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**Experimental Investigation of the Air
and Fuel Heating Devices Used on
The Case 15-27 Kerosene Tractor. , ,**

**A Report Submitted to
The Faculty of
MICHIGAN AGRICULTURAL COLLEGE**

By

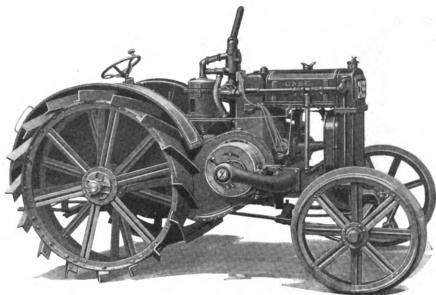
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**Candidates for the Degree of
Bachelor of Science.**

June, 1921

THESIS



CASE 15-27 KEROSENE TRACTOR

94097

EXPERIMENTAL INVESTIGATION OF THE AIR AND FUEL HEATING
DEVICES USED ON THE CASE 15-27 KEROSENE TRACTOR

PURPOSE

The purpose of this investigation was to study, experimentally, the air and fuel heating devices necessary to the efficient use of kerosene in tractor motors, especially, the devices used on the Case 15-27 Kerosene Tractor.

APPARATUS AND EQUIPMENT

The apparatus used in the investigation consisted of the following:

CASE 15-27 Kerosene Tractor, No. 42526.

Prony Brake, with its equipment.

Fuel Weighing Apparatus.

Thermometers.

Speed Counter.

Incidental equipment.

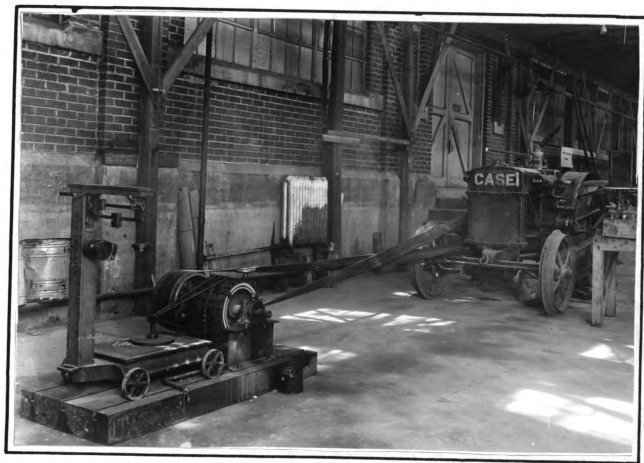


Fig. 1. VIEW OF APPARATUS.

THE CASE 15-27 KEROSENE TRACTOR NO. 42526

For our experimental work we secured, thru the M. A. C. Farm Mechanics department, the use of a stock 15-27 J. I. Case Kerosene tractor from the Branch office of the Company in Lansing. Mr. Miller, General Manager of the office, generously gave us the use of the tractor and the permission to make any tests we desired on the tractor.

The Case Tractor as-shown in Fig. uses a special designed intake and exhaust manifold. The details of this manifold are shown by the blue print in the envelope in the back of this report. By the use of the manifold, the temperatures of the vaporized mixture as it comes from the carburetor can be raised until it will completely burn in the cylinders of the motor. In addition to the heating within the manifold, the air is heated by an exhaust air heater before it enters the carburetor. The air-heater, -washer, and -passageways are shown in Fig. 2 and also on the blue-print in the envelope on the back cover.

PRONY BRAKE EQUIPMENT

The prony brake equipment consisted of a water-cooled brake pulley mounted on a two-bearing shaft, a belt pulley, brake and arm, and platform scales. This equipment was mounted on a heavy iron bed. A 5-inch rubber belt was used to connect the engine with the brake. This equipment is shown in the photograph Fig. 1.

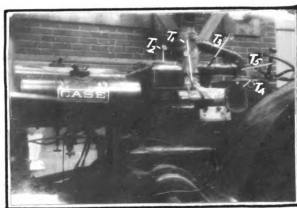
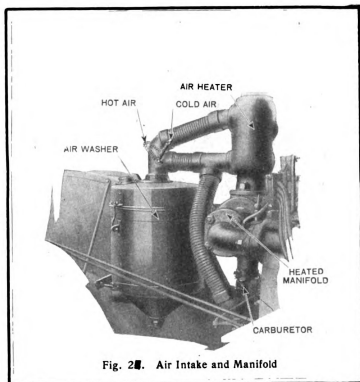


Fig. 3. THERMOMETERS IN PLACE.

- T1- Temperature of left manifold intake.
- T2- Temperature of right manifold intake.
- T3- Temperature of preheated air.
- T4- Temperature of vaporized mixture.
- T5- Temperature of incoming air.

FUEL WEIGHING EQUIPMENT

This equipment consisted of platform balances, fuel reservoir with stop-cock connections, and weights. This equipment can also be seen in the photograph Fig. 1.

THERMOMETERS

The thermometers used in this investigation were of Fahrenheit scale. Two were high reading mercury thermometers, reading to 400°, and the other three reading to 220°F_A. The two 400° thermometers were placed in thermometer wells in the manifold intake close up to the cylinder blocks. One 220 thermometer was placed in a well at a point in the passageway for the heated air. The third was placed in a well just above the air washer.

In our preliminary tests we used oil-thermometer wells. These wells were made of a piece of 1/4 inch copper tubing, 5 or 6 inches long, one end hammered shut and soldered oil tight. We found that in the manifold temperature wells the high temperature melted the solder and oil leaked out. To remedy this, instead of using oil we plugged the space around the thermometer tightly with asbestos paper. This type of well proved to be satisfactory as fluctuations in manifold temperatures were easily detected.

For the manifold thermometer wells, a short piece of copper tube closed at one end was pressed into a 2-inch piece of 1/4 inch threaded iron pipe. A hole was drilled and tapped for this pipe in the manifold intake in place of the priming cup.

The other thermometer wells were soldered in place.

INCIDENTAL EQUIPMENT

Incidental equipment such as speed counters, wrenchs, etc., need no explanation.

THE TESTS

After our preliminary tests had been made to determine the behavior of the tractor and other apparatus, we started the experimental tests. These tests were really divided into two main parts. The first part consisted of the tests made on the tractor without any change in its standard equipment. The second part consisted of the tests made after the standard equipment had been changed. The tests themselves were practically the same in both cases.

The change in the equipment for the second group of tests was this: the manifold was taken apart and the exhaust manifolds for the two outside cylinders were truned so as to exhaust the gases out into the air instead of out the exhaust pipe. Asbestos board was bolted to the ends of the main part of the exhaust manifold to cover the opening made by the removal of outside cylinder manifolds. Fig. 3 shows the tractor with the change made.

Both of the groups of tests were divided into three parts. The first division of tests under this classification were the tests made using the air preheater. The second division were the tests made with the air preheater off. The third division were the tests made using air taken in at the carburetor directly from the room. This classification might be more clearly

understood if put in this way: the air taken in at the carburetor was heated to a high temperature under the first division of tests, was heated slightly under the second division, and under the third division the air was taken into the carburetor at room temperature.

DESCRIPTION OF TEST

Before any of the tests were begun, the engine was started on gasoline and allowed to run a few minutes under load. As soon as the motor became hot enough to vaporize the kerosene, the gasoline was turned off and the kerosene turned on. The engine was always started with heated air. The tests were never started until the engine had run long enough to adjust itself to the load and its speed had become fairly constant. At the beginning of each test, the fuel in the fuel reservoir on the balances was weighed, just at the second the time was taken, the thermometers having been placed in their proper places before the starting of the test. Every five minutes the temperatures were read and recorded and every ten minutes the speed of the brake was taken. The brake load was kept constant during the test, one man doing nothing but watch and adjust the brake. At the end of each test, the unused fuel in the fuel reservoir was weighed just as the time was taken as in the beginning of the test. The barometer readings were recorded with the other data taken. All measurements, weights, time, etc., were taken with great care, so that the results of the tests might be as accurate as possible.

From the data obtained for each test, the brake horse

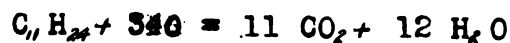
power, the thermal efficiency, and the fuel consumption was calculated. Every test was made in the manner described so that we are reasonably sure that the averages which are the results of all the tests in each group are data that show the true performance of the tractor. The averages were made showing the results of each test in each group and from them the curves were made. The curves show graphically all the average results of our tests.

DESCRIPTION OF FUEL ANALYSIS

A distilling apparatus of 100 cc. capacity was used to determine the different vaporization points of a composite sample of the kerosene used in the tractor motor.

The vaporization points so obtained in the chemical laboratory were duplicated and the results plotted on a graph, using volume in cubic centimeters as abscissa and temperature in degrees centigrade as ordinate. The results so plotted show a wide range of temperatures. Within this range of temperature there are two hydrocarbon compounds, $C_{11}H_{24}$ and $C_{12}H_{26}$. The carbon content in these two compounds is 84.7% and 84.6% respectively. The hydrogen content is 15.3% and 15.4%. The average theoretical B. T. U. value of these compounds is 20,376.

Assuming complete combustion the following method was used to calculate the B. T. U. value per lb. of fuel.



$$\text{Carbon Content} = \frac{132}{156} = 84.7\%$$

$$\text{Hydrogen Content} = \frac{24}{156} = 15.3\%$$

$$\text{Heating value } Q = 14,600C + 52,230(H - \frac{O}{8})$$

$$\text{Heating value} = (14,600 \times 84.7 + 52,230 \times 15.3)$$

The same method was used with C H and average B. T. U. used in our calculations was 20,376, the average B. T. U. value of the two compounds.

The specific gravity was determined by weighing a portion of the composite sample in a specific gravity bottle on an analytical balance. The specific gravity was found to be 0.8038. The weight per gallon was 6.70 lbs. at room temperature of 74 F.

CALCULATIONS

The calculations necessary to complete the report were quite simple. The calculations that were used are:

Brake Horse Power

$$\text{Brake Constant} = .0004$$

$$\text{Brake Horse Power} = .0004 \times \text{R.P.M.} \times \text{Load}$$

Thermal Efficiency

$$\text{By fuel analysis, Kerosene} = 20,376 \text{ B.t.u.}$$

$$\text{Per lb. 1 H. P. per hour} = 2,546 \text{ B.t.u.}$$

$$\therefore \text{Thermal Efficiency in \%} = \frac{2,546 \times \text{Horse Power per hour}}{20,376 \times \text{Fuel Consumption (lbs. per hour)}}$$

FUEL CONSUMPTION

$$1 \text{ gallon} = 6.70 \text{ lbs. Kerosene (By Sp. Gr.)}$$

$$\therefore \frac{\text{lbs Kerosene used 1 hr.}}{6.70} = \text{gallons used 1 hr.}$$

$$\frac{\text{Horse Power 1 hr.}}{\text{Gallons per hr.}} = \text{H. P. hrs. per gal.}$$

CONCLUSIONS

Air Conditions:

(1) The air conditions under which these tests were run closely approximate the average conditions of air temperature, pressure, and humidity under which tractors in this part of the country are likely to operate.

Air Heater:

(1) In starting the engine the air heater is advantageous because it aids carburization until the engine is thoroughly warmed.

(2) Our tests show that the air is heated to quite an extent with the air damper in the cold air position.

(3) Heated air has a higher saturation point than cold air, consequently, when passed thru the carburetor it absorbs more fuel than is used in the engine cylinder. This excess fuel is vaporized in the exhaust manifold. Its latent heat of vaporization is probably responsible for the lower manifold temperatures which we obtained when using heated air compared to the higher temperatures which we obtained when taking cold air at room temperature in at the carburetor.

(4) Thus, the use of heated air tends to lower the thermal efficiency and to increase the fuel consumption.

Air Washer:

(1) The temperature conditions within the engine are not effected by the use of the air washer.

The Use of Cold Air at the Carburetor:

(1) Our tests show that the use of air at room temperature in the carburetor after the engine has been thoroughly heated increases the temperature in the manifold, decreases the fuel consumption, and increases the thermal efficiency.

(2) That in order to use the air washer and at the same time take in air at room (atmospheric) temperature, it would be necessary to pass the air from the air washer to the carburetor without its being heated.

The Effect of Lower Manifold Temperatures:

(1) Our tests show that the lowering of the temperature within the manifold (by by-passing some of the exhaust gases) and at the same time using air at the carburetor at room temperature increases the thermal efficiency and decreases the fuel consumption.

1.

Air Preheated before entering Carburetor by
Preheater.

742 80 30

3a.

304	332	166	130	
320	342	168	129	880
322	345	168	129	
326	348	166	128	874
328	348	168	128	
<u>330</u>	<u>350</u>	<u>170</u>	<u>128</u>	<u>860</u>

Ave. 322 344 169 129 72 29.25 4.36 6.35 871 27.8 11.9

Same as (3a) but with better
adjustment of carburetor.

742 80 30

3a1

324	338	164	126	
327	340	166	128	900
335	346	167	126	
335	348	169	128	892
334	346	168	129	
<u>334</u>	<u>344</u>	<u>168</u>	<u>129</u>	<u>880</u>

Ave. 333 345 167 128 62 29.25 4.36 6.55 891 28.6 12.2

The kerosene for these tests weighed 6.70 lbs.
per gallon. Fuel consumption given per hour. Temperature
in degrees F.

2.

With Preheater as before.

742

80

30

5a

331	364	184	144	
333	366	185	145	880
355	367	186	146	
338	368	186	145	900
338	370	186	146	
<u>338</u>	<u>369</u>	<u>186</u>	<u>146</u>	<u>880</u>

Ave. 335 367 186 145 84 31.25 4.66 6.52 890 28.5 11.8

With Preheater and Air Washer.

742

80

30

6a.	352	300	180	144	
	360	302	186	146	
	364	302	186	147	860
	364	305	185	147	870
	367	304	186	146	
	<u>367</u>	<u>306</u>	<u>186</u>	<u>148</u>	<u>884</u>

Ave. 365 305 184 145 74 31.13 4.65 6.03 871 28.0 11.7

The kerosene for these tests weighed 6.70 lbs. per gallon. Fuel consumption given per hour. Temperature in degrees F.

1427 745

3.

The exhaust from the two outside cylinders was directed into the air instead of into manifold heater. With Preheater.

745 80 30

10a

246	242	160	134									928
252	257	161	136									908
256	260	163	137									
258	264	164	138									904
257	263	163	138									
<u>258</u>	<u>264</u>	<u>163</u>	<u>138</u>									<u>910</u>

Ave. 255 258 162 137 91 30.63 4.68 6.11 912 29.2 11.8

Made without the air Preheater. Air preheated to some extent in the air-passage ways.

742 80 30

2b

308	296	138	99									
306	296	141	100									906
309	301	144	101									
307	300	144	102									920
306	302	140	102									
<u>308</u>	<u>304</u>	<u>141</u>	<u>102</u>									<u>910</u>

Ave. 307 298 140 101 70 25.5 3.81 7.66 913 29.2 14.8

The kerosene for these tests weighed 6.70 lbs. per gallon. Fuel consumption given per hour. Temperature in degrees F.

4.

Without Air Preheater.

743

80

30

4b

322	340	136	97	
319	338	139	97	920
318	338	140	98	
³ 22	340	142	99	920
318	337	142	100	
<u>317</u>	<u>336</u>	<u>141</u>	<u>99</u>	<u>910</u>

Ave.	319	338	141	98	62	25.13	3.75	7.80	912	29.2	14.50
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Without Air Preheater.

742

80

30

5b.	325	360	152	117	
	326	364	160	118	920
	326	364	160	120	
	326	364	160	120	900
	328	365	162	121	
	<u>329</u>	<u>360</u>	<u>161</u>	<u>121</u>	<u>910</u>

Ave.	327	364	159	120	85	27.25	4.07	7.18	910	29.2	13.3
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The kerosene for these tests weighed 6.70 lbs. per gallon. Fuel consumption given per hour. Temperature in degrees F.

5.

Without Air Preheater.

745 80 30

8b.

325	304	138	112
330	306	139	114
330	310	140	115
332	314	141	113
333	314	141	114
<u>336</u>	<u>312</u>	<u>140</u>	<u>113</u>

920

910

910

Ave.	331	309	140	113	76	25.75	3.84	7.60	913	29.2	14.2
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Two outside cylinders exhausting into the air.

745 80 30

10b

256	258	180	120
259	250	153	122
258	260	156	124
258	260	158	124
258	260	157	123
<u>258</u>	<u>259</u>	<u>156</u>	<u>123</u>

920

900

912

Ave.	257	259	156	123	92	27.13	4.05	7.21	912	29.2	13.4
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The kerosene for these tests weighed 6.70 lbs. per gallon. Fuel consumption given per hour. Temperature in degrees F.

6.

Experiments

Cold Air at room Temperature taken at the Carburetor.

	742		80					30		
2c	334	322	89							
	342	328	90					934		
	342	331	90							
	342	331	90					918		
	340	330	90							
	<u>338</u>	<u>330</u>	<u>90</u>					<u>916</u>		
Ave.	339	328	90	70	20.00	3.01	9.77	920	29.4	18.3

Same as above.

	742		80					30		
4c	344	360	86							
	346	364	86					904		
	348	368	87							
	350	370	87					910		
	352	372	89							
	<u>352</u>	<u>372</u>	<u>88</u>					<u>905</u>		
Ave.	347	368	87	60	19.88	2.96	9.77	906	29.0	18.25

The kerosene for these tests weighed 6.70 lbs. per gallon. Fuel consumption given per hour. Temperature in degrees F.

7.

Air taken in a Room Temperature thru the carburetor.

742

80

30

. 5c

338	376	104	
332	372	105	895
333	372	105	
328	369	104	910
325	364	104	
<u>325</u>	<u>366</u>	<u>104</u>	<u>914</u>

Ave.	330	370	104	85	21.75	3.25	8.91	906	29.0	16.75
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Same as above.

737

80

30

7c.	339	350	105	
	342	356	110	930
	344	360	110	
	343	362	113	920
	339	360	114	
	<u>339</u>	<u>360</u>	<u>115</u>	<u>914</u>

Ave.	341	358	113	86	21.88	3.26	9.02	920	29.4	16.9
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The kerosene for these tests weighed 6.70 lbs. per gallon. Fuel consumption given per hour. Temperature in degrees F.

8.

Air taken in at Room Temperature in the Carburetor.

	737		80				30
8c							
	341	328	108				
	341	333	107				912
	340	336	108				
	338	337	110				900
	335	333	108				
	<u>334</u>	<u>332</u>	<u>107</u>				<u>920</u>
Ave.	338	333	108	80	21.00	3.13	9.3
							910
							29.1
							17.30

Air taken in thru Caruretor as before.

	742		75				30
9c							
	346	345	116				
	344	339	116				904
	349	347	120				
	347	344	120				904
	344	344	120				
	<u>344</u>	<u>345</u>	<u>121</u>				<u>914</u>
Ave.	346	341	120	95	20.5	3.06	8.91
							907
							27.2
							16.35

The kerosene for these tests weighed 6.70 lbs. per gallon. Fuel consumption given per hour. Temperature in degrees F.

9.

Two outside cylinders exhausting in the air.

	745		80		30	
10c						
	262	262	108			
	274	275	110		920	
	280	281	112			
	283	283	114		920	
	283	283	114			
	<u>282</u>	<u>283</u>	<u>114</u>		<u>910</u>	
Ave.	275	276	112	95	19.88	2.96
				9.8	916	29.3
						18.4

Same as above.

	746		80		30	
11c	277	256	110			
	277	252	110			
	278	256	110			
	278	258				
	278	260				
	279	276*				
	280	277 ^A				
	280	278				
	279	276				
	278	278				
	279	278				
	<u>278</u>	<u>277</u>				
Ave.	278	277	110	95	20.19	3.00
				9.8	9.17	29.4
						18.05

* Thermometer not in tight.

^A Changed.

The kerosene used for this test weighed 6.70 lbs.

Fuel consumption given per hour. Temperature in degrees F."

AVERAGE OF TESTS.

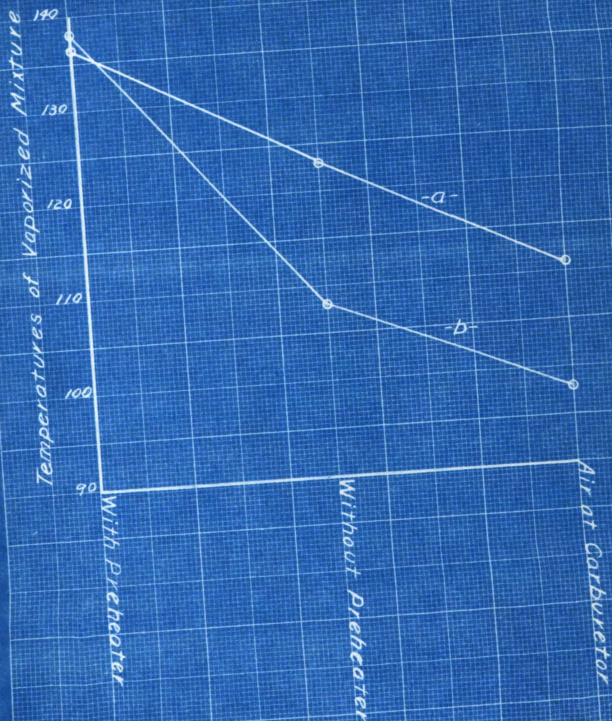
Using Preheater:

3a	322	344	169	129	72	4.36	6.35	28.8	11.9
3a	333	345	167	128	62	4.36	6.55	28.6	12.2
5a	335	367	186	145	84	4.66	6.52	28.5	11.8
6a	<u>365</u>	<u>305</u>	<u>184</u>	<u>145</u>	<u>74</u>	<u>4.65</u>	<u>6.03</u>	<u>28.0</u>	<u>11.7</u>
Ave.	339		174	138	73	4.51	6.36	28.2	11.9

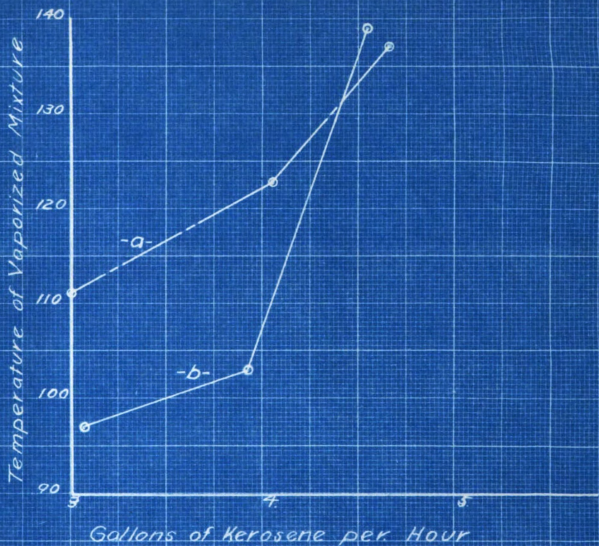
Without Preheater but thru passageway.

2b	307	298	140	101	70	3.81	7.66	29.2	14.8
4b	319	338	141	98	62	3.75	7.80	29.2	14.5
5b	327	364	159	120	85	4.07	7.18	29.2	13.3
8b	<u>331</u>	<u>309</u>	<u>140</u>	<u>113</u>	<u>76</u>	<u>3.84</u>	<u>7.60</u>	<u>29.2</u>	<u>14.2</u>
Ave.	324		145	108	73	3.87	7.56	29.2	14.2

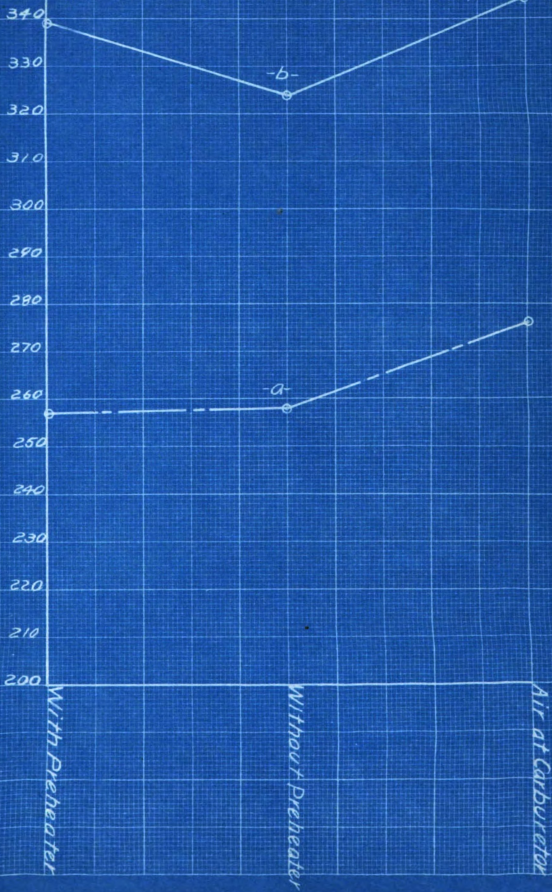
Vaporized Mixture Temperatures
-a- With & -b- Without Exhaust Bypassed



*Relation Between Temperature of
Mixture and Fuel Consumption
-a- With & -b- Without Exhaust Bypassed*



Temperatures in Manifold
a- With & b- Without Exhaust Bypassed

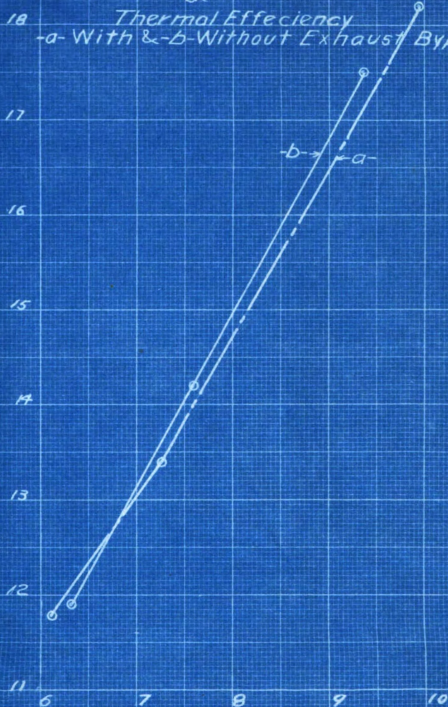


Relation Between HP Hrs. Per. Gallon of Kerosene &

Thermal Efficiency

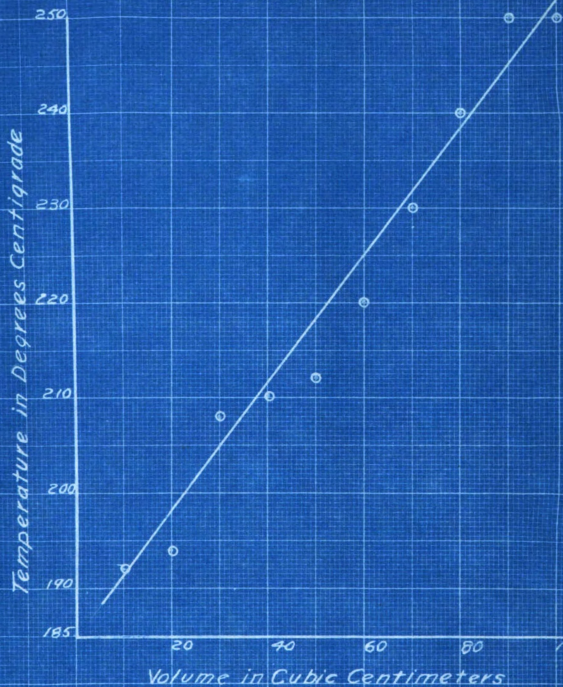
-a- With & -b- Without Exhaust Bypassed

Thermal Efficiency in Per. Cent.

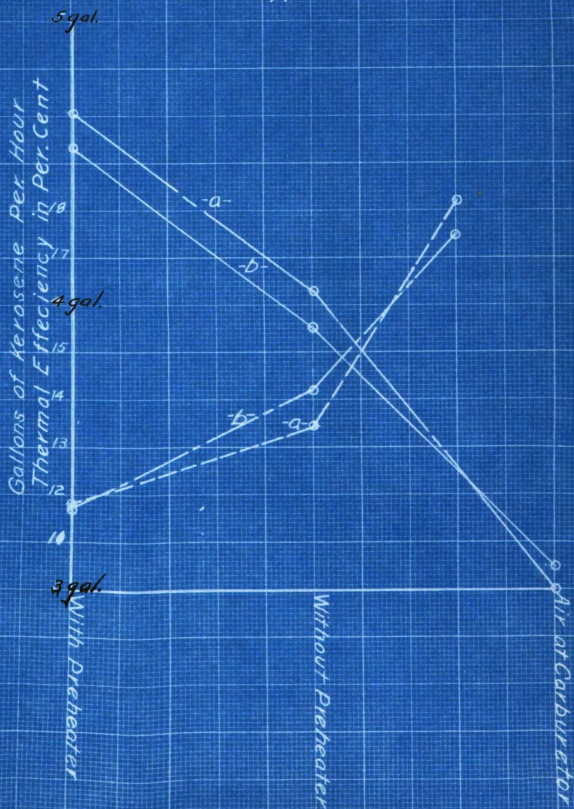


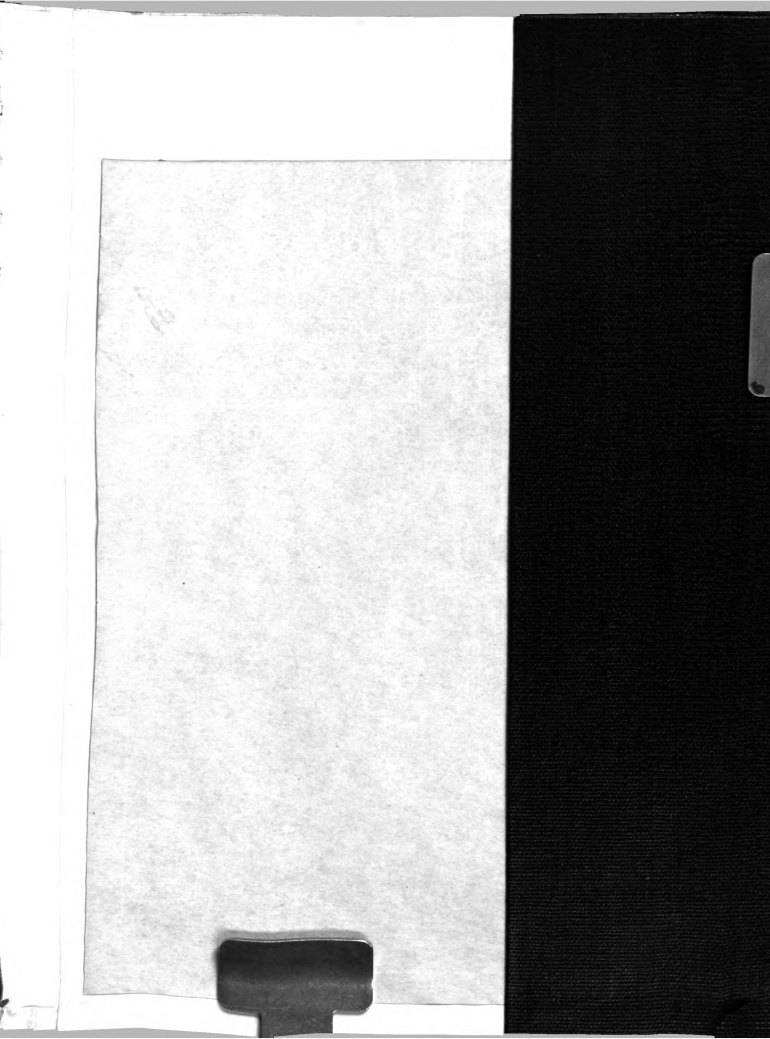
Horse Power Hrs. Per. Gallon of Kerosene

*Vaporization Points of Kerosene
Used in This Experimental Test*



Fuel Consumption & Comparison
Between
Thermal Effeciencies-a-With & b-Without
Exhaust Bypassed





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