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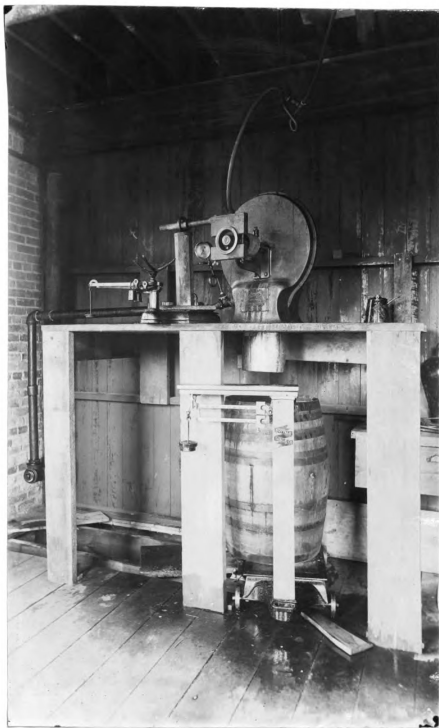
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Seymour and Whitlock motor and apparatus.

1891.

SOME WATERMILLS

1891

IMPACT WATER MOTORS.

R. S. 1891

July 20, 1893.

Amos
A. C. Furbush.

THESIS

SOLE EXPERIMENTS WITH IMPACT WATER MOTORS.

THE moving water upon the surface of the earth represents immeasurable power, and it was in attempting to find means by which some of this immense power might be utilized that the water motor was evolved. In general these motors are divided into two classes: large water wheels or turbines, and smaller enclosed ~~wheels~~ wheels known as impact motors. A third class, less frequently met with, are the water engines or piston motors.

At present we are concerned with impact motors only. Of these there are many kinds manufactured; but among them all the only significant difference lies in the form of cup and the manner of impact. Among the more important of these motors made in the United States are the Pelton, Backus, Turck, Cooper, Benham, Syracuse, Belknap, Seymour and Whitlock or parabolic, and others.

Impact motors are used in many places, under many conditions and for many purposes. They are generally used where water can be had conveniently and where the power needed is small; but recently large ones also have come into use in the West working under immense heads and furnishing very great power.

The object of these experiments was to obtain the comparative efficiencies of the three wheels at hand - a 12" Pelton, a 22" Backus and a 22" Seymoure and Whitlock- and to note as far as possible other characteristics.

Plates 6,7, and 8 show the ~~forms~~ construction of these motors, the forms and number of cups and the different manners of impact.

The work was done entirely independently and without regard to any work previously done in the same line. In fact, very few results of tests of water motors seem to have been published, and no references, except to a report of tests made by Professor L.P. Breckearidge and published by J.H. Mills in his HEAT FOR THE WARMING AND VENTILATION OF BUILDINGS and to the catalogues of the various motors, can be given. All results are recorded exactly as found, and all irregularities are, as far as possible, accounted for,

The Pelton motor was tested with $1/4$ inch, $3/8$ inch and $1/2$ inch cast iron nozzles; the Backus, with $1/4$ inch and $3/8$ inch nozzles made of brass; and the Seymoure and Whitlock, with $1/4$ inch $3/8$ inch and $5/16$ inch nozzles of cast iron. All nozzles are ~~xxx~~ shown full scale on Plate 5.

The photographs show the manner in which each motor was set up, the power measured and the water weighed. For each nozzle it was assumed that, for the ordinary variations in number of revolutions, the amount of water flowing through motor per minute, for any one head, was constant. Thus, for any one motor and nozzle, the number of revolutions per minute being kept as nearly as possible at the average, the amount of water flowing per minute was determined once for all by noting the time required to run one hundred pounds.

The horse power of the water was determined by the formula:

$$H.P. = \frac{3.46W}{33000} \times P$$
 where W equals weight in pounds of water ~~xx~~ flowing through motor per minute, and P equals head of water in pounds pressure. This assumes that a pressure of 15 pounds will hold a water column of 34 feet, but the slight error due to this assumption was thought to be within the limit of error ~~xxxx~~ obtainable in the conducting of the experiments themselves.

The brake wheel was 5 inches in diameter with 1 1/2 inch ~~xx~~ face and with a flange 1/4 inch high on each edge to prevent the brake from slipping off. The brake back was of oak wood 1 1/4 inches square and was continued to form the brake arm 1 1/4 inches in diameter. The rubbing surfaces were of pine wood with face of 1 1/4 inch. The length of brake arm, or the distance from center of brake wheel to knife-edge over small scales, was one foot. This arrangement gave good results, but it is believed that a 4 inch brake wheel would, ~~give~~ for the larger loads, give better results. The pressure upon the small scales used for determining the horse power of the brake, and shown in the photographs, was varied in the course of all the experiments from 1/4 of a pound to 11 pounds, as will appear in the tables of results. The method of varying this pressure was by tightening or loosening the thumb nuts at the lower edge of the brake, and thus increasing or decreasing the friction between the brake and the wheel. In every case, before begin-

During an experiment, the weight of the overhanging portion of the brake and arm was balanced on one of the scale beams, so that the weight recorded on the other should be that due to the friction of the brake alone.

The horse power of the motor which was absorbed by the brake was determined by the formula: H.P. of motor equals $2 \text{ anw} + 38000$, where a equals length of brake in feet, n equals number of revolutions per minute of brake wheel, and W equals pressure in pounds on small scales.

The following tables show the record of observations of all the experiments together with the computed results. The letters at the tops of the columns have the following significance:

P at top of first column - - - - head in pounds pressure.

L " " " second " - - - - load on small scales.

In all other cases, -

R.P.M. - - - - revolutions per minute.

p.m. - - - - pounds per minute flowing
through motor

H.P. Motor. - - - - horse power of motor.

H.P. Water. - - - - horse power of water.

% Eff. - - - - percentage of efficiency.

P. - - - - Pelton motor.

B. - - - - Backus motor.

SSW - - - - Seymoure and Whitlock motor.

Results for 3/8 inch nozzles.

P.L.	R.P.M.			P.M.			H.P. Motor.			H.P. Water.			Eff.		
	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W
8 0	303	176	172	64	71	64	0	0	0	.018	.024	.018	0	0	0
10 0	546	282	222	76	109	79	0	0	0	.083	.075	.054	0	0	0
4	426	254	200	"	"	"	.021	.013	.010	"	"	"	39.6	17.4	18.5
1/2	326	216	184	"	"	"	.031	.022	.017	"	"	"	65.5	29.4	31.4
3/4		162	176	"	"	"		.024	.026	"	"	"	32.0	48.1	
1			162	"	"	"			.031	"	"	"		57.4	
1 1/4			160	"	"	"			.036	"	"	"		66.6	
20 0	557	454		120	148	114	0	0		.062	.201	.155	0	0	
1/4			344							.017				10.8	
1/2	667	406	330				.064	.041	.031				39.1	20.2	19.9
3/4	597		322				.086		.045				52.5		30.8
1	529	346	286				.108	.066	.035				64.0	32.7	35.4
1 1/4	468		286				.111		.064				65.5		41.1
1 1/2		292	240					.085	.070				42.3	45.2	
1 3/4			196						.065					41.7	
30 0	1059	542		143	176	138	0	0		.294	.362	.284	0	0	
1/4			434						.022					7.8	
1/2		528	420					.033	.040				14.7	14.1	
3/4	589		406				.147		.061				52.0		21.5
1	537	488	396				.167	.092	.075				56.5	25.4	26.4
1 1/2	750	464	390				.214	.134	.111				72.5	37.0	39.1
2	643	406	330				.245	.154	.127				83.3	42.5	44.7
2 1/2		386	288					.171	.138				77.2	45.6	
3		306						.174					78.1		
40 0	1241	620		174	222	171	0	0		.478	.609	.469	0	0	
1/4			510						.018					10.2	
1/2	973	568	486				.174	.105	.093				40.6	17.5	19.9
3/4	847	548	468				.242	.159	.140				50.6	26.1	28.9
1	780	520	442				.286	.178	.163				57.8	32.6	35.9
1 1/2	654	486	412				.312	.233	.197				65.3	38.5	42.1
2		454	364					.267	.205				42.5	44.3	
2 1/2		388						.279					43.8		
3		358						.298					45.5		
3 1/2		316						.272					48.0		

Results for 3/8 inch nozzles.

#	#	R.P.M.			# p.m.			H.P. Motor.			H.P. Water.			# Eff.		
P L	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	
50	0	1354	664		193	240	187	0	0		721	524	680	0	0	
	1/2		566							.054						8.0
	1		542							.103						15.2
	1 1/2	1059	526					.303		.157				420		24.1
	2	947	610	504				.361	.232	.192				50.1	28.1	283
	2 1/2	837	570	488				.399	.277	.234				56.3	33.9	34.4
	3	735	542	456				.420	.309	.260				58.3	37.1	38.9
	3 1/2	654	500					.435	.335					607		40.2
	4		470						.357							44.8
	4 1/2		450						.387							46.4
	5		412						.392							47.1
	5 1/2		390						.409							49.6
	6		360						.414							50.3
60	0	1500	716		242	261	207	0	0		873	1072	853	0	0	
	1/2		620							.057						7.9
	1		592							.115						13.8
	1 1/2	1220	562					.350		.168				40.1		19.9
	2	1143	540					.436		.205				49.9		24.0
	2 1/2	1059	528					.504		.254				57.7		28.8
	3	947	554	498				.541	.316	.284				61.9	29.4	33.3
	3 1/2	857	516					.574	.346					65.7	32.2	
	4	782	500					.596	.380					68.3	35.4	
	4 1/2		466						.401							37.3
	5		442						.520							39.1
	5 1/2		436						.535							40.5
	6		390						.549							41.8
70	0	1636	776		231	256	222	0	0		1106	1378	1067	0	0	
	1/2		628							.061						5.7
	1		624							.125						11.7
	1 1/2	1358	620					.390		.186				35.3		17.4
	2	1268	610					.481		.232				43.5		21.8
	2 1/2	1220	590					.581		.281				52.6		26.6

Results for 5/8 inch nozzles.

# #		R.P.M.			# p.m.			H.P.Motor.			H.P.Water.			Eff.		
P L	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	
70	3	1143		570	231	286	222	653		325	1106	1375	1067	59.1		30.5
	3½	1075	626					920	352					65.9	25.6	
	4	1000	508					762	386					68.9	30.1	
	4½		485						420						30.6	
	5		447						447						32.6	
	5½		448						471						34.3	
	6		440						506						36.9	
	6½		418						578						37.7	
80	0	1800	800		250	304	235	0	0		1373	1670	1291	0	0	
	½			720						.068						68
	1			692						.138						107
	1½	1532		667				438	.200					32.0		154
	2	1440		643				549	.244					39.3		189
	2½	1333		621				635	.298					46.3		240
	3	1286		590				735	.337					43.5		261
	3½	1180						790						57.5		
	4	1125	542					859	.412					62.4	24.7	
	4½		520						.447						26.6	
	5		504						.474						28.7	
	5½		486						.521						31.2	
	6		472						.543						32.5	
	6½		454						.563						33.7	
	7		434						.582						34.9	
	7½		426						.609						36.5	
	8		422						.643						38.5	
	8½		410						.664						39.8	
90	0		812		261	333	245	0	0		1613	2008	1514	0	0	
	½			735						.070						7.5
	1			720						.144						7.5
	1½	1714		706				490	.211					30.4		139
	2	1674		692				639	.263					39.6		154
	2½	1600		680				810	.327					60.2		216
	3	1601		667				888	.380					80.1		251

Nominals for 3/8 inch nozzles.

#	#	R.P.M.			P.P.			R.P. Motor			R.P. Water			Eff.		
		P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W
90	32	1333			261	333	248	888			1613	204	1514	55.1		
	4	1241						945						58.6		
	4 1/2		590					505						25.4		
	5		540					513						25.6		
	5 1/2		520					546						27.3		
	6		484					568						28.4		
	6 1/2		484					590						28.5		
	7		468					627						31.3		
	7 1/2		490					629						31.7		
	8		424					646						32.2		
	8 1/2		416					673						33.6		
	9		412					706						34.3		

Nominals for 1/2 inch nozzles.

5	0	125		142	25		32	0		0	.008	.010	0		0
10	0	419	121		41	35		0	0		.027	.023	0	0	
	1/4	246		182			46.1	.012				.031	44.4		29.6
	1/2			160											51.6
	3/4			138						.021					69.5
20	0	750	382		64	61	67.4	0	0		.086	.082	.091	0	0
	1/4	442	302	298				.022	.015					25.6	18.3/16.5
	1/2	276	246	268				.028	.023					32.6	25.9 25.6
	3/4		174	222				.026						31.7	36.2
	1			212					.040						43.9
	1 1/4			122					.029						31.8
30	0	985	489		80	78	79.1	0	0		.168	.164	.166	0	0
	1/4		454	382				.023							14.0/11.5
	1/2	574	506	368				.057	.041					33.9	26.0 21.9
	3/4	380	366	342				.057	.053					33.9	32.3 31.1
	1	280	304	306				.053	.058					31.6	35.3 33.3
	1 1/4		296	292				.059							36.0 42.6
	1 1/2		232	260				.067							40.9 45.6
	1 3/4			240					.082						49.9
	2								.085						57.2

Results for 1/4 inch nozzles.

#	#	R.P.M.			# p.m.			H.P. Motor.			H.P. Water.			Eff.		
		P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W
40	0	1161	581		875	89	875	0	0		236	240	225	0	0	
	1/2	896	536	470				.090	.054					381	225	206
	1	696	468	430				.132	.089					561	371	360
	1 1/2	524	334	386				.152	.077					644	404	492
	2 1/4		302	330				.163		.125				439		54.9
	2 1/2			274						.132						57.8
50	0	1286	643		100	101	90.9	0	0		.340	343	309	0	0	
	1/2		616	534					.062					150	171	
	1	888	566	498				.269	.108					497	314	297.5
	1 1/2	764	468	460				.264	.136					60.0	396	426
	2	550	386	410				.190	.147					55.9	42.9	51.4
	2 1/2		300	372					.144	.178				41.9		57.5
	3			320						.182						58.9
60	0	1411	708		108	109	98.3	0	0		.442	447	403	0	0	
	1/2			598												14.6
	1	1076	640	538				.204	.122					451	272	26.3
	1 1/2	830	576	528				.240	.167					542	372	380
	2	732	490	486				.278	.186					629	41.5	45.9
	2 1/2	522	408	460				.250	.196	.221				565	43.9	54.8
	3		306	420					.178	.239				390		57.3
70	0	1583	769		118	113	103.2	0	0		.566	542	504	0	0	
	1/2			678												13.1
	1			640												24.2
	1 1/2	866	720	608				.251	.209					438	385	350
	2	846	610	580				.321	.232					561	42.7	49.1
	2 1/2	712	530	530				.341	.254	.264				596	469	52.1
	2 3/4	660						.350						61.9		52.3
	3		480	574					.274	.293						58.1
	3 1/2		386						.254							49.7

Results for 1/4 inch nozzles.

#	#	R.P.M.			p.p.m.			H.P. Motor			H.P. Water			Eff.		
P.	L.	P.	B.	S.&W.	P.	B.	S.&W.	P.	B.	S&W	P.	B.	S&W	P.	B.	S&W
80	0	1675	790		128	125	1132	0	0		.691	.675	.611	0	0	
	1/2			730												120
	1			692												21.5
	1 1/2		762	668				.221						32.7	36.8	
	2	1124	712	640				.427	.271					61.8	401	39.8
	2 1/2	898	604	608				.431	.290	.292				62.4	42.9	47.8
	3	754	534	590				.427	.304	.336				62.1	45.0	54.9
	3 1/2	684						.424						61.4		
	3 3/4		494						.282						49.0	
	4		412						.313						46.3	
	4 1/2		375						.323						47.9	
90	0	1756	860		136	130	1224	0	0		.829	.793	.746	0	0	
	1/2			770												10.3
	1			734												19.6
	1 1/2			710												27.6
	2	1200	746	694				.456	.283					55.4	35.7	34.6
	2 1/2	1060	696	664				.508	.334	.309				61.4	42.1	42.1
	3	910	628	630				.513	.358	.359				61.8	45.1	48.1
	3 1/2	744	592					.496	.397					60.2	50.0	
	4		546						.415						52.3	
	4 1/2		502						.432						54.6	
	5		414						.393						49.5	

Pelton- Results for 1-2 inch nozzle.

#	#	#	H.P.	H.P.	#	#	#	#	H.P.	H.P.	#
P.	L.R.P.M.	p.m.	Motor	Water	Eff.	P.	L.R.P.M.	p.m.	Motor	Water	Eff.
5	0	375	105	0	.035	0	60	0	1560	455	0
10	0	602	175	0	.117	0	3	1216	.789		44.2
	$\frac{1}{2}$	584		.056	47		3 $\frac{1}{2}$	1250	.837		50.2
	$\frac{3}{4}$	300		.045	38.4		4	1188	.902		54.1
	1	274		.052	44.4		4 $\frac{1}{2}$	1128	.990		58.2
20	0	878	216	0	.292	0	5	1092	1.035		62.1
	$\frac{1}{2}$	774		.099	26.2		5 $\frac{1}{2}$	986	1.035		62.1
	1	744		.149	50.3		6	954	1.099		65.8
	1 $\frac{1}{2}$	608		.176	60.1		6 $\frac{1}{2}$	892	1.106		66.4
	2	504		.193	66.0		7	876	1.174		68.4
	2 $\frac{1}{2}$	436		.209	71.5		7 $\frac{1}{2}$	866	1.224		74.6
30	0	1091	286	0	.600	0	8	768	1.175		73.5
	1	936		.197	29.3		8	1674	429	0	205.9
	$\frac{1}{2}$	868		.251	41.6		4	1464	1.113		53.4
	2	756		.287	47.6		5	1300	1.235		59.0
	2 $\frac{1}{2}$	688		.330	54.9		6	1240	1.428		68.5
	3	608		.347	57.9		7	1160	1.541		73.9
	3 $\frac{1}{2}$	496		.332	56.1		8	1074	1.643		78.9
40	0	1333	315	0	.860	0	9	1004	1.726		83.8
	$\frac{1}{2}$	1072		.310	36.4		10	740	1.406		68.2
	2	1030		.391	46.6		50	0	1800	500	0
	2 $\frac{1}{2}$	976		.468	54.8		5	1408	1.337		50.5
	3	906		.516	64.3		6	1348	1.560		57.4
	3 $\frac{1}{2}$	766		.513	60.0		7	1238	1.658		61.0
	4	656		.497	57.4		8	1158	1.771		65.6
	4 $\frac{1}{2}$	618		.531	62.5		9	1014	1.745		64.4
50	0	1440	363	0	1.234	0	10	908	1.720		63.6
	2 $\frac{1}{2}$	1126		.428	34.6		90	0	2000	540	0
	3	1082		.616	49.4		6	1468	1.678		50.6
	3 $\frac{1}{2}$	1070		.697	66.4		7	1426	1.912		57.3
	4	988		.741	60.2		8	1356	2.075		62.1
	4 $\frac{1}{2}$	930		.800	64.8		9	1310	2.253		67.5
	5	878		.834	67.6		10	1202	2.284		68.0
	5 $\frac{1}{2}$	782		.821	66.5		11	1116	2.343		70.4
	6	720		.828	67.0						

Seymour & Whitely- Results for 5/16 inch nozzle.

#	P	R.P.M.	H.P.	Motor	Water	Eff.	#	P	R.P.M.	H.P.	Motor	Water	Eff.
5	0	152	46.1	0	.515	0	50	3	425	160	.242	.544	44.5
10	$\frac{1}{4}$	222	72.3	.011	.048	23.9	60	$\frac{1}{2}$	592	167	.059	.684	8.6
	$\frac{1}{2}$	194		.019		39.6		1	578		.115		18.8
	$\frac{3}{4}$	160		.024		50.0		$\frac{1}{2}$	582		.160		23.1
20	$\frac{1}{4}$	322	98.3	.016	.133	12.1		2	528		.201		29.3
	$\frac{1}{2}$	302		.030		22.8		$2\frac{1}{2}$	506		.243		36.1
	$\frac{3}{4}$	280		.042		31.9		3	482		.275		46.2
	1	264		.050		39.5	70	$\frac{1}{2}$	620	190	.062	.912	12.4
	$\frac{1}{4}$	260		.060		45.6		1	604		.120		24.0
	$\frac{1}{2}$	224		.065		48.9		$\frac{1}{2}$	588		.171		17.2
	$\frac{3}{4}$	194		.066		49.6		2	574		.218		22.0
30	$\frac{1}{4}$	392	121.2	.019	.254	7.5		$2\frac{1}{2}$	552		.265		27.0
	$\frac{1}{2}$	380		.038		15.1		3	534		.304		33.4
	$\frac{3}{4}$	364		.054		21.1	80	$\frac{1}{2}$	678	196	.067	1.058	6.4
	1	350		.070		27.9		1	660		.132		12.5
	$\frac{1}{2}$	324		.094		36.6		$\frac{1}{2}$	640		.186		17.6
	2	218		.113		44.5		2	627		.238		22.6
40	$\frac{1}{2}$	486	144.5	.048	.390	12.4		$2\frac{1}{2}$	618		.297		28.2
	1	464		.092		23.9		3	602		.343		32.4
	$\frac{1}{2}$	448		.130		33.8	90	$\frac{1}{2}$	706	203	.070	1.238	5.6
	2	414		.157		40.8		1	694		.138		11.0
	$2\frac{1}{2}$	398		.191		49.6		$\frac{1}{2}$	672		.195		15.6
	3	372		.212		54.3		2	664		.252		20.1
50	$\frac{1}{2}$	570	160	.054	.544	9.9		$2\frac{1}{2}$	642		.308		24.6
	1	574		.102		18.8		3	624		.356		28.9
	$\frac{1}{2}$	494		.143		26.3							
	2	480		.182		33.5							
	$2\frac{1}{2}$	460		.221		40.6							

From these data, the efficiency of the different nozzles under all conditions; the discharge, single curves showing maximum efficiency under all tests, and the curves showing horse power for the different nozzles, nozzles and heads. The efficiency curves for the 3/4" and 1/4" nozzles for all the nozzles are shown in Plates 1 and 2 respectively; the characteristic curves are shown on Plate 3, and the curves for the different nozzles, on Plates 4. Instead of attempting to construct the curves, these were plotted from the exact results obtained. They should, no doubt in every case, be smooth, regular curves, and the irregularities are probably due to slight variations, in the results obtained, either by the nozzles or the heads. The method of construction of the diagrams is indicated on the Plates and needs no explanation.

The curves on the following page show the amount of water per minute flowing through the different nozzles for each nozzle and the different heads. The black lines are for the Pelton nozzle; the blue lines, for the Reaumur; the red lines, for the Sawyer; the dotted lines, for the 3/4" nozzle; the solid lines, the 1/4" nozzle; and the dotted lines, the 1/2" nozzle for the Pelton; and the 5/16" nozzle for the Sawyer and 1/4" nozzle. It will be noticed from these curves that the coefficient of discharge is not constant, and that the efficiency is not constant for either of the nozzles.

ounds
of
water
per

500
minute
flowing
to
1000
minute
flowing

100

200

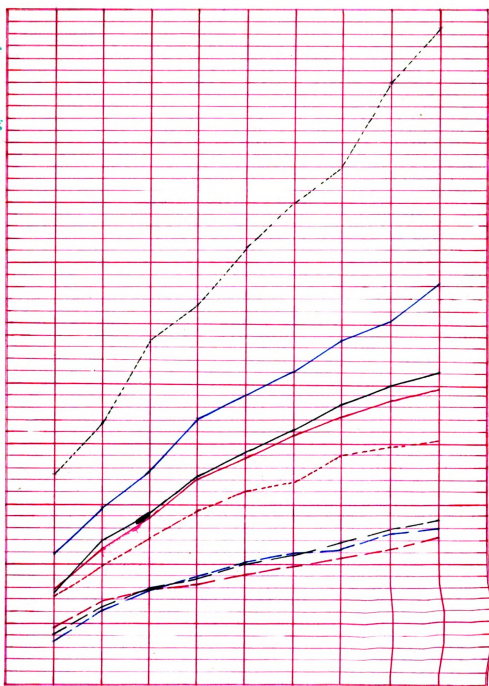
300

400

500

600

700



10 20 30 40 50 60 70 80 90

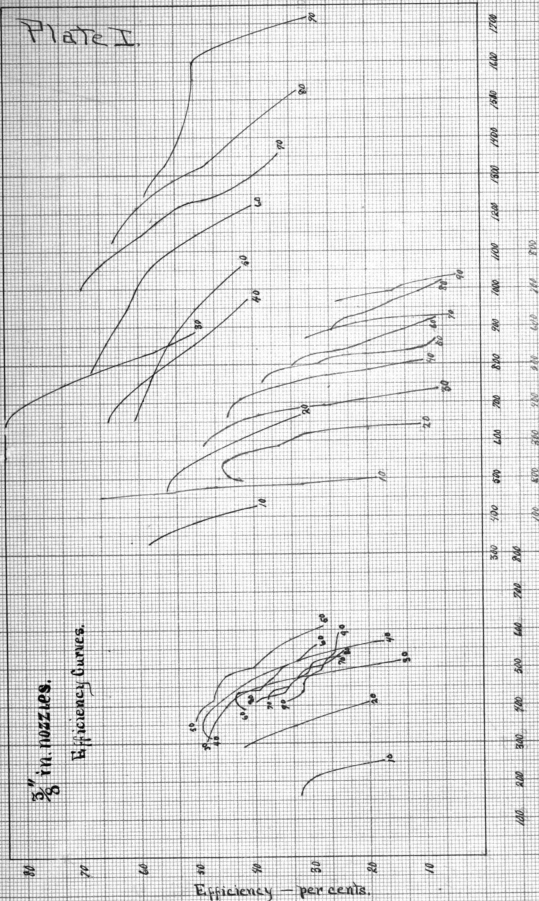
Head in working pressure.

Plate I.

Small nos. at ends of curves denote heads.

$\frac{5}{8}$ in. nozzles.

Efficiency Curves.

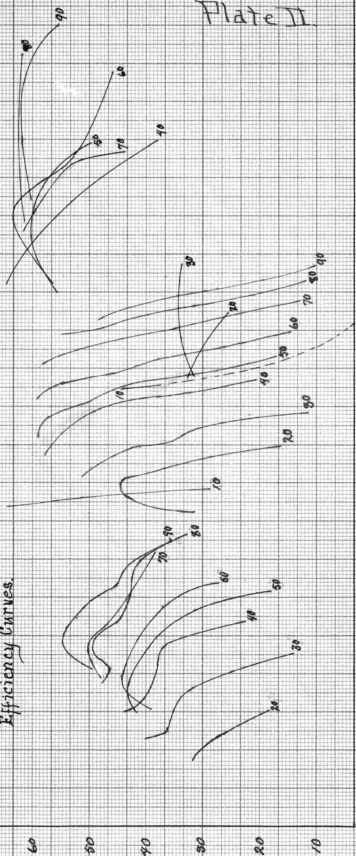


Small nos. at ends of Curves denote heads in # pres.

$\frac{1}{4}$ " nozzles.

Efficiency Curves.

Efficiency - per cents.

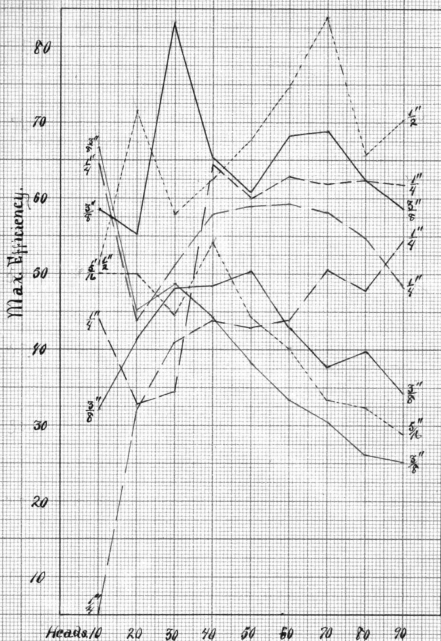


Revolutions per minute.

Backus.

Seymour and Whitlock.

Pelton.

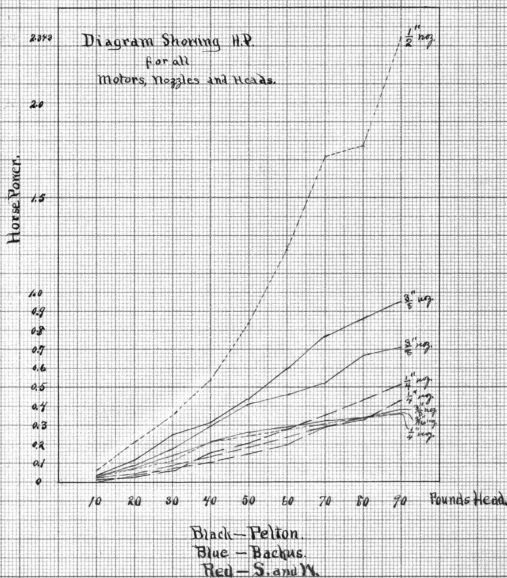


Characteristic Curves.

Plate III.

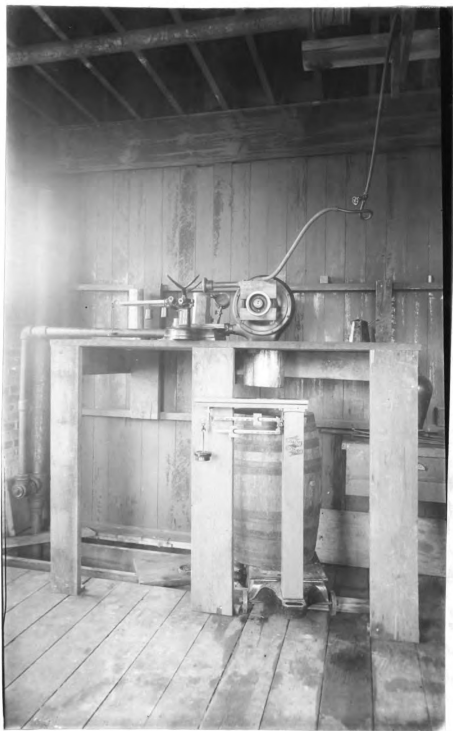
Ave. Max. Eff. { Pelton — 52.1%
 Backus — 43.1%
 S. and W. — 46.7%

Plate IV.



The determining points of these curves are directly over the heads shown and are connected by straight lines. The true curves would be continuous and would vary from the straight lines at intermediate points.

Pelton motor and apparatus



Pellon Motor and apparatus.

It will be seen that not in all cases was the point of best efficiency reached and thus the efficiency curves do not begin to fall off and indicate a smaller efficiency for a slower speed. Where, however, this point was reached in the course of the experiments, it was noticed that the motor gave every evidence of being working at its greatest capacity and ran with much unsteadiness and variation in speed. The experiments thus indicate that, for best efficiency, all motors should be run at their fullest capacity and at as low a speed as they will run and run steadily.

The most important point to be known in using water motors is the proper speed to run them in order to get the best efficiency. For, the horse power any motor is capable of delivering at its best efficiency being known, one can determine upon the size of motor and nozzle to be used to fulfil any conditions as to head, horse power required, etc. It then remains only to know the proper speed at which to run to give the maximum efficiency. For this purpose the following table was arranged to as nearly as it was possible to cover the data of the experiments on the different motors and results, the number of revolutions per minute being the most desirable to run each motor for all nozzles and heads.

13
Table showing Approximately the R.P.M. for Best

Efficiency for each Nozzle and Motor under all Heads.

Head.	Revolutions per minute.							
	1/4 inch nozzle			3/8 inch nozzle.			5/16 in. nozzle.	1/2 in. nozzle.
	Pelton.	Backus	S&W	Pelton	Backus	S&W	S&W	Pelton.
10	200		125	250	150	150	150	300
20	300	150	150	350	250	200	190	400
30	400	200	200	450	285	250	250	500
40	475	275	260	500	320	350	325	600
50	550	315	300	600	325	400	400	700
60	650	325	400	700	350	425	425	800
70	700	350	450	800	365	450	450	900
80	800	375	475	850	375	475	475	950
90	850	400	500	900	400	500	500	1000

Considerably more loss of power due to friction in the bearings was found in the Backus motor than in either of the others tested. In fact, with a 1/4 inch nozzle this motor could not be run unloaded with a five pound head, while very little power was necessary to run either of the others when unloaded.

The following are the average efficiencies for the three motors tested, as found by taking the maximum efficiency for each head for all nozzles used with each motor and averaging them:

<u>Motor</u>	<u>Efficiency</u>
Pelton - - - - -	51.1%
Boston - - - - -	48.1%
Sigbee and Whitlock - - -	48.8%

By far the greatest source of loss in any of the motors tested was in the friction of the water in the fore and aft position of the nozzle, especially in the Pelton. By reference to Plate 5, it will be seen that the openings in the nozzles for this motor are parallel sides for some distance before the water is released; the nozzles are thereby solid round bodies. This, in itself, causes some ill action, in all the water is utilized; as the nozzle is placed at an angle a large portion of the water, especially from the rear nozzles, does not quit in the same line, and some comes through the motor with its velocity and little decreased. Thus much power is lost. This, no doubt, was the original cause in reducing the efficiency of this motor below that of the Pelton motor. I believe the motor as now tested was sufficient, and is quite good for its age, as the water is not over 100 feet high. The efficiency of this motor is more than 40 per cent. This conclusion is substantiated by the fact that, if the water were 100 feet high, there would be no loss of water in the nozzles with a 1/4 inch diameter.

with a 1/8 inch nozzle; the maximum overall efficiency being about three per cent higher for the smaller nozzle.

Very respectfully,

July 20, 1908.

A. C. Jordan.

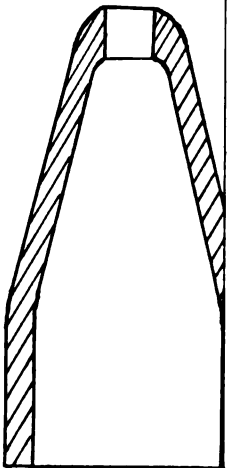
Seymour and Whitlock

22" Impact motor.

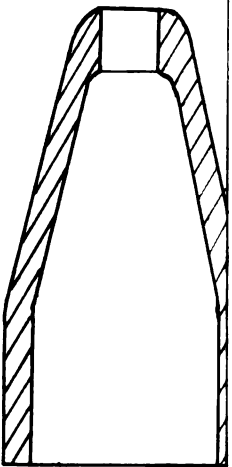
Plate VIII



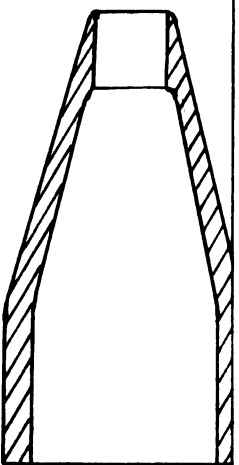
$\frac{1}{4}$ "



$\frac{5}{16}$ "



$\frac{3}{8}$ "

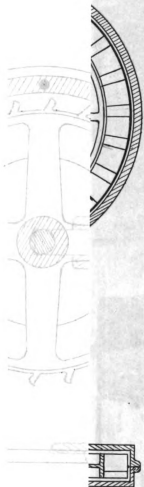


Seymour and Whitlock.

Seymour and Whitlock

22" Impact motor.

Plate VIII



12" R.

12" R.

12" R.

Seymour and Whitlock

22" Impact motor.

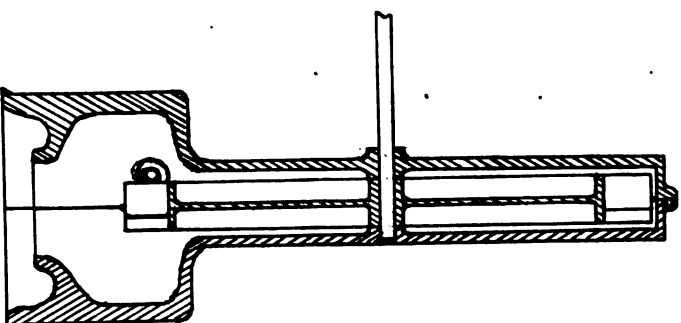
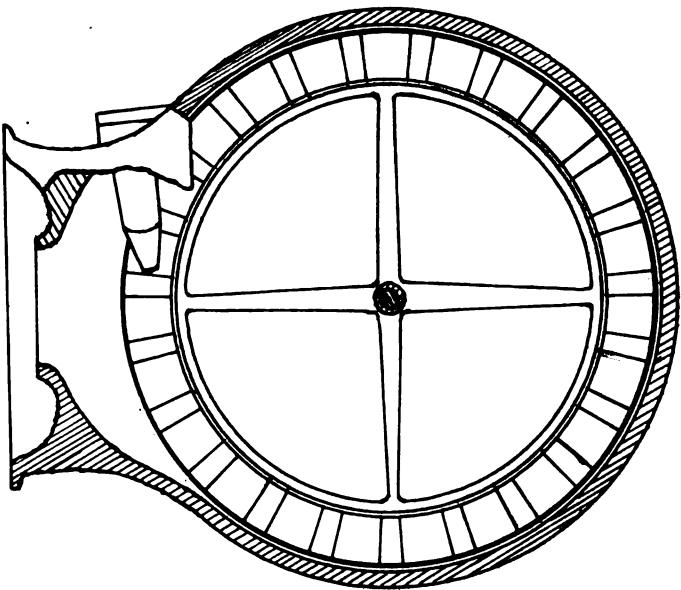
Plate VIII.



Seymour and Whitlock

22" Impact motor.

Plate VIII.

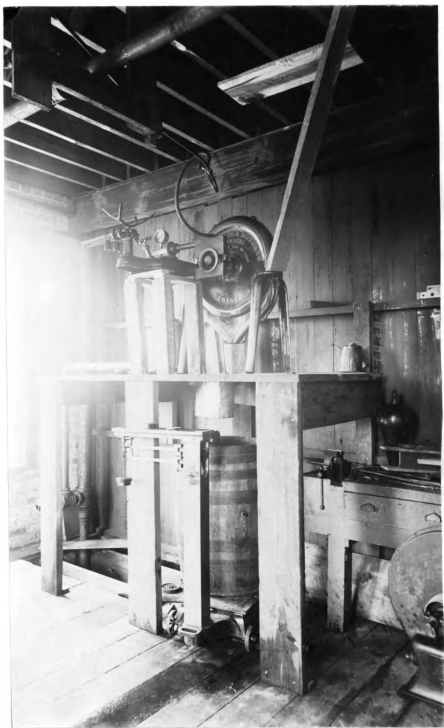


Showing manner of impact.

Scale— $\frac{1}{8}$

No. of cups — 22.

H.C. Burnham.



Backus Motor and apparatus.

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