month.



### Alley Cleaning Systems

Among the survey farms, six were confinement facilities using some type of tractor scraper to clean the alleys, and one utilized an automatic alley scraper. The six tractor scraped facilities were combined with two other such farms which were part of an earlier study comparing alternate alley cleaning systems. Table 13 summarizes the alley dimensions of the barns, the type of equipment used to clean alleys and the time required for cleaning using the various equipment available.

Table 13 reveals that confinement barns with either two or four alleys are the most common for herd sizes of 80 to 160 cows. Alley length is a function of cattle numbers and number of alleys, and in this study the range was 150 feet to 320 feet. The shorter barns allow manure to be pushed to one end of the facility for removal or movement to storage. When barn lengths approach 200 feet, the tendency is to scrape one-half the alley to each end or from each end to the middle. It may be pushed into a pit or tank under the barn, off a ramp directly into a storage basin, or into a cross conveyor for movement to a stacker or piston pump. One problem with scraping long alleys all to one end is that the manure generally spills over or off the blade, thus reducing scraping efficiency. This situation is more of a problem for automatic alley scrapers than tractor scrapers.

Alleys in five of the eight confinement facilities were scraped twice daily. Confinement lessens floor space per animal,

Table 13.--Tractor scraping of confinement barn alleys.

Farm No.	Number of Alleys	Scrapings/Day	Minutes/Alley	Minutes/Scraping Event	Total Time/Day	Alley Length	Tractor Type
1	2	1	10	20	20	280	Utility
2	2	1	15	30	30	320	Utility
3	2	2	6	12	24	150	Utility
4	4	2	4	15	30	150	Skidsteer
5	2	2	10	20	40	150	Utility
6	2	1	15	30	30	260	Skidsteer
7	2	2	9	18	36	184	Garden
8	2	2	10	20	40	175	Garden
$\bar{X} = 2.25$		$\bar{X} = 1.6 \pm 5$	$\bar{X} = 9.9 \pm 3.8$	$\bar{X} = 20.6 \pm 6.4$	$\bar{X} = 31.3 \pm 7.2$	$\bar{X} = 208.6 \pm 67.8$	

and their feet are always wet. Manure accumulation per square foot of area is greater in confinement barns and this factor, combined with concern for cow cleanliness and foot problems, has many dairymen convinced that twice daily scraping is essential. Greater incidence of foot problems has not been substantiated, and stall cleanliness is probably more of a determinant of cow cleanliness. Finally, clean floors make the barn more presentable to visitors and to many dairymen this is important enough to justify the frequent cleaning with an alley scraper.

Cleaning time per alley averaged about 10 minutes regardless of the type of tractor used or alley length. Most barn lengths range from 170 to 250 feet and, as previously mentioned, long alleys usually are scraped in halves. Consequently, turning ability is important to speed of cleaning in many circumstances. Each of the three tractor types have specific advantages which offset each other. The utility tractor is less maneuverable but has a wider blade and is faster than either skidsteers or garden tractors. The skidsteer and garden tractor are more maneuverable than utility tractors when tight turns are necessary. Apart from the tractors themselves, alley design is the largest factor determining speed of cleaning. If curbs are straight or have no abutments projecting into the alley, the job is easy to complete in a short time. In many barns such obstructions exist which may increase cleaning time. With tractor scraping as described in this section, daily scraping time would be approximately 40 minutes, or 243 hours annually.

The utility tractors being used for alley cleaning are not the old, 25 HP Fords or Fergusons of 25 years ago. The average horsepower rating was 53 for utility tractors and 38 for skidsteers. Such utility tractors are popular due to their versatility for scraping, loading, moving wagons and use on PTO driven equipment. The skidsteer is limited mainly to scraping and loading operations and this makes it difficult for many dairymen to justify owning one.

Table 14 presents the cost for new utility tractors and skidsteer loaders of the horsepower rating previously described. The initial cost of the utility tractor and blade is about \$1,100 more than a skidsteer loader and, partly due to its greater horsepower rating, consumes more fuel. This initial price was charged entirely to the waste handling routine, but ownership costs, etc., were charged only according to the amount of time the unit was used on a yearly basis in doing that job, i.e., scraping, loading, etc. Charging all of the initial cost to waste handling is meant only to show how much such equipment would cost if it had to be purchased. Ownership costs are a more realistic view of machinery costs as it takes into consideration the time that machine is used for a particular job. Based on 500 to 600 yearly hours of use, the hourly fixed costs when using the utility tractor were calculated to be approximately \$7.75 and for skidsteer loaders it was \$8.00 per hour. This higher hourly charge for the skidsteer reflects the lesser number of hours the machine is utilized.

Table 14.--Cost and energy usage of scraping tractors (1978 figures).

50-60 HP Utility Tractor & Blade	Initial Cost (\$)	Fuel Used Per Hour	35-40 HP Skidsteer	Initial Cost (\$)	Fuel Used Per Hour
1	11,415	4.2	1	10,295	2.8
2	12,876	4.1	2	8,645	3.2
3	10,823	-	3	8,635	3.4
4	12,092	4.0	4	8,496	3.1
5	11,353	3.9	5	10,100	3.2
6	11,635	4.0	6	9,793	-
7	11,337	4.2	7	12,896	2.6
8	<u>11,350</u>	<u>4.3</u>	8	<u>13,587</u>	<u>2.5</u>
	$\bar{X}=11610.13$ $\pm 621.20$	$\bar{X}=4.10$ $\pm 0.14$		$\bar{X}=10,435.73$ $\pm 1,864.84$	$\bar{X}=2.95$ $\pm 0.32$

#### Automatic Alley Scrapers For Confinement Housing

When cleaning freestall barn alleys with tractor scrapers, the routine usually involves moving one group of cows into the holding pen for milking and then scraping the alley which the cows just vacated. Because this routine requires labor and the use of a fairly expensive tractor, some dairymen have looked for alternatives. Several firms currently manufacture automated alley scrapers which generally consist of some type of scraper blade attached to a continuous chain or cable set in a groove in the concrete floor that runs the entire length of the barn. This continuous chain is





pulled by a drive unit similar to that in a gutter cleaner. It generally is powered by an instant reversing 2.0 horsepower electric motor. The blades may be either rigid or folding. Both types of scrapers are illustrated in Figures 1A and 1B.

The blade is pulled down the alley at eight to ten feet per minute and the manure is pushed along in front of it. This speed is slow enough to allow cattle to step over it or move out of the way with no problem. Such cleaners generally have a safety switch designed to automatically stop the motor if the blade is obstructed, such as with a cow lying in the alley. Despite this safeguard, some mishaps have still occurred. The alley cleaners may be operated continuously, manually or with a time clock set for any interval desired. The latter is the most commonly observed.

Such scrapers allow floors to be cleaned frequently without moving the cows or disturbing them. They save labor and keep floors quite clean depending on the scraping interval. They are well suited for high density housing situations where excessive manure buildup could pose a problem. Also, cattle do not have to be moved out during cleaning. They are limited, however, by barn lengths exceeding 200 feet due to blade overloading. In such cases nearly continuous operation is required which results in increased wear and greater energy consumption. In most cases observed the units ran approximately 10 to 12 hours per day, or about one-half hour out of each hour.

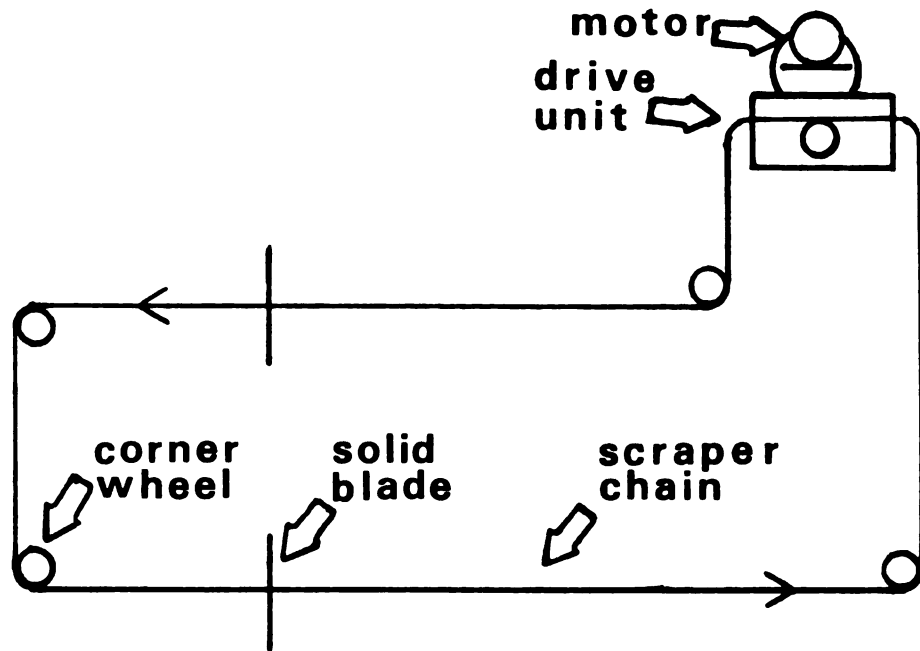


Figure 1A.--Solid blade scraper.

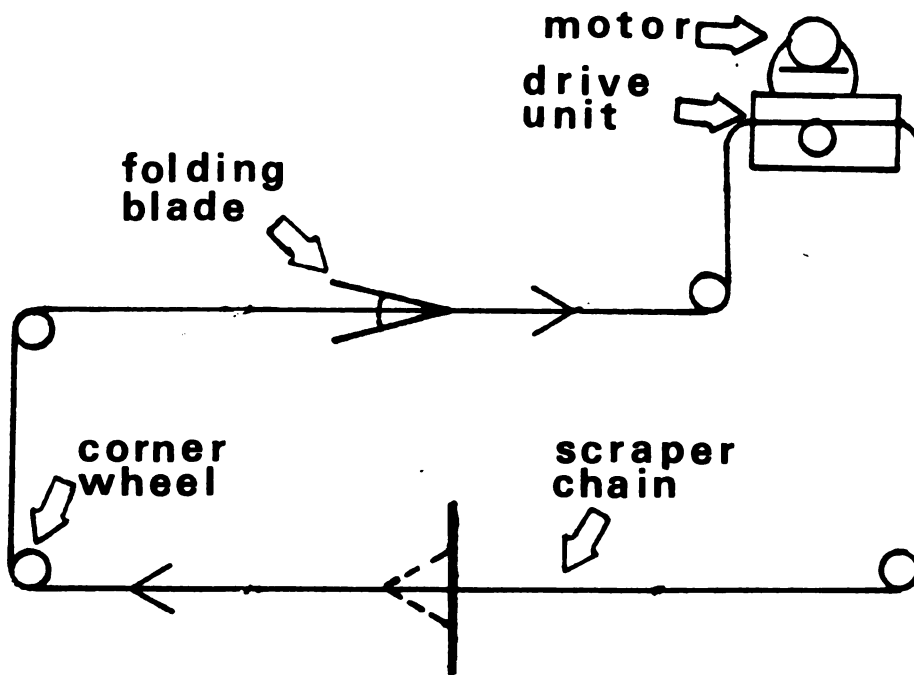


Figure 1B.--Folding blade scraper.



The cost of such units varies according to the manufacturer and a total cost is comprised of the cost for the chain, motor, drive unit, corner wheels and blades. Typical cost figures for several different brands are shown in Table 15.

Table 15.--Cost figures for alley scraper components (1978).

Company	2 HP Motor & Drive Unit & Corner Wheels (\$)	Cost/Foot of Chain	Cost/Foot of Groove Liner	Blades
1	2,686.00	-	-	226.45
2	2,175.00	5.40	-	260.00
3	2,575.00	6.50	1.85	145.00
4	1,702.00	5.05	2.00	225.00
5	<u>1,986.00</u>	<u>5.40</u>	<u>1.50</u>	<u>250.00</u>
	$\bar{X}=2,224.50$ $\pm 365.56$	$\bar{X}=5.59$ $\pm 0.63$	$\bar{X}=1.78$ $\pm 0.26$	$\bar{X}=221.29$ $\pm 45.23$

A drive unit package usually includes the gearing system, four corner wheels and the transmission. The cost of a single phase, reversing 2 horsepower motor must be added to the drive unit package. Chain costs and runner costs amount to approximately \$7.37 per foot. The groove liner listed in Table 15 is a plastic type track that fits into the bottom of the groove in the concrete floor. It resists wear and, due to its smoothness, lessens chain wear as well. Example 1 in Table 15 used a 3/8 inch cable to pull the blade. It was strung about two inches above the floor and

needed no groove in which to run. This system is less common than those with drag chains running in a groove. The standard chain costs about \$5.60 per foot and is nearly identical to gutter cleaner chain. Finally, scraper blades cost about \$220.00 apiece and there is one per alley. The abrasiveness of the concrete causes wear, and may increase the frequency of repair or replacement depending on how frequently they are operated.

#### Movement of Waste Material to Various Storage Units

The method used to move manure to storage depends primarily on the consistency of the material and the type of storage utilized. The most basic combination involves a slatted floor over a pit. Defecated waste drops directly through the slots or is worked through by the action of cattle hooves. Another simple technique utilizes a concrete pit under a barn, with the barn floor being part of the tank roof. A slot is built into the floor and manure is scraped to it and allowed to drop into the tank. Tractor scrapers and automatic alley scrapers can be used with this type of storage. Both systems eliminate the equipment, labor and energy necessary to move waste to storage, but storage costs can be high. Concrete pits cost approximately \$1.00 per cubic foot of storage and when urine, feces and milk house cleaning water is all added to the pit the volume per cow per day can approach 3.0 cubic feet. One hundred eighty-day storage costs approximately \$54,000 per 100 cows. Such storage units are only for liquid wastes; too many solids create emptying problems.

Other liquid storage units include above-ground concrete and steel silos and earth basins. Here again, about 3.0 cubic feet/cow/day is needed along with a factor to account for rainfall that may add to the volume to be stored. Concrete silo storage costs about \$0.70 per cubic foot and steel silos cost approximately \$0.90 per cubic foot. Earth basins with no concrete in the bottom and a cement ramp average about \$1.25 per cubic yard excavated. This lack of concrete makes the earth basin the most economical form of storage.

The most common method used to fill silos and earth basins is with a piston pump which is situated in the barn. The manure is moved into the receiving hopper and it is then forced by the piston through a 12-inch diameter PVC pipe which empties into the bottom of the storage unit. Figure 2 illustrates how this type of system might work with various types of storage. The manure can be scraped directly into the hopper. More liquid materials facilitate pumping. Drier material is difficult to pump for long distances and may cause plugging. Often the parlor waste water is pumped into the cross conveyor or water is added directly to the receiving hopper from a water source near the pumping unit to optimize pumping.

The piston itself can be either hollow or solid. The hollow piston tends to plug more easily with coarse bedding. Turns in the pipe are kept to a minimum with each elbow being embedded in concrete to stabilize it. Pumping distances up to 160 feet are possible. Greater pumping distances increase the risk of plugging. This causes many such units to be manually operated and observed while

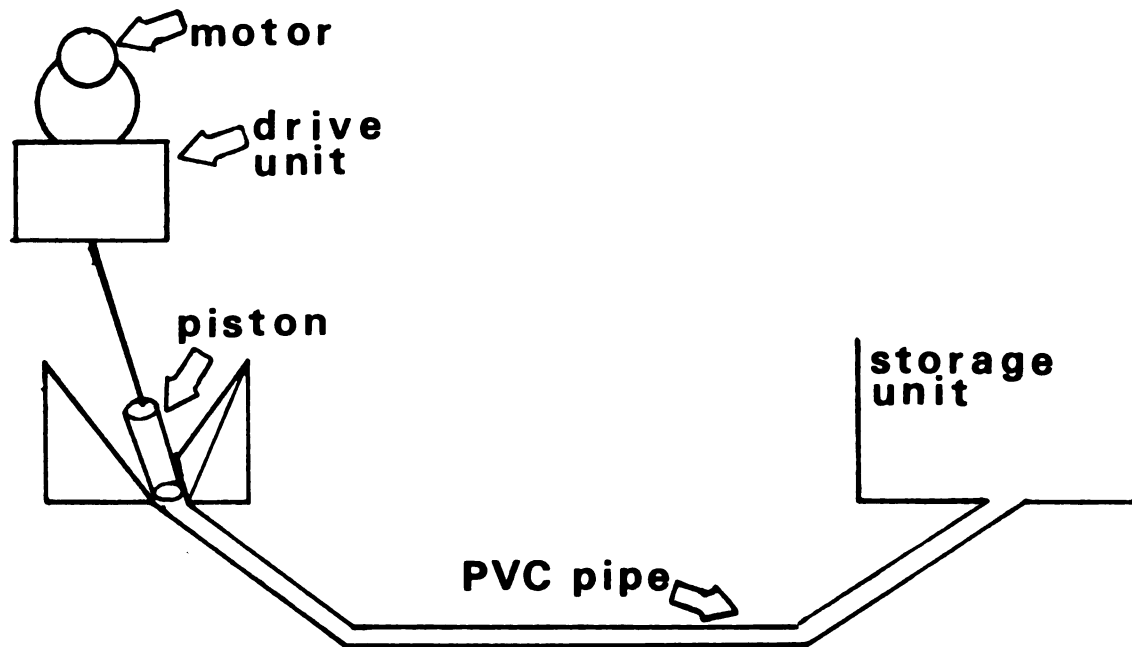


Figure 2.--Piston pump and PVC pipe.



in operation. This may require extra labor but tends to reduce breakdowns and shutdowns due to plugging. The power source is generally a 10 HP electric motor and pumping time usually involves two 15-minute periods per day.

The advantages of the piston pump system are (1) underground pipe prevents freezing, and (2) bottom filling of storage facilities limits the exposure of fresh manure to air, which reduces odors and improves retention of nutrients mainly by preventing ammonia loss. Straw or sawdust bedding in liquid storage forms a thick crust or mat which serves to keep odors in and lessens nutrient loss. The main disadvantage of the mat is the difficulty in breaking it up when the facility is being emptied. It requires a high volume impellor pump in combination with a 80-90 HP tractor and 12 to 14 hours of agitation time to homogenize the stored material. Periodic agitation during storage unloading is also necessary to keep the solids in suspension.

The most common solids storage is a concrete slab with at least one wall available for pushing against when loading. Currently many of the slabs have been placed in a six to eight foot deep earthen basin with the earth walls on the inside of the basin having a 2:1 or 3:1 slope. The cement slab is surrounded by earth walls on three sides and on the fourth side is located a gradually sloped cement exit ramp. This ramp is generally about 40 feet wide to allow a loader to maneuver. Graves and Loudon (1977) and MWPS-18 (1972) offer more detailed descriptions and designs for such facilities.

A major problem with such units is the accumulation of rain water which makes the stored waste too sloppy to remove with a front loader, and too thick and solids laden to pump with an impellor pump. Several types of dewatering devices have been used, such as perforated pipes and a "picket dam" which is 2x6's placed on end with small gaps in between. This latter approach has been used successfully on many Michigan farms. The drained-off fluid has a high pollution potential and must be kept from waterways by allowing it to drain through grass waterways or collect in small basins which may also be used to store milkhouse wastes. Such liquids have a low solids content which allows it to be easily pumped out if the need arises.

Loading such solids holding facilities is most commonly done with a cross conveyor and a 40- to 60-foot stacker or a push-off ramp. This allows manure to be dropped into the deepest part of the pit. Obtaining a certain amount of solids buildup before severe freezing occurs is necessary to prevent the whole pile from freezing and building up too high. When there is the initial manure buildup, the bottom manure won't freeze but slowly spreads out, allowing the cone to slowly sink down. Solids storage facilities can also be filled from the bottom with a piston pump. In the latter case fresh manure is always added to the inside of the pile. Although such a technique is frequently described, it is not commonly used in Michigan. The various equipment and storages previously described have been summarized in Tables 16A and 16B.

Table 16.A.--Manure transfer equipment for solid waste material (cross conveyor and stacker).

Manu- facturer Number	Basic System Cost*	2HP Motor Cost**	Chain Cost per Foot	Complete Unit Cost for 40 Foot Barn Plus 50 Foot Stacker
1	2,750	248	7.50	4,348
2	2,820	248	6.75	4,283
3	3,698	248	6.90	5,188
4	3,400	248	6.89	4,888
5	2,650	248	8.45	4,419
6	<u>2,469</u>	<u>248</u>	<u>6.60</u>	<u>3,845</u>
	$\bar{X}=2,964.50$ $\pm 479.28$	$\bar{X}=248$ $\pm 0.0$	$\bar{X}=7.18$ $\pm 0.69$	$\bar{X}=4,495.16$ $\pm 475.30$

\* Drive unit, 50-foot elevator plus supports.

\*\* Same brand name motor used for each system.

Table 16.A lists the cost of individual components needed for movement of solid wastes to storage. A 2 HP motor provides sufficient power and total costs approximate \$4,500.00 for the 40-foot wide barn. Liquid transfer systems are more expensive, with the piston pump combination costing about \$6,500.00 versus \$9,800.00 for the compressed air system. A 10 HP motor with the piston pump provides sufficient power to handle all wastes without undue motor strain. Some early piston pump installations used 7.5 HP motors, but overloading caused the switch to more powerful motors. Compressed air systems are a new concept and not widely used in Michigan. The concept is simple, but it appears they can be used in combination with silo storage.

Table 16.B.--Manure transfer systems using piston pump or compressed air unit.

Unit	Basic Unit Cost*	10 HP Motor Cost**	Cost/Foot 12" O.D. PVC Pipe	Complete System Costs with 140' Distance to Storage****
Piston Pump Units				
1	4,450	700	8.10	6,284
2	4,500	700	10.00	6,600
3	4,500	700	7.50	6,250
4	4,000	700	8.50	5,890
5	4,590	700	-	-
6	<u>5,500</u>	<u>700</u>	<u>-</u>	<u>-</u>
	$\bar{X}=4,590$ $\pm 492.34$	$\bar{X}=700$	$\bar{X}=8.53$ $\pm 1.07$	$\bar{X}=6,256$ $\pm 290.47$
Compressed Air Unit				
1	8,120	480***	8.50	9,790

\* Includes collection hopper, drive unit, piston and check valves.

\*\* Same brand name electric motor used for all systems.

\*\*\* 5 HP electric motor.

\*\*\*\* Does not include installation fee.

Concrete push-off ramps can be used with tractor scrapers to move both solids and semisolids into appropriate storage basins. Accurate cost figures for ramps are unavailable, but \$1,000.00 would probably be a fair estimate. They provide one of the simplest methods for loading storage facilities along with slats and floor openings with pits underneath. They are dangerous and some users

have installed a heavy steel railing across the front to prevent accidentally driving a tractor off the ramp into the manure pit.

Table 17 presents cost figures for the various storage systems and includes all the costs involved for excavating, concrete work, etc. It does not include unloading equipment, etc. The table indicates concrete pits are the most expensive to initially install, steel silos the next most expensive, and an earth basin for liquids the least expensive. Earth basins for solids and slurry basins both cost about one-fourth that of the pits and silos. Each unit requires a large volume of concrete and the solids basin cost includes a picket fence dewatering device and a small liquids basin for runoff water and milkhouse waste water. The least expensive storage is the earthen basin for liquids which has a narrow concrete ramp. The price includes the cost of concrete and the price for excavating and building of the earthen berms.

#### Impellor Pump for Emptying Liquid Storage Units

Most dairy farms utilize significant amounts of fibrous bedding material to keep cattle clean and dry. This material eventually ends up in the storage facility and, with liquids storage, it tends to float to the surface and form a thick mat. This mat keeps odors in, but at emptying it must be blended into the rest of the mixture to allow pumping. The most frequently utilized piece of equipment for this task is a low head, high volume impellor pump powered by an 80-90 HP tractor. The intake impellor is usually equipped with cutting blades which allow the bedding

Table 17.--Cost of various storages designed for 100 cows and 180 day storage.

Storage Type	Cost
Cement silo	\$35,280
Steel silo	45,360
Earth Basin, Solids	11,190
Earth Basin, Liquids	3,750
Cemented Slurry Basin	11,101
Pit Under Slats	50,400
Tank Under Barn	50,400

material to be chopped finer and be more easily pumped. Up to 20 hours of agitation time may be necessary to properly homogenize a volume from 100 cows for six months.

Once the slurry has been adequately mixed and is pumpable, the same impellor pump can be used to fill tank wagons. Loading rates of 2,000 gallons per minute are feasible if the liquid wastes are sufficiently dilute. Such pumping rates allow 3,200 gallon tankers to be filled in 1½ to 2 minutes.

#### Impellor Pump and Irrigation Pump for Emptying Liquid Storage Units

In circumstances where large volumes of dilute liquids such as lot runoff, flush water or milkhouse and parlor waste water are added to manure storage units, irrigation appears to be a convenient way of transferring it to fields. Despite the extra water, such

material usually needs substantially more dilution water to allow pumping with irrigation pumps. This may involve adding one to two volumes of fresh water per volume of stored wastes to lower the solids content to 3 or 4 percent. Mixing this complete mixture with an impellor pump is generally done in conjunction with using the irrigation pump. The dilution water may triple the total volume to be pumped and total pumping time may be increased due to the low pumping rates of irrigation pumps and the large volume to be pumped. A pumping rate of 300 to 500 gallons per minute is common for such pumps.

One note of caution is the need to have ventilation systems functioning properly when agitating pits under slats. Trapped gases may be released in sufficient quantities to asphyxiate or poison cattle if air transfer is inadequate. Another problem associated with agitation is that it allows a lot of ammonia gas to be released, which lessens the nutrient content of the waste. Tables 18 and 19 summarize the costs and pumping capacities of commonly used impellor and irrigation pumps.

Many companies manufacture impellor pumps, and the average price was \$3,500.00, while the average price of three irrigation pumps capable of moving liquid manure through a half mile of pipe and out a sprinkler gun was \$2,570.00.

Previously it was explained how a basin with a bottom liner of concrete was sometimes used to collect and store manure and rain water. The resulting mixture is often too flowable to handle with a front end loader and not dilute enough to be pumped





Table 18.--Cost, agitating capacity and pumping capacity of  
impellor pumps.

Company	Impellor Pump Cost	Pumping Capacity (GPM)
1	3,332	1,850
2	3,487	2,000
3	3,230	-
4	3,392	1,950
5	4,733	1,900
6	3,150	1,850
7	3,263	-
8	3,213	1,950
9	3,360	2,000
10	3,550	1,850
11	3,806	1,900
12	<u>3,032</u>	<u>-</u>
	$\bar{X}=3,462.33$ $\pm 448.43$	$\bar{X}=1,916.67$ $\pm 61.24$

Table 19.--Cost of irrigation pumps.

Company	Cost
1	2,887
2	2,450
3	<u>2,375</u>
	$\bar{X}=2,570.66$ $\pm 276.51$

with an impellor pump. One firm manufactures and markets a self-loading spreader for such slurry type material. The unit is backed directly into the flowable mixture and a continuous paddle belt at the rear of the spreader is immersed into the waste material. When operated this continuous paddle belt moves the waste to an intake auger which loads the tank wagon. The main restriction is the waste material must be fluid enough to flow to the paddle belt. Such a unit is manufactured in three sizes ranging from 1500 to 3200 gallon capacity. Loading time for the 2200 gallon model is approximately seven minutes and the cost of the spreader is \$8,500.00. At this time their use is limited, but they are available.

#### Solids Storage Unloading Equipment

Solids material stored on concrete slabs surrounded by earthen walls is removed with either a skidsteer loader or a utility tractor equipped with a front end loader. On farms where manure is handled as solids, these tractors would also be used to scrape the alleys. In each case these units would have multiple uses, but waste handling would utilize the most equipment time. Ownership costs per hour of use were \$4.75 for the skidsteer and \$8.00 per hour for the utility tractor. This lower rate for the utility tractor is due to its being used more hours annually than the skidsteer. The front end loader unit was valued at \$2,500.00 with approximately 50 percent of its use time being for loading manure and bedding replacement. Total ownership costs for the utility tractor, front end loader combination consisted of both tractor and

front loader ownership costs. In Table 20, time to load a 275 bushel spreader with either a skidsteer or front end loader is given.

Table 20.--Time to load 275 bushel solids spreader with skidsteer or front end loader.

Farm Number	FEL Load Time (min)	Farm Number	SKS Load Time (min)
1	10	1	8
2	15	2	3
3	10	3	10
4	3	4	5
5	8	5	5
6	10	6	<u>3</u>
7	5		$\bar{X}=5.7$
8	5		$\pm 2.8$
9	10		
10	5		
11	10		
12	8		
13	5		
14	4		
15	<u>7</u>		
	$\bar{X}= 7.7$		
	$\pm 3.2$		

Based on 15 survey responses, loading time with a front end loader is 7.7 minutes, with the range being 3 to 15 minutes. The time involved and variability depend a great deal on the consistency of the manure, the loading area and room for maneuvering. On the average, skidsteer loaders used 5.7 minutes to load a spreader. Superior maneuverability in confined areas and faster shifting time may partially explain the more efficient loading time.

#### Movement of Waste Materials From Storage to the Field

Four choices exist for this job, and the selection depends partially on the consistency of the waste material. The use of liquid hauling tankers or solids spreaders had no effect on the hauling distance, which averaged 0.3 miles from site of loading to the unloading location.

Solids Spreaders.--Spreader capacity for those dairymen handling manure as solids averaged 270 bushels. The spreaders are equipped with tandem wheels and a hydraulic end gate. In many cases the manure being transported is quite sloppy and would flow out the back of the spreader if the end gates were not used. The average price for the spreader was \$5,000.00 and required a 75-80 HP tractor to pull it. Unloading time based on farm survey responses averaged  $5.7 \pm 2.8$  minutes for 18 operators and this did not include transit time to and from the field.

Liquid Tankers.--Eight farm survey participants used liquid spreaders to convey waste material to the field. Table 21 summarizes unloading times and spreader capacities for those eight dairymen.

Table 21.--Spreader capacities and unloading times for liquid tankers.

Farm Number	Spreader Capacity (Gallons)	Unloading Time (Minutes)	Unloading Rate (GPM)
1	1,500	2.5	600
2	3,250	5.0	650
3	3,200	5.0	640
4	3,200	5.0	640
5	2,250	5.0	450
6	3,000	5.0	600
7	3,200	4.0	800
8	<u>3,000</u>	<u>5.0</u>	<u>600</u>
	$\bar{X}=2,825 \pm 626.8$	$\bar{X}=4.56 \pm .90$	$\bar{X}=622.5 \pm 5.7$

Most dairymen use a liquid spreader with about 3,000 gallon capacity with no injectors. The unloading rate for such units is about 600 gallons per minute with an average unloading time for a 3,000 gallon spreader being nearly five minutes. The combined spreader and load weight is nearly 15 tons and requires a 90-100 HP tractor to pull it. Also, the weight can cause soil compaction in

row crops or soil which is wet. The use of injectors is possible with liquid spreaders and both 2-row and 4-row assemblies are available. A commonly used unit is a 4-row set of injectors on a tractor mounted tool bar. Liquid manure is forced through a hose connecting the spreader and injectors and the manure exits behind the chisels. When injecting the chisels are forced into the ground about ten inches deep and the waste is deposited in the furrow and then covered with dirt. This method greatly reduces odor and conserves maximum amounts of nitrogen, but does require a 100-120 HP tractor to do the job. According to manufacturers, injecting does not slow down the unloading process because four large diameter exit ports prevent restrictions. Row crop injecting does go slower due to turning at row ends and attempting to minimize crop damage.

The average cost for a 3,200 gallon liquid spreader was \$7,335.00 and a set of four injectors added another \$2,500.00 in costs.

#### Irrigation Equipment for Waste Handling

With longer storage time and larger herd sizes, the large volumes of accumulated liquid wastes cause many farmers to seriously consider irrigation equipment for storage emptying and field application. None of the 25 survey farms had irrigation, but several were interested in it. For this project, manufacturer supplied performance and cost data were used in conjunction with Midwest Planning Service Manual-18 (1975) and the Soil Conservation's Field Hand Book (1975). Two basic irrigation systems were examined.

One involved use of aluminum pipe and a manually relocated big gun sprinkler nozzle with a  $1\frac{1}{4}$  to  $1\frac{1}{2}$  inch diameter nozzle. The second system involved a combination consisting of aluminum pipe, flexible hose and a traveling sprinkler nozzle with a potential total run length of 800 yards.

Stationary Big Gun Sprinkler.--This particular system involves a lower investment than the traveler system but requires much more manual labor. The large bore nozzle is set up with a stabilizing stand and attached to the irrigation pump with six inch diameter aluminum pipe. Such equipment would seldom be purchased simply to irrigate liquid waste and for the computer program it was assumed 25 percent of the use time would be for waste handling. The normal wetted circle diameter was approximately 400 feet, or about three acres. Following the completion of each set the unit must be shut down, the pipe disconnected and the stand and nozzle relocated for the next set. It was assumed one man could do this in one hour.

Traveling Gun Sprinkler.--This unit involves some of the same equipment as the big gun sprinkler. A similar impellor pump and irrigation pump are used along with 800 yards of six inch diameter aluminum pipe. In addition, 400 yards of flexible hose is used to connect the aluminum pipe outlets to the traveling gun sprinkler. The traveler itself is comprised of a portable winch powered by a 20 HP gas motor. The winch unit is anchored firmly and the cable is reeled out to its maximum and attached to a three-

wheeled trailer on which is mounted a  $1\frac{1}{4}$  to  $1\frac{1}{2}$  inch diameter nozzle. To the nozzle is attached the flexible hose through which is piped the liquid waste from the storage unit. As the material is pumped through the nozzle the winch pulls it along at a predetermined rate which essentially governs the rate of waste application. The process continues until the cable is completely reeled in and then the rig must be reset by repositioning the winch. Labor usage is minimal with this system; mainly it is used in conjunction with a tractor to reposition the winch and trailer and handle the agitating process.

Table 22 presents a comparison of the cost of both systems along with labor requirements for specific tasks involving each unit as used in the computer program.

It is obvious that these two systems represent different levels of labor-saving technology. The traveler system is much less of a labor user, but initial cost and energy usage are greater. The traveler unit is probably the smallest user of labor of all waste application systems. One of the penalties for use of an irrigation system is the loss of a large amount of nitrogen to the air. Agitation results in some losses and the spraying of the material into the air in a large arc further increases the escape of ammonia nitrogen, which detracts somewhat from the labor savings. The hand set sprinkler is probably no less of a user of labor than hauling solids or liquids with a spreader. Due to the tripling of the total volume with dilution water, many sets have to be made and this causes a large input of labor. If such a system is used



Table 22.--Comparison of stationary big gun sprinkler and the traveling gun system for irrigating liquid wastes.

	Stationary Gun Sprinkler	Traveler System
Length of aluminum pipe (feet)	3,960	2,640
Feet of flexible hosing	-	1,320
Cost/foot--aluminum pipe	\$3.25	\$3.25
Cost/foot--flexible hose	-	\$8.50
Cost for 1¼ to 1½ nozzle and support	\$750.00	-
Cost for traveling gun sprinkler	-	\$8,000
Percent of time used to irrigate waste	25	25
Men used to set up	2.0	2.0
Hours to set up	2.0	2.0
Time to set up from scratch (hours)	5.0	4.0
Hours/set (0.5 inch application rate)	2.0	-
Area covered/set	3.0	24
Time to reset (hours)	1.0	1.0
Men to reset	1.0	1.0
Men to dismantle	2.0	2.0
Time to dismantle (hours)	5.0	2.0

with a flush system where the dilution water is already added to some extent, then irrigation is much more useful than with other systems.

Comparison of Systems Available  
for 100 Cow Herds

When the program was working properly and the descriptive equations had been specified, all possible systems were synthesized for a 100 cow unit by using the 000 option at the beginning of the program. This generated 4,208 feasible systems based on the restrictions that had been incorporated to prevent impossible option-option combinations. Liquids storage was used for 2,672 systems, 1,024 handled wastes in the solid form and 512 slurry basin systems were possible. Handling animal wastes as a liquid appears to permit a lot more flexibility in system design. In order to make some meaningful comparisons among systems, two approaches were taken.

Comparison Method 1

All feasible systems were developed for the 100 cow herd and were stored on a permanent file tape for later analysis. For this herd size only, all options were compared on the basis of total initial cost, annual costs of ownership (DIRTI), yearly labor needs and labor cost, annual energy needs and cost, yearly bedding used and its cost, total annual costs, nutrient value of the material and net annual costs.

Clay stalls for 100 cows cost \$1,080.00 for curbing and clay while concrete platform stalls were \$3,900.00. The concrete costs made up the approximately \$2,000.00 difference in price. The initial bedding costs were \$90.00 for sawdust, \$169.00 for shavings and \$270.00 for sand. If rubber mats were used in concrete stalls, they added another \$50.00 per stall initially but did lessen

bedding usage in stalls to some degree. Addition of bedding material with a skidsteer loader used about one-third as many man hours of labor as did the front end loader. This results primarily from the superior in-barn maneuverability of the skidsteer. The faster addition of bedding and more precise dumping into stalls results in a lot less labor for leveling the material. The skidsteer is very handy with heavy sand bedding for the above-mentioned reasons.

The annual bedding material used cost \$1,576.00, \$3,450.00 and \$2,956.00 for shavings, straw and sand, respectively. The per unit costs used were the market prices for the individual bedding materials. Farmers may be able to obtain bedding cheaper than this if they grow their own straw or use sand from their farm.

Slatted vs. Solid Floors.--Slats cost approximately \$2.25 per square foot to install versus \$1.75 for solid floors. Cattle on slats usually are given less floor space per animal, which helps force the manure through the slots and into the pit beneath. Using less space per cow somewhat offsets the higher per unit costs, but the slatted floor still costs \$10,125.00 compared to \$7,500.00 for the solid surface.

Alley Cleaning Options.--Floor cleaning labor requirements in many systems represent 50 to 60 percent of the total labor annually used to handle wastes. If labor is to be saved, this is one place to attempt it. Many floor cleaning options exist, and in Table 23 those available in the computer program are listed and compared.

Table 23.--Cost, labor and energy needs of floor cleaning options.

Option	Initial Cost	Annual Cost	Annual Energy Costs	Annual Labor Costs	Total Annual Own and Operating Costs
Alley scraper	5,042	1,326	503	60	1,889
Skidsteer	10,500	1,927	419	843	3,289
Garden Tractor	2,500	410	196	843	1,448
Utility Tractor	11,500	1,144	501	843	2,488
Flushing	10,950	3,074	211	559	3,445

If the initial purchase price of a skidsteer and utility tractor were charged solely to alley cleaning, then flushing and tractor scrapers would have the highest initial cost, with automatic alley scrapers being next and the garden tractor would cost the least. The ability to use the tractors for other jobs spreads the cost of ownership over several enterprises and makes the utility tractor's annual costs comparable to those of the alley scraper. The skidsteer is less versatile and has higher ownership costs, while flushing is the highest at \$3,074.00.

Energy costs for the alley scraper and skidsteer are both \$500.00 annually, while the garden tractor and flushing use about \$200.00 yearly, which is the least.

The main advantage the alley scraper provides is less labor. Apart from repairs, the only labor needed is a few minutes per week to lubricate and check the system. This compares with

approximately 20 minutes per alley per day when tractor scraping twice daily. Flushing also uses less labor but winter scraping and occasional alley scraping result in higher labor needs than the alley scraper.

On the basis of total annual costs, the garden tractor is lowest, the alley scraper is next, and the flushing system is the highest. If a dairyman were interested in lessening the labor needed for waste handling, an alley scraper or flush system might fit his needs.

Storage of Waste and Waste Transfer Equipment.--When an operator decides to build waste storage, he actually has to make three major decisions. One involves the style of the storage unit and the other two involve how he will fill and empty the facility.

In Table 24 are presented the most commonly used storage systems for Michigan conditions. The five liquid units range in price from \$3,750.00 for an earth basin to \$50,400.00 for concrete pits under the barn. For solids storage some form of the concrete bottom earth basin is most commonly used. It is similar to the earth basin for liquids, but the large amount of concrete in the bottom forces up the price. The concrete lined slurry basin also has a higher cost due to the great amount of poured concrete.

The under-barn pits for liquids may have the highest initial cost, but they do eliminate storage filling equipment in those systems where they are used, and this may be an \$8,000.00 expenditure. The upright silo storages are generally filled with a

Table 24.--Comparison of storage units for 100 cow herd size.

Storage Facility	Initial Cost	Annual DIRT Costs
Cement silo	35,280	4,410
Steel silo	45,360	5,670
Earth basin, solids	11,190	1,622
Earth basin, liquids	3,750	544
Concrete slurry basin	11,100	1,332
Concrete tank under barn	50,400	6,300
Concrete pit under slats	50,400	6,300
None	0	0
Settling basin, Flush lagoon	17,850	2,588

piston pump located in the barn and linked to the storage by underground PVC pipe. This unit is also used to fill earthen basins for liquids and solids. The cross conveyor and stacker combination are the most common units to fill concrete-bottomed earth basins, but in some cases concrete push-off ramps are used in conjunction with tractor scraping. The options available for storage filling are listed and compared in Table 25.

Whenever a piston pump or compressed air unit is used in a waste handling system, it will be the most expensive transfer unit in terms of initial cost, annual ownership costs, labor and energy requirements and total annual costs. As indicated in Table 25, cross conveyors are less expensive in all categories, while the concrete push-off ramp is the least expensive.

Table 25.--Storage filling options.

Option	Initial Cost	Annual Costs of Owning	Yearly Labor Costs	Annual Energy Costs	Total Annual Costs
Cross conveyor, short elev.	3,267	925	102	25	1,052
CC + stacker	4,706	1,331	102	25	1,459
Piston pump, PVC	6,665	1,953	639	105	2,697
CC, PP, PVC	9,438	2,738	639	130	3,507
CC, air, PVC	12,863	3,358	639	84	4,081
Ramp	1,000	135	0	0	135
None	0	0	0	0	0
Concrete flume	1,575	197	0	0	0
None (slats)	0	0	0	0	0

When storage is utilized, it must eventually be emptied and this may pose some problems in certain situations if adequate unloading equipment is unavailable. With liquids storage the bedding material tends to float to the top and, before emptying, this must be thoroughly mixed in as described previously. Only one option, the impellor pump, is designed for this agitation and unloading job. If the mixture is well homogenized first with an impellor pump and is sufficiently dilute, an irrigation pump may be used to empty and transfer the material to the field.

For solids removal both front end loaders and skidsteer loaders are used to load spreaders. If the material is high in solids, these loaders can fill a 275 bushel spreader in five to seven minutes. The skidsteer is a bit faster due to its superior maneuverability, but utility tractors designed for loading also are very efficient. Table 26 compares the various unloading units available for 100 cow operations.

Table 26.--Storage unit emptying options.

Option	Initial Cost	DIRTI Costs	Annual Labor Costs	Energy Costs	Total Annual Costs
Impellor pump	3,500	1,025	209	202	1,886
Front end loader	14,000	454	104	46	746
Skidsteer	10,500	193	84	39	317
Self-unloading spreader	8,400	738	344	306	2,126
None	0	0	0	0	0
Impellor and irrigation pump	6,100	1,216	175	1,029	4,606

Handling stored wastes as liquids or as a slurry requires equipment which costs the most, uses the most labor and energy, and has the highest total annual costs. This is due to at least two factors. One is the large volumes of water which are moved with liquid manure and this takes more energy and labor. In addition,



there is a great deal of time and energy expended to break up the crust of bedding and thoroughly blend it into the liquid portion. In all cases except the skidsteer in Table 26, total annual cost column has in it an ownership factor for the tractor used to power the unloading equipment. As an example, for an 80-90 HP tractor used to power the impellor pump, this amounts to the hourly use charge for the tractor for ownership multiplied by the hours actually used annually. In this case it amounts to \$450.00.

Unloading solids from storage requires less labor and energy and is accomplished with multiple use equipment that is usually available on dairy farms. The self-unloading spreader requires a large tractor to power it, is slow to load and has a fairly high initial cost but is useful in situations where the waste material is too thick to pump but too liquid to load with conventional loaders.

Movement to Field and Land Application.--For this project deposition of manure on the land was the only end-point considered. With the exception of irrigation of highly diluted wastes, some type of liquids or solids spreader was used. The specifics of the various options have been previously described, and Table 27 presents a comparison of them on the basis of cost, energy and labor.

The figures in Table 27 deal only with movement of waste material to fields and do not pertain to loading time or the energy required to pump the material. Such data were presented in Table 26. Irrigation systems are very expensive to buy, especially

Table 27.--Equipment used to move dairy wastes to the field.

Option	Initial Cost	Annual Cost	Labor Costs	Energy Costs	Total Annual Costs
Self-loading tanker	8,400	1,512	283	252	2,667
3200 gallon tanker	9,500	2,688	229	179	3,588
Tanker plus 4-row injectors	12,000	3,313	234	212	4,361
Solids spreader	5,000	1,250	306	218	2,431
Aluminum pipe & stationary sprinkler	13,620	817	330	0	1,147
Aluminum pipe, hose, traveling gun sprinkler	27,800	1,460	124	172	2,937

traveler units, but it was assumed for this study that only 25 percent of their total use time would be allocated to application of wastes to the field. On an annual cost basis, the tanker with injectors was the most expensive and the stationary gun sprinkler the least costly. All the transfer to field equipment other than irrigation options is used only for manure movement, which causes their ownership costs to be higher than multiple-use irrigation works.

The labor needs of the stationary gun sprinkler unit was the highest of all options. This system must deal with a doubled or

tripled volume of wastes due to the addition of dilution water and the sprinkler and pipe must be repositioned after each area has been irrigated. This need for a lot of hand labor plus the extra volume makes this a heavy user of labor. At the other extreme is the traveler system. Given sufficient hose and a large field, the unit may run 8 to 12 hours with no need for labor. When it has to be repositioned, this is accomplished with a man and tractor. Of the spreader units, the solids spreader has a bit higher labor requirement than the others, with the 3,200 gallon liquids hauler having the least.

Energy usage is zero for a stationary sprinkler system in this program because all the pumping energy has been charged to the emptying and agitation option. Other movement to field options use energy, with the large tanker requiring the least and the self-loading spreader the most. Injecting and application from a solids spreader require about the same amount of energy. This may be due to the larger number of trips to the application site with the smaller volume solids spreader. Dairymen with 100 cows might use a 2,200 gallon unit with injectors; however, tractor mounted 4-row injectors would require about the same amount of energy because the rolling resistance offered by the tanker is small compared to that of the injector.

On the basis of total annual costs, the injector unit with a 3,200 gallon liquid spreader was highest, followed by the traveler system, while the stationary gun sprinkler was lowest.

If dairymen want to use irrigation equipment for transferring liquid wastes to the field, they should understand that stationary, hand moved systems require at least as much labor as other hauling units. Traveling gun sprinklers use much less labor than other units but initial cost would prohibit installing such a system just for waste removal, unless it could be purchased as second hand equipment for a reasonable price. In many cases farmers buy such equipment to irrigate corn and then using it for waste removal is feasible and justified.

Comparison of Waste Handling Systems for  
100 Cows on the Basis of Storage Type

Most systems are classified as either liquids or solids and, while technically this refers to the solids content of the waste material, it can also define storage types. To compare various systems using different storage types, mean totals were calculated for all complete eight option systems using each of the storage facilities. A complete listing of all criteria mean totals is presented in Table 28.

Total component costs for systems using under-barn concrete pit or tank storage were the most expensive, followed by the silos. The daily haul system was by far the cheapest in terms of initial cost. When earthen basins were used, waste handling components up to the storage phase were quite similar and storage costs were also about the same as were the total systems cost. Flushing increased total system costs a substantial amount due to the cost for extra

Table 28.--Summary of waste systems according to storage types.

Storage Types	Total Initial Cost	Annual Costs of Ownership	Annual MHS Labor Cost	Annual Energy Costs	Annual Operating Costs	Annual Bedding Costs	Total Annual Costs	Manure Nutrient Value	Net Annual Costs
Cement silo	77,139	13,781	2,649	1,323	3,972	1,996	21,868	5,136	16,731
Steel silo	87,219	15,041	2,649	1,323	3,972	1,996	23,128	5,136	17,991
Earth basins for solids	52,141	7,201	1,498	658	2,156	1,996	12,021	4,978	7,042
Earth basin liquids (non flush)	53,445	9,433	2,053	914	2,967	1,996	14,396	4,792	9,604
Earth basin liquids (flush)	58,654	10,193	2,410	1,570	3,980	1,996	16,169	4,792	11,377
Concrete slurry basin	51,541	8,870	2,364	1,434	3,793	1,996	12,708	5,083	7,625
Concrete pit	89,582	12,380	1,726	1,471	3,197	1,996	19,635	4,900	14,734
Concrete tank	89,954	12,452	1,783	1,497	3,280	1,996	19,873	4,898	14,975
None	27,292	5,136	1,372	634	2,006	1,996	9,734	5,083	4,650
Settling basin and lagoon	62,544	10,809	1,696	1,389	3,085	1,996	17,634	4,687	12,948

storage capacity. With silo storage systems, storage costs account for 50 to 60 percent of the total system costs, whereas with lagoons or earth basins the storage costs as a percent of total system costs ranged from 6 percent for the earth basin for solids to approximately 30 percent for the settling basin and lagoon for the flush system. Liquid systems in general require more labor due to extensive pumping times and greater volumes to be handled.

Energy usage was greatest for liquid basin systems and next highest for below building tanks and silos. The first two system types were compatible with irrigation unloading equipment, which has the greatest energy needs of any of the unloading units, as is noted in Table 26. Also, liquid systems in general use more energy for the same reasons they require more labor. This is also reflected in total annual operating costs and total annual costs, which show liquids systems to have higher costs than solids systems.

#### Nutrient Retaining Ability of Systems

One other factor that needs to be considered when selecting a waste handling system is its ability to retain nutrients. This topic was discussed in the review of literature section. Loss of nutrients at any stage of the waste handling operation is of concern to both the farmer and to the environment as well.

It was assumed for this project that freshly defecated fecal material contained 100 percent of the phosphorus, potassium and nitrogen. As the manure is moved through each waste handling phase, the potential exists for losses, especially of nitrogen in the form

of volatile ammonia. Phosphorus and potassium are more stable and losses tend to be low.

Nitrogen losses concern the farmer because of its value as a plant nutrient especially for corn, and its loss to the environment contributes to the pollutant load of streams and lakes. For nitrogen losses, literature reports were used to assign a percentage loss to each waste handling option. All losses for the eight sections were totaled and subtracted from the original 100 percent which left the cow. Of the total nitrogen making it to the field, only 50 percent of it will be available to growing crops during the first year post application. This quantity was multiplied by the per unit price of commercial nitrogen to obtain a value for the nitrogen portion. It was assumed 60 percent of the phosphorus would be available and 100 percent of the potassium. Each was also priced on a basis similar to nitrogen and the three added to give a total value for the manure nutrients.

People are correct in assuming that liquids systems have the potential to save the most nutrients, especially nitrogen, but various handling procedures associated with liquid wastes may drastically reduce its nutrient content. Agitation with an impellor may cause losses of ammonia from stored liquids greater than those associated with emptying a solids basin with a front end loader. Systems using impellor pumps were penalized accordingly and if irrigation was used they were further penalized. Another factor in nutrient losses is the post application procedure. If waste is not rapidly incorporated into soil, up to 80 percent of the ammonia may

be lost in three to five days. Farmers need to be aware of this factor in addition to which handling procedures cause the greatest nutrient loss. No attempt was made to calculate losses of nutrients associated with post application practices for this study.

Based on the procedures used for this study to assess nutrient losses, silo storage systems were ranked the best, followed by daily haul and cemented slurry basins. Earth lagoons for liquids systems were ranked as the worst for nutrient conserving ability. As mentioned earlier, liquid storage is an efficient conserver of nitrogen compounds, and Safley (1977) indicated a steel silo had retained 99 percent of the nitrogen up to the time of emptying. Most liquid units require a lot of agitation and pumping and if irrigation is used there is more potential for loss. Each procedure causes ammonia loss which may more than offset the superior nitrogen retaining ability of the liquids storage unit. Each 5 percent loss of nitrogen results in a loss of about 1,000 pounds of total nitrogen per 100 cows on an annual basis. This amounts to about \$180.00 per 5 percent nitrogen loss when nitrogen is valued at 18¢ per pound. In terms of total nutrient value, two systems would have to differ a great deal in the nitrogen conserving ability before a great difference would be noted. This area of nutrient losses is difficult to accurately estimate and is subject to interpretation in most cases.

When all factors are considered, daily haul systems had much the lowest net annual costs, solids basin systems were next,



while silo systems resulted in the highest net annual costs followed by the underbarn tank systems and the flush lagoon systems. Nutrient retention was not sufficient to lower the liquid storage systems net annual costs to those of the solids or slurry system.

#### Comparison of Commonly Used Waste Handling Systems

The trend toward larger herd sizes and confinement housing, coupled with a scarcity of farm labor and rising energy costs, has forced dairymen to adopt energy and labor efficient waste handling systems as well as other farm systems. Herd sizes considered for this part of the study ranged from 100 to 300 milking cows. This range was chosen for two reasons. First, many Michigan dairy herd expansions result in this approximate number of cows. Second, individual confinement barns can usually accommodate up to 300 cows. When cow numbers exceed this, buildings are replicated. With most expansions, only one building is considered.

Rather than attempt to somehow compare all feasible systems over a range of herd sizes, 58 systems common to Michigan or showing potential for Michigan dairymen were chosen. This group was then ranked to discover the five highest and lowest in terms of initial cost/cow, annual labor/cow, yearly energy costs/cow, total annual costs/cow, and net annual costs/cow. The ranking procedure was conducted for 100, 150, 200, 250, and 300 cow herds. Appendix Tables C-1 to C-5 contain the output for the 58 systems according to herd size.

### Initial Cost

The most expensive systems ranged in price from \$900.00 to \$1,050.00 per cow at the 100 herd size. Such units utilized liquid storage, either below building tanks or above ground steel silos. Irrigation equipment or liquid tankers with injectors were used for movement of waste to the field. As herd size increased, per-cow costs declined. This scale effect has been noted by Forster (1974) and Ogilvie et al. (1975), among others. Even though per-head costs decline, the same systems which proved most costly for 100 cow herds also were highest for the 300 cow operation. Unit costs of \$710.00 to \$775.00 per cow existed at this herd size.

At the other extreme, the least expensive systems at all herd sizes were either daily haul solids systems or units with earth basin storage for solids. Daily haul systems averaged \$220.00 per cow at the 100 cow herd size and \$150.00 per cow with 300 cows.

### Energy and Labor Needs

Despite their high cost, many dairymen have installed or are considering systems with slatted floors, below building storage, silo storage, and irrigation equipment. The intent is to exchange capital for labor and energy. When the 58 systems were ranked according to labor needs, several of the tank and slatted floor combinations required the least labor annually irrespective of herd size. Slatted floor systems averaged 1.29 man hours/cow/year at the 100 cow herd size and 0.81 man hours/cow/year with 300 cows. However, a daily haul system also ranked among the five systems

requiring the least labor. Unfortunately there is no accurate or easy way of affixing a cost factor to the inconvenience of daily hauling of waste or to the potential for environmental damage due to runoff and water contamination.

The units requiring the most labor were flush systems and liquid basin systems. These systems have a fairly high labor demand at each phase and require a lot of labor and energy for agitation and pumping due to crust formation and the increased waste volume associated with flushing. The annual per-cow labor needs ranged from 7.0 man hours for 100 cow herds to 5.5 man hours at the 300 cow level.

Energy demands of the slatted floor systems using tankers or stationary gun sprinklers were the lowest among the 58 units selected. Such systems use little or no energy for alley cleaning or movement of waste to storage. This lowers annual energy costs to \$4.00 to \$5.00 per cow for 100 cow herds and \$3.00 to \$4.00 for 300 cow herds. Irrigation with the hand moved gun sprinkler system is a labor demanding job, however, so there is a tradeoff between energy and labor when this component is used. In most cases the slatted floor units are the costliest, but they do allow a reduction in the labor and energy required.

Systems using silo storage units are the next most expensive in terms of initial cost, but they have a high energy and labor requirement at all phases. This tends to make them less acceptable because there really is no tradeoff between capital investment and labor or energy.

The heaviest energy users were flush system utilizing irrigation equipment. This was true at all herd sizes. Energy for pumping water, occasional scraping, agitation and pumping of a greatly increased volume of waste material forces the energy costs to be high. For 100 cows the five most costly systems in terms of energy costs ranged from \$31.50/cow/year for a flush system with a traveler unit for irrigation to \$17.50 for the flush unit utilizing a tanker plus injectors for field application of waste. Siphoning flush water from the lagoon could reduce energy demands both by lessening the volume to be handled and cutting down on energy needs for fresh water pumping.

When compared on total annual costs, silo systems and flush systems were the most expensive due primarily to high costs of ownership associated with expensive storage facilities. In addition, both systems use great amounts of energy and labor, as has been previously discussed. Daily haul systems and slurry basin systems had the lowest annual costs for ownership and operating. They both use moderately priced equipment, there is no agitation required, and there is no need for elaborate and expensive movement to storage equipment. Such factors contribute to higher ownership and energy costs.

The liquid systems have the highest nutrient conserving ability, but this does not lower the total annual costs sufficiently to allow them to approach the low net annual costs of daily haul and slurry system. If as stated earlier a value could be placed on

inconvenience of daily hauling and the associated pollution potential, the outcome might well be reversed or rearranged. As it is, silo and flush systems have the highest net annual costs for all herd sizes.

## CONCLUSIONS AND RECOMMENDATIONS

Two primary objectives existed for this study. First was the development of an interactive computer program capable of assembling operator designated components into complete waste handling systems. Objective two involved comparing various waste handling systems based on costs, energy and labor needs and nutrient conserving ability.

The computer program has been completed and is capable of interacting with an operator via telephone. With the options provided for each section, approximately 4,000 individual systems can be assembled. The program is also capable of accepting new options without revamping the complete package. This may be of benefit in future years as new equipment evolves.

During the farm visits for data collection, it was made clear by dairymen that labor savings, convenience and minimal intrusion on the time available for other farm activities were the main factors dictating the choice of waste systems. Initial cost and nutrient conserving ability were considered to a lesser degree. Waste handling is still viewed by most dairymen as strictly a labor and energy demanding function with little return on their investment.

Many dairymen use outside lots for cattle and the potential for runoff exists in many cases. Few dairymen feel threatened by

current EPA regulations, but most new facilities being constructed do include storage units capable of holding 180 days waste material. Also, many of the new units are total confinement barns. Environmental regulations contribute some to this trend, but the improved ability to production group and mechanize feeding and waste handling activities has also been a major factor.

Many more options exist for handling dairy wastes as a liquid than as a solid. This stems primarily from the large assortment of storage facilities and movement to field options. With the exception of earth basin storage, systems utilizing liquids storage are much more expensive than solids systems. Such facilities may represent 50 to 70 percent of total system costs.

The two heaviest users of labor were the twice daily cleaning of barn alleys and the movement of waste material from storage to the field. Automatic alley scrapers and slatted floors provided the only reduction of labor needed for daily cleaning. Flushing also is a labor saver, which may have application in Michigan, but some winter scraping may be required.

Storage emptying requires a large amount of labor and energy regardless of whether solids or liquids are being handled. With liquids, added water from several sources increases the total volume to be hauled and this causes them to utilize more energy and labor than solids. Irrigation requires the addition of large amounts of dilution water and unless a traveling sprinkler unit is used, the amount of labor involved is as great as with other emptying systems.

The nutrient conserving ability of liquids systems is higher than solids systems, mainly due to the storage facility. However, most liquid storage units require large amounts of agitation which causes nitrogen losses, and some of the advantage may be lost. In terms of its monetary value as a fertilizer, a lot of nitrogen can be lost and yet the dollar loss may be only \$200.00 or \$300.00. As a consequence, most dairymen do not consider their manure supply to be worth as much as some of the research reports would indicate.

This program has potential to benefit dairymen considering new facilities. The designing of a successful waste system involves defining the needs of the operator, incorporating his preferences and limitations, and then assembling the appropriate components to meet those needs. The program would allow this to be done for several feasible systems to allow comparison. The most logical user of the program would be dairy specialists at the county agent level.

In order to do this the program should be made available as a Michigan Tel-Plan program. Extension people are knowledgeable in the use of such programs from prior experience with other such units. Someone would have to take responsibility for getting it into the proper format and keep cost figures, etc., in the program current.



## SUMMARY

An interactive computer program has been developed which allows individual dairymen to assemble waste handling systems that meet their specific needs. The user can construct systems for 100 to 300 cows and receive an output describing total costs, annual labor and energy costs, value of the manure, total annual costs and net annual costs. The program was designed with enough flexibility to accommodate new options and allow new systems to be assembled and compared.

When all systems were compared, it was found that no single system emerged as best. Rather, it depended on the operator's needs. Exchanging large sums of initial capital in some cases lowered annual labor needs, but usually increased energy needs. Only two opportunities exist where major savings of labor can occur. One is at the alley cleaning phase and the other is with movement of waste to storage. Automatic alley scrapers, flushing, and slats lessen alley cleaning labor, while below-building tanks, cross conveyors and stackers and gravity flow flumes reduce movement to storage labor. The traveling gun irrigation system is the only way to reduce movement to field labor, but the energy requirement is high.

Liquids storage with the exception of earthen basis is expensive, often constituting 50 to 70 percent of the total system.

They also require a lot of energy and labor to agitate the contents due to the formation of a tough layer of bedding material. Liquid storage is the best method to conserve nitrogen, but many of the post storage phases for liquids tend to lose a good deal of the retained nitrogen.

Liquid system combinations are much more numerous than solids systems, with great ranges occurring in initial price, labor and energy needs. With all systems a scale effect was noted as herd size increased. This was true for liquids and solids systems.

Nearly 70 percent of farms interviewed for this study either used outside lots and needed to incorporate runoff control or had no storage facility. It is also reasonable to assume that many Michigan dairymen will be altering their system sufficiently to require the use of the program which has been developed. The most logical user of this program is the county extension dairy specialist, who has both the need for such a program and the opportunity to run it often enough to become proficient at it.

## BIBLIOGRAPHY

## BIBLIOGRAPHY

- Agpro Incorporated. 1977. Waste handling equipment information. Paris, Texas.
- Agromatic Division of A.F. Klinzing Co., Inc. 1977. Unpublished price list and equipment information. Fond Du Lac, Wisconsin.
- Amir, I. and J.R. Ogilvie. 1977. A mixed integer programming model for choosing an optimal swine manure handling system. ASAE, Paper No. 77-4028. St. Joseph, Michigan.
- Barker, J.C. 1975. Livestock manure production rates and approximate fertilizer content. Leaflet 198, North Carolina Agricultural Extension Service, North Carolina State University, Raleigh, North Carolina.
- Berge, O.J. 1971. Waste management, what does it cost? Hoard's Dairyman. April, 10.
- Bomgardner, J.H. 1977. Unpublished price list and equipment information. Hesston Corporation, Hesston, Kansas.
- Boyd, L.J.; A.L. Rippen; C.R. Hoglund; J.S. Boyd; and G. McBride. 1972. The Michigan dairy industry of 1985. Research Report 183. Agricultural Experiment Station and Cooperative Extension Service, Michigan State University, East Lansing, Michigan.
- Buxton, B.M. and S.J. Ziegler. 1974. Economic impact of controlling surface water runoff from U.S. dairy farms. Agricultural Economic Report No. 260, U.S. Department of Agriculture, Economic Research Service.
- Calhoun, G.D. 1977. Unpublished price list and equipment information. The DeLaval Separator Company, Poughkeepsie, New York.
- Clay Equipment Corporation. 1977. Unpublished price list and equipment information. Fort Wayne, Indiana.
- Clinton County Circuit Court File No. 844. 1971. St. Johns, Michigan.

- Cleuver, L. and L. Lukinus. 1977. Animal waste management. Confinement, 2:5.
- Cristafulli, F.D. 1977. Unpublished price list and equipment information. The Cristafulli Pumps Company, Inc. Glendive, Montana.
- Diggs, R.E. 1977. Unpublished price list and equipment information. General Irrigation Company, Carthage, Missouri.
- Dorsetl, W. 1977. Unpublished price list and equipment information. Valmont Industries, Valley, Nebraska.
- Enpo-Cornell Pump Company. 1977. Unpublished price list and equipment catalog.
- Environmental Protection Agency. 1973. National pollutant discharge elimination system (NPDES). Federal Register, 38.
- \_\_\_\_\_. 1975. National pollutant discharge elimination system. Concentrated animal feeding operations. Federal Register, 40:54182.
- \_\_\_\_\_. 1976. National pollutant discharge elimination system. Concentrated animal feeding operations. Federal Register, 41:11458.
- Farmway Company, Inc. 1977. Unpublished price list and equipment information. Manawa, Wisconsin.
- Fleming Manufacturing Company. 1977. Unpublished price list and equipment information. Long Lake, Minnesota.
- Fogg, C.E. 1974. Use of manure for nitrogen fertilizer. Personal communication, 1978.
- Forster, D.L. 1974. The effects of selected water pollution control rules on the simulated behavior of beef feedlots. Ph.D. Thesis, Michigan State University.
- Fowler, S. 1976. Unpublished price list and equipment information. A.O. Smith Harvestore Products, Inc.
- Gage, L.E. 1977. Unpublished price list and equipment information. H.D. Hudson Manufacturing Company, Chicago, Illinois.
- Gehl Company. 1977. Unpublished price list and equipment information. West Bend, Wisconsin.

- Gingerich, J. 1977. Unpublished price list and equipment information. Gingway Products Co., Plain City, Ohio.
- Good, D. 1972. Potential impacts of environmental pollution abatement alternatives on the Michigan dairy farming industry. Ph.D. Thesis, Michigan State University.
- Graves, R.E. 1975. Considerations in selecting dairy manure handling systems. AEN-7, Agricultural Engineering Department, University of Wisconsin, Madison, Wisconsin.
- Hale Fire Pump Company. 1977. Unpublished price list and equipment catalog. Conshohocken, Pennsylvania.
- Hanratty, M. 1975. PERT programming methods for project appraisal --A computer program. Agricultural Economics Report 290. Department of Agricultural Economics, Michigan State University, East Lansing, Michigan.
- Hawk Bilt Company. 1977. Unpublished price list and equipment information. Vinton, Iowa.
- Hedlund Manufacturing Company, Inc. 1977. Unpublished price list and equipment information. Boyceville, Wisconsin.
- Heck, A.F. 1931. Conservation and availability of the nitrogen in farm manure. Soil Sci., 31:467.
- Heubet, E.L. 1977. Unpublished price list and equipment information. Avco New Idea, Farm Equipment Division, Coldwater, Ohio.
- Hoglund, C.R.; L.J. Connor; and J.B. Johnson. 1972. Waste management practices and systems on Michigan dairy farms. Agricultural Economics Report 208. Department of Agricultural Economics, Michigan State University, East Lansing, Michigan.
- Hoglund, C.R. 1976. Dairy systems analysis handbook. Agricultural Economics Report 300. Department of Agricultural Economics, Michigan State University, East Lansing, Michigan.
- Horsfield, B.D.; R.Z. Wheaton; J.C. Nye; and J.V. Mannering. 1973. Irrigation for land application of animal waste. ID-88, Cooperative Extension Service, Purdue University, West Lafayette, Indiana.
- Humenik, F.J. 1976. Federal regulations relative to dairy waste management. Paper presented at American Dairy Science Association National Meeting, North Carolina State University, Raleigh, North Carolina.

- Hunt, E.H. 1976. Unpublished price list and equipment information. Badger Northland, Inc., Kaukauna, Wisconsin.
- Johnson, J.B. and G.A. Davis. 1974. The economic impact of imposing EPA effluent guidelines on the U.S. fed-beef industry. Proceedings of the 1974 Cornell Agricultural Waste Management Conference, Syracuse, New York.
- Johnson, J.B.; C.R. Hoglund; and B. Buxton. 1972. An economic appraisal of alternative dairy waste management systems designed for pollution control. Symposium: Animal Waste Management. J. Dairy Sci. 56.
- Knight Manufacturing Corporation. 1977. Unpublished price list and equipment information. Brodhead, Wisconsin.
- Lauer, D.A.; D.R. Bouldin; and S.D. Klausner. 1976. Ammonia volatilization from dairy manure spread on the soil surface. J. Environ. Qual., 5:134.
- Loehr, R.C. 1974. Agricultural Waste Management. Academic Press, New York, New York.
- Loudon, T. 1975. Irrigation of animal waste. Agricultural Engineering Facts. No. 45, Department of Agricultural Engineering, Michigan State University, East Lansing, Michigan.
- MacLachlan, D.L. 1967. A study of dairy chore labor under different systems of free-stall housing. M.S. Thesis, Michigan State University, East Lansing, Michigan.
- Maddex, R.L. 1975. Waste handling systems identification. Agricultural Engineering Facts, No. 49, Department of Agricultural Engineering, Michigan State University, East Lansing, Michigan.
- Midwest Plan Service. 1975. Livestock Waste Facilities Handbook.
- Morgan, R.J. 1977. Unpublished price list and equipment information. Butler Manufacturing Company, Jamesway Division, Fort Atkinson, Wisconsin.
- Morton Ford Tractor, Inc. 1977. Unpublished price list and equipment information. Lansing, Michigan.
- Mote, C.R. and E.P. Taiganides. 1975. A computer simulation of storage and land disposal of wastes. The Proceedings of the 3rd International Symposium on Livestock Wastes. American Society of Agricultural Engineers. St. Joseph, Michigan.

- Murphy, T.A. 1974. Nonpoint source control to meet water quality goals. Proceedings of the 1974 Cornell University Agricultural Waste Management Conference, Syracuse, New York.
- Nesseth Incorporated. 1976. Unpublished price list and equipment information. Dafer, Michigan.
- North Central Regional Publication 222. 1975. Livestock Waste Management with Pollution Control.
- Nye, J.C.; D.D. Jones; D. Bache; and A.L. Sutton. 1975. Selecting a waste management system. Publication ID-107, Cooperative Extension Service, Purdue University, West Lafayette, Indiana.
- Official Guide Tractors and Farm Equipment, Fall, 1977. National Farm and Power Equipment Dealers Association, St. Louis, Missouri.
- Ogilvie, J.R.; P.A. Phillips, and K.W. Lievers. 1975. Shortest path network analysis of manure handling systems to determine least cost-dairy and swine. The Proceedings of the 3rd International Symposium on Livestock Wastes. American Society of Agricultural Engineers, St. Joseph, Michigan.
- Pearson Bros. Company. 1977. Unpublished price list and equipment information. Galia, Illinois.
- Pherson, C.L. 1974. Beef waste management economics for Minnesota farmer-feeders. Proceedings of the 1974 Cornell Agricultural Waste Management Conference, Rochester, New York.
- Price, D.R.; L.M. Safley, Jr.; and D.A. Haith. 1977. System studies of waste management alternatives. Dairy Chore Reduction Program Progress Report.
- Public Law 92-500. 1972. Federal Water Pollution Control Act Amendments of 1972. United States Congress.
- Roberts, I.P. 1884. Experiments on the cost and value of stable manure. Third Report of the Cornell University Experiment Station, Cornell University, Ithaca, New York.
- \_\_\_\_\_. 1891. The production and core of farm manures. Fourth Annual Report of the Cornell University of Agricultural Experiment Station, Cornell University, Ithaca, New York.
- Rohlf, T. 1977. Unpublished price list and equipment information. Calumet Company, Inc., Algoma, Wisconsin.



- Safley, L.M., Jr. 1974. Decision model for animal manure handling. M.S. Thesis, Cornell University, Ithaca, New York.
- \_\_\_\_\_. 1977. System selection and optimization models for dairy manure handling systems. Ph.D. Thesis, Cornell University, Ithaca, New York.
- Safley, L.M., Jr., and D.R. Price. 1976. Systems analysis of animal waste handling alternatives. American Society of Agricultural Engineers. Paper No. 76-5537.
- Safley, L.M., Jr.; D.A. Haith; and D.R. Price. 1977. Decision tools for dairy manure handling systems selection. American Society for Agricultural Engineers. Paper No. 77-4028.
- Salesky, A.J. 1977. Unpublished price list and equipment information. Allegan Pipe and Supply Company, Allegan, Michigan.
- Sempers, F.W. 1893. Manures: How to Make and Use Them. 2nd Edition, W.A. Burpee and Company, Philadelphia, Pennsylvania.
- Schaffer, W.H.; J.J. Jacobs; and G.L. Casler. 1974. An economic analysis of policies to control nutrient and soil losses from a small watershed in New York State. Proceedings of the 1974 Cornell Agricultural Waste Management Conference. Syracuse, New York.
- Smith, M.R. 1977. Unpublished price list and equipment information. Starline Division of Chromalloy, Harvard, Illinois.
- Stoll, T.L. 1974. An analysis of the effect of expansion on cash flow, management income, and various management factors. M.S. Thesis, Michigan State University, East Lansing, Michigan.
- Taylor, H.E. 1977. Unpublished price list and equipment information. Stevens Point, Wisconsin.
- Trimble, R.L.; L.J. Connor; and J.R. Brake. 1971. Michigan farm management handbook. Agricultural Economics Report 191. Department of Agricultural Economics, Michigan State University, East Lansing, Michigan.
- United States Department of Agriculture Soil Conservation Service. 1975. Agricultural waste management field manual.
- Van Arsdall, R.N. 1974. Economic impact of controlling surface water runoff from point sources in U.S. hog production. Proceedings of the 1974 Cornell Agricultural Waste Management Conference, Rochester, New York.

- Van Dale. 1977. Unpublished price list and equipment information. Long Lake, Minnesota.
- Vanderholm, D.H. 1976. Nutrient losses from livestock waste during storage, treatment, and handling. The Proceedings of the 3rd International Symposium on Livestock Wastes, University of Illinois, Urbana-Champaign, Illinois.
- Vermeer Manufacturing Company. 1977. Unpublished price list and equipment information. Pella, Iowa.
- Vitosh, M.L. 1975. Unpublished news release, personal communication.
- Walsh, L.M.; R.F. Hensler; and E.E. Schulte. 1975. Manage manure for its value. University of Wisconsin Extension Bulletin, A1672, University of Wisconsin, Madison, Wisconsin.
- Warfel, R.R. 1977. Unpublished price list and equipment information. Sperry New Holland, New Holland, Pennsylvania.
- Waud, D.C. 1977. Unpublished price list and equipment information. King Hydraulic Power Ltd., Woodstock, Ontario.
- Wheeler, H.J. 1913. Manures and Fertilizers. The Macmillan Company, New York, New York.
- Williamston Irrigation, Inc. 1977. Unpublished price list and equipment information. Williamstown, New York.
- Young, R.A. and C.K. Mutchler. 1976. Pollution potential of manure spread on frozen ground. J. Environ. Qual., 5:174.

APPENDIX A

SURVEY QUESTIONNAIRE FORMS

Table A-1. Farm survey form for waste handling systems

- 
1. Farm Code \_\_\_\_\_
  2. Farm Owners Name \_\_\_\_\_
  3. Number of cows housed in the facility \_\_\_\_\_
  4. Available labor on a daily basis \_\_\_\_\_

## HOUSING SYSTEMS

1. Which style housing is used for milking herd
  - a. Cold enclosed freestall, total confinement \_\_\_\_\_
  - b. Cold enclosed freestall, outside lot \_\_\_\_\_
  - c. Warm enclosed freestall, total confinement \_\_\_\_\_
  - d. Warm enclosed freestall, outside lot \_\_\_\_\_
  - e. Stanchion barn \_\_\_\_\_
  - f. Bedded pack, outside lot \_\_\_\_\_
2. If outside lot used, how much area must be scraped daily \_\_\_\_\_
3. If freestalls used, indicate the following:
  - a. Number of alleys \_\_\_\_\_
  - b. Length of alleys \_\_\_\_\_
  - c. Width of alleys \_\_\_\_\_
4. What type of bedding is used
  - a. sawdust \_\_\_\_\_
  - b. straw \_\_\_\_\_
  - c. woodchips or shavings \_\_\_\_\_
  - d. sand \_\_\_\_\_
  - e. other \_\_\_\_\_

Table A-1 (cont'd.)

- 
5. What type of equipment or method is used to clean alleys in the freestall barn
- |                                   |                                                 |
|-----------------------------------|-------------------------------------------------|
| a. automatic alley scraper_____   | d. 25-70 HP tractor_____                        |
| b. skid steer style loader_____   | e. flushing with occasional tractor scrape_____ |
| c. garden tractor with blade_____ | f. slotted floors_____                          |
6. How many times/day is alley cleaned\_\_\_\_\_
7. When is the alley cleaning done
1. continuously\_\_\_\_\_
  2. only while cows are in holding pen\_\_\_\_\_
  3. while cows are in freestall barn\_\_\_\_\_
8. How long does each cleaning require\_\_\_\_\_
9. How many men required per cleaning\_\_\_\_\_
10. Is the manure cleaned from each stall every day Yes\_\_\_\_ No\_\_\_\_
11. How many times/day is this done 1\_\_\_\_ 2\_\_\_\_
12. How much time does this require on a daily basis\_\_\_\_\_
13. How often is bedding material normally replaced or added to
1. once/week\_\_\_\_\_
  2. once/2 week\_\_\_\_\_
  3. once/3 week\_\_\_\_\_
  4. other\_\_\_\_\_
14. How long does this require each time
1. 1-2 hours\_\_\_\_\_
  2. 2-3 hours\_\_\_\_\_
  3. 3-4 hours\_\_\_\_\_
  4. 4-5 hours\_\_\_\_\_
  5. more\_\_\_\_\_

Table A-1 (cont'd.)

## 15. How is manure handled

- a. scraped directly into a cross conveyor \_\_\_\_\_
- b. " " " a piston pump \_\_\_\_\_
- c. " " " storage unit \_\_\_\_\_
- d. " " " an area with a buck wall \_\_\_\_\_
- e. " " " a pile in a lot area \_\_\_\_\_
- f. flushed directly into a flume or sump \_\_\_\_\_

## 16. If a cross conveyor is used, how many times per day is it operated

- a. one time \_\_\_\_\_
- b. 2 times \_\_\_\_\_
- c. more \_\_\_\_\_

## 17. How long does it run with each operation \_\_\_\_\_ minutes

## 18. Does someone observe it while it's operating Yes \_\_\_\_\_ No \_\_\_\_\_

## 19. If a piston pump is used, how many times/day is it operated \_\_\_\_\_

## 20. Time/operation \_\_\_\_\_

## 21. Does someone observe it while it is working Yes \_\_\_\_\_ No \_\_\_\_\_

## SOLIDS HANDLING SYSTEMS

## 1. Which method is used to load spreaders

- a. push manure off from a ramp directly into a spreader \_\_\_\_\_
- b. use of a skid steer loader \_\_\_\_\_
- c. use of a conventional tractor with a bucket \_\_\_\_\_
- d. gutter cleaner and short elevator \_\_\_\_\_

## 2. Spreader size in bushels A. \_\_\_\_\_ B. \_\_\_\_\_

## 3. How much time is needed to load the spreader with a loader \_\_\_\_\_

## 4. Approximately how far is it to the most commonly used unloading site \_\_\_\_\_

## 5. How long does it take to unload a load \_\_\_\_\_

Table A-1 (cont'd.)

- 
6. Approximately how many days of manure storage do you have \_\_\_\_\_
  7. How long does it take to empty when full \_\_\_\_\_ days

## LIQUID AND SEMI LIQUID SYSTEMS

1. Which type of storage is used for manure storage only
  - a. upright steel silo \_\_\_\_\_
  - b. upright cement silo \_\_\_\_\_
  - c. earthen lagoon \_\_\_\_\_
  - d. underground cement tank \_\_\_\_\_
  - e. under barn pit \_\_\_\_\_
2. Storage unit dimensions
  - a. height or depth \_\_\_\_\_
  - b. length \_\_\_\_\_
  - c. width \_\_\_\_\_
3. What is approximate storage time with this system \_\_\_\_\_
4. Is washwater and milking parlor water added to the storage system Yes \_\_\_\_\_ No \_\_\_\_\_
5. How long must storage unit be agitated prior to pumping \_\_\_\_\_ days
6. What is capacity of the pump used for agitating and filling tanks \_\_\_\_\_ GPM
7. What is volume of tankers being used A. \_\_\_\_\_ Gal. B. \_\_\_\_\_ Gal.
8. How long is required to load a tanker \_\_\_\_\_
9. What HP tractor is used on the pump \_\_\_\_\_ HP
10. What HP tractor is used on the tanker \_\_\_\_\_ HP
11. How long does it normally take to unload a load \_\_\_\_\_ minutes
12. With irrigation, how long does the initial setup take \_\_\_\_\_
13. How many people needed \_\_\_\_\_
14. How long for each reset \_\_\_\_\_

Table A-1 (cont'd.)

- 
15. How many people \_\_\_\_\_
  16. How long per set \_\_\_\_\_
  17. How many people to observe \_\_\_\_\_
  18. How completely do you empty the storage \_\_\_\_\_
  19. How long does this take \_\_\_\_\_

## YOUNG STOCK INFORMATION

1. Number
  2. Housing style
  3. Frequency cleaned
  4. Storage system used
  5. Time needed to clean
-



Table A-2. Introductory letter to equipment dealers

---

MICHIGAN STATE UNIVERSITY

---

College of Agriculture and Natural Resources      East Lansing · Michigan  
Department of Dairy Science · Anthony Hall      · 48824  
Telephone (517) 355-8433

Dear Sir:

I am currently a graduate student in the Dairy Department at Michigan State University and part of my thesis project involves a very detailed cost and labor analysis of commonly used waste systems for dairy cattle. The herd sizes being considered are 75-400 milking cows. Due to the detail and scope of this study I am requesting information from more companies than before and also I'm asking for updated catalogues and price lists from companies that may have participated previously.

I realize there are reservations on the part of companies to divulge price information for something such as this. Let me assure you that my only need for such figures is to compute an average price and a range in prices for each components of each waste handling system. No ranking or comparison of systems by brand name will be made and all contributing companies will be acknowledged.

If possible I would greatly appreciate receiving an up to date equipment catalogue as well as a current price list. In the event a catalogue is unavailable, please include any available information and prices regarding the items checked on the following page. If this is not possible please advise me of the name and location of your nearest dealer so that I might discuss my needs with him.

Sincerely,

Winston Ingalls

Return to:

Winston Ingalls  
Dairy Department  
Room 17 Anthony Hall  
Michigan State University  
East Lansing, Michigan 48824

WI/lb  
Enc.

---

Table A-3. Equipment information check list

---

I Would Appreciate Receiving Technical Information and Cost Data on the Following Items:

- ☐ 1. Front end loaders for use with a 45-60 H.P. tractor
  - ☐ 2. 250-350 bushel conventional solids spreader with hydraulic end gate
  - ☐ 3. 2500-3500 gallon liquid manure spreaders
  - ☐ 4. Injector systems for liquid manure spreaders
  - ☐ 5. Flail type tank spreaders
  - ☐ 6. Self loading slurry spreader
  - ☐ 7. Cross conveyors for barns up to 100 feet wide
  - ☐ 8. Manure stacker or elevator (30-50 feet)
  - ☐ 9. Portable liquid manure pumps for agitating and filling tankers
  - ☐ 10. Stationary pump to agitate and fill tank wagons
  - ☐ 11. Irrigation pump designed to move lagoon wastes up to one-half mile through irrigation pipe and big gun sprinkler
  - ☐ 12. Big gun sprinkler for manure slurry
  - ☐ 13. Irrigation pipe (price/foot or per standard length)
  - ☐ 14. Traveling gun sprinkler
  - ☐ 15. Free stall barn alley scrapers (chain, blade, drive unit)
  - ☐ 16. Above ground liquid manure tanks with recycling pump
  - ☐ 17. Hollow piston or solid piston manure pumps (pump, drive unit, hopper and PVC pipe)
  - ☐ 18. Compressed air manure mover
  - ☐ 19. Slotted floors for dairy cattle (cement)
-

## APPENDIX B

COMPUTER PROGRAMS FOR DETERMINING COSTS,  
ENERGY DEMANDS AND LABOR DEMANDS FOR  
VARIOUS WASTE HANDLING SYSTEMS

```

PROGRAM WASTE(INPUT,OUTPUT,TAPE1,TAPE2,TAPE3)
DIMENSION MTITLE(8,4),MOTITLE(10,4),MOT(4),IFESS(10,10,10)
DIMENSION COSTINT(3,13),DIRTPCT(8,13),DIRTTOT(8,13)
DIMENSION HRLABOR(8,13),COSTLAB(8,13),UNITENE(8,13),COSTENE(8,10)
DIMENSION ANNABEO(8,13),COSTAB(8,13),COSTOP(8,13),T(13)
DIMENSION IS(10)
DIMENSION ISOPT(3)
DIMENSION VALN(10,10)
DIMENSION ISO(8)
NSN=1
DO 10 I=1,10
DO 10 J=1,10
DO 10 K=1,10
IFESS(I,J,K)=J
C PEAD IN SECTION TITLES
DO 2 I=1,8
READ(1,1) MTITLE(I,J),J=1,4)
FORMAT(2X,4A8)
C PEAD IN OPTION TITLES
READ(1,3) ISE,(MOT(J),J=1,4)
FORMAT(13,4A8)
IF(EOF(1))10,5
DO 5 I=1,8
MOTITLE(I,ISE,I)=MOT(I)
GO TO 4
C PEAD IN FEASIBLE OPTIONS
READ(2,7) ISE,IPO,INO,IOC
FORMAT(3I2,3)
IF(EOF(2))20,3
IFESS(I,ISE,IPO,INO)=IOC
GO TO 10
C ASK QUESTIONS
PRINT 11
FORMAT(1 THIS PROGRAM CALCULATES THE COSTS ASSOCIATED WITH A PARTICULAR WASTE MANAGEMENT SYSTEM)
PRINT 13
FORMAT( THERE ARE 8 SECTIONS OF CRITERIA NEEDED TO COMPLETE THIS TASK)
PRINT 14
FORMAT( THE SECTIONS ARE AS FOLLOWS: )
DO 15 I=1,8
PRINT 16,1 MTITLE(I,J),J=1,4)
FORMAT(5,5X,4A8)
PRINT 17
FORMAT( FOR EACH SECTION THERE ARE SEVERAL OPTIONS )
PRINT 18
FORMAT( WHEN PROMPTED WITH AN ASTERISK TYPE IN THE CODE FOR THE OPTION DESIRED. TYPE 002 FOR ALL POSSIBLE OPTIONS FROM THIS POINT ON-TYPE 00C )
NN=1
DO 30 I=1,8
DO 30 J=1,10
COSTINT(I,J)=DIRTPCT(I,J)+DIRTTOT(I,J)+HRLABOR(I,J)+COSTLAB(I,J)+UNITENE(I,J)+COSTENE(I,J)+ANNABEO(I,J)+COSTAB(I,J)+COSTOP(I,J)
IFLAG=0
DO 40 I=1,10
IS(I)=J
I(I)=0
J=1
DO 100 I=1,8
PRINT 33,1 MTITLE(I,L),L=1,4)
FORMAT(8,12,5X,4A8)
PRINT 34
FORMAT( CODE OPTION )
DO 27 K=1,10
IF(I,ESS(I,J,K).EQ.0) GO TO 23
PRINT 27, I,ESS(I,J,K), (MOTITLE(L,LL),LL=1,4)
FORMAT(13,13,5X,4A8)
CONTINUE
READ 25, KODE
FORMAT(13)
IF(KODE.EQ.9) GO TO 105
DO 43 K=1,10
IF(I,ESS(I,J,K).EQ.KODE) GO TO 41
CONTINUE
PRINT 42
FORMAT( THIS IS NOT A FEASIBLE OPTION, RETYPE CODE )
GO TO 24
PRINT 29, (MOTITLE(KODE,LL),LL=1,4)

```

```

29  FORMAT(* YOU WISH TO USE *148,* IS THAT CORRECT=*/,
    * TYPE Y FOR YES, N FOR NO*)
28  READ 23,IR
    FORMAT(I1)
    IF (IR.EQ.318) GO TO 26
31  PRINT 30
30  FORMAT(* TYPE IN NEW OPTION*)
    GO TO 24
26  IF (I.EQ.1) GO TO 101
    IF (I.GE.6) NN=NN-1
    JS=CODE-(1*10)+NN
    JS(1)=J
    GO TO 102
105  PRINT 106
105  FORMAT(* YOU WISH TO MAKE NO MORE CHOICES, IS THAT CORRECT=*/,
    * TYPE Y FOR YES, N FOR NO*)
    READ 23,IR
    IF (IR.EQ.318) GO TO 102
    GO TO 31
101  JS=CODE
    JS(1)=J
    IF (JS.EQ.5) GO TO 200
102  CONTINUE
102  C READ IN VARIABLE CRITERIA
200  PRINT 201
201  FORMAT(* TYPE IN THE FOLLOWING VARIABLES WHEN ASKED*)
202  PRINT 203
203  FORMAT(* NUMBER OF COWS IN 13 FORMAT, IE 000*)
    READ 23,NCOWS
    FORMAT(I3)
205  PRINT 202,NCOWS
202  FORMAT(* SYSTEM COSTS WILL BE CALCULATED FOR *,I3,* COWS*/
    * IS THAT CORRECT= TYPE Y FOR YES, N FOR NO*)
    READ 23,IR
    IF (IR.EQ.318) GO TO 500
    PRINT 207
207  FORMAT(* TYPE IN NEW NUMBER OF COWS*)
    GO TO 204
500  PRINT 300
    COWS=NCOWS
300  FORMAT(* TYPE IN STYLE OF BARN YOU HAVE*)
    PRINT 301
301  FORMAT(* 1=PENN STYLE DRIVE THRU,CENTRAL ALLEY,4 ALLEYS*)
    PRINT 302
302  FORMAT(* 2=CENTER FEED-2 ALLEYS*)
    PRINT 303
303  FORMAT(* 3=NONE OF THE ABOVE*)
    READ 304,IBARN
304  FORMAT(I1)
    GO TO(1,2,3,4)IBARN
310  ALLEYNO=4.0
    ALLLNTH=((COWS*0.9/ALLEYNO)+0.20*(COWS*0.9/ALLEYNO))*3.5+20
    GO TO 400
311  ALLEYNO=2.0
    ALLLNTH=((COWS*0.9/ALLEYNO))*3.5
    GO TO 400
312  PRINT 313
313  FORMAT(* TYPE IN NUMBER OF ALLEYS IN YOUR BARN*)
    READ 314,ALLEYNO
    FORMAT(I2.0)
314  PRINT 315,ALLEYNO
315  FORMAT(* YOU WILL HAVE*,F3.0,*ALLEYS IN YOUR BARN,CORRECT=*,
    * TYPE Y FOR YES,N FOR NO*)
    READ 23,IR
    IF (IR.EQ.318) GO TO 316
    GO TO 312
316  PRINT 317
317  FORMAT(* TYPE IN THE ALLEY LENGTH PER ALLEY, I.E. BARN LENGTH*)
    READ 318,ALLLNTH
    FORMAT(F3.0)
    PRINT 319,ALLLNTH
319  FORMAT(* THE ALLEY LENGTH OF BARN WILL BE*,F5.0,/
    * IS THAT CORRECT, TYPE Y FOR YES, N FOR NO*)
    READ 23,IR
    IF (IR.EQ.318) GO TO 400
    GO TO 316
400  CONTINUE
    CPA=COWS/ALLEYNO
    IF (CPA.LE.75) GO TO 401
    PRINT 402

```

```

8320
8330
8400
8450
8500
8550
8600
8650
8700
8750
8800
8850
8900
8950
9000
9100
9200
9300
9400
9500
9600
9700
9800
9900
1000
1010
1020
1030
1040
1050
1060
1070
1080
1090
1100
1110
1120
1130
1140
1150
1160
1170
1180
1190
1200
1210
1220
1230
1240
1250
1260
1270
1280
1290
1300
1310
1320
1330
1340
1350
1360
1370
1380
1390
1400
1410
1420
1430
1440
1450
1460
1470
1480
1490
1500
1510
1520
1530
1540
1550
1560
1570
1580
1590
1600
1610
1620

```

```

402  FORMAT('YOU WILL HAVE MORE THAN 75 COWS PER ALLEYWHICH',
  *MAY RESULT IN ALLEY LENGTHS APPROACHING 300 FEET WHICH',
  *EXCEEDS THE LENGTH THAT A ALLEY SCRAPER MAY HANDLE',
  *DO YOU WISH TO CONSIDER CHANGING THE NUMBER OF COWS OR',
  *EARN TYPE (I.E.NO OF ALLEYS),TYPE Y FOR YES,N FOR NO')
  READ 2,IR
  IF(IR.EQ.319) GO TO 234
401  CONTINUE
  IF(YS(4).NE.0) GO TO 440
  PRINT 430
430  FORMAT('TYPE ?N 2 FOR FLUSH SYSTEM',
  *TYPE IN 0 FOR NON-FLUSH SYSTEM')
  READ 3,IS(10)
431  FORMAT(11)
440  CONTINUE
C ALL CALCULATIONS AND CONSTANTS
C INITIALIZATION OF DEFAULT VARIABLES
C STALL SPECIFICATIONS AND BEDDING NEEDED
C LABOR COSTS PER HOUR
  CCLABOR=1.5
C CEMENT COSTS PER CUYD
  CCEMST=25.00
C COST PER SQ FT OF CEMENT POURED FOR FLOORING
  CFCSSQFT=1.50
C COST OF CONCRETE PER SQFT FOR STORAGE
  CCNCSQFT=1.25
C COST OF CLAY/CUYD
  CLAYCST=5.00
C INITIAL VOL OF CLAY/STALL (CUYDS)
  CLAYVOL=1.00
C VOL OF CURB PER FOOT OF 10 INCH CURB (CUYDS)
  CURBVOL=0.016
C CURB COST PER FOOT
  CURBCST=1.00
C COST OF INDIVIDUAL COW MATS
  COSTMAT=50.00
C NUMBER OF STALLS PER COW
  STNPCOW=0.9
C SAND USED PER DAY/STALL (CUYDS)
  SANDDAY=0.25
C INITIAL SAND COVER PER STALL (CUYDS)
  SNDCOV=1.0
C COST OF SAND/CUYD ($/YD)
  SNDCST=3.00
C COST OF SHAVINGS/LB ($/LB)
  SSCSTL=0.60
C INITIAL SHAVINGS/STALL (LBS)
  STALSHAV=75.0
C COST OF STRAW/LB ($/LB)
  STALCST=0.25
C INITIAL STRAW/STALL (LBS)
  STALSTRA=75.0
C STALL DEPTH FROM CURB TO FRONT(FT)
  STALPTH=7.0
C SHAVINGS USED/MATTED STALL/DAY
  SHAVHSD=2.0
C DAILY STRAW/MATTED TALLS
  SHAVTSD=1.0
C CEMENT THICKNESS IN BASE OF STALL (FT)
  STTHCK=0.03
C WIDTH OF EACH STALL(FT)
  STWIDTH=3.5
C WEIGHT OF SHAVINGS USED PER STALL PER DAY(LBS)
  WTSHTD=4.0
C WEIGHT OF STRAW USED PER STALL PER DAY (LBS)
  WTSSTD=6.2
C YRLY TIME SPENT FIXING EACH CLAY STALL
  CLFXT=0.5
C STALL DEPR RATE
  STDEPR=0.05
C STALL INT RATE
  STINTR=0.05
C STALL RMT RATE
  STRMIR=0.035
C CURB SALVAGE VALUE
  CURBSLV=0.00
C DAILY N EXCRETED PER COW
  CLYNNPC=0.50
C YRLY TOTAL N EXCRETED
  YRLYNN=CLYNNPC*COWS*365
C DAILY PHOSPHOROUS PER COW

```

```

1630
1640
1650
1660
1670
1680
1690
1700
1710
1720
1730
1740
1750
1760
1770
1780
1790
1800
1810
1820
1830
1840
1850
1860
1870
1880
1890
1900
1910
1920
1930
1940
1950
1960
1970
1980
1990
2000
2010
2020
2030
2040
2050
2060
2070
2080
2090
2100
2110
2120
2130
2140
2150
2160
2170
2180
2190
2200
2210
2220
2230
2240
2250
2260
2270
2280
2290
2300
2310
2320
2330
2340
2350
2360
2370
2380
2390
2400
2410
2420
2430

```



```

C STRAM COSTS/YR MATS=FEL*
C STHMFCY=SHATTY
C TOTAL CLAY USED
CLAYTOT=(STALLN*CLPEST)
C SHALNGS7FT WITH MATTED STALLS,FEL*
SHMFL=SHATV*
C TOTAL CLAY INITIALLY USED (COST)
CLAYTOTS=(CLAYTOT*CLMCT)
C CURB AND INITIAL CLAY COSTS
CLERCCS=(CURBCST*CLATCCS)
C COST OF CURB,SAND AND CLAY
CSTSCC=(SANDTCC*CLATCCS+CURBCST)
C TOTAL COST OF CEMENT CURB SLAY AND SHAVINGS
C TOTAL COST OF CURB,CST,CLAYTCCS,SSTOCCST
STOCCS=(CU*BCST+CLAYTCCS*SSTOCCST)
C TOTAL COST OF CURB+CLAY BASE+STRAW
STCCS=(CURBCST*CLATCCS+STMTCT)
C CEMENT VOL PER STALL PLATFORM (CUYDS)
STOCHVL=(STMTCT*STOPTH*STTHCK)/27
C TOTAL YDS CEMENT IN STALLS
STCHMT=(STOCHVL*STALLN)
C COST OF STALL PLATFORM CEMENT
STPLCST=(CLCCSOP*STWIDTH*STDPTH)*STALLN
C COST OF CURB AND PLATFORM
CURBPLC=(STPLCST+CURBCST)
C CEMENT STALL AVE VALUE
CURBPC=(CURBPLC*STOTRTR)
C TOTAL COSTS OF MATS+INITIAL SHAVINGS
COSTMAT=(COSTMAT*STALLN)+(0.5*SSTOCCST)
C TOTAL COST OF MATS+INITIAL STRAW
COSTMAT=(COSTMAT*STALLN)+(0.5*STMTCT)
C COST OF CURB+CEMENT PLATFORM+MATS
STPLCPC=(STPLCST+CURBCST+SSTOCCST)
C COST OF CEMENT PLATFORM+CURB+INITIAL SHAVINGS
STPCCS=(STPLCPC+CURBCST+SSTOCCST)
C COST OF CEMENT PLATFORM CURB AND STRAW
STPCCS=(STPLCPC+CURBCST+STMTCT)
C WASTE PRODUCTION VOLUMES ETC
C INITIALIZATION OF DEFAULT VALUES
VMSANDY=1
VMANDAY=1.85
C DAILY MILKHOUSE WASTE VOLUME (CU FT PER COW)
VMSHTDY=80
C DAILY VOLUME OF SAND ENTERING WASTE SYSTEM (CUFT)
VMSANDY=1
C WASTE PRODUCTION CALCULATED VALUES
C TOTAL DAILY VOLUME OF MILKHOUSE WASTE PRODUCED DAILY
VMSANDY=1
C TOTAL DAILY MANURE PRODUCED
TVMANDY=(1.85*COVS)
C DAILY VOLUME OF SHAVINGS ENTERING MANURE STORAGE
VOLSHTDY=(VMSHTDY*STALLN*0.5)/8
C DAILY VOL OF STRAW ENTERING STORAGE
VOLSHTDY=(VMSHTDY*STALLN*0.5)/8
C DAILY VOL SHAVINGS AND MANURE
VOLSHTDY=VOLSHTDY+TVMANDY
C DAILY VOL OF MANURE SHAVINGS AND WASTE WATER
VOLSHTDY=(VOLSHTDY+VMSHTDY+TVMANDY)
C 90DAY SHAV AND MANURE ETC
VLS90DY=(90*VOLSHTDY)
C 180DAY SHAV AND MANURE
VLS180DY=(180*VOLSHTDY)
C 270DAY SHAV AND MANURE
VLS270DY=(270*VOLSHTDY)
C 365DAY SHAV AND MANURE
VLS365DY=(365*VOLSHTDY)
C 365 DAY VOLUME SHAVINGS AND MANURE
VLS365DY=(365*VOLSHTDY)
C DAILY VOL OF MANURE STRAW AND WASTE WATER
VLSHTDY=(TVMANDY+VMSHTDY+VOLSHTDY)
C 90 DAY STRAW AND WASTE VOL
VLS90DY=(90*VLSHTDY)
C 180DAY STRAW AND WASTE VOL
VLS180DY=(180*VLSHTDY)
C 270DAY VOL STRAW
VLS270DY=(270*VLSHTDY)
C 365DAY VOL STRAW
VLS365DY=(365*VLSHTDY)
C TOTAL COSTS
COSTMAT=(COSTMAT*STALLN)+(0.5*SSTOCCST)
COSTMAT=(COSTMAT*STALLN)+(0.5*STMTCT)
C DAILY VOLUME OF MANURE,SAND AND MILKHOUSE WATER
VLSNDY=(VMSANDY+VMANDAY+VMSHTDY)

```

```

3250
3260
3270
3280
3290
3300
3310
3320
3330
3340
3350
3360
3370
3380
3390
3400
3410
3420
3430
3440
3450
3460
3470
3480
3490
3500
3510
3520
3530
3540
3550
3560
3570
3580
3590
3600
3610
3620
3630
3640
3650
3660
3670
3680
3690
3700
3710
3720
3730
3740
3750
3760
3770
3780
3790
3800
3810
3820
3830
3840
3850
3860
3870
3880
3890
3900
3910
3920
3930
3940
3950
3960
3970
3980
3990
4000
4010
4020
4030
4040
4050

```



```

C 90DAY SAND AND WASTE VOLUME                                4060
VL90SD=(90*VLMSNDM)                                           4070
C 1800DAY SAND WASTE VOL                                       4080
VL180SD=(180*VLMSNDM)                                         4090
C 270 DAY SAND WASTE                                           4100
VL270SD=(270*VLMSNDM)                                         4110
C 365 DAY SAND WASTE VOL                                       4120
VL365SD=(365*VLMSNDM)                                         4130
C DEFAULT VARIABLES ASSOCIATED WITH UTILITY TRACTOR          4140
C UTILITY TRACTOR DEP RATE                                     4150
UTDPR=0.16                                                      4160
C HOURS/DAY UTILITY TRACTOR USED FOR SCRAPING ONE ALLEY 2> DAILY 4170
UTRSDY=0.33                                                      4180
C UTILITY INTEREST RATE                                         4190
UTINTPR=0.06                                                     4200
C UTILITY MISC RATE                                             4210
UTMSCPR=0.02                                                     4220
C COST OF NEW UTILITY TRACTOR AND BLADE                       4230
UTNCOST=1500.00                                                  4240
C UTILITY TRACTOR YRLY FIXED COSTS                             4250
UTRFXC=0.75                                                      4260
C GALLONS/HR OF FUEL USED                                       4270
UTGALHR=3.0                                                      4280
C PHI RATE                                                     4290
UTRHIR=0.10                                                      4300
C SALVAGE VALUE AFTER 10 YRS                                   4310
UTSLV=0.01                                                       4320
C PERCENT OF TRACTORS TCTAL TIME USED FOR SCRAPING           4330
UTSCRPR=0.30                                                      4340
C COST OF GASOLINE                                             4350
FUELCST=0.53                                                     4360
C DIESEL FUEL COSTS                                           4370
FUEDSL=0.52                                                      4380
C CALCULATED VALUES FOR UTILITY TRACTOR                     4390
C HRS UTILITY TRACTOR USED PER DAY FOR SCRAPING              4400
UTRSDC=ALLEYNO*UTRSDY                                           4410
C HOURS USED SCRAPING/YR                                       4420
UTRHSYR=(UTRSDC*365)                                           4430
C LABOR COSTS/YR FOR SCRAPING                                  4440
UTLABYR=(UTRHSYR*CSLABOR)                                       4450
C FUEL USED/DAY                                                4460
UTFUEL= (UTGALHR*UTRSDY*ALLEYNO)                                4470
C FUEL/YR                                                       4480
UTFUELY=(UTFUEL*365)                                           4490
C FUEL COSTS/YR                                                4500
UTFCYST=(UTFUELY*FUEDSL)                                       4510
C OPERATING COSTS FOR YR                                       4520
UTOPCSY=(UTLABYR+UTFCYST)                                       4530
C UTILITY TRACTOR OIRT RATE                                     4540
UTDIRTP=(UTDPR+UTINTPR+UTMSCPR+UTRHIR)                          4550
C YRLY OWNERSHIP COSTS FOR UTILITY TRACTOR                   4560
UTYOWCS=UTDIRTP*UTNCOST                                         4570
C UTILITY TRACTOR OWN COSTS DUE TO SCRAPING                   4580
UTOWNCS=UTRHSYR*UTRFXC                                          4590
C TOTAL YEARLY COSTS OF OWNERSHIP PLUS OPERATING             4600
UTYOWCS=(UTOWNCS+UTOPCSY)                                       4610
C FLOOR OR ALLEY DIMENSIONS                                   4620
C INITIALIZATION OF DEFAULT VALUES                          4630
C SLOTTED FLOOR AREA/COW(SQFT)                                4640
SLOTACH=45.0                                                     4650
C COST OF SLOTTED FLOOR ALLEY ($/SQFT)                        4660
SLOTCT=2.25                                                      4670
C SLOTTED FLOOR DEP RATE                                       4680
SLFDEPR=0.05                                                     4690
C SLOT FLOOR INT RATE                                          4700
SLFINTR=0.05                                                     4710
C SLOT FLOOR RHI RATE                                          4720
SLFRHIR=0.035                                                    4730
C SOLID FLOOR DEP RATE                                         4740
SOFDEPR=0.05                                                     4750
C SOLID FLOOR INT RATE                                         4760
SOFINTR=0.05                                                     4770
C SOLID FLOOR RHI RATE                                         4780
SOFRHIR=0.035                                                    4790
C ALLEY AREA PER COW ON SOLID FLOORS                          4800
CFACOW=50.0                                                      4810
C THICKNESS OF CEMENT IN ALLEYS(FT)                           4820
CFTHICK=0.33                                                     4830
C CALCULATED VALUES FOR FREESTALL ALLEYS                     4840
C TOTAL SLOTTED FLOOR AREA                                    4850
SLOTATL=(SLOTACH*CFOWS)                                         4860

```

```

C COST OF TOTAL SLOTTED FLOOR 4870
  SLOTTCS=(SLOTCF+S.OIATL) 4880
C SLOTTED FLOOR DIRT RATE 4890
  SLFDIRTR=(SLFDCPR+SLFINTR+SLFRMR) 4900
C YEARLY SLOTTED FLOOR OWN COSTS 4910
  SLFOCS=(SLOTTCS*SLFDIRTR) 4920
C TOTAL AREA OF SOLID FLOOR 4930
  TOTCEMA=(COMS*CFACOM) 4940
C VOLUME OF CEMENT IN FLOORS OR ALLEYS (CUYDS) 4950
  CFCVOL=(TOTCEMA*CFTHICK)/27 4960
C COST OF CEMENT IN SOLID FLOOR 4970
  CSTCFLO=CFCVOL*COMS*CFACOM 4980
C SOLID FLOOR DIRT RATE 4990
  SOFDIRTR=(SOFDCPR+SOFINTR+SOFRMR) 5000
C YEARLY SOLID FLOOR OWN COSTS 5010
  SOFPCS=(SOFDIRTR*CSTCFLO) 5020
C INITIALIZATION OF VALUES FOR SKID STEER LOADER 5030
C FUEL CONSUMPTION PERHR 5040
  GALNHR=2.8 5050
C SKID STEER AVE TRADE IN OF OLD LOADER 5060
  SKAVECD=1.00 5070
C NEW PRICE FOR SKID STEER 5080
  SKCOST=10500 5090
C HOURS USED/DAY HANDLING MANURE (SCRAPING ALLEYS) 1 ALLEY, 2X DAILY 5100
  SKHRDSA=0.33 5110
C TIME TO LOAD 1 SPREADER (280BU) 5120
  SKLOACT=5.5 5130
C C/OF TIME SKID STEER USED FOR MANURE HANDLING ACTIVITIES 5140
  SKMSPE=0.35 5150
C SKIDS DEPR 5160
  SKSDEPR=0.125 5170
C SKID STEER INT RATE 5180
  SKSINTR=0.05 5190
C SKS RMI RATE 5200
  SKSRMR=0.065 5210
C SKS MISC RATE 5220
  SKSMSCR=0.02 5230
C PERCENTAGE OF SKS TIME SCRAPING 5240
  SKSPER=0.25 5250
C HRLY FIXED COSTS ON SKS 5260
  SKHRFXC=0.00 5270
C CALCULATED VALUES FOR SKID STEER 5280
C TOTAL SKS DIRT RATE 5290
  SKSDIRT=(SKSDEPR+SKSINTR+SKSRMR+SKSMSCR) 5300
C HRS/DAY SKID STEER USED FOR SCRAPING 5310
  SKSHOSC=ALLEYNO*SKHRDSA 5320
C HOURS PER YEAR SKID STEER USED FOR MANURE HANDLING SCRAPING ALLEYS 5330
  SKHRYR=SKSHOSC*365 5340
C SKID STEER LABOR COSTS FOR YEAR SCRAPING 5350
  SKLST=(SKHRYR*CSLABOR) 5360
C TOTAL FUEL USED IN A YR SCRAPING 5370
  FUELYR=(SKHRYR*GALNHR) 5380
C FUEL COSTS/YEAR SCRAPING 5390
  SKFCSTY=(FUELYR*FUELCST) 5400
C SKS OWN COSTS 5410
  SKSONNC=((SKSDIRT*SKCOST)*SKSPER) 5420
C OWNERSHIP COSTS ON SKS DUE TO ALLEY SCRAPING 5430
  SKALSOC=SKHRYR*SKHRFXC 5440
C SKID STEER TOTAL COSTS 5450
  SKTCST=SKALSOC+SKFCSTY+SKLST 5460
C TIME TO BED COWS WITH STRAW OR SANDUST USING EITHER A SKIDSTER OR FROM 5470
C COST OF FEL 5480
  FELCST=2500.00 5490
C TOTAL COST OF UTILITY TRACTOR AND FEL 5500
  FELUTTC=FELCST+UTNCST 5510
C DEPRECIATION RATE ON FEL 5520
  FELDEPR=0.10 5530
C INTEREST RATE ON LOADER 5540
  FELINTR=0.06 5550
C RMI RATE ON FEL 5560
  FELRMR=0.07 5570
C MISC RATE ON LOADER 5580
  FELMISC=0.02 5590
C SALVAGE VALUE OF FEL 5600
  FELSAV=0.00 5610
C PERCENTAGE OF FRONT LOADERS TOTAL TIME SPENT ON BEDDING (DEFAULT VARIA 5620
  FDTTFR=0.10 5630
C PERCENT OF TIME FEL USED BEDDING MATS 5640
  FOMFPR=0.06 5650
C NUMB OF PEOPLE JOINING BEDDING WITH FRONT LOADER 5660
  BEDLABR=2 5670

```

C NUMBER OF MEN USED TO BED WITH SKIDSTER	56.80
BEDSKLBS	56.90
C PERCENT TOTAL TIME SKIDSTER USED FOR BEDDING	57.00
BEDSKLBS	57.10
C TIME PER MONTH TO BED 1 STALL WITH FRONT LOADER	57.20
BEDSKLBS	57.30
C TIME/MONTH TO BED MATS WITH FEL, SHAVINGS.	57.40
BEDSKLBS	57.50
C TIME/MONTH TO BED MATS WITH FEL AND STRAW	57.60
BEDSKLBS	57.70
C TIME/MONTH TO BED WITH SKIDSTER (STRAW OR SHAVINGS, NO MATS), *4860.	57.80
BEDSKLBS	57.90
C TIME/MONTH TO BED MATS WITH SKS AND SHAVINGS	58.00
BEDSKLBS	58.10
C TIME/MONTH TO BED MATS WITH SSKS AND STRAW	58.20
BEDSKLBS	58.30
C CALCULATED VALUES FOR SKIDSTER AND FEL FOR STRAW, SHAVINGS AND SANDUST	58.40
C HRS/YR FOR BEDDING USED IN BEDDING WITH SHAVINGS	58.50
BEDSKLBS	58.60
C FEL TOTAL DMRH	58.70
FELCST*(FELDPR+FELINTR+FELMISR+FELAHIR)	58.80
C FEL OWN COSTS	58.90
FELCST*(FELDPR+FELCST)	59.00
C MONTHLY MENHRS TO BED MATS WITH FEL	59.10
BEDSKLBS	59.20
C YRLY HRS TO BED WITH FEL AND SHORT STRAW	59.30
BEDSKLBS	59.40
C YEARLY LABOR COSTS WITH FEL (BDOHMMH)	59.50
BEDSKLBS	59.60
C YRLY HRS TO BED MATS WITH FEL AND SHAVINGS	59.70
BEDSKLBS	59.80
C YRLY HRS TO BED MATS WITH FEL AND STRAW	59.90
BEDSKLBS	60.00
C FUEL USE FOR FEL FOR BEDDING STRAW ETC	60.10
BEDSKLBS	60.20
C FUEL COSTS FOR FEL FOR BEDDING	60.30
BEDSKLBS	60.40
C FEL OWNERSHIP COSTS (ATTRIBUTED) TO BEDDING	60.50
BEDSKLBS	60.60
C OWN COSTS FOR BEDDING WITH FEL MATS SHAVINGS	60.70
BEDSKLBS	60.80
C OWN COSTS FOR FEL MATS STRAW	60.90
BEDSKLBS	61.00
C YEARLY TOTAL COST FOR FEL FOR BEDDING	61.10
BEDSKLBS	61.20
C LABOR COSTS SHAVINGS MATS FEL	61.30
BEDSKLBS	61.40
C LABOR COSTS SHAVINGS MATS FEL	61.50
BEDSKLBS	61.60
C SKIDSTER HRS PER MONTH SPENT BEDDING	61.70
BEDSKLBS	61.80
C TOTAL MONTHLY MAN HRS FOR BEDDING WITH SKIDSTER	61.90
BEDSKLBS	62.00
C YEARLY MANHRS FOR BEDDING WITH SKIDSTER	62.10
BEDSKLBS	62.20
C ANNUAL LABOR COSTS ASSOCIATED WITH SKIDSTER BEDDING	62.30
BEDSKLBS	62.40
C YRLY HRS TO BED MATS WITH SKS AND SHAVINGS	62.50
BEDSKLBS	62.60
C YRLY HRS TO BED MATS WITH SKS AND STRAW	62.70
BEDSKLBS	62.80
C LABOR COSTS SHAVINGS MATS SKS	62.90
BEDSKLBS	63.00
C LABOR COSTS SHAVINGS MATS SKS	63.10
BEDSKLBS	63.20
C ANNUAL SKIDSTER FUEL USE FOR BEDDING	63.30
BEDSKLBS	63.40
C FUEL USED FOR SHAVINGS BEDSKLBS*GALNHR	63.50
BEDSKLBS	63.60
C FUEL USED MATS STRAW FEL	63.70
BEDSKLBS	63.80
C FUEL USED MATS SHAVINGS SKS	63.90
BEDSKLBS	64.00
C FUEL USED MATS STRAW SKS	64.10
BEDSKLBS	64.20
C ANNUAL SKIDSTER FUEL COSTS ASSOCIATED WITH BEDDING	64.30
BEDSKLBS	64.40
C FUEL COSTS SHAVINGS MATS FEL	64.50
BEDSKLBS	64.60
C FUEL COSTS SHAVINGS MATS FEL	64.70
BEDSKLBS	64.80
C FUEL COSTS SHAVINGS MATS FEL	64.90
BEDSKLBS	65.00

C FUEL COSTS SHAVINGS MATS SKS	64.90
BDSKFLC=BSKFLC+BSKFLC	65.00
C FUEL COSTS SHAVINGS MATS SKS	65.10
BDSKFLC=BSKFLC+BSKFLC	65.20
C ANNUAL SKIDSTER OWNERSHIP COSTS DUE TO BEDDING (NO MATS)	65.30
BDSKFLC=BSKFLC+BSKFLC	65.40
C OWN COSTS FOR BEDDING MATS WITH SKS SHAVINGS	65.50
BDSKFLC=BSKFLC+BSKFLC	65.60
C OWN COSTS TO BED MATS WITH SKS AND STRAW	65.70
BDSKFLC=BSKFLC+BSKFLC	65.80
C ANNUAL TOTAL COSTS ASSOCIATED WITH SKST AND BEDDING	65.90
SKSTTYC=(BDSKFLC+BSKFLC+BSKFLC)	66.00
C BEDDING WITH SAND BEDDING	66.10
C INITIALIZATION OF DEFAULT VARIABLES	66.20
C NUMBER OF PEOPLE NEEDED WITH FRONT LOADER	66.30
FLSMEN=3	66.40
C TIME/MONTH TO BED 1STALL WITH SAND AND FRONT LOADER	66.50
FLSTOTM=FLSTOTM+1	66.60
C PERCENTAGE OF TOTAL TIME FEL IS USED FOR SAND BEDDING	66.70
FLSPER=0.20	66.80
C MEN NEEDED TO BED COWS WITH SAND USING A SKIDSTER	66.90
SNOSLSB=2.4	67.00
C TIME/MONTH TO BED 1 STALL WITH SAND USING SKIDSTER	67.10
SNOSLS=0.3	67.20
C PERCENT OF TIME SKST USED FOR SAND BEDDING	67.30
SNOSSPR=0.05	67.40
C CALCULATED VALUES FOR SAND BEDDING	67.50
C TIME TO BED COMPLETE HERD/MONTH WITH SAND AND FL	67.60
FLSTOTM=FLSTOTM+1	67.70
C YRLY UTILITY TRACTOR TIME TO BED WITH SAND	67.80
FLSTYTH=FLSTOTM*12	67.90
C TOTAL MONTHLY MANHRS TO BED WITH SAND AND FRONT LOADER MONTHLY	68.00
FLMHRS=(FLSTOTM*FLSMEN)	68.10
C YRLY MHS TO BED WITH SAND AND FEL	68.20
FLSYRMH=(FLMHRS*12)	68.30
C YEARLY LABOR COSTS FOR SAND AND FL	68.40
FLSYLCS=((12*FLMHRS)*3.50)	68.50
C YEARLY FUEL USED TO BED WITH SAND AND FRONT LOADER	68.60
FLSNFLU=(FLSTOTM*2)*UTGALHR	68.70
C YEARLY FUEL COSTS DUE TO THIS JOB	68.80
FLSNFYC=(FLSNFLU*FUEDSLCC)	68.90
C YEARLY OWNERSHIP COSTS DUE FRONT LOADER AND SAND	69.00
FLSNOCSC=(FLSNFYC*FLSNPER)+(UTHRFXC*FLSTYTH)	69.10
C TOTAL YEARLY COSTS OF OPERATING FRONT LOADER FOR SAND BEDDING	69.20
FLSNFYC=(FLSNFYC+FLSNOCSC+FLSYLCS)	69.30
C TOTAL MONTHLY TIME TO BED ALL STALLS, SAND AND SKS	69.40
SNOSSTT=SNOSLS*STALLSN	69.50
C TOTAL MANHRS PER MONTH NEEDED TO BED WITH SAND AND SKST	69.60
SNOTHLB=(SNOSSTT*SNOSLSB)	69.70
C YEARLY LABOR FOR BEDDING WITH SAND AND SKIDSTER	69.80
SNOSSYL=(SNOTHLB*12)	69.90
C YEARLY LABOR COSTS FOR SAND AND SKIDSTEP	70.00
SNOSSLC=(SNOSSYL*CSLABOR)	70.10
C YEARLY FUEL USE FOR SAND BEDDING AND SKIDSTER	70.20
SNOSSFU=(SNOSSTT*GALNHR)	70.30
C YEARLY FUEL COSTS WITH SAND AND SKIDSTER	70.40
SNOSFFC=(SNOSSFU*FUELCST)	70.50
C YEARLY OWNERSHIP COSTS OF SKST DUE TO BEDDING SAND	70.60
SNOSSYO=SNOSSTT*2*SKHFXC	70.70
C TOTAL YEARLY COSTS OF OPERATING SKIDSTEP	70.80
SNOSSTC=(SNOSFFC+SNOSSYO+SNOSSLC)	70.90
C INITIALIZATION OF ALLEY SCRAPER DEFAULT VARIABLES	71.00
C HOURS ALLEY SCRAPER MOTOR(S) RUN DAILY	71.10
ALLMHS=10.0	71.20
C AMPERAGE OF WORKING MOTOR FOR SCRAPER	71.30
AMPSCRM=12	71.40
C COST OF CHAIN/FT	71.50
CHNCSTF=6.00	71.60
C COST OF TIME CLOCKS	71.70
CLCKCST=70.00	71.80
C COST OF DRIVE UNIT	71.90
CSTDRUN=170.00	72.00
C COST OF CORNER WHEEL	72.10
CSTCMHL=60.00	72.20
C HORSEPOWER OF SCRAPER MOTOR	72.30
HPMOSCR=2.0	72.40
C COST OF KWH OF ELECTRICITY (DOLLARS)	72.50
HKWCOST=0.05	72.60
C MOTOR COSTS PLUS REVERSING SWITCH	72.70
COSTMOT=350.00	72.80
C NUMBER OF CORNER WHEELS PER UNIT	72.90

C CORNNO=4.0	7300
C NO. OF MEN REQD TO OPERATE SCRAPERS	7310
ALMENNO=1.0	7320
C NO. OF SCRAPER BLADES	7330
SCRPENO=2.0	7340
C NO. OF HOURS SPENT BY PERSONS RUNNING SCRAPER FOR/ROUTINE UPKEEP PER WK	7350
SCOPHRS=0.33	7360
C SCRAPER BLADE COST	7370
SCRBCST=240.00	7380
C VOLTAGE OF SCRAPER MOTOR	7390
VLTSCRH=230	7400
C WIDTH BETWEEN TWO ALLEYS ON SAME SCRAPER	7410
WIDHIDD=16.0	7420
C ALLEY SCRAPER DEP RATE	7430
ALDEPR=0.143	7440
C ALLEY SCRAPER INTEREST RATE	7450
ALINTR=0.06	7460
C ALLEY SCRAPER RHI RATE	7470
ALRHIR=0.04	7480
C ALLEY SCRAPER MISC RATE	7490
ALMISCR=0.02	7500
C CALCULATED VALUES FOR ALLEYSRAPERS	7510
C ALLEY SCRAPER DIRT	7520
ALDIRTH=(ALDEPR+ALINTR+ALRHIR+ALMISCR)	7530
C TOTAL ALLEY SCRAPER CHAIN	7540
ALCHAIN=(12*WIDHIDD)+(2*ALLNTH)+20	7550
C TOTAL CHAIN NEEDED	7560
TOTCHN=(ALLEYNO/2)*ALCHAIN	7570
C TOTAL COST OF CHAIN	7580
TOTCHNC=(CHNCSTF*TOTCHN)	7590
C NUMBER OF DRIVE UNITS	7600
DRIVUNT=(ALLEYNO/2)	7610
C TOTAL COST OF DRIVE UNITS	7620
TOTDRUNC=(DRIVUNT*CSDRUN)	7630
C NO OF SCRAPER MOTORS	7640
ALNMOTR=(ALLEYNO/2)	7650
C TOTAL COST OF MOTORS	7660
TOTMOCST=(ALNMOTR*CSMOT)	7670
C TOTAL COST OF SCRAPER BLADES	7680
TOTSCCS=(SCRPENO*SCRBCST)*(ALLEYNO/2)	7690
C TOTAL NUMBER OF CORNER WHEELS	7700
TOTAHWS=(CORNNO*(ALLEYNO/2))	7710
C TOTAL COSTS OF WHEELS	7720
TOTWCST=(TOTAHWS*CSHCWL)	7730
C TOTAL ALLEY SCRAPER COSTS	7740
TOTALCST=(TOMOCST+TOTDRUNC+TOTWCST+TOTSCCS+TOTCHNC)	7750
C NO OF CLOCKS	7760
CLOCKNO=(ALLEYNO/2)	7770
C TOTAL COST OF CLOCKS	7780
TOTCLCST=(CLOCKNO*CCLOCKNO)	7790
C TOTAL COSTS OF SCRAPERS AND CLOCKS	7800
TOTCLLC=(TOTCLCST+TOTALCST)	7810
C TOTAL ANNUAL OWNERSHIP COSTS	7820
DIRTHAL=TOTCLLC*ALDIRTH	7830
C WEEKLY MANHRS OF LABOR	7840
WKYMHR=SCOPHRS*ALMENNO	7850
C WEEKLY LABOR COSTS	7860
WKYLCST=CSLABOR*WKYMHR	7870
C ALLEY SCRAPER MHRS/YR	7880
ALYMHRS=WKYMHR*52	7890
C YEARLY LABOR COSTS	7900
YRLCST=WKYLCST*52	7910
C DAILY ELECTRICITY USED/MOTOR	7920
HKMDAY=(VLTSCRH*AMPSCRH*ALLMHR)/1000	7930
C TOTAL DAILY KWH	7940
THKMDAY=(HKMDAY*ALNMOTR)	7950
C YEARLY KWS USED	7960
HKMYRLY=(THKMDAY*365)	7970
C YEARLY ELECTRICITY COSTS	7980
KMCSTYR=(HKMYRLY*CKMCSTYR)	7990
C TOTAL ANNUAL COSTS OF OWNING ELECTRICITY AND LABOR	8000
ALANCS=(DIRTHAL+KMCSTYR+YRLCST)	8010
C-INITIALIZATION OF DEFAULT VALUES FOR GARDEN TRACTOR	8020
C GARDEN TRACTOR HOURLY FUEL CONSUMPTION (GAL/HR)	8030
GDFUEL=1.4	8040
C GARDEN TRACTOR DAILY USE(ONE ALLEY 2X DAILY)	8050
GDMDAY=0.33	8060
C GARDEN TRACTOR COST INCLUDING BLADE	8070
GDMTCST=2500.00	8080
C DEPRECIATION RATE FOR GDN TRACTOR	8090
GDMDEP=0.014	8100

C INTEREST RATE ON CONTRACTOR	8110
CONTINT=0.06	8120
C MISCELLANEOUS FACTORS FOR GARDEN TRACTORS	8130
GONTMIS=0.02	8140
C RHI FACTOR FOR GARDEN TRACTORS	8150
GONTRHI=0.67	8160
C SALVAGE VALUE OF 2 YR OLD GARDEN TRACTOR	8170
GONTVAL=0.00	8180
C CALCULATED VALUES FOR GARDEN TRACTORS	8190
C HRS GARDEN TRACTOR USED / DAY FOR SCRAPING	8200
GOTHOSC=GONHDAY*ALLEYNO	8210
C HOURS PER YEAR FOR GARDEN TRACTOR	8220
GONHYP=(GOTHOSC*365)	8230
C ANNUAL OWNERSHIP % FOR GARDEN TRACTOR	8240
GONDRHT=GONTJEP+GONTINT+GONTRHI+GONTMIS	8250
C FUEL USED PER YEAR	8260
GONFLYR=(GONHYP*GONFUEL)	8270
C FUEL COSTS FOR YEAR	8280
GONFCYR=(FUELCST*GONFLYR)	8290
C YEARLY LABOR COSTS FOR RUNNING GARDEN TRACTOR	8300
GONLCYR=CSLABOR*GONHYP	8310
C TOTAL OWNERSHIP COSTS FOR GARDEN TRACTOR	8320
GONOCST=GONTCST+GONDRHT	8330
C TOTAL OWNERSHIP AND OPERATING COSTS	8340
GONOCOS=(GONOCST+GONLCYR+GONFCYR)	8350
C INITIALIZATION OF FLUSH SYSTEM VARIABLES	8360
C DEPRECIATION ON FLUSH EQUIPMENT (RATE)	8370
FLDEPP=0.065	8380
C DAYS OF YEAR FLUSH SYSTEM USED AS FLUSH SYSTEM	8390
FLDY305=305	8400
C FUEL USED BY TRACTOR WHEN SCRAPING (GAL/MR)	8410
FLFUEL=3.0	8420
C GALLONS OF WATER USED DAILY FOR FLUSHING PER COM	8430
FLMGOWH=100	8440
C COST OF ONE FLUSH GATE	8450
FLGATEC=750.00	8460
C NUMBER OF FLUSH GATES	8470
FLGATEN=ALLEYNO	8480
C FLUSH EQUIPMENT INTEREST PERCENTAGE	8490
FLINTP=.08	8500
C LABOR PER DAY TO FLUSH SYSTEM (HRS)	8510
FLLDY=0.25	8520
C PUMP MOTOR AMPERAGE	8530
FLMOAMP=50	8540
C FLUSH MOTOR HP FOR PUMP	8550
FLMOTHP=15.0	8560
C FLUSH MOTOR VOLTAGE	8570
FLMOLT=220	8580
C PUMP CAPACITY (GAL/MIN)	8590
FLP4PCP=250	8600
C TIMES PER DAY ALLEYS FLUSHED	8610
FLTIMDY=2.0	8620
C FLUSH PUMP COST	8630
FLPUMPC=800.00	8640
C NO OF PUMPS USED	8650
FLPUMPN=1	8660
C APPROXIMATE COST OF WELL	8670
FLWELC=8000	8680
C WELL DEPTH	8690
FLWOPR=.05	8700
C WELL INT RATE	8710
FLWINTR=.05	8720
C INTEREST RATE ON WELL	8730
FLWINNS=.01	8740
C RHI PERCENTAGE FOR FLUSH EQUIPMENT	8750
FLRMTD=0.065	8760
C NO OF FLUSH TANKS	8770
FLTNKNO=2	8780
C TANK COST PER GALLON STORAGE CAPACITY	8790
FLTNCGL=0.13	8800
C PERCENT OF TOTAL TRACTOR TIME USED FOR SCRAPING	8810
FLTUPER=0.15	8820
C DAILY LABOR FOR WINTER SCRAPING 1 ALLEY, 2X DAILY	8830
FLWSHR=0.33	8840
C WEEKLY LABOR FOR SCRAPING DURING NON-WINTER SEASON	8850
FLWKLBR=1.0	8860
C MISCELLANEOUS PERCENTAGE ON FLUSH EQUIP	8870
FLPMISC=0.02	8880
C VALUE OF UTILITY TRACTOR+BLADE USED WITH FLUSH SYSTEM	8890
FLTUVAL=1200	8900
C FLUSH TRACTOR DEP RATE	8910

FLTJPER=0.065	89.20
C FLUSH TRACTOR INT RATE	89.30
FLTIMR=0.16	89.40
C FLUSH TRACTOR RMI RATE	89.50
FLTRMIS=0.045	89.60
C FLUSH TRACTOR MISC RATE	89.70
FLTMISC=0.12	89.80
C CALCULATIONS FOR FLUSH SYSTEMS	89.90
C FLUSH TRACTOR TOTAL DIRT RATE	90.00
FLTDTR=(FLTDPP+FLTIMR+FLTRMIR+FLTMISR)	90.10
C FLUSH DAILY LABOR FOR 305 DAYS OF FLUSHING	90.20
FLT305=(FLTBPDY*305)	90.30
C FLUSH DAILY LABOR COSTS FOR 305 DAY PERIOD (OPERATING THE FLUSH UNIT)	90.40
FLLC305=(FLT305*CSLABOR)	90.50
C FLUSH SYSTEM 4 WEEK LABOR FOR SCRAPING	90.60
FLLC4WK=(FLLC305*4)	90.70
C FLUSH LABOR COSTS FOR SCRAPING FOR 4WK	90.80
FLLCSCR=(FLLC4WK*CSLABOR)	90.90
C 60 DAY LABOR FOR WINTER SCRAPING	91.00
FLWSC60=FLWSC*ALLEYNO*60	91.10
C COST FOR LABOR FOR WINTER SCRAPING	91.20
FLWSCST=FLWSC60*CSLABOR	91.30
C TOTAL YEARLY FLUSH LABOR	91.40
FLLABTO=(FLT305+FLLC4WK+FLWSC60)	91.50
C FLUSH TRACTOR OWN COSTS DUE TO SCRAPING	91.60
FLTUOWN=(FLTRFXC*FLLABTO)	91.70
C TOTAL YEARLY LABOR FOR FLUSH SYSTEM(COSTS)	91.80
FLLABTC=(FLWSCST+FLLCSCR+FLLC305)	91.90
C TOTAL FLUSH WATER USED DAILY	92.00
FLTWDAY=CWS*FLWGDCW	92.10
C FLUSH TANK CAPACITY	92.20
FLTNKCP=((CWS/ALLEYNO)*FLWGDCW)/FLTIMOV)	92.30
C HOURS FLUSH PUMPS RUN/DAY	92.40
FLPMPHR=(FLTWDAY/(FLPMPCP*60))	92.50
C DAILY KM USED BY MOTORS ON FLUSH TANK PUMPS	92.60
FLMOYKM=((FLMOVLT*FLMOAMP*FLPMPHR)/1000)*FLPMPN	92.70
C KM USED TO PUMP WATER FOR 305 DAYS	92.80
FLKM305=(FLMOYKM*305)	92.90
FLYRKWC=FLKM305*HKWCST	93.00
C TOTAL FUEL USED BY TRACTOR FOR SCRAPING	93.10
FLTOTFL=((FLLC4WK*(60*FLWSHR))*FLFUELUI)	93.20
C TOTAL FUEL COSTS FOR FLUSH SYSTEM	93.30
FLFLCST=(FLTOTFL*FUEDSLC)	93.40
C TOTAL COST OF FLUSH GATES	93.50
FLGATC=(FLGATEN*FLGATEC)	93.60
C FLUSH TANK TOTAL COST	93.70
FLTNKTC=FLTNKGL+FLTNKCP+FLTNKNO	93.80
C TOTAL COSTS OF FLUSH PUMPS	93.90
FLPMPCS=(FLCUPN*FLPMPHPC)	94.00
C WELL DIRT RATE	94.10
FLWDTR=FLWDPP+FLWINTR+FLWINMS	94.20
C ANNUAL OWNERSHIP COSTS ON WELL	94.30
FLWOWNC=FLWLCST+FLWDTR	94.40
C FLUSH TANK GATES AND MOTOR COSTS	94.50
FLTGHC=(FLTNKTC+FLGATC+FLPMPCS+FLWELCS)	94.60
C FLUSH EQUIPMENT TOTAL OWN PERCENTAGE	94.70
FLTJUPHNT=FLDEP+FLINTP+FLRMIP+FLMISC	94.80
C TOTAL FLOWCSTSHIP COSTS OF FLUSH SYSTEM	94.90
FLWCST=FLTJUPHNT*FLTGHC+FLWOWNC	95.00
C FLUSH YEARLY ENERGY COSTS	95.10
FLYENCA=FLYRKWC+FLFLCST	95.20
C YRLY OWNERSHIP COSTS FOR TRACTOR+FLUSH EQUIPMENT	95.30
FLTOWNC=(FLTUOWN+FLWCST)	95.40
C YRLY OWN AND OPERATING COSTS FOR FLUSH SYSTEM	95.50
FLTOOPC=FLTOWNC+FLFLCST+FLYRKWC+FLLABTO	95.60
C CC DAILY LABOR	95.70
CCDYLB=0.50	95.80
C CC DEPR RATE	95.90
CCDEPR=0.143	96.00
C CC INT RATE	96.10
CCINTR=0.06	96.20
C CC MOTOR AMPERAGE	96.30
CCMAPO=12	96.40
C CCMOTOR HRS/DAY	96.50
CCMHWD=0.50	96.60
C CC MISC RATE	96.70
CCMSCR=0.02	96.80
C CC MOTOR VOLTAGE	96.90
CCMVLT=230	97.00
C CC RMI RATE	97.10
CCRMIR=0.06	97.20

C CC COST/FOOT OF CHAIN	97.30
C CC CRCCPCF=7.25	97.40
C CC NUMBER OF CORNER WHEELS	97.50
C CC CRCCRNW=1.0	97.60
C CC COST OF CORNER WHEELS	97.70
C CC CRCCRNC=80.00	97.80
C CC DRU COST	97.90
C CC CRCDRUC=1750.00	98.00
C CC NUMBER DRUS	98.10
C CC CRCDRUS=1.0	98.20
C CC MOTOR HP	98.30
C CC CRCHMP=2.0	98.40
C CC MOTOR COST	98.50
C CC CRCHMST=250.00	98.60
C CC NUMBER OF MOTORS	98.70
C CC CRCHMOT=1.0	98.80
C CC CLOCK COST	98.90
C CC CRCTCCS=75.00	99.00
C CC CLOCK MECHS	99.10
C CC CRCCMEC=1.0	99.20
C CC SALV	99.30
C CC CRCSALV=0.00	99.40
C CALCULATED VALUES FOR CC ONLY	99.50
C CC YRLY LABOR	99.60
C CC CRCLBY=CRCDYLE*365	99.70
C CC YRLY LABOR COSTS	99.80
C CC CRCYRLC=(CRCLBY*CSLABOR)	99.90
C CC MOTOR DAILY KM USED	100.00
C CC CRCHKMD=(CRCHVLT*CRCHAMP*CRCHMRD)/1000*CRCHMOT	100.10
C CC YRLY KM USED	100.20
C CC CRCHKMY=(CRCHKMD*365)	100.30
C CC YRLY ELEC COSTS	100.40
C CC CRCELCY=(CRCHKMY*HKMGOST)	100.50
C CC YRLY OP COSTS	100.60
C CC CRCYOPC=(CRCYRLC+CRCELCY)	100.70
C BARN WIDTH	100.80
C CC BARNWD=(ALLEYNO*21.5)+(ALLEYNO-2)*0.5	100.90
C CC CHAIN LENGTH	101.00
C CC CRCCHNL=(2*BARNWD)	101.10
C CC CHAIN COST	101.20
C CC CRCCHNC=(CRCCHNL*CRCCPCF)	101.30
C CORNER WHEEL COST FOR CC	101.40
C CC CRCCNTC=(CRCCRNW*CRCCRNC)	101.50
C CC DRIVE WHEEL COST	101.60
C CC CRCTDUC=(CRCDRUC*CRCDRUS)	101.70
C CC MOTOR COSTS	101.80
C CC CRCHMCT=(CRCHMST*CRCHMOT)	101.90
C CC CLOCK COSTS	102.00
C CC CRCTCTC=(CRCTCCS*CRCCMEC)	102.10
C CC TOTAL COST	102.20
C CC CRCTCTC+CRCHMCT+CRCTDUC+CRCCNTC+CRCCHNC	102.30
C CC TOTAL DIRT	102.40
C CC CRCTDRH=(CRCTINTR+CRCTDEPR+CRCHMSCR+CRCHMIR)	102.50
C CCYRLY OWN COSTS	102.60
C CC CRCTCST=(CRCTDRH*CRCTCST)	102.70
C CC YRLY OP+OWN COSTS	102.80
C CC CRCCOCS=(CRCCOCS+CRCYOPC)	102.90
C CROSS CONVEYOR DEFAULT VARIABLES	103.00
C WEEKLY LABOR REQD FOR CROSSCONVEYOR	103.10
C CC DAYL3=0.68	103.20
C DEPR RATE	103.30
C CC DEPR=3.143	103.40
C INT RATE	103.50
C CC INTR=0.06	103.60
C AMPE AGE OF MOTOR	103.70
C CC CHAMP=12	103.80
C HRS/DAY MOTORS RUN	103.90
C CC CHMRDY=0.50	104.00
C MISC RATE FOR CONVEYOR	104.10
C CC CHMSCR=0.02	104.20
C MOTOR VOLTAGE	104.30
C CC MVOLT=230	104.40
C PHIRATE	104.50
C CC PHIR=0.06	104.60
C CONVEYOR CHAIN AND PADDLES COST/FT	104.70
C CC CONCSFT=7.25	104.80
C NUMBER OF CORNER WHEEL ASSEMBLIES	104.90
C CC CORNWH=1.0	105.00
C COST/CORNER WHEEL	105.10
C CC CORNWHC=80.00	105.20
C DRIVE UNIT COSTS/UNIT	105.30



C NUMBER OF DRIVE UNITS	10550
C COST/FOOT OF ELEVATOR	10550
C ELEVATOR LENGTH INCLUDING DISTANCE TO DRIVE WHEEL	10550
C NUMBER OF ELEVATORS	10550
C CONVEYOR MOTOR HP	10550
C COST/MOTOR	10550
C NUMBER OF MOTORS	10550
C COST PER TIME CLOCK MECHANISM	10550
C NUMBER OF CLOCK MECHANISMS	10550
C SALVAGE VALUE OF COMPLETE UNIT	10550
C CALCULATED VALUES FOR CROSS CONVEYOR UNIT	10550
C CC TOTAL DIRT PERCENTAGE	10550
C CROSS CONVEYOR ANNUAL LABOR	10550
C LABOR COSTS/DAY TO OPERATE	10550
C LABOR COST/YR ON SYSTEM	10550
C KWH USED/DAY BY MOTOR	10550
C KWH USED/YEAR	10550
C ELECTRICITY COSTS/YR TO RUN THE CROSS CONVEYOR	10550
C YEARLY OPERATING COSTS	10550
C TOTAL CHAIN LENGTH	10550
C TOTAL COST OF CONVEYOR SYSTEM	10550
C TOTAL COST OF CORNER WHEELS	10550
C DRIVE UNITS TOTAL COST	10550
C MOTOR COST	10550
C COST PER TIME CLOCK UNITS	10550
C TOTAL COST OF ELEVATOR	10550
C TOTAL COST OF COMPLETE CROSS CONVEYOR	10550
C TOTAL COST OF CLOCKS AND CONVEYOR UNITS	10550
C OWN COSTS WITH CC AND SHORT ELEV	10550
C TOTAL COSTS OF OWNING AND OPERATING	10550
C CROSS CONVEYOR LONG ELEV DEFAULT VARIABLES	10550
C CC LONG ELEV DAILY LABOR	10550
C CC LONG ELEV DEP RATE	10550
C CC LONG ELEV INTR RATE	10550
C CC LONG ELEV MOTOR AMPS	10550
C CC LONG ELEV MOTOR HRS/DAY	10550
C CC LONG ELEV MISC RATE	10550
C CC LONG ELEV MOTOR VOLTAGE	10550
C CC LONG ELEV RMI RATE	10550
C CC LONG ELEV COST/FOOT OF CHAIN AND PADDLES	10550
C CC LONG ELEV NUMBER OF CORNER WHEELS	10550

C CC LONG ELEV COST/CORNER WHEEL	11350
CLORNMC=80.30	11360
C CC LONG ELEV DRIVE UNIT COST/UNIT	11370
CLDRUCS=1750.00	11380
C CC LONG ELEV NO OF DRIVE UNITS	11390
CLDRUNS=1.0	11400
C CC LONG ELEV COST/FOOT	11410
CLELVCS=30.0	11420
C CCLONG ELEV LENGTH	11430
CLEVLN=5.0	11440
C CC LONG ELEV NJS	11450
CLELVNS=1.0	11460
C CC LONG MOTOR HP	11470
CLMOTHP=2.0	11480
C CC LONG MOTOR COSTS	11490
CLMOTCS=250.00	11500
C CC LONG MOTORS(NO)	11510
CLNMOT=1.0	11520
C CC LONG COST/TIME CLOCK	11530
CLTCCST=70.00	11540
C CC LONG NUMBER OF CLOCK TECH	11550
CLTCHCH=1.0	11560
C CC LONG SALV VALUE	11570
CLTUSLV=0.00	11580
C CC LONG ELEV CALCULATED COSTS	11590
C LABOR COST DAY WITH LONG ELEV	11600
CCLDAYL=CCDAYL*365	11610
C DAILY LABOR COSTS FOR CC+LONG ELEVATOR	11620
CCLBCD=(CCLDAYL+CCLSLABOR)	11630
C CC LONG LABOR COST/YR	11640
CCLYLAB=(CCLBCD*365)	11650
C CC LONG MOTOR KW/DAY	11660
CCLMKWD=((CCLVLT*CCLHAMP*CCLMHQY)/1000)*CLNMOT	11670
C CC LONG KWH/YR	11680
CCLMKWY=(CCLMKWD*365)	11690
C CC LONG YRLY ELEC COST	11700
CCLLECY=(CCLMKWY*MKWCOST)	11710
C CC LONG YRLY OP EXPENSES	11720
CCLYOPC=(CCLYLAB+CCLLECY)	11730
C CC LONG CHAIN LNH	11740
CCLCHLN=2*BARNWD+2*ELVNS+CLEVLN	11750
C CC LONG TOTAL COST	11760
CCLNVCS=(CCLCHCF+CCLCHLN)	11770
C CCLONG TOTAL COST OF CORNER WHEELS	11780
CCLCRNC=(CLORNMC*CLORNWH)	11790
C CC LONG TOTAL DRIVE UNIT COST	11800
CCLJRTC=CLDRUNS*CLDRUCS	11810
C CC LONG MOTOR COSTS	11820
CCLMCST=(CLMOTCS*CLNMOT)	11830
C CC LONG TIME CLOCKS	11840
CCLTCCS=(CLTCCST*CLTCHCH)	11850
C CC LONG ELEV TOTAL COSTS	11860
CCLTELC=CLELVCS*CLEVLN*CLELVNS	11870
C CC LONG TOTAL COSTS	11880
CCLTCST=CCLMCST+CCLJRTC+CCLNVCS+CCLTELC+CCLCRNC	11890
C CC LONG CLOCK AND CONVEYOR COSTS	11900
CCLCLCC=CCLTCST+CCLTCCS	11910
C CCLONG TOTAL CHRT	11920
CCLDRHT=(CCLDEPR+CCLINTR+CCLMSGR+CCLRMIR)	11930
C CC LONG TOTAL OWN COSTS	11940
CCLOWNC=(CCLDRHT+CCLTCST)	11950
C CC LONG YRLY OWN AND OP COSTS	11960
CCLTOOC=(CCLOWNC+CCLYOPC)	11970
C SLOTTED FLOOR DEFAULT VARIABLES	11980
C DAILY LABOR WITH SLOTTED FLOOR	11990
SFDAYLB=0.00	12000
C SLOTTED FLOOR DEPRECIATION RATE	12010
SFDEPR=0.05	12020
C SLOTTED FLOOR INTEREST RATE	12030
SFINTR=0.05	12040
C SLOTTED FLOOR MISC RATE	12050
SFMISC=0.01	12060
C SLOTTED FLOOR RHI RATE	12070
SFRHIR=0.035	12080
C SLOTTED FLOOR SALVAGE VALUE	12090
SFSALV=0.00	12100
C CALCULATED VALUES FOR SLOTTED FLOOR	12110
C SLOTTED FLOOR DAILY LABOR COST	12120
SFDLCST=(CCLSLABOR*SFDAYLB)	12130
C SLOTTED FLOOR YEARLY LABOR COSTS	12140
SFYRCST=(SFDLCST*365)	12150

C SLOTTED FLOOR AVE VALUE	121.50
C SLOTTED FLOOR AVE SALV	121.50
C SLOTTED FLOOR DEPR	121.50
C SLOTTED FLOOR YEARLY TOTAL COSTS	121.50
C PISTON PUMP DEFAULT VARIABLES	121.50
C NUMBER OF CHECK VALUES IN SYSTEM	121.50
C COST/CHECK VALUE	121.50
C COST/ELBOW	121.50
C NUMBER OF ELBOWS USED	121.50
C PISTON PUMP COST	121.50
C PISTON PUMP DEP RATE	121.50
C PISTON PUMP INTEREST RATE	121.50
C DAILY LABOR WITH PISTON PUMP	121.50
C AMPS FOR PISTON PUMP MOTOR	121.50
C PISTON PUMP HRS OPERATED/DAY	121.50
C PISTON PUMP MISC RATE	121.50
C PISTON PUMP MOTOR COST	121.50
C PISTON PUMP MOTOR HP	121.50
C PISTON PUMP MOTOR VOLTAGE	121.50
C PISTON PUMP RHT RATE	121.50
C PVC COST PER FOOT	121.50
C NUMBER OF FEET OF PVC PIPE	121.50
C SALVAGE VALUE OF SYSTEM	121.50
C CALCULATED VALUES FOR PISTON PUMP	121.50
C PISTON PUMP YEARLY LABOR	121.50
C PISTON PUMP TOTAL ANNUAL COSTS FOR LABOR	121.50
C KWHRS USED PER DAY WITH PISTON PUMP	121.50
C PISTON PUMP ANNUAL KWHR ELECTRICITY	121.50
C ELECTRICITY COSTS FOR PISTON PUMP/DAY	121.50
C TOTAL PVC PIPE COSTS	121.50
C COST OF CHECK VALUES	121.50
C TOTAL COSTS OF ELBOWS	121.50
C PISTON PUMP YEARLY ELECTRIC COSTS	121.50
C TOTAL COST OF PISTON PUMP SYSTEM	121.50
C PP TOTAL DIRH RATE	121.50
C PP ANNUAL OWN COSTS	121.50
C PP ANNUAL OP COSTS	121.50
C TOTAL ANNUAL COSTS FOR PISTON PUMP SYSTEM	121.50
CCC +RAM PUMP	121.50
C CCR DRHT	121.50
C CCR YRLY LABOR	121.50
C CCR TOTAL COST	121.50
C CCR ANNUAL OWNERSHIP COSTS	121.50
C CCR OWNNG	121.50

C CCR YRLY LABOR	12970
C CCR BCY=CCRLBTY*CSLABOR	12980
C CCR YRLY KWH	12990
C CCR YRLY KWH=(CRCMKWY+PPMKWY)	12990
C CCR YRLY ELEC COST	13000
C CCR YRLY ELC=(CCRYHKW*MKMCOST)	13010
C CCR YRLY OP COSTS	13020
C CCR YRLY OP=(CCRLBCY+C2BYELC)	13030
C CCR YRLY OP AND OWN COST	13040
C CCR YRLY OP AND OWN COST	13050
C CCR YRLY OP AND OWN COST	13060
C CCR YRLY OP AND OWN COST	13070
C CCR YRLY OP AND OWN COST	13080
C CCR YRLY OP AND OWN COST	13090
C CCR YRLY OP AND OWN COST	13100
C CCR YRLY OP AND OWN COST	13110
C CCR YRLY OP AND OWN COST	13120
C CCR YRLY OP AND OWN COST	13130
C CCR YRLY OP AND OWN COST	13140
C CCR YRLY OP AND OWN COST	13150
C CCR YRLY OP AND OWN COST	13160
C CCR YRLY OP AND OWN COST	13170
C CCR YRLY OP AND OWN COST	13180
C CCR YRLY OP AND OWN COST	13190
C CCR YRLY OP AND OWN COST	13200
C CCR YRLY OP AND OWN COST	13210
C CCR YRLY OP AND OWN COST	13220
C CCR YRLY OP AND OWN COST	13230
C CCR YRLY OP AND OWN COST	13240
C CCR YRLY OP AND OWN COST	13250
C CCR YRLY OP AND OWN COST	13260
C CCR YRLY OP AND OWN COST	13270
C CCR YRLY OP AND OWN COST	13280
C CCR YRLY OP AND OWN COST	13290
C CCR YRLY OP AND OWN COST	13300
C CCR YRLY OP AND OWN COST	13310
C CCR YRLY OP AND OWN COST	13320
C CCR YRLY OP AND OWN COST	13330
C CCR YRLY OP AND OWN COST	13340
C CCR YRLY OP AND OWN COST	13350
C CCR YRLY OP AND OWN COST	13360
C CCR YRLY OP AND OWN COST	13370
C CCR YRLY OP AND OWN COST	13380
C CCR YRLY OP AND OWN COST	13390
C CCR YRLY OP AND OWN COST	13400
C CCR YRLY OP AND OWN COST	13410
C CCR YRLY OP AND OWN COST	13420
C CCR YRLY OP AND OWN COST	13430
C CCR YRLY OP AND OWN COST	13440
C CCR YRLY OP AND OWN COST	13450
C CCR YRLY OP AND OWN COST	13460
C CCR YRLY OP AND OWN COST	13470
C CCR YRLY OP AND OWN COST	13480
C CCR YRLY OP AND OWN COST	13490
C CCR YRLY OP AND OWN COST	13500
C CCR YRLY OP AND OWN COST	13510
C CCR YRLY OP AND OWN COST	13520
C CCR YRLY OP AND OWN COST	13530
C CCR YRLY OP AND OWN COST	13540
C CCR YRLY OP AND OWN COST	13550
C CCR YRLY OP AND OWN COST	13560
C CCR YRLY OP AND OWN COST	13570
C CCR YRLY OP AND OWN COST	13580
C CCR YRLY OP AND OWN COST	13590
C CCR YRLY OP AND OWN COST	13600
C CCR YRLY OP AND OWN COST	13610
C CCR YRLY OP AND OWN COST	13620
C CCR YRLY OP AND OWN COST	13630
C CCR YRLY OP AND OWN COST	13640
C CCR YRLY OP AND OWN COST	13650
C CCR YRLY OP AND OWN COST	13660
C CCR YRLY OP AND OWN COST	13670
C CCR YRLY OP AND OWN COST	13680
C CCR YRLY OP AND OWN COST	13690
C CCR YRLY OP AND OWN COST	13700
C CCR YRLY OP AND OWN COST	13710
C CCR YRLY OP AND OWN COST	13720
C CCR YRLY OP AND OWN COST	13730
C CCR YRLY OP AND OWN COST	13740
C CCR YRLY OP AND OWN COST	13750
C CCR YRLY OP AND OWN COST	13760
C CCR YRLY OP AND OWN COST	13770

```

C PAMP INTEREST RATE
C PAMP CRMPINR=0.05
C PAMP CRHIRT=0.035
C PAMP TOTAL DIRHRT RATE
C PAMP CRDRHTR=CRHIRT+CRMPINR+CRMPDPR
C PAMP YEARLY OWNERSHIP COSTS
C PAMP CRYOWNC=CRDRHTR+CRHPCST
C CCA R RATE
C CCA DR RATE
C CCA DRMT=CFCTDRH
C CCA YRLY TOTAL LABOR
C CCA CCAALBTY=CAVALTO
C CCA TCTAL COSTS
C CCA CCAHTC=CFCTCST+CAASYSCS)
C CCA CCAOWNC=CAOWNCY+CRCCOST
C CCA YRLY LABOR COSTS
C CCA CCAALBTY=CCALBTY+CSLABOR
C CCA YRLY KWH COSTS
C CCA CCAHKW=(CRCHKWY+CAHKWY)
C CCA YRLY ELEC COSTS
C CCA CCAVELC=CRCHKWY+CAHKWY+CAHKWCOST)
C CCA YRLY OP COSTS
C CCA CCAOPCY=CCALBCTY+CCAYELC
C CCA YRLY OP OWN COSTS
C CCA CCAOCY=(CCALBCTY+CCAYELC)
C CEMENT FLUME (4*2.5)
C LENGTH OF FLUME
C CFLNTH=140
C COST/FOOT OF FLUME LENGTH
C CFLCFT=11.35
C TOTAL FLUME COST
C CFLTCT=CFLLNTH+CFLCFT
C ANNUAL DIRT RATE
C CFLDR=3.125
C ANNUAL OWN COSTS ON FLUME
C CFLOWNC=CFLDR+CFLTCT
C ANNUAL OWN + OPERATING COSTS
C CFLOWPC=CFLOWNC
C DEFAULT VALUES FOR COVERED TANK
C COST/CUFT
C CTCUFT=1.00
C DEP RATE ON CEMENT TANK
C CTDEPR=0.05
C INTEREST RATE ON CEMENT TANK
C CTINTR=0.05
C MISC ON CEMENT TANK
C CTMISCR=0.00
C RHI FACTOR RATE ON TANK
C CTRHTR=0.025
C SALVAGE VALUE OF TANK
C CTSALV=0.00
C USEABLE VOLUME OF TANK (PERCENT)
C CTUSVOL=0.85
C VOLUME REQ/DAY/COM (CUFT)
C CTVOLDC=2.80
C DAYS STORAGE REQD
C CTVOLDY=180
C CALCULATED VALUES FOR CEMENT TANK
C CUBIC FT OF TANK NEEDED
C CTCFNEO=(CTVOLDC-COWS*CTVOLDY)
C TOTAL COST TO BUILD A CEMENT TANK
C CTCOST=(CTCFNEO+CTCUFFT)
C CEMENT TANK TOTAL DIRT RATE
C CTDRHTR=(CTDEPR+CTINTR+CTRHTR+CTMISCR)
C CEMENT TANK OWN COSTS
C CTOWNCS=(CTDRHTR+CTCOST)
C DEFAULT VARIABLES FOR PIT UNDER SLATS
C COST/CUFT OF PIT STORAGE
C PITCFT=1.00
C DEP RATE ON PIT
C PITDEPR=0.05
C INTEREST RATE ON PIT
C PITINTR=0.05
C PIT MISC RATE
C PITMISCR=0.00
C PIT RHI RATE=0.025
C PITRHT=0.025
C PIT SALVAGE VALUE
C PITSALV=0.00

```

```

13780
13790
13800
13810
13820
13830
13840
13850
13860
13870
13880
13890
13900
13910
13920
13930
13940
13950
13960
13970
13980
13990
14000
14010
14020
14030
14040
14050
14060
14070
14080
14090
14100
14110
14120
14130
14140
14150
14160
14170
14180
14190
14200
14210
14220
14230
14240
14250
14260
14270
14280
14290
14300
14310
14320
14330
14340
14350
14360
14370
14380
14390
14400
14410
14420
14430
14440
14450
14460
14470
14480
14490
14500
14510
14520
14530
14540
14550
14560
14570
14580

```

```

C USEABLE PIT VOLUME (PERCENT)
PITUSVL=0.85
C VOL REQD/COM/DAY
PITVLOC=2.8C
C DAYS STORAGE REQD
PITVLCY=18C
C PIT CALCULATED VALUES
C CUBIC FEET OF PIT NEEDED
PITCFT=(COMS*PITVLOC*PITVLDY)
C TOTAL PIT COST
PITCST=(PITCFT*PITCOST)
C PIT TOTAL ORHT RATE
PITDRHT=PITDEPR*PITINTR+PITRHR+PITMSGR
C PIT YLY OWN COSTS
PITOWNC=PITDRHT*PITCST
C CEMENT SILO
C CS DEP RATE
CSLDEPR=0.05
C CS DIAMETER
CSLDIA=61.3
C CS I RATE
CSLINT=0.05
C CSRHR RATE
CSLRHR=0.025
C CS SALV VALUE
CSLSLV=0.3C
C CSCS SUMP COST
CSLSCC=1000.00
C COST PER CUFT OF STORAGE FOR CEMENT SILOS
CSLCCFT=0.7C
C CUBIC FEET NEEDED PER CIM
CFMCDAY=2.8C
C CS TOTAL COST
CSLTCST=CSLCCFT*COMS*18C*CFMCDAY
C TOTAL CS ORHT RATE
CSLDRHT=(CSLDEPR+CSLINT+CSLRHR)
C CS YLY OWN COSTS
CSLOWNC=(CSLDRHT*CSLTCST)
C COST PER CUFT OF STORAGE FOR STEEL SILOS
SSLCCFT=0.3C
C SS DEP RATE
SSLDEPR=0.05
C SS INTEREST RATE
SSLINTR=0.05
C SS RHR RATE
SSLRHR=0.025
C SS SALVAGE VALUE
SSLSLV=0.00
C SX SUMP COST
SSLSMOC=1000.00
C SS TOTAL COST
SSLTCST=SSLCCFT*COMS*18C*CFMCDAY
C SS DRHT TOTAL
SSLDRHT=SSLDEPR+SSLINTR+SSLRHR
C SS YLY OWN COSTS
SSLOWNC=(SSLDRHT*SSLTCST)
C DEFAULT VARIABLES FOR EARTH BASIN FOR LIQUIDS
C AREA CEMENTED INCLUDING RAMP AND BOTTOM (SQFT)
EBCMA=100C
C THICKNESS OF CEMENT
EBC4THK=0.5C
C COST PER CUBIC YD OF BASIN EXCAVATED
EBCYCCS=1.25
C DEPRECIATION RATE ON BASIN
EBCDEPR=0.065
C INTEREST RATE ON EARTH BASIN
EBINTR=0.06
C MISC RATE ON EARTH BASIN
EBMISC=0.01
C EARTH BASIN RHR RATE
EBRHR=0.01
C CUBIC FEET OF VOLUME IN BASIN
EBVC180=540
IF (15(4).EQ.5) EBVC180=EBVC180*5.5
IF (15(10).NE.0) EBVC180=EBVC180*5.5
C BASIN SALVAGE VALUE
EBSALV=0.00
C CALCULATED VALUES FOR EARTH BASIN FOR LIQUIDS
C VOLUME TO BE EXCAVATED FOR 180 DAY STORAGE
EBVOLCF=COMS*EBVC180
C EXCAVATION COSTS FOR EARTH BASIN

```

```

14590
14600
14610
14620
14630
14640
14650
14660
14670
14680
14690
14700
14710
14720
14730
14740
14750
14760
14770
14780
14790
14800
14810
14820
14830
14840
14850
14860
14870
14880
14890
14900
14910
14920
14930
14940
14950
14960
14970
14980
14990
15000
15010
15020
15030
15040
15050
15060
15070
15080
15090
15100
15110
15120
15130
15140
15150
15160
15170
15180
15190
15200
15210
15220
15230
15240
15250
15260
15270
15280
15290
15300
15310
15320
15330
15340
15350
15360
15370
15380
15390

```



C COST OF EXCAVATING (PER CU YD)	16210
CSBDIGY=1.25	16220
C SLURRY BASIN INTEREST RATE	16230
CSBINTR=0.05	16240
C SLURRY BASIN MISC RATE	16250
CSBMISR=0.01	16260
C PMI RATE FOR SLURRY BASIN	16270
CSBRMR=0.01	16280
C SALVAGE VALUE FOR SLURRY BASIN	16290
CSBSALV=0.00	16300
C CEMENT AREA/CCW FOR 100 DAY STORAGE WITH 8 FT. DEPTH	16310
CSBCMA=74	16320
C VOLUME OF SLURRY BASIN (CU FT)	16330
CSBVOL=40000	16340
C CALCULATED VALUES FOR CEMENTED SLURRY BASIN	16350
C TOTAL CSB CEMENT AREA	16360
CSBTCZM=CSBCMA*COMS	16370
C COST OF CEMENT USED IN SLURRY BASIN	16380
CSBCCST=CSBTCZM*CONCSQ	16390
C TOTAL EXCAVATION COSTS FOR SLURRY BASIN	16400
CSBEXCS=CSBDIGY*(CSBVOL/27)	16410
C TOTAL COST OF SLURRY BASIN	16420
CSBTCST=(CSBEXCS+CSBCCST)	16430
C CSB PMI RATE	16440
CSBDRTR=(CSBDEPR+CSBINTR+CSBMISR+CSBRMR)	16450
C CSB OWN COSTS	16460
CSBOWNC=(CSBDRTR*CSBTCST)	16470
C DEFAULT VARIABLES FOR LIQUID MANURE PUMP	16480
C 60-90 HP TRACTOR -RLY FIXED COSTS	16490
TR90FXC=7.50	16500
C HRS OF AGITATION PRIOR TO EACH DUMPING PERIOD	16510
PLMAGT=20.0	16520
C COST OF LIQUID MANURE PUMP	16530
PLMCST=3500.00	16540
C DEPRECIATION RATE ON LIQUID MANURE PUMP	16550
PLMDEPR=0.143	16560
C GALLONS/HK TO OPERATE TRACTOR	16570
PLMGHR=6.5	16580
C GALLONS/MIN PUMPING CAPACITY	16590
PLMGMIN=2000	16600
C HP USED ON PUMP	16610
PLMHP=50.0	16620
C INTEREST RATE ON PUMP	16630
PLMINTP=0.06	16640
C MISCELLANEOUS RATE ON PUMP	16650
PLMHISR=0.02	16660
C PMI RATE ON PUMP	16670
PLMRMR=0.07	16680
C SALVAGE VALUE ON PUMP	16690
PLMSALV=0.00	16700
C NUMBER OF TIMES STORAGE EMPTIED/YR	16710
EMPTYNO=2.0	16720
C LIQUID MANURE PUMP MEN TO OPERATE	16730
PLMOP=1.0	16740
C CALCULATED VARIABLES FOR LIQUID MANURE PUMP	16750
C YEARLY AGITATION TIME WITH PUMP	16760
PLMAGTY=(PLMAGT*EMPTYNO)	16770
C PLM MANHRS TO AGITATE	16780
PLMAGMH=(PLMAGTY*PLMOP)	16790
C TIME TO PUMP OUT 100% OF VOLUME IN STORAGE UNIT	16800
PPLMTIM=(V.365ST*7.48/PLMGMIN)/60	16810
C PLM HRS TO PUMP	16820
PPLMMH=(PPLMTIM*PLMOP)	16830
C PLM YRLY TOTAL MHRS	16840
PLMYLBR=(PPLMMH+PLMAGMH)	16850
C TOTAL YRLY PUMPING AND AGITATING TIME	16860
PLTYRT=PLMAGTY+PPLMTIM	16870
C YEARLY LABOR COSTS TO RUN THE PUMP	16880
PLMLCST=(PLMYLBR*CSLABOR)	16890
C YEARLY FUEL USED	16900
PLMYFL=(PLMGHR*PLTYRT)	16910
C YEARLY FUEL COSTS	16920
BLMFLCY=(FUEDSL*PLMYFL)	16930
C PLM PMI RATE	16940
PLMDRTR=(PLMDEPR+PLMINTR+PLMHISR+PLMRMR)	16950
C PLM YRLY OWN COSTS	16960
PLMOCTST=(PLMDRTR*PLMCST)	16970
C TRACTOR FIXED COSTS ASSOCIATED WITH PUMPING/YR	16980
PLT90FC=PLTYRT*TR90FXC	16990
C TOTAL YEARLY OWNERSHIP AND OPERATING COSTS FOR LIQUID PUMP	17000
PLMOOCS=(PLMOCTST+PLMLCST+PLMFLCY+PLT90FC)	17010



```

C DEFAULT VALUES FOR IRRIGATION PUMP
C COST OF NEW IRRIGATION PUMP
  PPCST=2600.0
C DEP RATE ON IRRIGATION PUMP
  RPOEPR=0.143
C FUEL/HR TO RUN PUMP
  RPPGHR=4.0
C INTEREST RATE ON IRR PUMP
  RPPINTR=0.06
C MISC RATE ON IRR PUMP
  RPPMISC=0.02
C RMI RATE ON IRR PUMP
  RPPRMI=0.07
C IRRIGATION PUMP SALVAGE VALUE
  PPSALVV=0.60
C PERCENTAGE OF TOTAL USE SPENT WITH WASTE HANDLING
  RPPWHPER=0.25
C PUMPING CAPACITY OF DILUTED MANURE SLURRY (GAL/MIN)
  PMPSLCP=300
C HRS/YR TO OVERSEE PUMP WHEN RUNNING
  PMPYLS=10.0
C CALCULATED VARIABLES FOR IRRIGATION PUMP
C TOTAL VOL TO BE PUMPED YRLY
  RPTVPM=(3*VL365ST)
C TOTAL TIME SPENT YEARLY PUMPING WASTE (HRS)
  RPTPHPT=((17.1+8*(RPTVPM))/PMPSLCP)/60
C YEARLY LABOR COST TO RUN PUMP
  RPLABCS=(PMPYLS*CSLABOR)
C IP YRLY FUEL USE
  RPFUELY=(RPPGHR*RPTPHPT)
C IP YRLY FUEL COSTS
  RPYFCST=(RPFUELY*FUEOSLC)
C IRRIGATION PUMP RMI RATE
  RPDITR=(RPOEPR*RPPINTR+RPPRMI+RPPMISC)
C IP OWN COSTS
  RPOWNCST=(RPDITR*PPCST)
C 50-70 HP TRACTOR FIXED COSTS
  RPTFXC=UTHRFXC*RPTPHPT
C YEARLY OWNERSHIP COSTS DUE TO IRRIGATING SLURRY
  RPYCST=(RPPWHPER*RPOWNCST)
C TOTAL OWNERSHIP AND OPERATING COSTS
  RPTOCCS=(RPYCST+RPLABCS+RPYFCST+RPTFXC)
C DEFAULT VARIABLES FOR FRONT END LOADER
C CAPACITY OF LOADER WHEN USED WITH 50-70HP UTILITY TRACTOR(CUFT/HR)
  FELCAP=2600.0
C FUEL/HR TO RUN LOADER
  FELFHR=3.0
C PERCENT OF TIME LOADER USED FOR WASTE HANDLING AND BEDDING
  FELPERW=0.50
C CALCULATED VARIABLES FOR FEL
C HRS/YR TO RUN LOADER AND HANDLE WASTE
  FELLYR=(V365*SH/FELCAP)
C TRACTOR FIXED COSTS
  FELFXC=FELLYR*UTHRFXC
C TOTAL YEARLY LABOR CHARGES
  FELTLC=(FELLYR*CSLABOR)
C FUEL COST PER HOUR TO RUN LOADER
  FELFSTH=(FELFHR*FUEOSLC)
C FEL YRLY FUEL TO LOAD
  FELYFLU=(FELFHR*FELLYR)
C FEL YRLY FUEL COSTS
  FELYFC=(FELYFLU*FUEOSLC)
C OWNERSHIP COSTS ATTRIBUTED TO WASTE HANDLING
  FELOCH=(FELOCCST*FELPERW)+(FELLYR*UTHRFXC)
C TOTAL OWNING AND OPERATING COSTS FOR FEL
  FELOCCS=(FELOCH+FELYFC+FELTLC+FELFXC)
C USE OF SKIDSTEER LOADER TO LOAD MANURE
C DEFAULT VARIABLES FOR SKI
C LOADING CAPACITY (CUFT/HR) OF SKIDSTEER
  SKLCAPH=3200.0
C PERCENT OF TOTAL TIME SKIDSTEER USED FOR LOADING
  SKLPERL=0.20
C CALCULATED VARIABLES FOR SKIDSTEER LOADER
C HRS PER YR LOADER USED
  SKLHRSY=(V365*SH/SKLCAPH)
C LABOR COSTS/YR FOR LOADING
  SKLBRC=(SKLHRSY*CSLABOR)
C SKIDSTEER YRLY FUEL TO LOAD
  SKLYFLU=(SKLHRSY*GAL/HR)
C SKI YRLY FUEL COSTS
  SKLYFC=(SKLYFLU*FUELCST)

```

```

17020
17030
17040
17050
17060
17070
17080
17090
17100
17110
17120
17130
17140
17150
17160
17170
17180
17190
17200
17210
17220
17230
17240
17250
17260
17270
17280
17290
17300
17310
17320
17330
17340
17350
17360
17370
17380
17390
17400
17410
17420
17430
17440
17450
17460
17470
17480
17490
17500
17510
17520
17530
17540
17550
17560
17570
17580
17590
17600
17610
17620
17630
17640
17650
17660
17670
17680
17690
17700
17710
17720
17730
17740
17750
17760
17770
17780
17790
17800
17810
17820

```

```

C OWNERSHIP COSTS FOR SKL DUE TO LOADING          17830
SKLOWNC=SKHRFXC*SKLHRSY          17840
C TOTAL OWNERSHIP AND OPERATING COSTS             17850
SKLOOCS=SKLYFC*SKLLBRC+SKLOWNC    17860
C SELF LOADING SPREADER FOR SLURRY DEFAULT VALUES 17870
C MEN NEEDED TO LOAD SLS2                     17880
SLSMLD2=1.0                                17890
C COST OF 2000 GAL SLS                        17900
SLSST2=0.40C/JC                          17910
C DEPRECIATION RATE ON SLS2                   17920
SLSOPR2=0.143                             17930
C GALLONS OF FUEL/HF. TO FILL IT              17940
SLSGHR2=6.0J                              17950
C HOURS TO LOAD ONE LOAD WITH SLS             17960
SLSMLD2=0.68                              17970
C HRS TO HAUL, UNLOAD AND RETURN WITH SLS2    17980
SLSHRT=0.20C                              17990
C HP NEEDED TO HANDLE SLS2                    18000
SLSHP2=30.0                                18010
C INTEREST RATE ON SLS2                      18020
SLSINR2=0.16                               18030
C RMI RATE ON SLS2                          18040
SLSRHR2=0.08                               18050
C MISC RATE ON SLS2                         18060
SLSMR2=0.02C                              18070
C SALVAGE VALUE OF SLS2                     18080
SLSLV2=0.10C                              18090
C PERCENTAGE OF TIME SLS2 SPENT LOADING       18100
SLSPL2=0.25                                18110
C PERCENTAGE TIME SLS2 SPENT HAULING AND HAULING 18120
SLS2HPT=0.6C                              18130
C CALCULATED VALUES FOR 2000 GAL SLS        18140
C TOTAL LOADS/YR WITH SLS2                   18150
SLSLYR2=((VL365ST*(1.10*VLS365D))*7.40)/2000) 18160
C TOTAL TIME/YR TO LOAD SLS2                 18170
SLSLHR2=(SLSMLD2*SLSLYR2)                  18180
C YRLY HRS TO LOAD SLS2                      18190
SLSYHM2=(SLSLHR2*SLSMLD2)                  18200
C LABOR COSTS/LCAD WITH SLS2                 18210
SLSLBL2=(SLSMLD2*CSLABOR)                  18220
C TOTAL LABOR COSTS FOR LOADING SLS2        18230
SLSLTC2=(SLSLBL2*SLSLYR2)                  18240
C TOTAL FUEL USED/YR TO LOAD SLS2            18250
SLSGFL2=(SLSGHR2*SLSLHR2)                  18260
C TOTAL YRLY FUEL COSTS TO LOAD SPREADER     18270
SLSGFC2=(SLSGFL2*FUEDSL)                  18280
C 90-90 HP ACTOR FIXED COSTS ASSOCIATED WITH SLS2 18290
SLSRFXC=TR90FXC*SLSLHR2                   18300
C TOTAL YRLY HAUL AND UNLOAD TIME            18310
SLSLHUT=SLSHPT+SLSLYR2                    18320
C YRLY FUEL USED FOR HAULING ETC WITH SLS2   18330
SLSYRFH=SLSGHR2*SLSLHUT                   18340
C YRLY FUEL COSTS FOR HAULING, UNLOADING ETC. 18350
SLSFHCY=SLSYRFH*FUEDSL                    18360
C SLS2 YRLY OPR RATE                          18370
SLSORT2=SLSOPR2+SLSINR2+SLSRHR2+SLSMR2    18380
C SLS2 YRLY OWN COSTS                        18390
SLSOWC2=(SLSOPR2+SLSOCST2)                18400
C YRLY OWN COSTS DUE TO LOADING              18410
SLSOCL2=SLSOWC2*PL2CALSFTC                18420
C TOTAL YRLY OWN COSTS                        18430
SLSOCL2=SLSOCL2+OCL2CALSFTC+SLSFCS2+SLSFTC 18440
C TOTAL YRLY HRS FOR HAULING ETC.            18450
SLSLHMH=SLSLHUT*SLSMLD2                   18460
C YRLY LABOR COSTS FOR HAULING, ETC.         18470
SLSLMLC=SLSLHMH*CSLABOR                    18480
C YRLY OWN COSTS DUE TO HAULING AND SPREADING WITH SLS2 18490
SLSOCHS=SLSLHMH*SLSOWC2+SLSLHMH*TR90FXC  18500
C TOTAL OWN AND OPERATING COSTS ON SLS2 FOR HAULING 18510
SLSOCHS=SLSFHCY+SLSOCL2+SLSLMLC          18520
C IRIH COST                                  18530
RRIHLCST=(RPCOST+PLHLCST)                 18540
C IRIH YRLY LABOR                            18550
RRIHLBR=(RPHYLBR*PLHAGTY)                 18560
C IRIH LABOR COSTS                           18570
RRIHLC=(RRIHLBR*CSLABOR)                  18580
C IRIH YRLY OWN COSTS                        18590
RRIHOC=(RRIHLCST+PLHOCST)                 18600
C FIXED COSTS FOR PRACTICES USED WITH PUMPS 18610
RRIHFC=RRIHFC+TR90FXC*PLHAGTY            18620
C IRIH YRLY FUEL USED                        18630

```

```

C      RRIMYEN=RFUELY+PLMYFL
C      YRLY FUEL COSTS
C      RRIMYEC=RRIMYEN*FUEDSL
C      YRLY OP COSTS
C      RRIMOC= (RRIMOC+RRIMYEC+RRIMYLC+IRIMTFC)
C      LIQUID SPREADER (3200 GAL) DEFAULT VALUES
C      LOS NO OF MEN NEEDED
C      SLONMEN=1.0
C      CAPACITY OF LIQUID SPREADER IN GALLONS
C      SLQCAP=3200
C      COST OF LIQUID SPREADER
C      SLQCAP=950.00
C      LIQUID SPREADER DEP RATE
C      SLQDEPR=0.143
C      FUEL/HOUR TO RUN SPREADER TO AND FROM FIELD
C      SLQFCH=6.0
C      HP NEEDED TO RUN LIQUID SPREADER
C      SLQHSP=90
C      HAULING SPEED (MPH)
C      SLQHSP=8.0
C      INTEREST RATE ON SPREADER
C      SLQINTR=0.06
C      LOADED HAULING DISTANCE (MILES)
C      SLQLHD=0.5
C      TIME TO LOAD SPREADER (MIN)
C      SLQLTH=3.0
C      MISCELLANEOUS RATE ON LIQUID SPREADER
C      SLQMIS=0.02
C      LIQUID RMT RATE
C      SLQRMH=0.06
C      LIQUID SPREADER RETURN SPEED
C      SLQSP=8.0
C      SALVAGE VALUE OF SPREADER
C      SLQSLV=0.0
C      LIQUID SPREADER UNLOADING RATE (G/MIN)
C      SLQLR=330
C      YRLY FUEL USE BY SPREADER TRACTOR WHILE UNLOADING
C      SLQFC=7.5
C
C      LIQUID SPREADER CALCULATED VALUES
C      LOADS/YR WITH LIQUID SPREADER
C      SLQLDS=(VL365ST/(SLQCAP/7.48))
C      TOTAL YRLY LOAD TIME WITH LIQUID SPREADER
C      SLQLTY=(SLQLDS*SLQLTH)
C      HAULING TIME/LOAD
C      SLQHTM=(SLQLHD/SLQHSP)
C      UNLOADING TIME/LOAD (HRS)
C      SLQLT=(SLQCAP/SLQLR)/60
C      TIME TO RETURN TO LOADING AREA
C      SLQRTM=(SLQLHD/SLQSP)
C      TOTAL YEARLY TIME SPREADER USED (LABOR)
C      SLQLYR=(SLQLT+SLQHTM+SLQRTM+SLQLTH)*(SLQLDS)
C      YRLY FIXED TRACTOR COSTS WITH LOS
C      SLQFTC=TR9CFXC*SLQLYR
C      LOS YRLY MHRS
C      SLQMRY=(SLONMEN*SLQLYR)
C      LOS YRLY LABOR COST
C      SLQLCY=(SLQMRY*CSLABOR)
C      FUEL/LOAD OUT AND BACK
C      SLQFLD=((SLQHTM+SLQRTM)*SLQFCH)
C      FUEL TO UNLOAD ON LOAD
C      SLQFL=(SLQFC*SLQFLD)
C      LIQUID SPREADER FUEL/LOAD
C      SLQFLC=(SLQFLD+SLQFL)
C      ANNUAL FUEL USED WITH LIQUID SPREADER
C      SLQFLYR=SLQLDS*SLQFLC
C      LIQUID SPREADER FUEL COSTS/YR
C      SLQFCY=SLQFLYR*FUEDSL
C      LOS OPMT RATE
C      SLQDTR=SLQDEPR+SLQINTR+SLQMIS+SLQRMH
C      LOS YRLY OWN COSTS
C      SLQOWNC=SLQDTR*SLQCAP
C      TOTAL ANNUAL OWN AND OPERATING COSTS
C      SLQOOC=(SLQOWNC+SLQLCY+SLQFCY+SLQFTC)
C      DEFAULT VARIABLES FOR LIQUID SPREADER AND 4ROW INJECTORS
C      LOS+TNJNO OF MEN
C      TNJ=SLONMEN
C      COST OF INJECTORS
C      TNJCOST=2500.00
C      DEP RATE ON INJECTORS
C      TNJDEPR=0.10

```

```

18640
18650
18660
18670
18680
18690
18700
18710
18720
18730
18740
18750
18760
18770
18780
18790
18800
18810
18820
18830
18840
18850
18860
18870
18880
18890
18900
18910
18920
18930
18940
18950
18960
18970
18980
18990
19000
19010
19020
19030
19040
19050
19060
19070
19080
19090
19100
19110
19120
19130
19140
19150
19160
19170
19180
19190
19200
19210
19220
19230
19240
19250
19260
19270
19280
19290
19300
19310
19320
19330
19340
19350
19360
19370
19380
19390
19400
19410
19420
19430
19440

```

```

C INTEREST RATE ON INJECTORS          19450
  TNJINTR=0.06                          19460
C MISC RATE ON INJECTORS              19470
  TNJMISR=0.02                          19480
C PMI RATE ON INJECTORS               19490
  TNJPMIR=0.07                          19500
C SALVAGE VALUE ON INJECTORS          19510
  TNJSALV=0.00                          19520
C FUEL CONSUMPTION/HR WITH TRACTOR AND INJECTORS FOR HAULING 19530
  SLIJFCH=7.0                           19540
C FUEL CONSUMPTION/HP WHEN INJECTING  19550
  SLIJFCI=8.5                           19560
C HP ON INJECTOR TRACTOR              19570
  SLIJHP=100.00                         19580
C FIXED COSTS ON 100 HP TRACTOR/TR OPERATED 19590
  TR100FC=9.00                          19600
C HAULING SPEED WITH INJECTORS        19610
  SLIJHSP=SLQHSP                         19620
C LOADED HAULING TIME                 19630
  SLIJHMT=SLQHMT                         19640
C LOADED HAULING DISTANCE             19650
  SLIJLMD=SLQLMD                         19660
C LOAD TIME                           19670
  SLIJLTM=(SLQLTM)                      19680
C LOAD TIME/YR                        19690
  SLIJLTY=SLQPTY                         19700
C RETURN SPEED WITH INJECTORS         19710
  SLIJRSP=SLQRSP                         19720
C RETURN TIME WITH INJECTORS          19730
  SLIJRTH=SLQRTM                        19740
C UNLOADING RATE FOR INJECTORS (GPM)  19750
  SLIJULR=50.0                          19760
C YRLY LOADS HAULED                   19770
  SLIJYLD=SLQLDS                         19780
C CALCULATED VALUES FOR INJECTORS    19790
C INJ OWM RATE                        19800
  TNJORT=TNJDEPP+TNJINTR+TNJMISR+TNJPMIR 19810
C INJECTORS OWN COSTS                  19820
  TNJOWN=(TNJORT+TNJCOST)                19830
C COST OF FUEL AND INJECTORS          19840
  SLIJCS=(SLQJCS+TNJOWN)                 19850
C UNLOADING TIME WITH INJECTORS       19860
  SLIJULT=(SLQCAP/SLIJULR)/60            19870
C TOTAL FUELQ OWN COSTS                19880
  SLIJOWN=(SLQOWN+TNJOWN)                 19890
C FUEL USE/CAD WHEN INJECTING         19900
  SLIJUL=SLIJFCI*SLIJULT                 19910
C FUEL TO TAKE LOAD OUT AND EMPTY RETURN 19920
  SLIJFLD=(SLIJHMT+SLIJRTH)*(SLIJFCH)    19930
C FUEL/LOAD UNLOADING PLUS OUT AND BACK 19940
  SLIJFLC=(SLIJFLD+SLIJUFL)              19950
C YRLY FUEL WITH INJECTORS            19960
  SLIJFLY=SLIJYLD*SLIJFLC                19970
C FUEL COSTS/YR                       19980
  SLIJFCY=SLIJFLY*FUEDSLQ                19990
C YEARLY LABOR WITH INJECTORS         20000
  SLIJLYR=(SLIJULT+SLIJRTH+SLIJHMT+SLIJLTM)*(SLQLDS) 20010
C FIXED TRACTOR COSTS ASSOCIATED WITH 100 HP UNIT 20020
  SLIJFTC=SLIJLYR*TR100FC                20030
C LABOR COSTS/YR                      20040
  SLIJLYC=(SLIJLYR+CSLABOR)              20050
C YEARLY OPERATING AND OWNERSHIP COSTS 20060
  SLIJOPC=(SLIJOWN+SLIJLYC+SLIJFCY+SLIJFTC) 20070
C SOLIDS SPREADER (275-400 BUSHEL) CAPACITY WITH HYDRAULIC GATE 20080
C SOLIDS SPREADER DEFAULT VARIABLES  20090
C NO OF MEN FOR SOLIDS SPREADER      20100
C CAPACITY OF SOLIDS SPREADER IN BUSHELS 20110
  SOLSCAP=275                            20120
  SOLSMEN=2.0                             20130
C COST OF SOLIDS SPREADER             20140
  SOLSCST=5000.00                        20150
C DEP RATE                            20160
  SOLSDPR=0.10                           20170
C FUEL USED/HR TO RUN SPREADER        20180
  SOLSFCH=6.0                            20190
C HP OF TRACTOR PULLING UNIT          20200
  SOLSHP=85                              20210
C HAULING SPEED MPH                   20220
  SOLSHSP=6.0                            20230
C SOLID SPREADER INTEREST RATE        20240
  SOLSINR=0.06                           20250

```

```

C NORMAL HAULING DISTANCE TO UNLOADING SITE
SOLSLHD=0.5
C SPREADER LOADING TIME
SOLSLY=0.09
C MISCELLANEOUS RATE ON UNIT
SOLSMI=0.02
C RMI RATE ON SOLID SPREADER
SOLSRHR=0.07
C RETURN SPEED WITH EMPTY SPREADER
SOLSRSD=6.0
C SALVAGE VALUE OF OLD SPREADER
SOLSLV=0.00
C UNLOADING RATE CUFT/HR
SOLSULR=2000
C UNLOADING FUEL CONSUMPTION/HR
SOLSUFC=6.5
C CALCULATED VALUES FOR SOLIDS SPREADER
C SPREADER CAPACITY CU FT
SOLSCCF=SOLSCAP*1.25
C HAULING TIME/LOAD
SOLSHTH=(SOLSLHD/SOLSHSP)
C UNLOAD TIME/LOAD
SOLSULT=(SOLSCCF/SOLSULR)
C TIME TO RETURN TO LOADING AREA
SOLSRTH=(SOLSLHD/SOLSRSP)
C LOADS/YR WITH SOLIDS SPREADER
SOLSHDS=(1365SHH/SOLSCCF)
C TOTAL YEARLY TIME WITH SPREADER
SOLSHYR=(SOLSULT+SOLSRTH+SOLSHTH+SOLSLTH)*(SOLSLOS)
C FIXED COSTS OF TRACTOR
SOLSFTC=SOLSYR*TR90FXC
C HHRS/YEAR ON SOLIDS SPREADER
SOLSHHR=SOLSHEN*SOLSHYR
C LABOR COST/YR FOR HAULING WITH SOLIDS SPREADER
SOLSFCY=(SOLSLYR*CLABOR)
C FUEL TO UNLOAD ONE LOAD
SOLSUFL=(SOLSUFC*SOLSULT)
C FUEL/LOAD OUT AND RETURN
SOLSLD=(SOLSHTH+SOLSRTH)*SOLSFCY
C SOLID SPREADER FUEL/LOAD
SOLSFLC=(SOLSUFL+SOLSLD)
C TOTAL YEARLY LOAD TIME WITH SOLID SPREADER
SOLSHYR=(SOLSHYR+SOLSLD/SOLSHSP)
C SOLIDS SPREADER FUEL USE
SOLSHYR=(SOLSHYR+SOLSLD/SOLSHSP)
C SOLIDS SPREADER FUEL COST/YR
SOLSHYR=(SOLSHYR+SOLSLD/SOLSHSP)
C AVERAGE FUEL CONSUMPTION PER HOUR
SOLSHYR=(SOLSHYR+SOLSLD/SOLSHSP)
C SOLIDS SPREADER TOTAL FUEL RATE
SOLSHYR=(SOLSHYR+SOLSLD/SOLSHSP)
C YRLY OIL COSTS FOR SOLIDS SPREADER
SOLSHYR=(SOLSHYR+SOLSLD/SOLSHSP)
C TOTAL YEARLY OWNERSHIP AND OPERATING COSTS
SOLSHYR=(SOLSHYR+SOLSLD/SOLSHSP)
C BIG GUN SPRINKLER SYSTEMS
SOLSHYR=(SOLSHYR+SOLSLD/SOLSHSP)
C ALUMINUM PIPE UNIT/FT FOR 6 INCH DIAM
ALPCSTF=0.15
C FEET OF PIPE USED
ALPCSTF=0.15
C COST OF GUN SPRINKLER PLUS STAND
RRRBCCS=750.00
C DEP RATE ON PIPE ETC
RRRDEPR=0.10
C NO MEN INVOLVED IN DISMANTLING IRR EQUIPMENT
RRRDTSL=2.00
C HRS/YR INVOLVED IN DISMANTLING IRR
RRRDTSL=2.00
C SET TIME/SETTING
RRRSET=2.00
C INT RATE ON IRR
RRRINTR=0.05
C LABOR(MEN) NEEDED TO OBSERVE WORKING UNIT
RRRLSET=1.00
C MISC RATE FOR IRR
RRRMYSR=0.02
C PERCENT OF TOTAL USE FOR MANURE SLURRY
RRRPTMS=0.25
C RMI RATE FOR IRR
RRRRMIR=0.00
C MEN NEEDED TO RESET BGS

```

```

22 50
23 50
24 50
25 50
26 50
27 50
28 50
29 50
30 50
31 50
32 50
33 50
34 50
35 50
36 50
37 50
38 50
39 50
40 50
41 50
42 50
43 50
44 50
45 50
46 50
47 50
48 50
49 50
50 50
51 50
52 50
53 50
54 50
55 50
56 50
57 50
58 50
59 50
60 50

```

```

C TIME TO RESET=1.0
C MEN INVOLVED IN INITIAL SETUP
C NO OF TIMES UNIT SET UP FOR WASTE
C INITIAL SET UP TIME
C GALLONS PUMPED/BGS SET AT .5 INCHES/SET AND 400 FT DIAM.
C CALCULATE VALUE FOR IRRIGATION SYSTEM
C TOTAL YRLY MANHOUR FOR SET UP
C NUMBER OF YRS WITH BGS
C TOTAL YRLY LABOR TO SET IRR EQUIP
C HPS YRLY TO DISMANTLE BGS IRRIGATION EQUIPMENT
C TOTAL YRLY LABOR FOR IRRIGATION
C TOTAL YRLY LABOR COST FOR ALL IRR ACTIVITIES
C C ALUMINUM PIPE TOTAL COST
C TOTAL PIPE AND BGS COST
C BGS TOTAL COST RATE
C BGS OWN COSTS
C TOTAL YRLY OWN AND OPERATING COSTS
C DEFUALTY COST FOR TRAVELLING GUN SPRINKLER
C TGS PERCENTAGE OF TIME USED FOR MANURE
C COST OF TRAVELLING GUN SPRINKLER
C DEP RATE ON TGS
C FUEL (GAL/HR) TO RUN TGS
C COST OF FUEL
C FEET OF MANHOLE
C HPS TO RUN TGS SYSTEM
C INT RATE ON TGS SYSTEM
C SALVAGE VALUE OF TGS SYSTEM
C MEN NEEDED TO DISMANTLE TGS
C MISC GAIN ON TGS
C MEN INVOLVED IN RESETTING
C AREA COVERED PER QUARTER MILE TGS RUN
C DEPTH OF APPLICATION
C GALLONS/ACRE INCH
C NUMBER OF TIMES/YR UNIT IS SETUP
C HP REQD ON PUMP
C FUEL/YR USED BY PUMP
C PUMPING RATE OF SYSTEM GALLON/HR
C PMI RATE ON TGS
C PEOPLE NEEDED TO OBSERVE DURING OPERATION
C MEN NEEDED TO SET UP TGS SYSTEM
C TIME TO DISMANTLE
  
```

```

21179
21180
21181
21182
21183
21184
21185
21186
21187
21188
21189
21190
21191
21192
21193
21194
21195
21196
21197
21198
21199
21200
21201
21202
21203
21204
21205
21206
21207
21208
21209
21210
21211
21212
21213
21214
21215
21216
21217
21218
21219
21220
21221
21222
21223
21224
21225
21226
21227
21228
21229
21230
21231
21232
21233
21234
21235
21236
21237
21238
21239
21240
21241
21242
21243
21244
21245
21246
21247
21248
21249
21250
21251
21252
21253
21254
21255
21256
21257
21258
21259
21260
21261
21262
21263
21264
21265
21266
21267
21268
21269
21270
21271
21272
21273
21274
21275
21276
21277
21278
21279
21280
21281
21282
21283
21284
21285
21286
21287
21288
21289
21290
21291
21292
21293
21294
21295
21296
21297
21298
21299
21300
21301
21302
21303
21304
21305
21306
21307
21308
21309
21310
21311
21312
21313
21314
21315
21316
21317
21318
21319
21320
21321
21322
21323
21324
21325
21326
21327
21328
21329
21330
21331
21332
21333
21334
21335
21336
21337
21338
21339
21340
21341
21342
21343
21344
21345
21346
21347
21348
21349
21350
21351
21352
21353
21354
21355
21356
21357
21358
21359
21360
21361
21362
21363
21364
21365
21366
21367
21368
21369
21370
21371
21372
21373
21374
21375
21376
21377
21378
21379
21380
21381
21382
21383
21384
21385
21386
21387
21388
21389
21390
21391
21392
21393
21394
21395
21396
21397
21398
21399
21400
21401
21402
21403
21404
21405
21406
21407
21408
21409
21410
21411
21412
21413
21414
21415
21416
21417
21418
21419
21420
21421
21422
21423
21424
21425
21426
21427
21428
21429
21430
21431
21432
21433
21434
21435
21436
21437
21438
21439
21440
21441
21442
21443
21444
21445
21446
21447
21448
21449
21450
21451
21452
21453
21454
21455
21456
21457
21458
21459
21460
21461
21462
21463
21464
21465
21466
21467
21468
21469
21470
21471
21472
21473
21474
21475
21476
21477
21478
21479
21480
21481
21482
21483
21484
21485
21486
21487
21488
21489
21490
21491
21492
21493
21494
21495
21496
21497
21498
21499
21500
21501
21502
21503
21504
21505
21506
21507
21508
21509
21510
21511
21512
21513
21514
21515
21516
21517
21518
21519
21520
21521
21522
21523
21524
21525
21526
21527
21528
21529
21530
21531
21532
21533
21534
21535
21536
21537
21538
21539
21540
21541
21542
21543
21544
21545
21546
21547
21548
21549
21550
21551
21552
21553
21554
21555
21556
21557
21558
21559
21560
21561
21562
21563
21564
21565
21566
21567
21568
21569
21570
21571
21572
21573
21574
21575
21576
21577
21578
21579
21580
21581
21582
21583
21584
21585
21586
21587
21588
21589
21590
21591
21592
21593
21594
21595
21596
21597
21598
21599
21600
21601
21602
21603
21604
21605
21606
21607
21608
21609
21610
21611
21612
21613
21614
21615
21616
21617
21618
21619
21620
21621
21622
21623
21624
21625
21626
21627
21628
21629
21630
21631
21632
21633
21634
21635
21636
21637
21638
21639
21640
21641
21642
21643
21644
21645
21646
21647
21648
21649
21650
21651
21652
21653
21654
21655
21656
21657
21658
21659
21660
21661
21662
21663
21664
21665
21666
21667
21668
21669
21670
21671
21672
21673
21674
21675
21676
21677
21678
21679
21680
21681
21682
21683
21684
21685
21686
21687
21688
21689
21690
21691
21692
21693
21694
21695
21696
21697
21698
21699
21700
21701
21702
21703
21704
21705
21706
21707
21708
21709
21710
21711
21712
21713
21714
21715
21716
21717
21718
21719
21720
21721
21722
21723
21724
21725
21726
21727
21728
21729
21730
21731
21732
21733
21734
21735
21736
21737
21738
21739
21740
21741
21742
21743
21744
21745
21746
21747
21748
21749
21750
21751
21752
21753
21754
21755
21756
21757
21758
21759
21760
21761
21762
21763
21764
21765
21766
21767
21768
21769
21770
21771
21772
21773
21774
21775
21776
21777
21778
21779
21780
21781
21782
21783
21784
21785
21786
21787
21788
21789
21790
21791
21792
21793
21794
21795
21796
21797
21798
21799
21800
21801
21802
21803
21804
21805
21806
21807
21808
21809
21810
21811
21812
21813
21814
21815
21816
21817
21818
21819
21820
21821
21822
21823
21824
21825
21826
21827
21828
21829
21830
21831
21832
21833
21834
21835
21836
21837
21838
21839
21840
21841
21842
21843
21844
21845
21846
21847
21848
21849
21850
21851
21852
21853
21854
21855
21856
21857
21858
21859
21860
21861
21862
21863
21864
21865
21866
21867
21868
21869
21870
21871
21872
21873
21874
21875
21876
21877
21878
21879
21880
21881
21882
21883
21884
21885
21886
21887
21888
21889
21890
21891
21892
21893
21894
21895
21896
21897
21898
21899
21900
21901
21902
21903
21904
21905
21906
21907
21908
21909
21910
21911
21912
21913
21914
21915
21916
21917
21918
21919
21920
21921
21922
21923
21924
21925
21926
21927
21928
21929
21930
21931
21932
21933
21934
21935
21936
21937
21938
21939
21940
21941
21942
21943
21944
21945
21946
21947
21948
21949
21950
21951
21952
21953
21954
21955
21956
21957
21958
21959
21960
21961
21962
21963
21964
21965
21966
21967
21968
21969
21970
21971
21972
21973
21974
21975
21976
21977
21978
21979
21980
21981
21982
21983
21984
21985
21986
21987
21988
21989
21990
21991
21992
21993
21994
21995
21996
21997
21998
21999
22000
22001
22002
22003
22004
22005
22006
22007
22008
22009
22010
22011
22012
22013
22014
22015
22016
22017
22018
22019
22020
22021
22022
22023
22024
22025
22026
22027
22028
22029
22030
22031
22032
22033
22034
22035
22036
22037
22038
22039
22040
22041
22042
22043
22044
22045
22046
22047
22048
22049
22050
22051
22052
22053
22054
22055
22056
22057
22058
22059
22060
22061
22062
22063
22064
22065
22066
22067
22068
22069
22070
22071
22072
22073
22074
22075
22076
22077
22078
22079
22080
22081
22082
22083
22084
22085
22086
22087
22088
22089
22090
22091
22092
22093
22094
22095
22096
22097
22098
22099
22100
22101
22102
22103
22104
22105
22106
22107
22108
22109
22110
22111
22112
22113
22114
22115
22116
22117
22118
22119
22120
22121
22122
22123
22124
22125
22126
22127
22128
22129
22130
22131
22132
22133
22134
22135
22136
22137
22138
22139
22140
22141
22142
22143
22144
22145
22146
22147
22148
22149
22150
22151
22152
22153
22154
22155
22156
22157
22158
22159
22160
22161
22162
22163
22164
22165
22166
22167
22168
22169
22170
22171
22172
22173
22174
22175
22176
22177
22178
22179
22180
22181
22182
22183
22184
22185
22186
22187
22188
22189
22190
22191
22192
22193
22194
22195
22196
22197
22198
22199
22200
22201
22202
22203
22204
22205
22206
22207
22208
22209
22210
22211
22212
22213
22214
22215
22216
22217
22218
22219
22220
22221
22222
22223
22224
22225
22226
22227
22228
22229
22230
22231
22232
22233
22234
22235
22236
22237
22238
22239
22240
22241
22242
22243
22244
22245
22246
22247
22248
22249
22250
22251
22252
22253
22254
22255
22256
22257
22258
22259
22260
22261
22262
22263
22264
22265
22266
22267
22268
22269
22270
22271
22272
22273
22274
22275
22276
22277
22278
22279
22280
22281
22282
22283
22284
22285
22286
22287
22288
22289
22290
22291
22292
22293
22294
22295
22296
22297
22298
22299
22300
22301
22302
22303
22304
22305
22306
22307
22308
22309
22310
22311
22312
22313
22314
22315
22316
22317
22318
22319
22320
22321
22322
22323
22324
22325
22326
22327
22328
22329
22330
22331
22332
22333
22334
22335
22336
22337
22338
22339
22340
22341
22342
22343
22344
22345
22346
22347
22348
22349
22350
22351
22352
22353
22354
22355
22356
22357
22358
22359
22360
22361
22362
22363
22364
22365
22366
22367
22368
22369
22370
22371
22372
22373
22374
22375
22376
22377
22378
22379
22380
22381
22382
22383
22384
22385
22386
22387
22388
22389
22390
22391
22392
22393
22394
22395
22396
22397
22398
22399
22400
22401
22402
22403
22404
22405
22406
22407
22408
22409
22410
22411
22412
22413
22414
22415
22416
22417
22418
22419
22420
22421
22422
22423
22424
22425
22426
22427
22428
22429
22430
22431
22432
22433
22434
22435
22436
22437
22438
22439
22440
22441
22442
22443
22444
22445
22446
22447
22448
22449
22450
22451
22452
22453
22454
22455
22456
22457
22458
22459
22460
22461
22462
22463
22464
22465
22466
22467
22468
22469
22470
22471
22472
22473
22474
22475
22476
22477
22478
22479
22480
22481
22482
22483
22484
22485
22486
22487
22488
22489
22490
22491
22492
22493
22494
22495
22496
22497
22498
22499
22500
22501
22502
22503
22504
22505
22506
22507
22508
22509
22510
22511
22512
22513
22514
22515
22516
22517
22518
22519
22520
22521
22522
22523
22524
22525
22526
22527
22528
22529
22530
22531
22532
22533
22534
22535
22536
22537
22538
22539
22540
22541
22542
22543
22544
22545
22546
22547
22548
22549
22550
22551
22552
22553
22554
22555
22556
22557
22558
22559
22560
22561
22562
22563
22564
22565
22566
22567
22568
22569
22570
22571
22572
22573
22574
22575
22576
22577
22578
22579
22580
22581
22582
22583
22584
22585
22586
22587
22588
22589
22590
22591
22592
22593
22594
22595
22596
22597
22598
22599
22600
22601
22602
22603
22604
22605
22606
22607
22608
22609
22610
22611
22612
22613
22614
22615
22616
22617
22618
22619
22620
22621
22622
22623
22624
22625
22626
22627
22628
22629
22630
22631
22632
22633
22634
22635
22636
22637
22638
22639
22640
22641
22642
22643
22644
22645
22646
22647
22648
22649
22650
22651
22652
22653
22654
22655
22656
22657
22658
22659
22660
22661
22662
22663
22664
22665
22666
22667
22668
22669
22670
22671
22672
22673
22674
22675
22676
22677
22678
22679
22680
22681
22682
22683
22684
22685
22686
22687
22688
22689
22690
22691
22692
22693
22694
22695
22696
22697
22698
22699
22700
22701
22702
22703
22704
22705
22706
22707
22708
22709
22710
22711
22712
22713
22714
22715
22716
22717
22718
22719
22720
22721
22722
22723
22724
22725
22726
22727
22728
22729
22730
22731
22732
22733
22734
22735
22736
22737
22738
22739
22740
22741
22742
22743
22744
22745
22746
22747
22748
22749
22750
22751
22752
22753
22754
22755
22756
22757
22758
22759
22760
22761
22762
22763
22764
22765
22766
22767
22768
22769
22770
22771
22772
22773
22774
22775
22776
22777
22778
22779
22780
22781
22782
22783
22784
22785
22786
22787
22788
22789
22790
22791
22792
22793
22794
22795
22796
22797
22798
22799
22800
22801
22802
22803
22804
22805
22806
22807
22808
22809
22810
22811
22812
22813
22814
22815
22816
22817
22818
22819
22820
22821
22822
22823
22824
22825
22826
22827
22828
22829
22830
22831
22832
22833
22834
22835
22836
22837
22838
22839
22840
22841
22842
22843
22844
22845
22846
22847
22848
22849
22850
22851
22852
22853
22854
22855
22856
22857
22858
22859
22860
22861
22862
22863
22864
22865
22866
22867
22868
22869
22870
22871
22872
22873
22874
22875
22876
22877
22878
22879
22880
22881
22882
22883
22884
22885
22886
22887
22888
22889
22890
22891
22892
22893
22894
22895
22896
22897
22898
22899
22900
22901
22902
22903
22904
22905
22906
22907
22908
22909
22910
22911
22912
22913
22914
22915
22916
22917
22918
22919
22920
22921
22922
22923
22924
22925
22926
22927
22928
22929
22930
22931
22932
22933
22934
22935
22936
22937
22938
22939
22940
22941
22942
22943
22944
22945
22946
22947
22948
22949
22950
22951
22952
22953
22954
22955
22956
22957
22958
22959
22960
22961
22962
22963
22964
22965
22966
22967
22968
22969
22970
22971
22972
22973
22974
22975
22976
22977
22978
22979
22980
22981
22982
22983
22984
22985
22986
22987
22988
22989
22990
22991
22992
22993
22994
22995
22996
22997
22998
22999
23000
23001
23002
23003
23004
23005
23006
23007
23008
23009
23010
23011
23012
23013
23014
23015
23016
23017
23018
23019
23020
23021
23022
23023
23024
23025
23026
23027
23028
23029
23030
23031
23032
23033
23034
23035
23036
23037
23038
23039
23040
23041
23042
23043
23044
23045
23046
23047
23048
23049
23050
23051
23052
23053
23054
23055
23056
23057
23058
23059
23060
23061
23062
23063
23064
23065
23066
23067
23068
23069
23070
23071
23072
23073
23074
23075
23076
23077
23078
23079
23080
23081
23082
23083
23084
23085
23086
23087
23088
23089
23090
23091
23092
23093
23094
23095
23096
23097
23098
23099
23100
23101
23102
23103
23104
23105
23106
23107
23108
23109
23110
23111
23112
23113
23114
23115
23116
23117
23118
23119
23120
23121
23122
23123
23124
23125
23126
23127
23128
23129
23130
23131
23132
23133
23134
23135
23136
23137
23138
23139
23140
23141
23142
23143
23144
23145
23146
23147
23148
23149
23150
23151
23152
2
```

```

C TIME TO RESET UNIT
  TGRSET=1.1
C % ALUMINUM PIPE NEEDED
  TGALEPFT=2.0
C CALCULATED TGS VALUES
C TOTAL VOLUME OF WASTE APPLIED PER RUN
  TGTVRUN=(TGAPE*NT*GAPPOD*ACINCHG)
C TOTAL MANHRS/SET UP
  TGSUMHR=(TGHRSUP*TGSTMEN)
C TOTAL YRLY LABOR FOR SET UP
  TGSTUPL=(TGSUMHR*TGINSTUP)
C TOTAL VOLUME OF WASTE TO BE PUMPED
  TGVOLP=3*VL305ST
C NUMBER RESETS PER YEAR
  TGNRSET=TGVOLP/7.48/TGTVRUN*2.3
C TOTAL SET TIME PER YR
  TGSETTM=(TGVOLP/7.48)/TGMPMR
C TOTAL YRLY MHRS FOR SET TIME
  TGSETMH=(TGSETTM*TGSETMH)
C TOTAL RESET MHRS/YEAR
  TGRSMHR=(TGNRSET*TGRSET*TMGRSET)
C TOTAL MAN HRS/YR FOR DISMANTLING
  TGPYRHD=(TGDISM*TMGDISH*TGINSTUP)
C TOTAL LABOR/YR FOR TGS
  TGTLBRY=(TGPYRHD+TGRSMHR*TGSTUPL)
C TOTAL YRLY LABOR COSTS
  TGYLCST=(TGTLBRY*CSLABOR)
C FUEL/YR TO RUN TG
  TGYRFUL=(TGFUELH*TGSETTM)
C TOTAL YRLY FUEL COSTS
  TGYFLC=(TGYRFUL*0.58)
C % ALUMINUM PIPE COST
  TGALEPCS=TGALEPFT*ALPCSTF
C COST OF ALL HOSE
  TGHHCST=(TGHHCSEC*THHCSEF)
C COST OF HOSE PLUS GUN SPRINKLER+ALUMINUM PIPE
  TGIRRHCC=(TGHHCST+TGHHCST+TGALEPCS)
C TGS DRMT RATE
  TGDHRMT=(TGDPEP+TGINTR+TGRHIR+TGMISCR)
C TG YRLY OWN COSTS
  TGOHNC=(TGDHRMT*TGPMANS*TGIRRHCC)
C TOTAL OWN + OPERATING COSTS
  TGOOCS=(TGOHNC+TGYRFLC+TGYLCST)
COSTINT(1,1)=CLCRBCS
COSTINT(1,2)=CURBFLC
COSTINT(2,1)=STOCCST
COSTINT(2,2)=STOCCST
COSTINT(2,3)=STOCCST
COSTINT(2,4)=STOCCST
COSTINT(2,5)=STOCCST
COSTINT(2,6)=STOCCST
COSTINT(2,7)=STOCCST
COSTINT(2,8)=STOCCST
COSTINT(2,9)=STOCCST
COSTINT(2,10)=STOCCST
COSTINT(3,1)=CLALLC
COSTINT(3,2)=CLALLC
COSTINT(3,3)=CLALLC
COSTINT(3,4)=CLALLC
COSTINT(3,5)=CLALLC
COSTINT(3,6)=CLALLC
COSTINT(3,7)=CLALLC
COSTINT(3,8)=CLALLC
COSTINT(3,9)=CLALLC
COSTINT(3,10)=CLALLC
COSTINT(4,1)=SKCOST
COSTINT(4,2)=SKCOST
COSTINT(4,3)=SKCOST
COSTINT(4,4)=SKCOST
COSTINT(4,5)=SKCOST
COSTINT(4,6)=SKCOST
COSTINT(4,7)=SKCOST
COSTINT(4,8)=SKCOST
COSTINT(4,9)=SKCOST
COSTINT(4,10)=SKCOST
COSTINT(5,1)=CLTOCCST
COSTINT(5,2)=CLTOCCST
COSTINT(5,3)=CLTOCCST
COSTINT(5,4)=CLTOCCST
COSTINT(5,5)=CLTOCCST
COSTINT(5,6)=CLTOCCST
COSTINT(5,7)=CLTOCCST
COSTINT(5,8)=CLTOCCST
COSTINT(5,9)=CLTOCCST
COSTINT(5,10)=CLTOCCST
COSTINT(6,1)=CLTLCST
COSTINT(6,2)=CLTLCST
COSTINT(6,3)=CLTLCST
COSTINT(6,4)=CLTLCST
COSTINT(6,5)=CLTLCST
COSTINT(6,6)=CLTLCST
COSTINT(6,7)=CLTLCST
COSTINT(6,8)=CLTLCST
COSTINT(6,9)=CLTLCST
COSTINT(6,10)=CLTLCST
COSTINT(7,1)=FELCST
COSTINT(7,2)=FELCST
COSTINT(7,3)=FELCST
COSTINT(7,4)=FELCST
COSTINT(7,5)=FELCST
COSTINT(7,6)=FELCST
COSTINT(7,7)=FELCST
COSTINT(7,8)=FELCST
COSTINT(7,9)=FELCST
COSTINT(7,10)=FELCST

```

[illegible]

[illegible]









510

```
COSTOP(2,5)=BOYRCST+STRCSYR  
COSTOP(2,6)=FLSNNTI+SNOCSYR  
COSTOP(2,7)=SHDSSTT+SNOCSYR  
COSTOP(2,8)=BOSKONS+SMATHCY  
COSTOP(2,9)=BOWMMSF+SMATHCY  
COSTOP(2,0)=BOSKOFH+SMATTCTY  
COSTOP(3,1)=SOFOCSS  
COSTOP(3,2)=SLFOCSS  
COSTOP(4,1)=ALLANGCSS  
COSTOP(4,2)=SKTCSTCSS  
COSTOP(4,3)=GONOOCCS  
COSTOP(4,4)=UTTOOFCSS  
COSTOP(4,5)=FLTTOOFCSS  
COSTOP(5,1)=CCTOCCSCSS  
COSTOP(5,2)=CLLTOOCCS  
COSTOP(5,3)=PPANCST  
COSTOP(5,4)=CCRANOCY  
COSTOP(5,5)=CAAOOCY  
COSTOP(5,6)=CYOWNNC  
COSTOP(5,8)=CFLOWNNC  
COSTOP(6,1)=CLLOWNNC  
COSTOP(6,2)=SLOWNNC  
COSTOP(6,3)=FWOWNNC  
COSTOP(6,4)=ELOWNNC  
COSTOP(6,5)=CLOWNNC  
COSTOP(6,6)=PTOWNNC  
COSTOP(6,7)=CTOWNNC  
COSTOP(6,9)=FLLOWNNC  
COSTOP(7,2)=PLHOOCSS  
COSTOP(7,2)=ELLOOCSS  
COSTOP(7,3)=XLOOCCS  
COSTOP(7,4)=COLLOOCH  
COSTOP(7,6)=RRLOOCH  
COSTOP(8,1)=LWOOCSS  
COSTOP(8,2)=QWOOCSS  
COSTOP(8,3)=JWOOCSS  
COSTOP(8,4)=OLSOOCCS  
COSTOP(8,7)=RWLOOCCS  
COSTOP(8,8)=GOOCCS  
  
VALN(2,1)=0.00000000  
VALN(2,2)=0.00000000  
VALN(2,3)=0.00000000  
VALN(2,4)=0.00000000  
VALN(2,5)=0.00000000  
VALN(2,6)=0.00000000  
VALN(2,7)=0.00000000  
VALN(2,8)=0.00000000  
VALN(2,9)=0.00000000  
VALN(2,10)=0.00000000  
VALN(6,1)=0.00000000  
VALN(6,2)=0.00000000  
VALN(6,3)=0.00000000  
VALN(6,4)=0.00000000  
VALN(6,5)=0.00000000  
VALN(6,6)=0.00000000  
VALN(6,7)=0.00000000  
VALN(6,8)=0.00000000  
VALN(6,9)=0.00000000  
VALN(7,1)=0.00000000  
VALN(7,2)=0.00000000  
VALN(7,3)=0.00000000  
VALN(7,4)=0.00000000  
VALN(7,5)=0.00000000  
VALN(7,6)=0.00000000  
VALN(8,1)=0.00000000  
VALN(8,2)=0.00000000  
VALN(8,3)=0.00000000  
VALN(8,4)=0.00000000  
VALN(8,5)=0.00000000  
VALN(8,6)=0.00000000  
J1=JS(1)  
J2=JS(2)  
J3=JS(3)  
J4=J6+JS(4)  
J5=J5+JS(5)  
J6=J6+JS(6)  
J7=J7+JS(7)  
J8=J8+JS(8)  
IF(JS(1),NE,0) GO TO 52C  
11=1
```

25 1 30  
25 1 35  
25 1 45  
25 1 50  
25 1 60  
25 1 65  
25 1 70  
25 1 75  
25 2 00  
25 2 05  
25 2 20  
25 2 25  
25 2 30  
25 2 40  
25 2 50  
25 2 55  
25 2 70  
25 2 90  
25 3 00  
25 3 10  
25 3 20  
25 3 30  
25 3 35  
25 3 40  
25 3 50  
25 3 55  
25 3 60  
25 3 65  
25 3 70  
25 3 80  
25 3 90  
25 4 00  
25 4 10  
25 4 20  
25 4 30  
25 4 40  
25 4 50  
25 4 55  
25 5 00  
25 5 05  
25 5 10  
25 5 15  
25 5 20  
25 5 30  
25 5 40  
25 5 50  
25 5 55  
25 6 00  
25 6 10  
25 6 20  
25 6 30  
25 6 40  
25 6 50  
25 6 55  
25 6 60  
25 6 65  
25 6 70  
25 6 90  
25 7 00  
25 7 10  
25 7 20  
25 7 30  
25 7 40  
25 7 50  
25 7 60  
25 7 70  
25 7 80  
25 7 90  
25 8 00  
25 8 10  
25 8 20  
25 8 30  
25 8 40  
25 8 50  
25 8 60  
25 8 70  
25 8 80  
25 8 90  
25 9 00  
25 9 10  
25 9 20

```

520 J1=2
      IF (IS(2).NE.0) GO TO 530
      J2=1
      J3=10
530 IF (IS(3).NE.0) GO TO 540
      J3=1
      J4=2
540 IF (IS(4).NE.0) GO TO 550
      J4=1
      J5=6
550 IF (IS(5).NE.0) GO TO 560
      J5=1
      J6=3
560 IF (IS(6).NE.0) GO TO 570
      J6=1
      J7=3
570 IF (IS(7).NE.0) GO TO 580
      J7=1
      J8=5
580 IF (IS(8).NE.0) GO TO 700
      J8=1
      J9=5
700 DO 807 M=I1,J1
      DO 806 MM=I2,J2
      DO 805 MMM=I3,J3
      DO 804 MMMM=I4,J4
      DO 803 N=I5,J5
      DO 802 NNN=I6,J6
      DO 801 NNNN=I7,J7
      DO 800 NNNNN=I8,J8
      IOP(1)=M
      IOP(2)=MM
      IOP(3)=MMM
      IOP(4)=MMMM
      IOP(5)=N
      IOP(6)=NN
      IOP(7)=NNN
      IOP(8)=NNNN
      J1=1
      DO 62 I=1,8
      K=IOP(I)
      KK=FESS(I,J,K)
      IF (KK.NE.0) GO TO 416
      GO TO (837,806,805,804,833,802,801,800)IGO
      ISO(I)=KK
      J1=K
      DO 414 I=1,8
      IS(I)=IOP(I)
      PR=VT 60,NSN
414  FORMAT(4 THE FOLLOWING OPTIONS HAVE BEEN SELECTED FOR*/
60  +SYSTEM NUMBER*,I5)
      PRINT 61
61  FORMAT(20 SECTION COMPONENT OPTION*/)
      DO 699 I=1,8
699  PRINT 63,I,(MTITLE(I,J),J=1,4),(MTITLE(ISO(I),LL),LL=1,4)
63  FORMAT(16,5X,4A8,4A8)
C PRINT SUMMARY
      YRVALN=(YRLYNN*(1,10-VALN(2,MM)-VALN(6,NN)-VALN(7,NNN)
      +VALN(8,NNNN)))*0.50*PR*GEN
      YRVALP=YPLYPH*0.50*PRICEP
      YRVALK=YRLYKK*PRICEK
      YRVLHAN=YRVALN+YRVALP+YRVALK
      PRINT 701,NCOMS
701  FORMAT(21NETWORK ANALYSIS OUTPUT FOR DAIRY WASTE HANDLING SYSTEMS*
      +/* OUTPUTS ARE BASED ON THE NUMBER OF COWS IN THE HERD*,I5/)
      PRINT 702,NSN
702  FORMAT(1 * SYSTEM NUMBER=*,I5)
      PRINT 703
703  FORMAT(36X,ANNUAL COST*/1X,SYSTEM*,14X,INITIAL*,8X,
      +* OF OWNERSHIP DIST*/1X,COMPONENTS*,18X,COSTS*,10X,
      +*PCT(DIRTII) TOTALS*)
      PRINT 710,COSTINT(1,M),DIRTPCT(1,M),DIRTTOT(1,M)
710  FORMAT(8STALL TYPE*,8X,4(F8.2,7X))
      PRINT 711,COSTINT(2,MM),DIRTPCT(2,MM),DIRTTOT(2,MM)
711  FORMAT(8BEDDING MATERIAL*,4X,4(F8.2,7X))
      PRINT 712,COSTINT(3,MMM),DIRTPCT(3,MMM),DIRTTOT(3,MMM)
712  FORMAT(8FLOOR STYLE*,9X,4(F8.2,7X))
      PRINT 723
723  PRINT 713,COSTINT(4,MMMM),DIRTPCT(4,IS(4)),DIRTTOT(4,IS(4))
      FORMAT(8ALLEY CLEANING*)

```

```

713 FORMAT(* SYSTEM*,1X,4(F8.2,7X))
PRINT 714,COSTNT(1,N),DIRTPCT(1,N),DIRTTOT(1,N)
714 FORMAT(* MOVEMENT TO STORAGE *,4(F8.2,7X))
PRINT 715,COSTNT(6,NN),DIRTPCT(6,NN),DIRTTOT(6,NN)
715 FORMAT(* STORAGE SYSTEM*,6X,4(F8.2,7X))
PRINT 716,COSTNT(7,NNN),DIRTPCT(7,NNN),DIRTTOT(7,NNN)
716 FORMAT(* UNLOADING OF STORAGE*,4(F8.2,7X))
PRINT 727
PRINT 717,COSTINT(8,NNNN),DIRTPCT(8,NNNN),DIRTTOT(8,NNNN)
727 FORMAT(* MOVEMENT TO FIELD*)
717 FORMAT(* AND APPLICATION*,5X,4(F8.2,7X))
DO 760 I=1,8
T(1)=T(1)+COSTINT(1,IS(1))
T(2)=T(2)+DIRTPCT(1,IS(1))
T(3)=T(3)+DIRTTOT(1,IS(1))
T(4)=T(4)+HRLABOR(1,IS(1))
T(5)=T(5)+COSTLAB(1,IS(1))
T(6)=T(6)+UNITENE(1,IS(1))
T(7)=T(7)+COSTENE(1,IS(1))
T(8)=T(8)+ANNBED(1,IS(1))
T(9)=T(9)+COSTAB(1,IS(1))
T(10)=T(10)+COSTOP(1,IS(1))
760 CONTINUE
PRINT 728,(T(J),J=1,3)
718 FORMAT(* TOTAL SYSTEM COSTS *,4(F8.2,7X))
PRINT 728
728 FORMAT(1H0)
PRINT 750
750 FORMAT(21X,*YRLY MHRS OF YEARLY*,9X,*UNITS OF ENERGY*/
+*,* SYSTEM*,1X,*LABOR USED LABOR*,1X,*USED PER YEAR*/
+*,* COMPONENTS*,10X,* (COMP-EVENT) COSTS*,10X,* (COMP-EVENT)* )
PRINT 710,HRLABOR(1,M),COSTLAB(1,M),UNITENE(1,M)
PRINT 711,HRLABOR(2,MM),COSTLAB(2,MM),UNITENE(2,MM)
PRINT 712,HRLABOR(3,MMM),COSTLAB(3,MMM),UNITENE(3,MMM)
PRINT 723
PRINT 713,HRLABOR(4,MMMM),COSTLAB(4,IS(4)),UNITENE(4,IS(4))
PRINT 714,HRLABOR(5,N),COSTLAB(5,N),UNITENE(5,N)
PRINT 715,HRLABOR(6,NN),COSTLAB(6,NN),UNITENE(6,NN)
PRINT 716,HRLABOR(7,NNN),COSTLAB(7,NNN),UNITENE(7,NNN)
PRINT 727
PRINT 717,HRLABOR(8,NNNN),COSTLAB(8,NNNN),UNITENE(8,NNNN)
PRINT 718,(T(J),J=4,5)
PRINT 728
PRINT 770
770 FORMAT(22X,*YEARLY ENERGY YEARLY*,9X,*YEARLY ANNUAL*/
+*,* SYSTEM*,1X,*COSTS*,10X,*BEDDING*,8X,*BEDDING COSTS*/
+*,* COMPONENTS*,10X,* (COMP-EVENT) USED*,11X,*COSTS*,5X,
+*,* (COMP-EVENT) )
PRINT 710,COSTENE(1,M),ANNBED(1,M),COSTAB(1,M),
+COSTOP(1,M)
PRINT 711,COSTENE(2,MM),ANNBED(2,MM),COSTAB(2,MM),
+COSTOP(2,MM)
PRINT 712,COSTENE(3,MMM),ANNBED(3,MMM),COSTAB(3,MMM),
+COSTOP(3,MMM)
PRINT 723
PRINT 713,COSTENE(4,MMMM),ANNBED(4,IS(4)),COSTAB(4,IS(4)),
+COSTOP(4,MMMM)
PRINT 714,COSTENE(5,N),ANNBED(5,N),COSTAB(5,N),
+COSTOP(5,N)
PRINT 715,COSTENE(6,NN),ANNBED(6,NN),COSTAB(6,NN),
+COSTOP(6,NN)
PRINT 716,COSTENE(7,NNN),ANNBED(7,NNN),COSTAB(7,NNN),
+COSTOP(7,NNN)
PRINT 717,COSTENE(8,NNNN),ANNBED(8,NNNN),COSTAB(8,NNNN),
+COSTOP(8,NNNN)
PRINT 718,(T(J),J=7,10)
PRINT 411,YRVLHAN
411 FORMAT(* YRLY VALUE OF MANURE*,45X,F8.2)
COSTNET=T(10)-YRVLHAN
PRINT 412,COSTNET
412 FORMAT(* NET SYSTEM COST*,50X,F8.2)
WRITE(3,413)NSN,1,IOP(1),I=1,8,YRVLHAN,COSTNET,NCONS,ISAPN
417 FORMAT(9I3,2F10.2,2I3)
DO 418 I=1,8
WRITE(3,420)COSTINT(I,IOP(I)),DIRTPCT(I,IOP(I)),DIRTTOT(I,IOP(I)),
+HRLABOR(I,IOP(I)),COSTLAB(I,IOP(I)),UNITENE(I,IOP(I)),
+COSTENE(I,IOP(I)),ANNBED(I,IOP(I)),COSTAB(I,IOP(I)),
+COSTOP(I,IOP(I))
WRITE(3,420)I,T(I),I=1,18)
420 FORMAT(10F10.2)

```

27550  
27560  
27570  
27580  
27590  
27600  
27610  
27620  
27630  
27640  
27650  
27660  
27670  
27680  
27690  
27700  
27710  
27720  
27730  
27740

APPENDIX C

COMPARISON OF 58 COMMONLY USED WASTE  
HANDLING SYSTEMS FOR 100-300  
COW HERDS





Sys. No.	Option Codes	System Invest.	Annual Ownership Costs	Annual Labor MHS	Annual Labor Costs	Annual Energy Costs	Tons of Bedding	Annual Bedding Costs	Total Annual Costs	Manure Nutrient Value	Net Cost
1	1	1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3	3	3	3	3
4	4	4	4	4	4	4	4	4	4	4	4
5	5	5	5	5	5	5	5	5	5	5	5
6	6	6	6	6	6	6	6	6	6	6	6
7	7	7	7	7	7	7	7	7	7	7	7
8	8	8	8	8	8	8	8	8	8	8	8
9	9	9	9	9	9	9	9	9	9	9	9
10	10	10	10	10	10	10	10	10	10	10	10
11	11	11	11	11	11	11	11	11	11	11	11
12	12	12	12	12	12	12	12	12	12	12	12
13	13	13	13	13	13	13	13	13	13	13	13
14	14	14	14	14	14	14	14	14	14	14	14
15	15	15	15	15	15	15	15	15	15	15	15
16	16	16	16	16	16	16	16	16	16	16	16
17	17	17	17	17	17	17	17	17	17	17	17
18	18	18	18	18	18	18	18	18	18	18	18
19	19	19	19	19	19	19	19	19	19	19	19
20	20	20	20	20	20	20	20	20	20	20	20
21	21	21	21	21	21	21	21	21	21	21	21
22	22	22	22	22	22	22	22	22	22	22	22
23	23	23	23	23	23	23	23	23	23	23	23
24	24	24	24	24	24	24	24	24	24	24	24
25	25	25	25	25	25	25	25	25	25	25	25
26	26	26	26	26	26	26	26	26	26	26	26
27	27	27	27	27	27	27	27	27	27	27	27
28	28	28	28	28	28	28	28	28	28	28	28
29	29	29	29	29	29	29	29	29	29	29	29
30	30	30	30	30	30	30	30	30	30	30	30
31	31	31	31	31	31	31	31	31	31	31	31
32	32	32	32	32	32	32	32	32	32	32	32
33	33	33	33	33	33	33	33	33	33	33	33
34	34	34	34	34	34	34	34	34	34	34	34
35	35	35	35	35	35	35	35	35	35	35	35
36	36	36	36	36	36	36	36	36	36	36	36
37	37	37	37	37	37	37	37	37	37	37	37
38	38	38	38	38	38	38	38	38	38	38	38
39	39	39	39	39	39	39	39	39	39	39	39
40	40	40	40	40	40	40	40	40	40	40	40
41	41	41	41	41	41	41	41	41	41	41	41
42	42	42	42	42	42	42	42	42	42	42	42
43	43	43	43	43	43	43	43	43	43	43	43
44	44	44	44	44	44	44	44	44	44	44	44
45	45	45	45	45	45	45	45	45	45	45	45
46	46	46	46	46	46	46	46	46	46	46	46
47	47	47	47	47	47	47	47	47	47	47	47
48	48	48	48	48	48	48	48	48	48	48	48
49	49	49	49	49	49	49	49	49	49	49	49
50	50	50	50	50	50	50	50	50	50	50	50



[illegible]

[illegible]

MICHIGAN STATE UNIV. LIBRARIES



31293103942219