A STUDY OF MEMBRANE CURING COMPOUNDS

Thesis for the Degree of B. S.

MICHIGAN STATE COLLEGE

L. T. Oehler W. A. Bradley

1943

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A Study of

Membrane Curing Compounds

A Thesis Submitted to

The Faculty of MICHIGAN STATE COLLEGE

of

AGRICULTURE AND APPLIED SCIENCE

bу

L. T. Oehler

W. A. Bradley

Candidates for the Degree of

Bachelor of Science

June 1943

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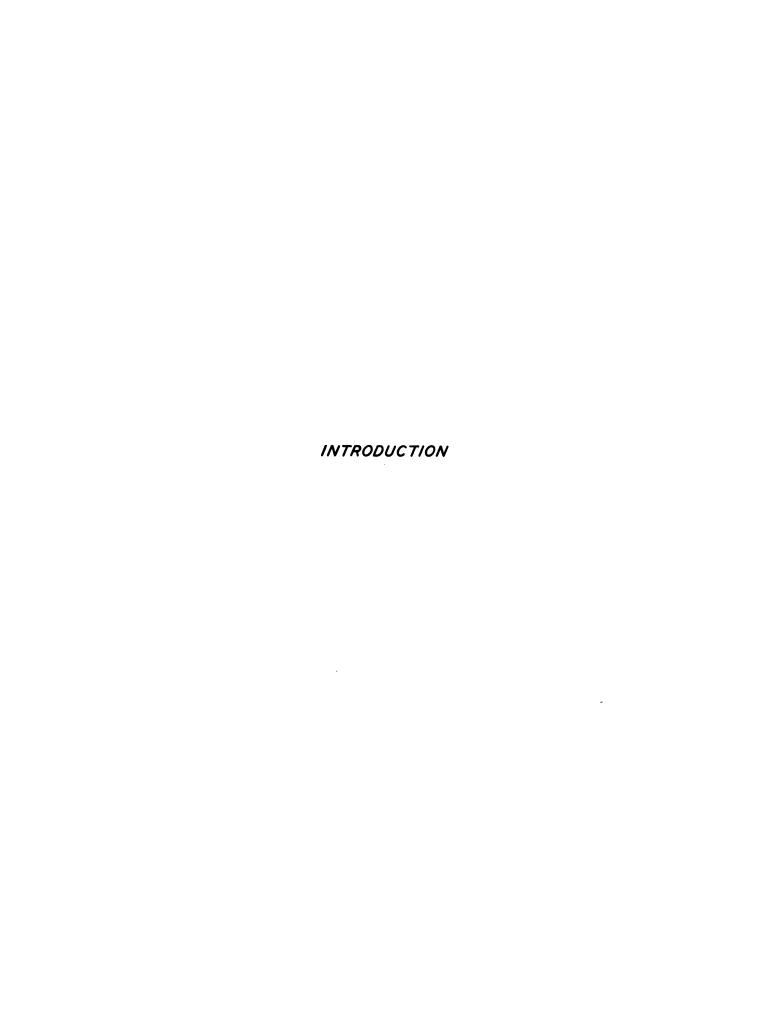
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We would like to acknowledge the aid given to us in this study by the members of the Michigan State Highway Department research division, and especially we wish to express our appreciation to Mr. E. A. Finney and to Mr. C. C. Rhodes for the invaluable suggestions and assistance given to us throughout this study.

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The coming of the war has brought about many changes in the lives of the people of this nation! Many luxuries have been dispensed with; even some of those articles which were once looked upon as necessities are now disappearing. In every field of endeavor it has become necessary to take short cuts which will involve the use of less and less of certain critical materials which either are unobtainable because of the war or are being used in enormous quantities by the Army and the Navy and by those involved directly in the furnishing of materials to the armed forces. Rubber became precious and nearly unobtainable; steel reinforcement for buildings became rare and steel shapes for any purpose whatsoever were greatly limited in both variety and quantity; other materials similarly were limited.

The need for new construction, however, didn't decrease with the same degree of rapidity as did the supply of construction materials. New buildings had to be built to hold the industries and to house the families of the workers; new roads were essential for the transportation to and from the growing industries; new air bases were needed to provide for the training of pilots to fly the hundreds of planes pouring out of the new industries; and, in turn, new roads had to be built to the bases. Thus, the need rose for the materials while the supply of these goods was decreasing. The engineers and industrialists of the United States soon recognized the problem before them and immediately started the development

of substitutes for the no longer obtainable products. The huge roof trusses of aircraft hangars, previously made of steel, were successfully fabricated out of wood; concrete slabs for roadways, instead of being reinforced with steel, were redesigned to eliminate that essential material; and similarly, all over the industrial nation, substitutes and new methods were found which took the place of the old--and did the job!

One of the problems which soon appeared in connection with the construction of new buildings and roads was that of the maximum strength and durability must be cured for a period of time under controlled conditions of moisture and temperature. Of the several methods used, the most satisfactory, or at least the most widely used, was the use of burlap sacks, sprinkled and kept wet for a period of from seven to ten days. Burlap, however, disappeared from use for the curing of concrete soon after the opening of the war. Cotton material and paper can still be used to some extent, but their use is limited for certain classes of work and in some localities. Bituminous curing materials are no longer available at all in the East and the restrictions are spreading to other sections of the country.

Of the methods yet remaining for the curing of concrete slabs, the best has not definitely been decided. Ponding and coverings of wet earth undoubtedly retain the water in the concrete during the curing period, but it isn't possible to apply wet earth to the surface of freshly-poured concrete without ruining the finish of the concrete; thus, the curing isn't applied until set occurs and by that time, much of the water has been drawn out of the concrete and the damage has already

been done.

Paper, still used in some cases, also has its problems. As with burlap, a definite period must elapse before application, and during the period, valuable water is lost. Also, water must be sprinkled onto the paper during the curing period, since drying out of the paper will cancel its effectiveness. This continual spraying introduces the human element, which is often apt to introduce error.

Another curing method, not entirely new but being promoted extensively since the shortage of other materials, makes use of a thin membrane, supposedly quite impervious to water, to secure retention of moisture during the curing period. It is this group of compounds which we have chosen to investigate.

The so-called membrane curing materials were used a decade before the development of the colorless membranes of today. Even as recently as 1938, when membrane curing compounds were mentioned, the bituminous compounds such as coal-tar, pitch, cutback asphalt, and asphalt emulsion, were usually understood. The first patent on membrane curing was granted to Paul Lechler of Stuttgart, Germany (German Patent No. 537,134) in 1921. The first American patent (No. 1,684,671) was issued in 1928. These first products differed greatly from the colorless compounds used today. It is quite natural that these compounds were first used in the semi-arid regions of the West, where it would be difficult to obtain sufficient water for curing purposes.

Investigations conducted in various laboratories and corroborated by use, demonstrate that certain of the coal-tar and asphalt cutback materials were

quite effective for the retention of concrete mixing water and, in some respects, a satisfactory substitute for water curing.

There were many disadvantages however, to these bituminout coatings. First, a bituminous coating is very objectionable for use on surfaces where the natural appearance is desirable; for example, highways. Secondly, the black bituminous coating causes very high heat absorption which, in time, produces excessive cracking when it is exposed to the sun's rays. Often these bituminous materials would be put on too heavily and would leave a slick black surface, which was dangerously slippery when wet.

Emulsified asphalt by its very nature will not form an impervious membrane. Since emulsified asphalt is asphalt suspended by a water solution, when the water dries, there are millions of small openings through which the moisture can escape from the concrete. Another disadvantage of bituminous materials is that the material remains tacky for weeks after its application, even in the summer months.

The first clear membrane curing compounds had such low water retention properties that engineers insisted that wet burlap or cotton mats be used for the initial twenty-four or even seventy-two hour period. Of course, this destroys one of the basic advantages of membrane curing compounds, because it is claimed that they may be applied immediately after fin-

¹ Technical Progress Section, <u>Journal of the American Concrete</u> Institute, Vol. 14, No. 4, p. 377.

²H. S. Meissner and S. E. Smith, "Concrete Curing Compounds"

<u>Journal of the American Concrete Institute</u>, Vol. 9, May-June 1938,
p. 549.

ishing, while wet burlap cannot be applied for the first several hours, The product sold in the West was a paraffin-vegetable cil base cut with a petroleum solvent. These initial products, besides failing to maintain a sufficient amount of water also imparted a blotched discoloration which is ascribed to the reaction of calcium bydroxide with the fatty acids of the compounds, resulting in the formation of calcium salts of the fatty acids. Besides giving an unsightly appearance to the surface, this reaction was detrimental to the concrete. Since the early compounds failed to give the desired results, further research was instigated with the following purposes in mind:

- 1. Immediately and effectively seal the surface against surface dehydration, and provide maximum retention of the original mixing water within the concrete.
- 2. Be chemically inert to any constituents of concrete.
- 3. Produce concrete having compressive and flexural strengths equal to 14-day water curing.
- 4. Produce concrete surfaces having erosion and abrasion resistance equal to 14-day water curing.³

In several of these purposes the manufacturers have made considerable progress. The water retention properties have been improved, chemically inert compounds are used, and the compression and abrasion resistance are comparing favorably

¹Technical Progress Section, <u>Journal of the American</u> Concrete Institute, Vol. 14, No. 4, p. 378.

²Ibid, p. 378

Deacon, Wm., President of Solvents and Plastics Co. Taken from a reply to letter requesting information.

with water curing. Here are some of the advantages now claimed by the producers for their type of product:

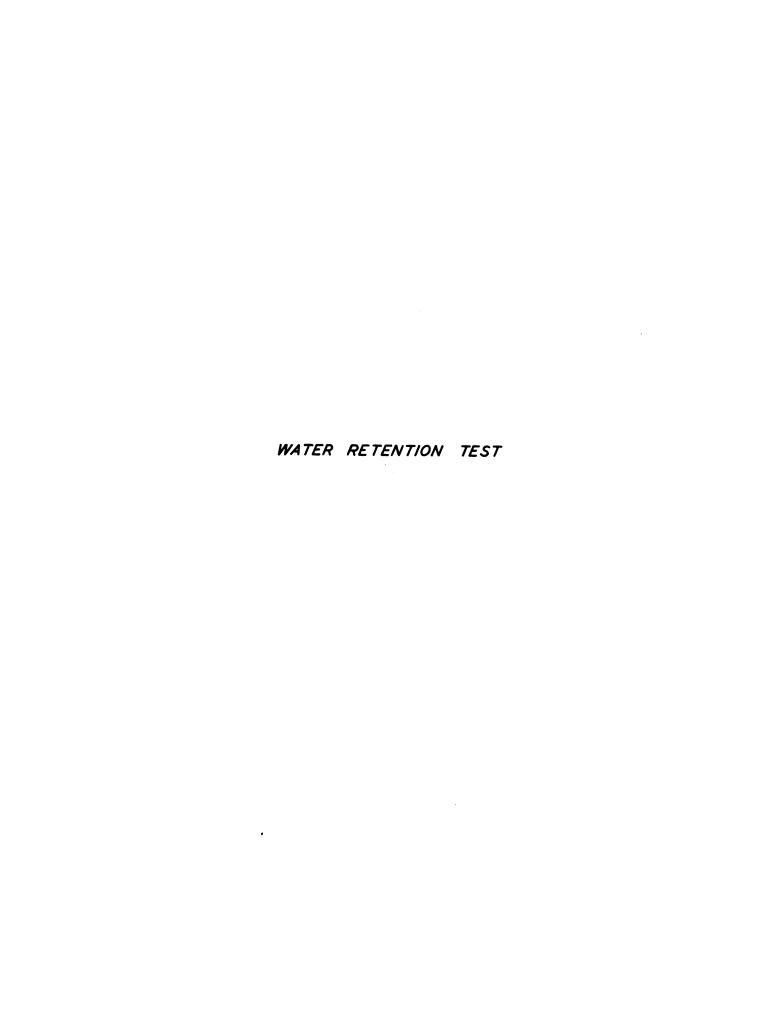
- 1. High early water retention. The fact that the compound may be applied immediately after finishing (no waiting for concrete to set) gives it at least one to three hour's start on other curing methods such as burlap or cotton mats.
- 2. Eliminates the burden and expense of prolonged supervision.
- 3. Its method of application is easy. A spray gun, hand or pressure type, may be used. It may be applied to vertical surfaces, the under side of concrete bridges, and other places where other curing methods cannot be used.
- 4. Keeps work area dry and prevents all delay incident to sloppy working conditions.
- 5. Avoids the possibility of decompaction through wet subgrade.
- 6. Effects definite economics in cost and adds materially to the speed of construction.
- 7. No after expense. After the material is applied, the job is completed with no expense of recleaning and storage of the materials.
- 8. It produces concrete of high strength with a maximum performance expectancy.

Not all of the above claims of manufacturers are to be taken as established facts, for when the shortage of essential materials necessitated a substitute, every manufacturer producing a compound which might, by remote chance, find a market as a curing agent, started to promote it. Many of the claims made for the various compounds were doubtful, and at best only the hopeful dreams of manufacturers expressed in print to serve as come-ons for unwary buyers.

In this study, we propose to test some of the better known commercial compounds and to establish, at least in our

own minds, which of them best fulfills the requirements of a good curing compound; and incident to this determination we hope to find a suitable method for testing in the laboratory any new compounds which may be brought out in the future, so that they may be evaluated by the same standards as their forerunners.

That is, in general, our purpose in this study.



THE WATER RETENTION TEST

Since it has long been recognized that the strength of Portland Cement Concrete is greatly affected by the hydration of the cement, a Water Retention Test seems a logical and fair method of testing the efficiency of various curing materials. The ideal concrete mix is the mix with the least water in relation to cement and yet providing a mix which is thoroughly plastic and workable. Abrams' water-cement-ratio law is usually stated as follows: "With given concrete materials and conditions of test, the quantity of mixing water used determines the strength of the concrete, so long as the mix is of a workable plasticity." After this mixing water is once added, everything possible should be done to retain it, for this retention of water during the formation period of the concrete is the greatest factor affecting the resultant concrete. This, in brief, is the purpose of curing.

Water retention is necessary, or the highly complicated chemical reactions taking place during the hydration of the cement will necessarily be retarded due to a lack of sufficient water. All the mixing water in the concrete, however, does not chemically combine; therefore these five classifications have been used:

- 1. There is free water that is only enclosed in the hardened cement and whose vapor pressure is somewhat reduced as a result of dissolved substances, but which is otherwise practically identical with pure water.
- 2. A certain amount of the water is fixed by the dis-

Abrams, D.A., "Design of Concrete Mixtures", Materials Research Laboratory, Lewis Inst. Bull. 1.

solved and solvated substances and more or less firmly attached to these.

- 3. Further, a part of the water functions as capillary-bound water with a vapor pressure varying according to the degree of dryness of the cement and the size of the capillaries.
- 4. A certain amount of the water is further bound by adsorption at the surfaces of the solid phases and is found engaged in varying degrees according to its nearness to the surfaces and the nature of these.
- 5. Finally, there is chemically bound water engaged in the chemical structure of the solid elements. 1

The water available for evaporation is affected by the rapidity with which these chemical reactions take place, for the
gypsum in the cement ties up water in ten to fifteen minutes,
the tricalcium silicate, tricalcium aluminate and the tetracalcium alumino ferrite bind the water in chemical combination
in twenty-four hours and the dicalcium silicate may continue
to bind water for several years.

If an evaluation of the quality of various membrane curing compounds is desired, a fair and equitable water retention test seems to be the logical solution. The problem at the first casual glance seems to be only a matter of laboratory technique, but in the ultimate analysis there are so many factors acting to influence the solution, that many variables have to be studied and analyzed, and others converted to laboratory controlled constants.

As the American Society for Testing Materials is usually considered the authority in matters of testing procedure, a

Staff of Research Division, Michigan State Highway Dept., Membrane Curing Report, May 28, 1942

study of their Tentative Method of Test for the Efficiency of Materials for Curing Concrete (C 156-40T) is of primary importance. This tentative test procedure, however, is looked upon by many laboratories with disfavor. They usually explain that it was disregarded by their laboratory because it was not definite enough on several important points, that it requires too large specimens, and that uniformly consistent results cannot be obtained. Perhaps this test procedure does need more clarification. Its inadequacy is probably due to the fact that it was not specifically designed for membrane curing materials, and such a broad test cannot give the required This has led to a confusing array of testing procedures. Diversity is the rule rather than the exception. To give only a few examples: Battenfield's Laboratory suggests slight modification of A.S.T.M. C 156-40T; Truscon Laboratory uses greater variations from A.S.T.M.; The War Department, represented by the Cincinnati and Mount Vernon Testing Laboratories, and also the Bureau of Reclamation, have still more variations.

With this labyrinth of diversity the only logical way that an analysis of such testing procedure can be made is to consider the factors that influence the test, and then point out how the different testing laboratories have tried to control these factors. In my opinion the most important of these are:

- 1. Proportioning of mix
- 2. Aggregate grading
- 3. Shape of moulds

- 4. Size of specimens
- 5. Methods of finishing
 - (a) Strike-off
 - (b) Troweling
 - (c) Wood float
 - (d) Brushing
- 6. Time of application of membrane
- 7. Rate of application
- 8. Methods of applying membrane
- 9. Storage of specimens -- Control cabinet
 - (a) Temperature
 - (b) Humidity
 - (c) Air flow

The following discussion will center about these points, and taken up in the order necessary in the organization of the test.

It is generally recognized that the storage of the specimens during the test will greatly affect the water lost. However, several laboratories do not seem to take a sufficient interest in the matter of developing a test that may be repeated time after time with the same results. By this, I mean that they have tests which may compare various materials at the same time, but the results are not reproducible, because the conditions are not held constant. The three conditions that must be held constant are the temperature, the humidity, and the air flow. The A.S.T.M. Test specifies that these conditions must be as follows: "Immediately after moulding, the mould and the specimen shall be weighed to the nearest gram and placed in an atmosphere maintained at a temperature of one hundred degrees Fahrenheit (100°F.) plus or minus five degrees (5°F.) and at a relative humidity con-

trolled within the limits of thirty to thirty-five percent (30-35%). Means shall be provided for circulating the air."

If a test is to be designed that may be used in every laboratory in the country at different times with as nearly as possible comparable results, the conditions must be controlled more closely than this.

We will consider first the temperature. Since this is easily regulated. it seems careless for several laboratories to fail to attempt more accurate control. Truscon has improved on the A.S.T.M. Test in this respect by stating in their test that the temperature must be regulated to plus or minus five-tenths degree (.5° F.).² The War Department specifies that the temperature of the cabinet should be ninety degrees plus or minus two (90 + 2° F.). The control range is satisfactory, but I see no reason why the temperate should be changed from the 100° F. of the A.S.T.M. procedure. The Bureau of Reclamation's procedure is probably the easiest to comply with, and one which would give only a comparison test under varying conditions. They use no cabinet, but state: "The room temperature should be operated on a 24 hour cycle. alternating between 120° F. maximum and 75° F. minimum." It is presumed that this variation is to similate the temperature

¹ Tentative Method of Test for Efficiency of Materials for Curing Concrete, American Society for Testing Materials, 1940 Supplement, p. 264.

²Truscon Laboratory uses an incubator as for hatching eggs, as their control cabinet and endorses its use (Brower Cabinet No. 42-600).

⁵Bureau of Reclamation Specifications for 45-Percent Solids Clear Curing Compounds.

range of the desert regions of the West, but since the specimens lose moisture much more rapidly the first few hours, it would be necessary to mix the specimens at exactly the same time each day or comparable results between different tests would not be obtained.

The next important factor that must be controlled in the storage of the specimens is the humidity. Again various laboratories differ. As noted before, the A.S.T.M. Test designates that the relative humidity should be 30 to 35%. Laboratory specifies 30% plus or minus 3%. The Cincinnati Testing Laboratory states it should be 45% plus or minus 5%. It is said that the Bureau of Reclamation has done considerable research in the membrane curing field, yet their test seems worthless to me. Their specification reads as follows: "The relative humidity range shall be approximately 15 to 35%."4 (The word "approximately" is added. I presume, in case the relative humidity should ever stray from this 20% range.) Needless to say, a specification like this is useless if the purpose of the test is to obtain reproducibility. A control cabinet seems to be an absolute necessity if the relative humidity must be controlled very accurately.

The third important factor, the air flow over the specimens, is not definitely specified in any proposed test. The A.S.T.M. Test merely states that, "Means shall be provided for circulating the air." The Truscon Test states the same. The Bureau of Reclamation and the War Department tests do not

Bureau of Reclamation Specifications for 45-Percent Solids Clear Curing Compounds.

even mention this item. The Battenfield Laboratory, Manufacturers of Satisfaction curing compound, specify: "The incubator shall have a small fan which slowly causes air movement, rather than a large fan that causes excessive evaporation, or air movement."

In considering the design of a control cabinet, a fundamental question is, "Shall the air flow be an open or closed system?" Perhaps a satisfactory control cabinet can be designed with either type, but it seems as if the easier and better control method would be the closed system. This appears logical, since after the conditions are once stabilized, the air must be conditioned only slightly each time that it passes However, if an open system is used, the conditioning agent. there is continually new and unprocessed air passing over the conditioning agent and the conditioning agent has only one chance to regulate the air before it passes over the specimens. This would be a more expensive method and more difficult to control, since the entering air may vary greatly according to conditions outside the cabinet. In a closed system, however, if the conditioning agents are adequate for the size of the cabinet, a stabilized condition is not difficult to maintain.

Following this line of reasoning, the control cabinet designed for this thesis was of the closed system type. It was designed to accomodate six specimens of the A.S.T.M. type with sufficient additional space for the conditioning agents.

Concrete Curing Compound Specifications in Use and Recommended, published by the Battenfield Grease and Oil Corp., p. 2



CONTROL CABINET



Of course, the size, expense, and the time element involved, controlled the design; but it was recognized that the larger the cabinet, the smoother and more regular the air flow would be. A cabinet 5' - 7 1/2" wide, 2' - 3 5/4" in depth, and 2' - 5 1/2" high was built, with structural wood frame and a celotex covering. To obtain as nearly as possible an airtight cabinet, a double celotex covering was used with an air pocket between the layers of celotex. It was desired that building paper be placed between the celotex layers, but this was not done, and it later proved satisfactory without it. The doors were of rabbitted construction and sufficiently air-tight for the purpose. The Carpenter Shop on the Campus constructed the cabinet from the sketches furnished them.

While the cabinet was under construction, the wiring arrangement was designed. The most satisfactory control of temperature is of course, obtained electrically. A resistance coil or electric lights were considered, but it was decided that light bulbs controlled by a thermostat would be the most satisfactory. The lights were wired in two banks, one bank of lights being controlled only by a switch on the outside of the cabinet, while the other bank was controlled by a thermostat within the cabinet and by a switch on the outside. It was intended that the one bank be used constantly and the other to regulate the temperature as close to 100° F. as possible. After the cabinet was completed, however, it was found that the thermostat-controlled bank, while working only infrequently, was sufficient to keep the temperature at the desired value. An outlet was needed inside the cab-

inet to connect an electric fan, which might also be controlled by a switch on the outside. To take temperature and humidity readings, a reading light, controlled by another switch on the exterior, was placed in the top of the cabinet, to be used only infrequently. 1

An inexpensive electric thermostat, taken from a water bath, was used in series with the light bulbs to regulate the temperature and, after the proper adjustment, controlled to 100° plus or minus 1° F. Since this method is very simple and inexpensive, it appears to me that every laboratory in the country should run its tests with the smallest control range possible, instead of the wide ranges (10° F.) specified at present.

As stated previously, the only comment in connection with the amount of air flow over the specimens was that it should be sufficiently small to prevent excessive evaporation. In line with this reasoning, a small Sterling electric fan with an eight-inch blade was used. The Air movement in the cabinet was first measured without using air baffles. This was done by the use of a Velometer (Boyle system). It was found that the air movement was greater near the top. At Mr. Reuling's 4

The wiring for the cabinet was done by the Electrical Shop of the college from the sketches furnished them.

EBattenfield Laboratory, op. cit., p. 2.

This Velometer was borrowed from the Power Lab., Olds Hall.

⁴A professor in the Michigan State College Mechanical Engineering Department.

suggestion, air baffles were designed for the corners of the cabinet. After these were installed, the air flow was again tested and proved satisfactory, being approximately two feet per second (1.36 m.p.h.). It is said that the Cincinnati Testing Laboratory is using a wind tunnel costing approximately \$15,000 to regulate the air flow to 15 m.p.h..2 air flow seems excessive as even field conditions would rarely be so severe. Truscon Laboratory is using an air flow slightly less than our own. 5 Controlling the humidity to the desired range is the most difficult. It was not until the middle of the testing period before it was solved satisfactorily. During the tests under Series I. calcium chloride or water was placed in pie tins (10 1/2" dia.), according to the regulation desired. It was necessary under this method to watch the humidity of the cabinet rather carefully, especially during the initial stage of the test, when the specimens were losing moisture rapidly. However, an error caused the control range to be lower than desired. There are five methods of measuring humidity, but the one simplest and most generally used depends upon the lowering of temperature of a wet bulb thermometer due to evaporation. This method was used and the relative humidity was controlled as close to 33% as possible. It was discovered later however, that this was not actually

¹ See datum on Measurement of Air Flow in the Control Cabinet.

²From a discussion with Mr. Fairbrother of Truscon Lab., Jan. 19. 1945.

⁵From a discussion with Mr. Fairbrother, of Truscon Lab., April 19, 1943.

giving the correct humidity reading, because the air flow over the wet bulb thermometer was not sufficient to obtain accurate results. To obtain accurate readings the air velocity must be three meters per second. Since it was much less than this, the actual humidity was approximately 22%. The necessary correction was obtained by use of a Dew Point Apparatus. 1 After the error was discovered, it seemed best to continue with these conditions until all the materials were tested, so that a comparison between the compounds could be obtained. However, by the time that Series II was started, a better method of controlling the humidity had been found. 2 Any aqueous solution which has a vapor pressure close to 0.649 inches of mercury at 100° F. will work satisfactorily if a sufficient surface is exposed to the air. For our test an area of 628 square inches of saturated magnesium chloride was used for a cabinet of 12.35 cubic feet. The solution of magnesium chloride must have some excess crystals at the bottom of the container, but any excess salt above the solution will cause the humidity to drop below 35%.

In connection with the variations that will be caused in water loss by changes in humidity, Test B, Series I, furnishes a good example. After the first several days a specimen will lose moisture in approximately equal amounts each day. (This may be seen from the graphs on Percent Water Loss in the con-

The Dew Point Apparatus was borrowed from the Physics Department of the college.

²Mr. Cecil Rhodes was the first to suggest and try this method of humidity control in the cabinet.

clusion.) The fourth day of the test the relative humidity was 22% and the average water loss was 5 1/4 grams. The next day the humidity was only 2% lower, yet the average water loss was 11 5/5 grams. This may not be a quantitative approach to the problem, but it does illustrate the fact that every attempt should be made to control the humidity as finely as possible.

Each laboratory has again adopted its own ideas in the proportioning of the mix for the specimens. The A.S.T.M.

Test states:

The mortar for making the test specimens shall be of plastic consistency and gaged to a definite water-cement ratio. The proportions of cement and sand shall be determined by adding to a paste having a water-cement ratio of 0.40 by weight, a sufficient quantity of saturated, surface-dried sand to produce a flow of 50 percent as measured on the 10 inch flow table using thirty one-eighth inch drops in thirty seconds.

Truscon Laboratory uses exactly the same words in its procedure, except for the fact that they substitute a 15% flow in place of the 50%. The Cincinnati Testing Procedure is, in effect, the same as the A.S.T.M., but the Bureau of Reclamation uses a concrete made of well rounded, sound, natural aggregate (5/4" max.) and modified portland cement in a mix proportioned by weight of 1:2.65:2.65 with a w/c of 0.55. A 50% flow is objected to because of the great amount of finishing water brought to the surface before a smooth surface is obtained. This finishing water forms a laitance on the surface of the specimen, which, after the application of the

A.S.T.M. C 156-40T, op. cit., p. 264.

membrane, may dry further and crack, leaving small openings for the water to escape. Reducing the amount of mixing water may remedy this somewhat, but the finishing operation still brings up water which may form a surface laitance.

The grading of the sand used in preparing the mortar may also affect the water retention of the specimen. The A.S.T.M. Test states that an approximate grading should be:

Percent Passing

No.	4	(4760-M	icron)	100
11	16	(1190-	Ħ	60
11	50	(297-	Ħ	15
**	100	(149-	#	2

Sieve

In order to make sure that the grading was not affecting the results, the sand for every specimen in both series of tests was sieved and then recombined exactly to the desired proportions. After recombining, the sand was saturated and then surface-dried. While the sand is in a saturated, surface-dried condition it has a tendency to segregate, which may again cause variations in specimens; therefore for future tests I would recommend that the sand be oven-dried, sieved, and then recombined separately for each specimen or each mix. (By oven-drying the sand the amount of additional mixing water needed to correct to a surface-dried condition may be obtained.)

The size of the specimen is another feature over which there has been much discussion. The larger specimen (approximately 12"x6"x2") of the A.S.T.M. Test is not very widely used. Instead the Truscon and Cincinnati Laboratories use a specimen with a top diameter of 5 3/8", a bottom diameter of 4" and 15/16" thick (approximately one-tenth of the size of the larger specimens). It is said that the larger specimen is objection-

able in several respects.

- 1. The specimen is so thick that the water loss is not a true measure of the surface dehydration.
- 2. Accurate balances cannot be used with such large specimens.
- 3. The larger specimens require much more work and only a few specimens may be run at the same time.

The last reason seems to be the most logical basis for changing the size of the specimen. Our cabinet would allow the use of six A.S.T.M. specimens or sixteen of the smaller ones. This means that if two blanks were used as controls only two curing materials (two specimens per curing material) could be tested at the same time, while with the smaller specimens four blanks and four curing materials (three specimens per curing material) could be tested simultaneously. In the tests under Series I the large specimens were used, but the smaller specimens were tested under Series II. Smaller variations were obtained with the larger specimens, but this will be discussed in greater detail later. The A.S.T.M. moulds are further objected to because of the one-half inch ridge projecting above the surface of the specimen. It is quite logically claimed that this causes a dead air space above the specimen, which is not affected by the movement of air in the cabinet.

Another variable affecting water retention is the type of finishing used. In this it seems the manufacturing laboratories have experimented until they found the finish which gave the greatest water retention, and then used it in their tests. The first question is, "Should the laboratory finish similate field conditions?" In my opinion this is not neces-



FINISHING WITH STRIKE-OFF

SERIES I

SPRAYING MEMBRANE





FINISHING WITH WOOD FLOAT

SERIES II

APPLYING MEMBRANE



sary, for this test is artificial in many respects, and if the finish in the laboratory were similar to that in the field, it would not yet prove that the concrete slab in the field would lose water in the same proportion as the laboratory specimen. Therefore a finish which is simple and reproducible is sufficient for the purpose. It might be worthwhile to discuss the effect of the different methods of finishing on the water retention properties. The membrane applied to a brushed surface will give the least water loss. A steel troweled surface will lose the greatest water, and a wood float finish gives it an intermediate value. In Series I the strike-off method as specified by the A.S.T.M. was used, while in Series II the surface was finished with a wood float and later brushed, as is done in the Truscon Procedure. A finish to the specimen which has distinct ridges and low spots is to be avoided, because the membrane when applied is quite fluid and the low spots get an excess amount of material, which is definitely detrimental to the water retention properties.

Nearly all the water retention tests now used specify that the membrane should be applied after the surface moisture has disappeared. The A.S.T.M. Test, however, specifies that the membrane should be applied after a storage period in the cabinet corresponding to the time the concrete in the field would be exposed without curing. Since in the field there is not much moisture brought to the surface when finishing, the membrane may be applied immediately. The speci-

From a discussion with Mr. Fairbrother, Jan. 19, 1943.

mens in the laboratory are, however, in a closed mould and when the specimens are finished a great deal of water comes to the surface, especially with the wetter mixes. Several of the curing compounds, if sprayed on this surface water, form very poor membranes. With a drier mix, Series I, the compounds Aquastatic 1-C-Red, Klearcure 60, Truscon 203, and Satisfaction 45 were tested, applying the membrane immediately. The water retention qualities were comparable with the results obtained when applying the membrane after the surface moisture disappeared. 2 If the curing material is not applied soon enough, the membrane will penetrate the surface of the mortar and the resulting membrane will be very poor. This is especially true of the more viscous materials. In some specifications, if the concrete has dried too much, it is specified that the concrete must be sprinkled before the membrane may be applied. In the laboratory it seems best to wait until the surface moisture disappears, but in the field the best practice indicates that it should be applied immediately.

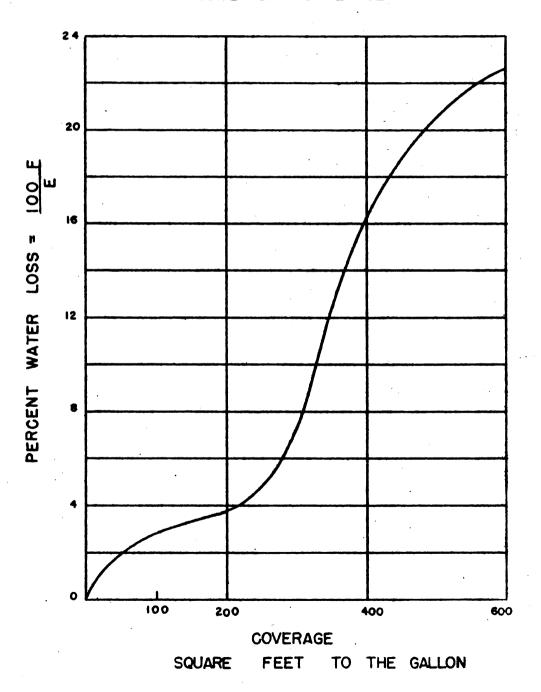
The present specifications usually indicate that the membrane should be applied at the rate of two hundred square feet to the gallon. In Series II, Test P, the specimens were sprayed at the rate of 100, 200, 400, and 600 square feet to the gallon. The graph on the following page clearly indicates that two hundred square feet to the gallon is the most logical coverage. However, if the coverage is not uniform, the con-

A notable exception is Klearcure 60, which forms a strong, dense film over this surface water.

²See data on Series II, Test N.

MEMBRANE CURING STUDY
WATER RETENTION TEST
SERIES II - TEST P

PERCENT WATER LOSS VARIATION
WITH RATE OF COVERAGE



stantially greater than that specified does little in improving the water retention, but a rate substantially less is very harmful. In the field a uniform coverage with the old type of spraying equipment was very difficult, but the Truscon Laboratory has, during the winter, developed a new type of spraying equipment which should give much better results.

On large jobs the most efficient method of applying the membrane curing material is, of course, by power-spray equipment, but if necessary, on small jobs the membrane may be applied by brushing. Spraying with an atomizer seems to be the best method of applying the membrane on the laboratory specimens, as the amount applied may be measured quite accurately. If the atomizer is connected to a low pressure air line, a steady, uniform spray can be obtained. This method was not used in any of the tests, but it appears to be the best method so far developed for laboratory specimens.

The Truscon Laboratory has dispensed with the idea that the edges of the specimen must be sealed with a foreign material to prevent water loss other than through the membrane. Instead they use the membrane itself as the sealing for the edges. This may be satisfactory under certain conditions, but in the wetter mixes the specimens shrink slightly, pulling away from the mold and leaving a small crack through which water may escape. As a precautionary measure, it seems best to use some other material to seal these edges. In Test Q, Series II, two specimens with sealer and two without were tested using the same curing material. The specimens without

sealer lost about twice as much water as those with sealer placed on the edges.

The next few pages will take up the procedure used in the tests under Series I and II; a summary of the results and conclusions will follow.

LABORATORY PROCEDURE Water Retention Test Series I

Scope - This method is intended for laboratory use in testing the efficiency of membrane curing products for the curing of concrete.

Apparatus - Cabinet - The cabinet has been described previously.

Moulds - Moulds shall be water-tight. They shall be rigidly constructed so as not to distort when the specimens are handled at early ages. The moulds shall be $21/2^n$ in depth $(1/2^n$ deeper than the thickness of the specimen in order to allow for proper sealing of the curing material), and the sides shall be beveled in order that the specimens may be readily removed.

Test Specimens - Test specimens shall be approximately 12" in length, 6" in width and 2" thick.

Proportioning and Mixing Mortar - (a.) Proportioning - The mortar for making the test specimens shall be of plastic consistency and gaged to a definite water-cement ratio. The proportions of cement and sand shall be determined by adding to a paste having a water-cement ratio of 0.40 by weight, a sufficient quantity of saturated, surfacedred sand to produce a flow of 25 percent as measured on the ten-inch flow table using thirty one-eighth inch drops in thirty seconds.

(b.) Mixing - Cement and water in quantities which will give a water-cement ratio of 0.40 by weight shall be placed in an appropriate vessel and the cement permitted to absorb water for one minute. The materials shall then be mixed with a trowel into a smooth paste. Saturated surface-dried sand shall be added to the mixture until the mortar is at the desired consistency (25 percent flow).

Moulding Specimens - After the mortar is thoroughly mixed, it shall immediately be placed in the mould and puddled

30

¹ This procedure is almost identical with A.S.T.M. C156-40T.

The A.S.T.M. Test states 50% flow; reasons for changing this have already been discussed.

⁵The A.S.T.M. Test designates a spoon, but this minor matter will not affect results and a trowel is much handier for larger mixes.

The A.S.T.M. Test states that a final mixing with the hands for two minutes should be used, but this was considered superfluous if the mortar was thoroughly mixed with a trowel; however, it was used in the tests under Series II.

with the trowel. It shall then be struck-off with a wooden template.

- Storage of Specimens Immediately after moulding, the mould and specimen shall be weighed to the nearest gram and placed in an atmosphere maintained at a temperature of 100° plus or minus 1° F. and at a relative humidity of 20 to 25%. The air flow over the specimens shall be approximately two feet per second.
- Procedure (a.) Application of Curing Material After a sufficient period has been allowed for the disappearance of the surface moisture (approximately 3 hours) the specimens shall again be weighed. The liquid curing material shall then be sprayed on the specimen uniformly with an atomizer at the rate of 200 square feet to the gallon. (This was measured as follows: the atomizer was partially filled with curing material and sprayed until no more could be exhausted. Then the desired amount, 9.5 ml. for 72 sq. in., was measured in a glass graduate and placed in the atomizer. The specimen was then sprayed until the atomizer was again exhausted. An additional check was used in that, the atomizer and contents were weighed before and after spraying the specimen.) After the application of the curing material, the specimen shall be weighed and replaced in the storage cabinet. After approximately 1/2 hour the specimen shall be taken from the cabinet, weighed, and the edges of the specimen sealed to the mould with a latex material. The specimen is again weighed and replaced in the control cabinet.
 - (b.) Determination of Water Loss The specimen shall be weighed daily for the duration of the test. In determining the water loss, corrections shall be made for the loss in weight of the curing material and the sealer compound. At the end of seven days the specimen shall be taken from the cabinet and the final weighing made.

⁵The reason why the humidity range was 20 to 25% was explained previously under the humidity control of the cabinet.

LABORATORY PROCEDURE Water Retention Test Series II

Scope - This method is intended for laboratory use in testing the efficiency of liquid materials for curing concrete.

Apparatus - Moulds - Moulds shall be made of metal and shall be water-tight. They shall be rigidly constructed so as not to distort when the specimens are handled at early ages. The moulds shall be in the shape of a frustum of a right cone having a top diameter of 5 5/8", bottom diameter of 4" and depth of 15/16".

Test Specimens - Test specimens shall be of a size which completely fills a mould to its upper rim.

Proportioning and Mixing Mortar - (a.) Proportioning - The mortar for making the test specimens shall be of plastic consistency and gaged to a definite watercement ratio. The proportions of cement and sand shall be determined by adding to a paste having a water-cement ratio of 0.40 by weight, a sufficient quantity of saturated surface-dried sand to produce a flow of 25% as measured on the ten-inch flow table using thirty one-eighth inch drops in thirty seconds. This flow test is described in the Standard Method of Test for Flow of Portland-Cement Concrete by Use of the Flow Table (A.S.T.M. Designation C124) of the American Society for Testing Materials. The sand to be used in the proportioning and mixing of the test specimens shall be sieved through U.S. Standard Sieves. After sieving and separating the retained portions, the sand shall be re-combined in the following exact proportions:

No. 4		Sieve	Percent Passing
		(4760-Micron)	100
#	16	(1190- *	60
Ħ	50	(297- " (149- "	15
Ħ	100	(149- #	2

(b.) <u>Mixing</u> - Cement and water in quantities which will give a water-cement ratio of 0.40 by weight shall be placed in a non-absorbent vessel and the cement permitted to absorb water for one minute. The materials

¹ Truscon Procedure with only slight modifications.

²Truscon Laboratory uses a 15% flow.

shall then be mixed with a spoon into a smooth paste. Saturated surface-dried sand shall be added to the mixture until the mortar shall be of 25% flow. Final mixing shall be accomplished by continuous squeezing and kneading with the hands for two minutes. Rubber gloves shall be worn during the mixing operation.

- Moulding Specimens The specified moulds shall be weighed to the nearest O.l gram. Portions of the batch of mortar shall be placed in weighed moulds, tamped and leveled off even with the rim of the moulds with a wood float. The edge of the specimen shall be grooved slightly so that the sealer may be applied later in this groove. The rim of the mould shall be wiped to remove any excess mortar.
- Storage of Specimens Immediately after wiping, each mould and specimen shall be weighed to the nearest 0.1 gram and placed in a storage cabinet. The storage cabinet shall be maintained at 100° plus or minus 1° F. and 53% plus or minus 1% relative humidity. The air flow shall be approximately two feet per second.
- Procedure (a.) Application of Curing Compound After approximately 1 1/4 hours, the specimens shall be removed from the cabinet, weighed, and the surface of the specimen brushed to remove any laitance. The specimen shall be weighed after brushing, and a latex sealer applied to the grooved edge of the specimen to prevent any water loss, other than through the membrane. The specimen shall be reweighed and placed in the cabinet for an additional thirty minutes. It should then be removed, weighed, and the liquid curing material applied uniformly by spraying on the specimen at the rate of 200 square feet to the gallon. (The amount of curing material applied to the specimen shall be measured by weighing the atomizer and contents before and after spraying the specimen.) The specimen shall then be replaced in the cabinet.

(b.) Determination of Water Loss - The specimen shall be weighed at 24 and 48 hours after the curing material is applied. In determining the water loss, corrections must be made for the changes in weight of the curing material and the sealing compound.

Truscon Laboratory uses no additional sealer other than the membrane itself.

The results of these tests indicate that the quality of the commercial membrane curing products varies a great deal. (Please refer to the tabulated data and graphs which show the results obtained much more clearly than they can be stated). The product manufactured by the Horn Company is practically useless in retaining the mixing water. It was found upon analysis to be sodium silicate, a material previously discarded because of its inefficiency. The results of the tests under Series I were probably affected by a relatively poor control of humidity. In Series II the tests were run with much better control and laboratory technique. It will be noted that the Percent Variation of the Percent Water Loss is much smaller in Series I. Considering the fact that these tests were run over a longer period and there were more variables to effect the results, I believe the conclusion may be drawn that the larger specimens will give more uniform and consistent results for the same material. The smaller specimens lose so little water and the better materials are so closely bunched that it is quite difficult to determine the relative efficiencies. The tests under Series II have the advantage in that more samples may be run in a given length of time, but the fact that wider variations in results were obtained is a definite disadvantage.

The data was not conclusive enough to prove that one certain material is definitely better than all others as variations may be noted between Series I and II. However, two materials, Satisfaction 45 and the Horn product, may be regarded as definitely inferior, even though their manufact-

MEMBRANE CURING STUDY

WATER RETENTION TEST

Averaged Results

Series I (7 day period)

	Percent water loss = $\frac{100 \text{ F}}{\text{E}}$	(100 - 100 F/E)
Aquastatic 1-C-Red	16.6 %	(F/E (blank)) 63.7 %
Klearcure 60	21.0	53.2
Aquastatic Slab Cure Red	22 .7	52.3
Truscon 203	23.1	47.6
Truscon 223	29.8	32.6
Satisfaction 45	39•5	16.30
Horn	44.2	1.20
Blank	45.5	
Ser	ies II (2 day period)	
Truscon 203	2.22	96.10
Klearcure 60	3.64	93.66
Aquastatic Slab Cure Red	4.09	93.14
Truscon 223	4.35	92.22
Aquastatic 1-C-Red	5.72	90.05
Satisfaction 45	17.74	69.1
Blank	57.60	

Percent Variation of Percent Water Loss from that of average specimen of each material

Series I - 6.66 %

Series II - 11.73 %

KLEARCURE KLEARCURE BLANK HORN 8-4 8-3 8 - 5 1 8 WATER RETENTION TEST B MEMBRANE CURING STUDY 20 30 9 TOSS = 100 X E

DAYS

TIME IN

36

MATER

NO. 2 PERCENT

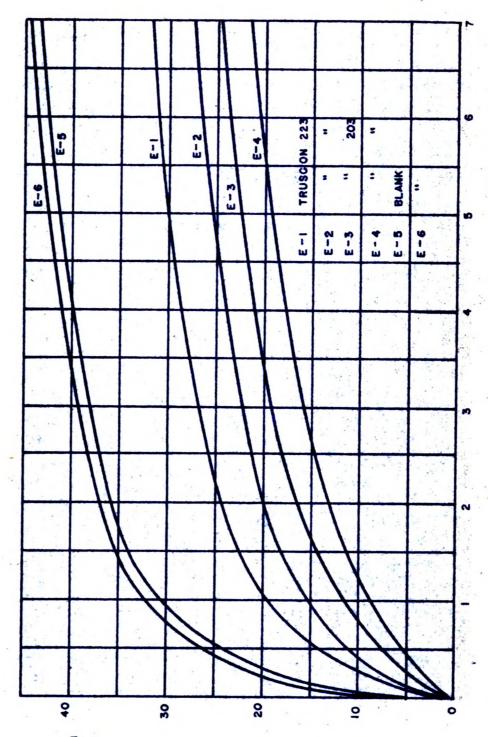
SATISFACTION TIME IN DAYS BLANK C-5 - N

5 MEMBRANE CURING STUDY WATER RETENTION TEST C 0

WATER LOSS = 100 X E NO. 2 PERCENT

7-0 WATER RETENTION TEST MEMBRANE CURING STUDY TEST D AQUASTATIC AQUASTATIC BLANK TIME IN DAYS 8 - 9 . 2-0 9 - 0 1-0 4-0 0-2 SERIES 50 2 8 0

MEMBRANE CURING STUDY
WATER RETENTION TEST
SERIES I TEST E



TIME IN DAYS

NO. 2 PERCENT WATER LOSS = 100 X E

KLEARCURE 60 AQUASTATIC I-C-RED 203 AQUASTATIC TRUSCON MEMBRANE CURING STUDY TEST PECIMENS 223 SATISFACTION TRUSCON 22 RETENTION SERIES MATERIAL 9 WATER RESULTS CURING EACH 036 FOR 8 0 20 8 0 3 x 001 NO. 2

DAYS

Z

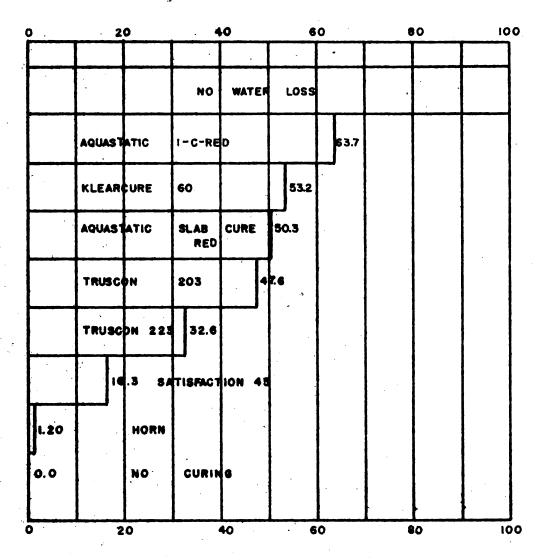
TIME

40

MEMBRANE CURING STUDY WATER RETENTION TEST

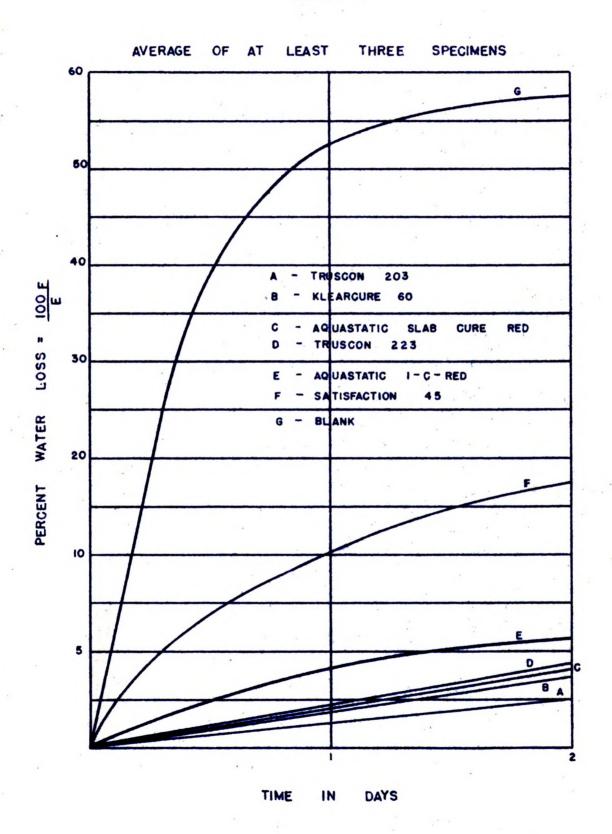
SERIES I

WATER RETENTION EFFICIENCY OF VARIOUS MEMBRANE CURING MATERIALS



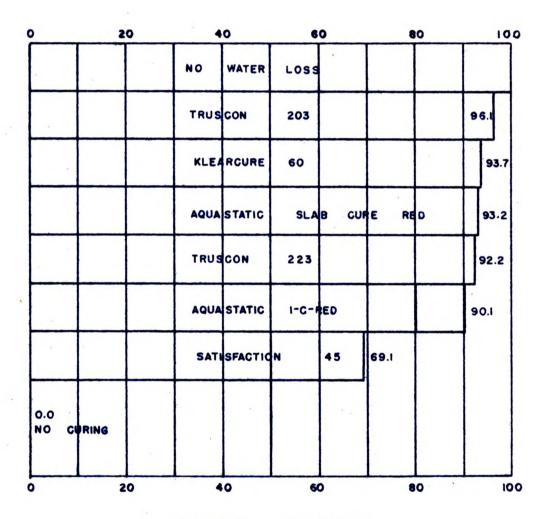
PERCENT EFFICIENT
AVERAGE OF TWO SPECIMENS FOR EACH COMPOUND

MEMBRANE CURING STUDY WATER RETENTION TEST . SERIES 2



MEMBRANE CURING STUDY WATER RETENTION TEST SERIES 2

WATER RETENTION EFFICIENCY OF VARIOUS MEMBRANE CURING MATERIALS



PERCENT EFFICIENT

AVERAGE OF THREE SPECIMENS FOR EACH COMPOUND

urers claim results comparable with the better curing materials. In fact, a better product such as Truscon 205 can be applied at the rate of 400 square feet to the gallon with a Percent Water Loss of 16.5%, while Satisfaction 45 applied at twice the coverage, or 200 square feet to the gallon has a water loss of 17.7%. The better curing compounds tested, Truscon 203 and 225, Aquastatic 1-C-Red and Slab Cure Red, and Klearcure 60 are close enough together to make it difficult to predict which is the best material to use. The individual characteristics of the different materials must be investigated before the best all-purpose curing compound may be found. For example, Truscon 225, if applied at the right time, will give good results; but if it is applied too soon the efficiency is greatly reduced.

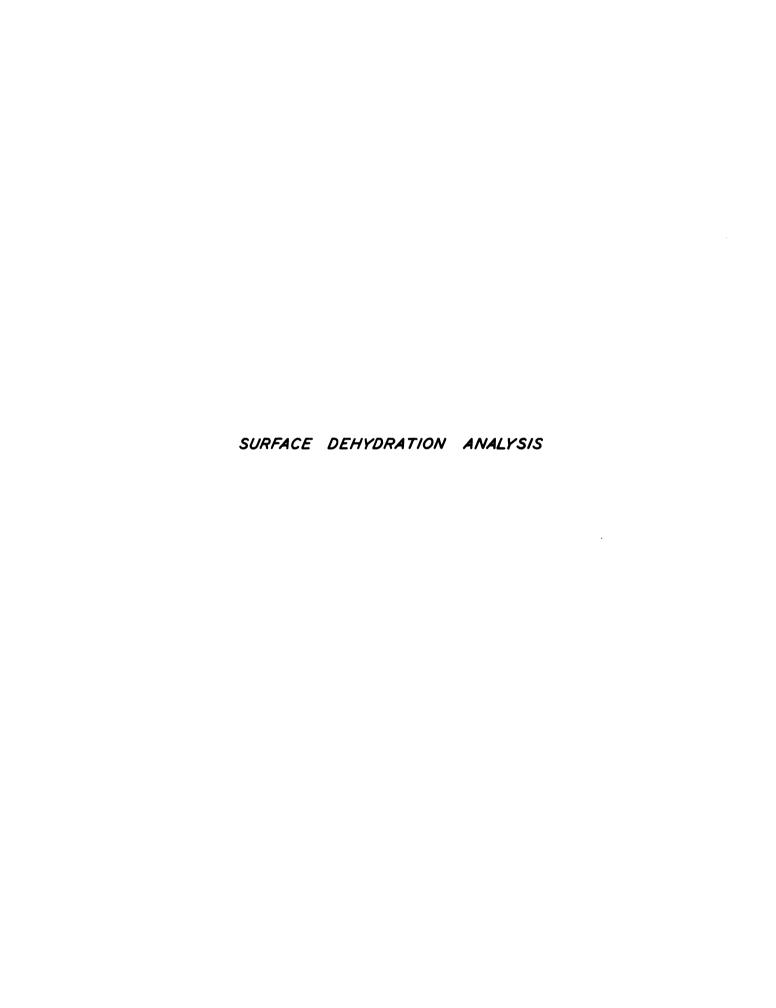
The War Department specifies that materials may be used which equal Klearcure (No. 70), Sealkure, Trucure (No. 199 or 205), or Aquastatic (1-C, 1 FMST, or Black) in laboratory tests or field performance. The specifications as to the Percent Water Loss allowable are still in a formative stage due to the fact that the variation in testing procedure of different laboratories makes uniform results impossible. As soon as a Standard Test can be developed which every laboratory will abide by, the sooner a definite allowable Percent Water Loss can be specified. From the data obtained from these tests, a few recommendations in regard to the development of an authoritative water retention test will be attempted.

1. The storage conditions of the test specimens must be very carefully regulated.

Recommended ranges.

- (a.) Temperature $100^{\circ} \pm 1^{\circ}$ F.
- (b.) Relative Humidity 33% + 2%, but finer regulation if possible.
- (c.) Air Flow A definite specification as to the amount, preferably less than 4 m.p.h.
- 2. The proportioning of the cement and sand should be reduced from 50% to a lower value; further investigation is necessary to determine the best value.
- 3. An exact grading of the sand should be specified, or further investigation should be made as to the effect of this variable.
- 4. The larger specimen (A.S.T.M.) is, in my opinion, the best, because more uniform results may be obtained from it.
- 5. The A.S.T.M. mould should be changed in that the 1/2" projection above the surface of the specimen should be removed, and a flat rim substituted, for sealing purposes.
- 6. Every material should be tested by applying the material at different intervals after finishing, so that the effect of the moisture of the surface upon the water retention properties of the membrane may be determined for various compounds.

If a standardized test is not developed quickly so that the inferior materials may be eliminated from the market, poor results in the field may cause engineers throughout the country to distrust this new type of product. The sooner these inferior materials are exposed and condemned, the greater will be the chance for the better products to compete successfully with the older methods of curing.



The results of poor curing are most apparent in the upper surface of a concrete slab. In many respects, the strength of this surface is the most important element in the concrete slab. If it is not properly cured, the surface will suffer from scaling and abrasion. A test which would evaluate the surface dehydration of the specimen with different methods of curing would be very useful to correlate with other tests, such as the Water-Retention Test and the Abrasion Test.

In order to analyze the amount of surface dehydration that took place, the specimen, after being broken in the Flexural Test, was immediately sprayed along the fractured surface with phenolphthalein. This indicator gave a reddish color to the surface which contained moisture, but the areas which had been dehydrated remained a natural color. The specimen was then photographed - the surface dehydration is indicated on the print by the lighter color. This procedure was originated by the Truscon Laboratory.

The results of this study show clearly that the better membrane curing compounds successfully retard surface dehydration, while the inferior membranes show a distinct line of surface dehydration which is almost as deep as those of uncured specimens. (Please refer to the photographed specimens on the following pages).



SERIES I
WATER LOSS SHOWN PICTORIALLY
TOP - NO COMPOUND - CURED IN MOIST ROOM
CENTER - AQUASTATIC I-C-RED
BOTTOM - NO COMPOUND - CURED IN CABINET



NO COMPOUND - GURED IN CABINET WATER LOSS - 31.3 GRAMS



HORN COMPOUND - CURED IN CABINET WATER LOSS-25.5 GRAMS



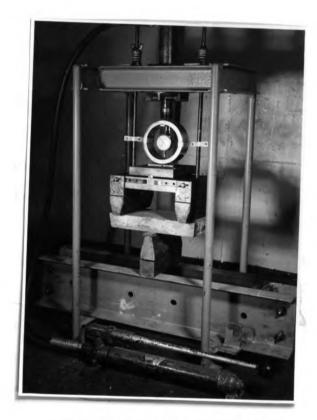
AQUASTATIC I-C-RED - CURED IN CABINET
WATER LOSS - 5.4 GRAMS



In an effort to determine what relation the curing compound used bore to resistance to a flexural force, we have included in this study a flexural test, to be used on the larger A.S.T.M. specimens. Concrete placed in slabs, as well as in various members of concrete building structures is continually being subjected to flexural stress, and since the makers of the various membrane curing preparations advocate the use of their individual and collective products in the curing of buildings and slabs, it is of importance just what effect, if any, the various types of curing have on the flexural strength. Very little has been done regarding flexural strength of membrane-cured concrete, and of the specifications recommended up to this time, none, to our knowledge, refer to any flexural tests which have been conducted as aids to evaluation of compounds.

The specimens used are the same ones as used in Series I for the water retention test and later used in the abrasion test. They have a top surface of 72 square inches, being 12 inches long and 6 inches wide; they are 2 inches thick, and the edges are slightly beveled to enable the finished specimen to be easily removed from the molds.

The apparatus used in the test for breaking the specimens is pictured in an accompanying photograph. The pressure was applied through the steel ring, transmitted to the two knife edges and thence through the specimens to the lower knife edge. Pressure was applied by means of the hydraulic jack. The distance between the two upper knife edges was nine inches with the lower knife edge being $4\frac{1}{2}$ inches from



FLEXURAL TEST APPARATUS

each of the two upper ones. Before starting the test, the steel dynamometer ring was calibrated using the Olsen testing machine in the Olds Hal testing laboratory. A Federal dial, sensitive to the variation of one-ten thousandth of an inch was mounted in the ring and adjusted to zero; known loads were then applied and the vertical compression of the ring, as registered on the dial, was noted and recorded. After two cycles of application and releasing of the test load, a calibration curve for the dynamometer ring was drawn, to be used in the flexural test on our specimens.

This test was run on each specimen seven days after removal from the test cabinet or the moist room, as the case might be, and in all cases, this was fourteen days after preparation. Since concrete is weakest in tension and any variation which might be present between the various specimens would occur in the surface region due to varied curing methods, the test was run so that the surface would be put in tension on application of the load. After the specimen was broken and results recorded, the two halves remaining were marked and kept for the running of the abrasion tests.

The results obtained in this test are shown on the following page in tabular form; the modulus of rupture was computed from the formula,

M c

in which s = stress in the extreme fiber of the specimen
 c = distance from neutral axis to extreme fiber
 M = bending moment at the section

I - moment of inertia of the section about its neutral axis

FLEXURAL TEST RESULTS

	PHENORE THAT REAL	Load	Modulus
	Curing	at rupture	of rupture
A-1	No compound-cured in moist room		
A-2	No compound-cured in moist room	925	529
B-4	Horn-cured in cabinet	970	554
B-1	Horn	1050	600
B-2	Klearcure 60	1150	656
B-3	Klearcure 60	1225	7 00
B-5	No compound-cured in cabinet	925	529
C-5	No compound-cured in cabinet	925	529
C-6	No compound-cured in cabinet	925	529
D-1	Aquastatic 1-C-Red	1075	614
D-2	Aquastatic 1-C-Red	1210	690
D-3	Aquastatic Slab Cure	1200	685
D-4	Aquastatic Slab Cure	1125	642
D-5	No compound-cured in cabinet	850	485
D-6	No compound-cured in cabinet	1000	570
E-1	Truscon 223	1025	585
E-2	Truscon 223	1125	642
E-3	Truscon 203	1075	614
E-4	Truscon 203	1063	607
E-5	No compound-cured in cabinet	775	442
E-6	No compound-cured in cabinet	813	464
F-1	No compound-cured in moist room	975	556
F-2	No compound-cured in moist room	925	529
F-5	No compound-cured in moist room	975	556
F-4	No compound-cured in moist room	813	464
F-5	No compound-wet burlap curing	1100	627
F-6	No compound-ponded	813	464

Compound used	Modulus of rupture in pounds / square inch		
Klearcure 60	678		
Aquastatic Slab Cure	664		
Aquastatic 1-C-Red	652		
No compound-cured under burlap	627		
Truscon 223	614		
Truscon 203	610		
Horn	577		
No compound-cured in moist room	527		
No compound-cured in cabinet	507		

The values in the above table are the averages for all specimens cured by like methods or compounds.

DISCUSSION

The results given here for the performance of specimens cured by the use of several different curing compounds and methods are in no way intended to represent the flexural strengths of concrete used in construction work. Structural concrete contains not only the mortar but also aggregates of various size and composition, and since the purpose of this test was to evaluate the efficiency of the membrane tested in retaining the water necessary for the cement to properly hydrate and develop full characteristics of strength, coarse aggregates were omitted and merely a mortar of cement, graded sand. I and water was used.

It will be seen that the results obtained are not entirely consistent; for example, of the tests run on Klearcure 60, one specimen had a modulus of rupture of 700 pounds per square inch and the other broke at 656 pounds per square inch. This variation may be caused by several different factors:

- 1. The arrangement of the aggregates may be such as to cause differences.
- 2. The curing may not be the same for all specimens. This idea is substantiated by the fact that on the water retention test, specimens cured at the same time under identical conditions did not lose identical amounts of water.
- 3. Variations in surface smoothness will alter the results.
- 4. Variations in thickness or other dimensions, including effect of shifting of the mortar in the pan before set occurs, or sagging of the bottom of the pan due to weight of mortar.
- 5. Differences in temperature between the cabinet

For the gradation of the sand, see Water Retention Test.

(100 F.) and the moist room (70 F.) may cause a variation in curing. If this is true, the moist room cured specimens could not be compared fairly with the membrane cured ones.

of the above, probably the last two are relatively insignificant, and the most important is probably the second. Even with exactly identical conditions of curing, however, it is probable that results would vary. Concrete acts inconsistently at times, and in the testing of beams, cylinders, briquets, and other similar samples of concrete, the individual result cannot be taken as representative, but a series of specimens must be made up and the average result taken. The Bureau of Reclamation suggests the use of one hundred specimens in a compression test, conclusions to be made only from the composite results of all these specimens. The use of one hundred specimens of each curing compound is of course out of the question in this study, but we feel that the test does give an indication of the relationship existing between cured and uncured specimens.

On examination of the results given in the foregoing table, it will be seen that, as would be expected, the poorest results were obtained on those specimens which were exposed to drying without the benefit of burlap, compound, or moist room curing. The best results were shown by the specimens that were cured by compound and the one cured under burlap; this last result must be taken lightly, however, since only one such specimen was tested and the use of further tests might bring this average result up or down somewhat. Enough

¹Concrete Curing Compound, a publication of the Battenfeld Grease and Oil Co. p. 6

tests were run on the specimens with no compound (seven in number) and those cured in the moist room (six) to compare these with the various membrane cured specimens, and when this comparison is made, it will be seen that the compounds are far superior in results to no compounds whatever, and it would appear that the specimens cured by membrane are also superior to moist room cured specimens, although the heat element mentioned before may alter this result.

It must be remembered, also, that the above results are for 14 day tests and the water cured specimens might, on further curing, continue to gain in strength to a greater degree than those cured under the membrane.



INTRODUCTION

It is a generally assumed fact that the value of a membrane curing compound lies in its ability to retain, during the curing period, that water which was used in the preparation of the concrete. However, the value of a concrete structure is not measured by the amount of water that was retained during curing, but rather by the performance of the concrete after it is put into use. For example, in highways, sidewalks, floors, and other structures making use of concrete slabs, the resistance to certain flexural stress and abrasive force is the yardstick by which the value of the concrete is measured.

Thus, before it can be said conclusively that the membrane is effective as a curing agent, the resistance of membrane cured concrete to some outside force must be compared with the resistance of specimens cured by some other method when subjected to the same force. One of the tests used to compare the qualities of various concretes is the flexural test, the results of which are given in another section of this study. The other test being used to evaluate various curing compounds is the abrasion test; this test also measures an important property of concrete. Although a compound may very effectively retain the water during the curing period, it is very possible that it also might react unfavorably with the cement constituents, thus producing a finished concrete product of inferior quality with little resistance to wear.

The abrasion test has been used to some extent in previous studies to measure the quality of concrete produced by different methods of curing. The Bureau of Reclamation, one

of the earliest experimenters in the field of curing compounds, made use of an abrasion test which utilized steel grit. The grit was blasted from a nozzle at an angle of 45 degrees with the surface of the specimen and 4 inches away from it. After a given period, the blasting was stopped, the surface brushed, and the loss of weight was determined. 1

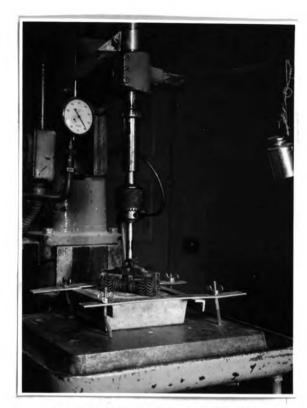
Another wear test of a different type is used by the Cincinnati Testing Laboratory of the War Department. A special tool fastened in the chuck of a drill press is run for three two-minute intervals. After each interval, the specimen is brushed, and the loss in weight is measured; the result is the average loss in weight for the three intervals.

Other experimenters have devised other abrasion tests but they operate, in general, on the principles of the two outlined above, and they all have the same object-to evaluate the abrasive properties of the curing compounds being produced. This, along with an attempt to gain some idea of the correlation between water loss and wear in concrete, is the purpose of this abrasion test.

APPARATUS

The apparatus used in the abrasion test was built up using the drill press as the basis. Two photographs are included on the following page which illustrate the set-up. The wear tool itself was constructed as follows. The shaft was

H. S. Meissner and S. E. Smith, "Concrete Curing Compounds", <u>Journal of the American Concrete Institute</u>, Vol. 9, May-June 1938, p. 555.



ABRASION TEST SET-UP



CLOSE-UP OF WEAR TOOL

made of such a size that it could be mounted in the chuck of the drill press; to this shaft was hinged the main part of the tool, the hinge permitting uniform transfer of the load to the specimen being tested. The pointed wheels which were in contact with the concrete surface are No. O Huntington emery wheel dresser cutters, and ordinary washers were used to keep the wearing wheels in the proper position. During the preliminary tests, some difficulty was encountered with the shaft on which the wheels rotated, due to the fact that the shaft wore nearly as fast as the concrete. After substituting a case-hardened shaft, however, the trouble was completely remedied.

For measuring the amount of wear, several methods were considered. The one finally adopted made use of the Federal dial with calibrations to the thousandths of an inch. The dial was mounted from a stationary part of the drill press frame and an arm was secured to the main drill-press shaft sleeve. This arm moved downward as the specimen became worn, and the end bearing against the dial shaft caused the amount of wear to be registered on the dial.

The drill press operating arm was twelve inches long and a weight of one pound was suspended twelve inches from the center of rotation of the arm. This caused a force of approximately 24 pounds to be transmitted to the specimen through the wheels. The speed of operation of the press for this test was about 375 revolutions per minute, varying slightly at the different periods of the test; that is, as the tool wore down slightly into the specimen, a slight amount of binding between

the tool and the specimen occured, and the speed was slightly reduced. This reduction, however, was small and thus was neglected.

PROCEDURE

In this test, as well as in the water-retention test, there are two main series of specimens, logically known as Series I and Series II. The specimens in Series I were made according to A.S.T.M. specifications—they are 6 inches wide, 12 inches long, and 2 inches thick—and two tests were run on each specimen. In Series II, the specimens were made in the small round molds, as explained in the water-retention test, and only one test was run on each. The procedure was practically the same for both Series I and Series II, and the following explanation will apply for both unless otherwise stated.

In Series I, the various specimens were cured in the cabinet under controlled conditions of for a period of 7 days and were allowed to cure further in the laboratory for another 7 days, at which time they were subjected to the flexural test and then tested to determine abrasion resistance. The specimens in Series II were cured for two days in the cabinet and the abrasion test was run immediately except in two cases. Thus the large specimens of Series I were cured 14 days before testing, and the smaller specimens of Series II were cured 2 days.

At the start of the test, the specimens were clamped securely to the table of the drill press and leveled, using a small carpenter's level. The abrasion tool was then brought

¹ See Water Retention Test for the exact conditions.

down onto the specimen and the table was adjusted so that the drill press arm formed an angle of about 10 degrees with the horizontal. As the specimen wears, the arm drops, and this slight elevation is to allow for the drop; the 10 degrees will cause a difference of only 1.5 percent in the horizontal lever arm, and this will be reduced since the arm swings through the horizontal as the specimen wears.

The next step in the procedure is to take the initial dial readings. The tool was rotated one complete revolution and readings were taken at each of the four quarter points; the average result is that used. As soon as preliminary readings were taken, the drill press was started. An Eastman timer was used to time the test and readings were taken at the one, three, five, and ten minute points in Series I and the one, three, five, and eight minute points in Series II. These readings were taken in exactly the same manner as at the beginning of the test, and were recorded for use in plotting the result curves.

Because the emery wheel cutters used in the test showed a tendency to wear, after each test, the tool was dismantled and the worn cutters were replaced. Since the outer cutter showed the greater wear, this cutter was removed each time and a new cutter put at the inside. This kept the cutters working from inside to outside and insured uniform conditions for each test.



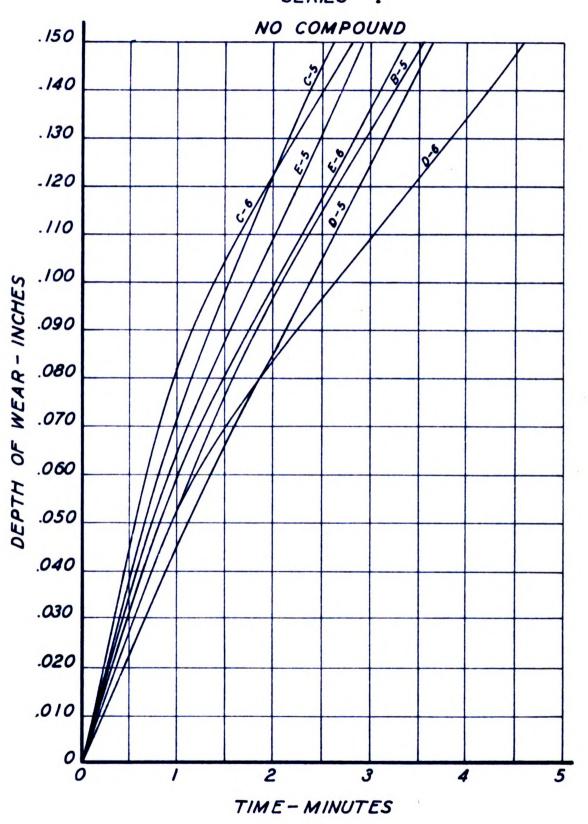
SPECIMEN AFTER WEAR

RESULTS

The results of both Series I and Series II tests are shown by the graphs which are drawn up on the following pages. For each specimen, there is a separate curve, and also a summary graph is given which shows the average curves of all of those specimens cured under the same conditions.

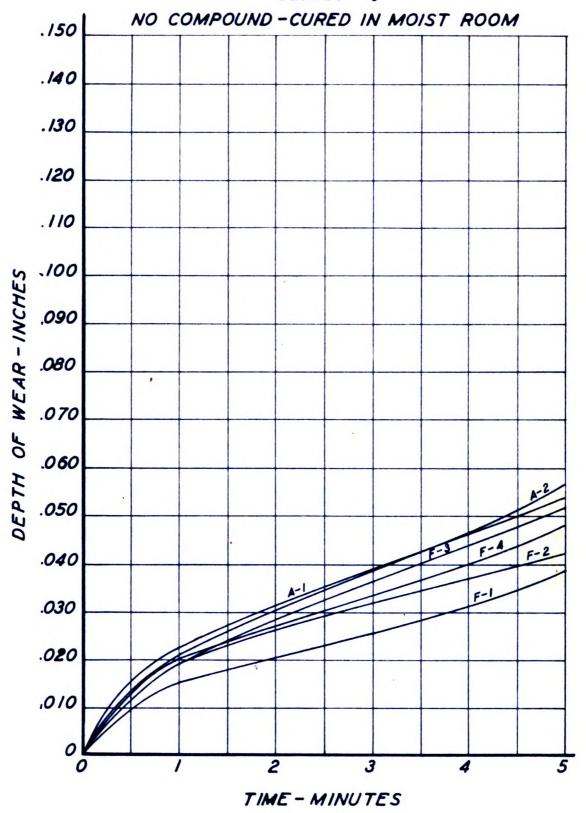
Before drawing any final conditions from the curves, certain factors must be considered. The fact that, during the five minute interval, one specimen suffered a slightly greater depth of wear than another does not necessarily prove that it is less resistant to wear than the other, because on the surface of every specimen, there is a certain amount of laitance and irregularities which may wear off rapidly. After these irregularities are worn off, however, the abrasion resisting qualities may be of the highest order. So, besides noting the total wear of each specimen, the slope of the wear curve should be examined when final evaluation of the various curing methods is made.

MEMBRANE CURING STUDY ABRASION TEST SERIES I

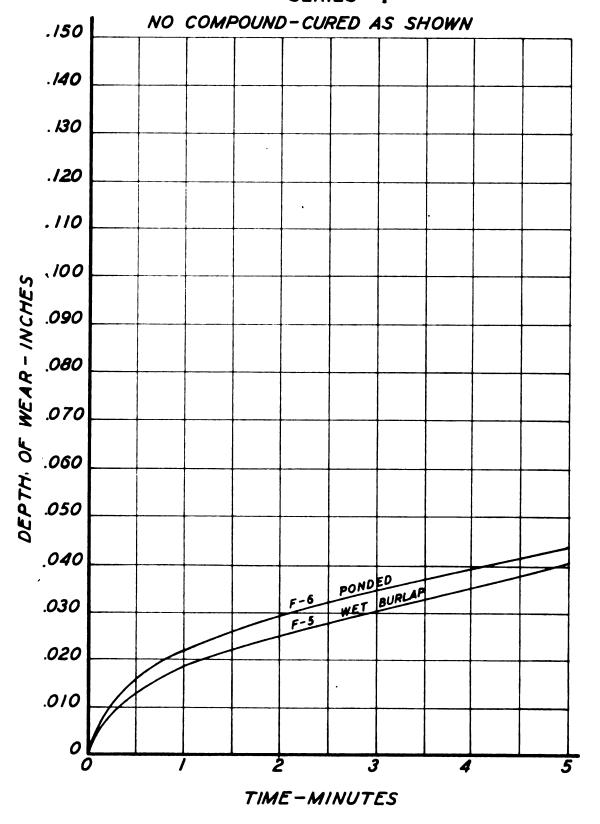


MEMBRANE CURING STUDY

ABRASION TEST SERIES 1

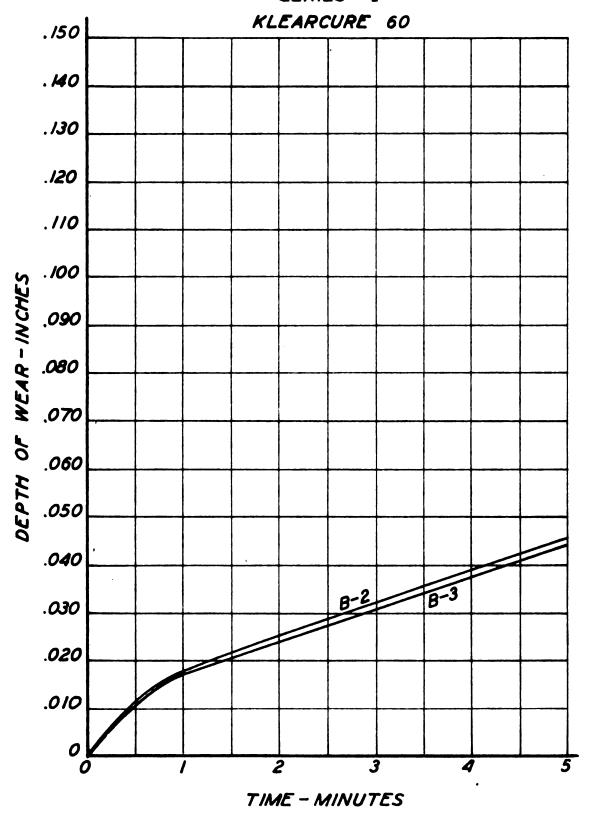


MEMBRANE CURING STUDY ABRASION TEST SERIES 1

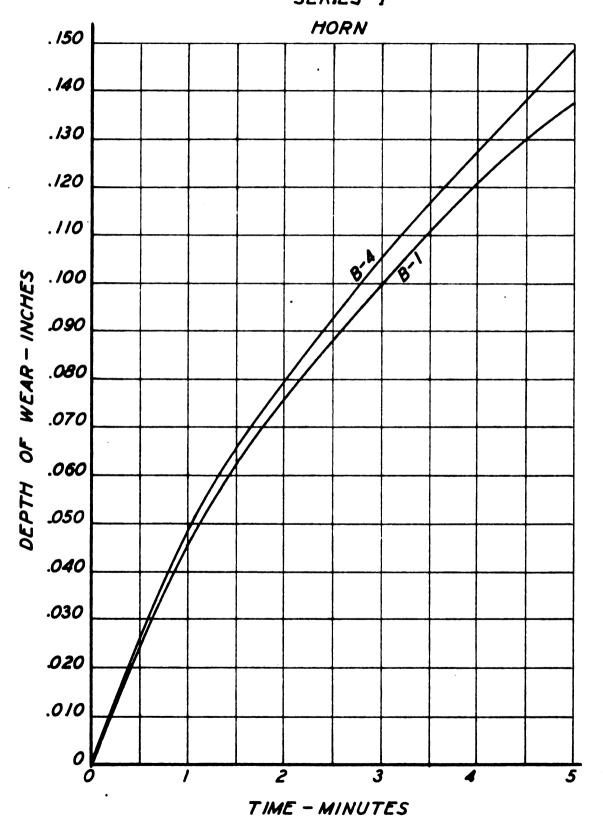


MEMBRANE CURING STUDY

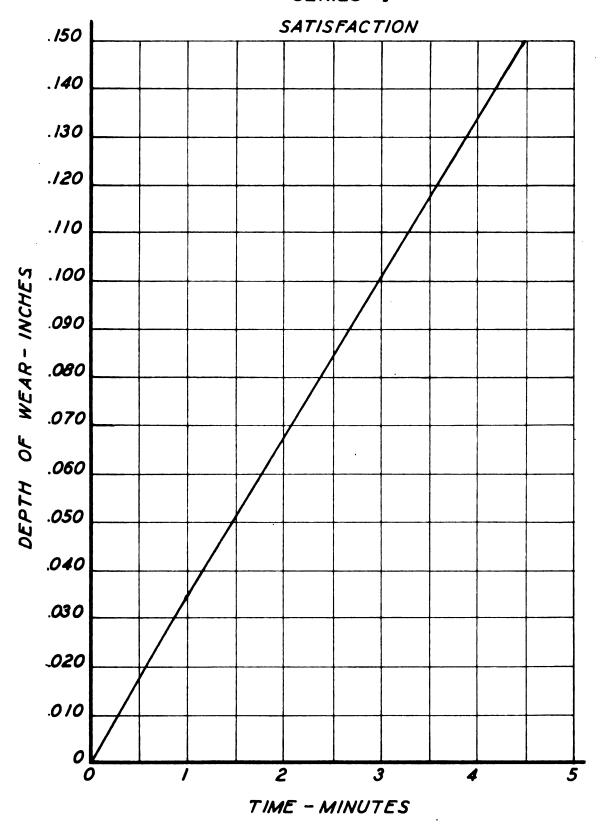
ABRASION TEST SERIES I



MEMBRANE CURING STUDY ABRASION TEST SERIES I

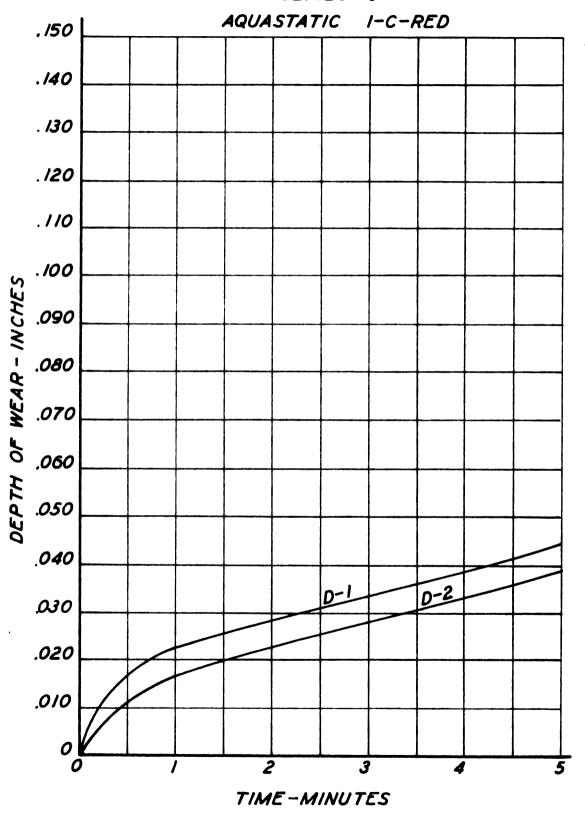


MEMBRANE CURING STUDY ABRASION TEST SERIES I

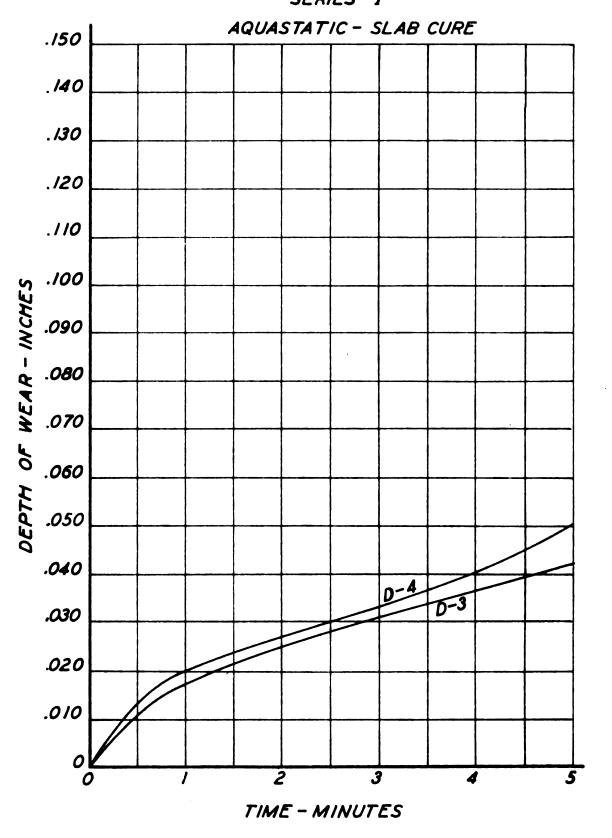


MEMBRANE CURING STUDY

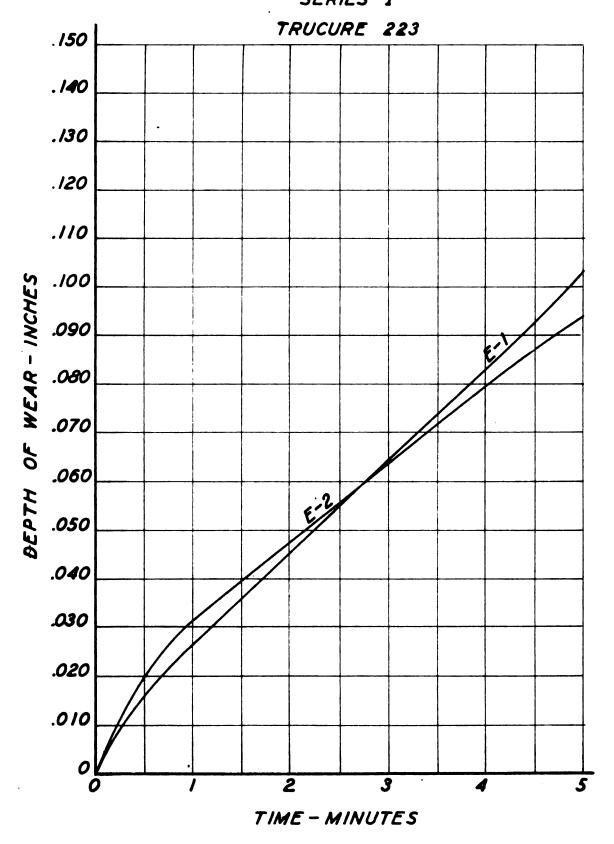
ABRASION TEST SERIES I



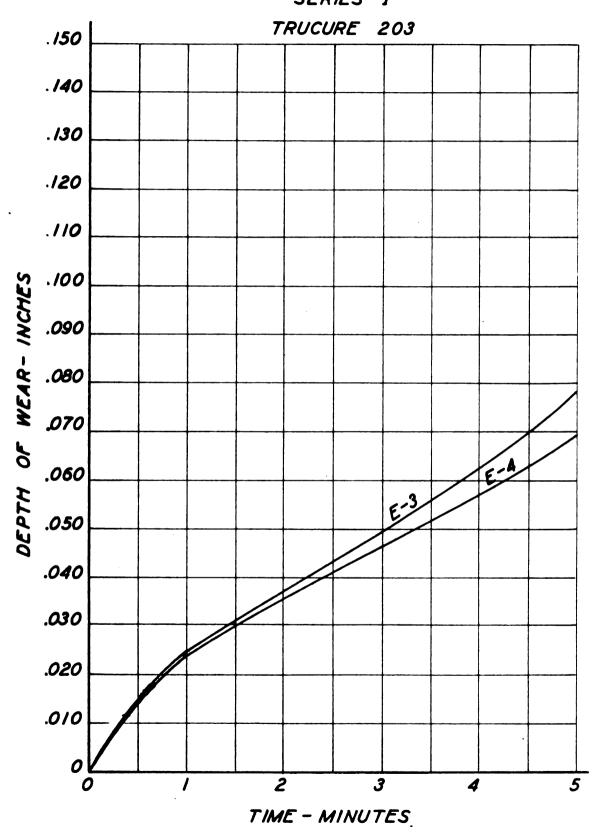
MEMBRANE CURING STUDY ABRASION TEST SERIES I



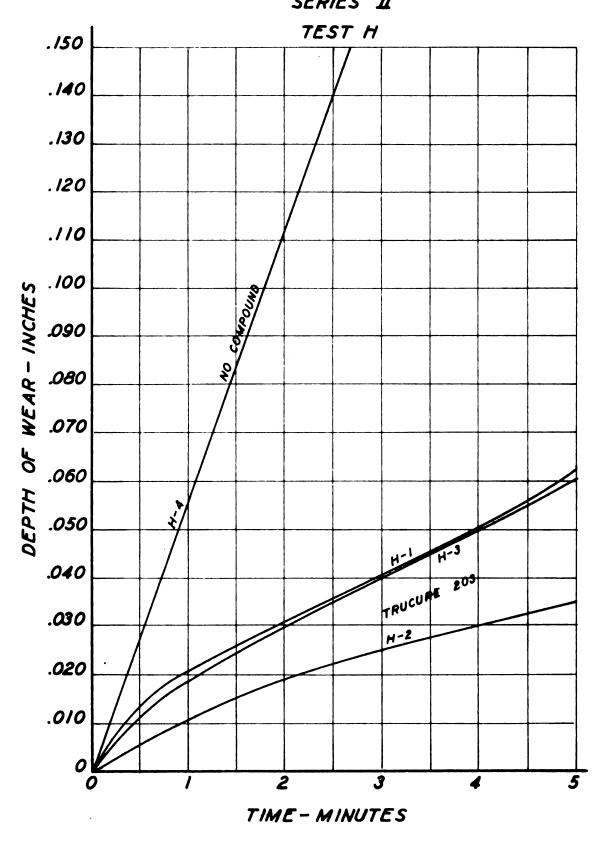
MEMBRANE CURING STUDY ABRASION TEST SERIES I



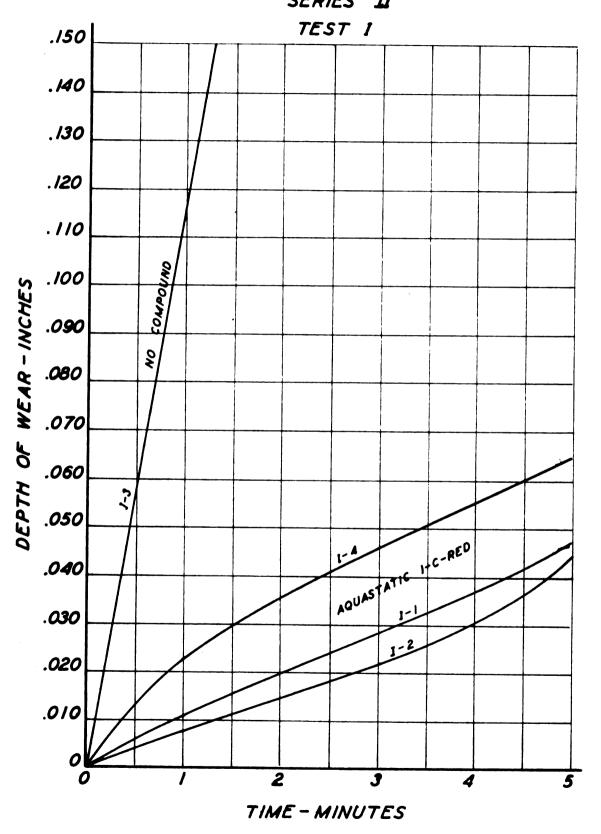
MEMBRANE CURING STUDY ABRASION TEST SERIES 1



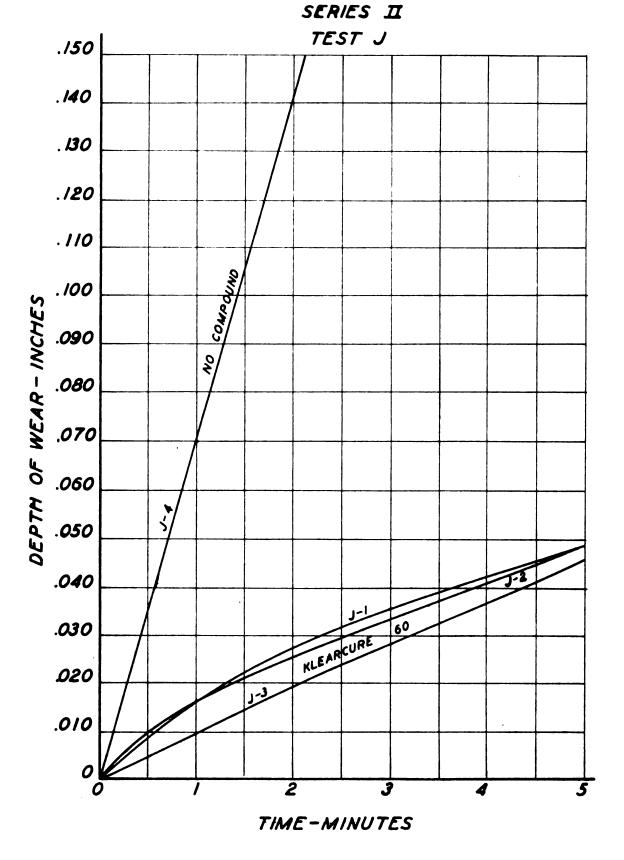
MEMBRANE CURING STUDY ABRASION TEST SERIES II



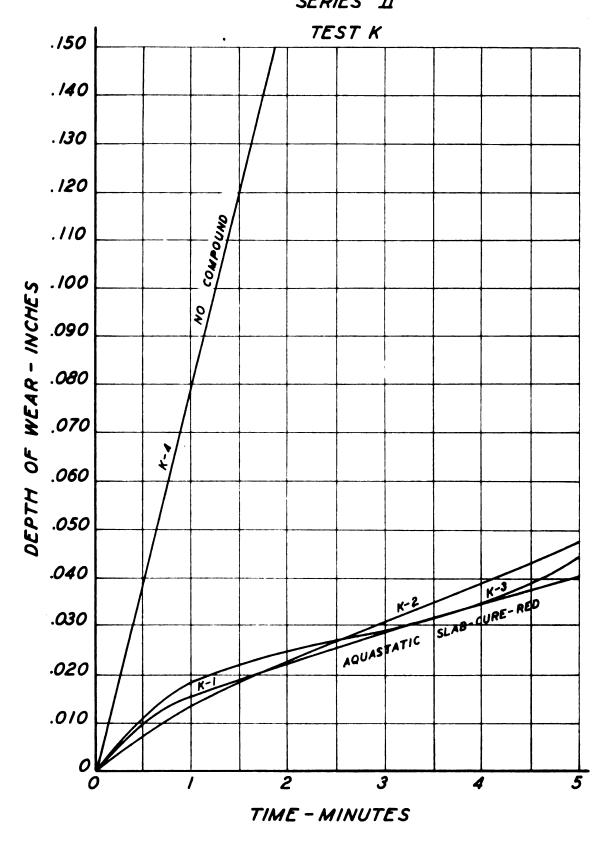
MEMBRANE CURING STUDY ABRASION TEST SERIES II



MEMBRANE CURING STUDY ABRASION TEST

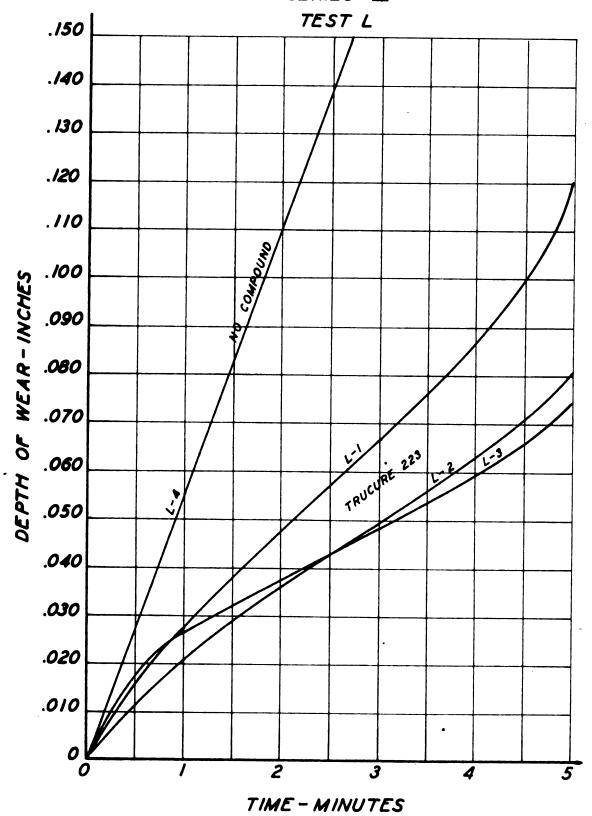


MEMBRANE CURING STUDY ABRASION TEST SERIES II



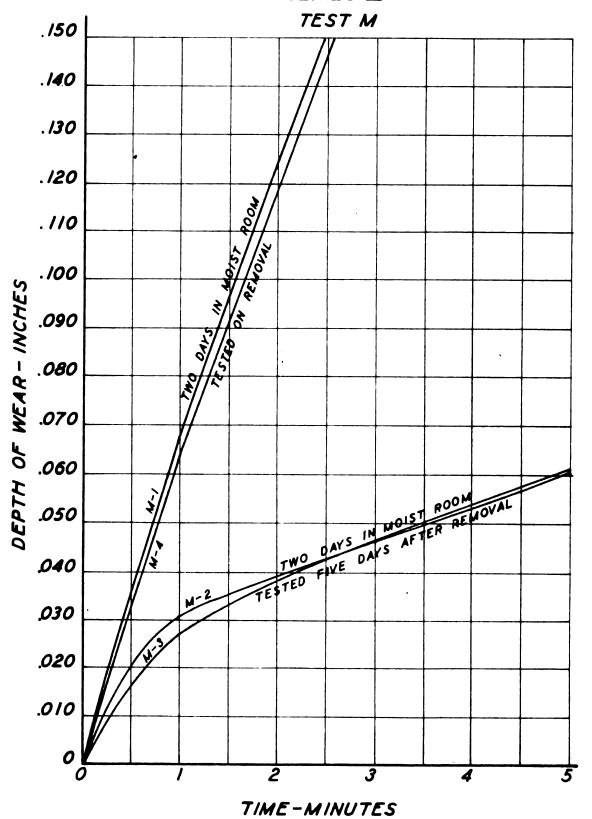
MEMBRANE CURING STUDY

ABRASION TEST SERIES II

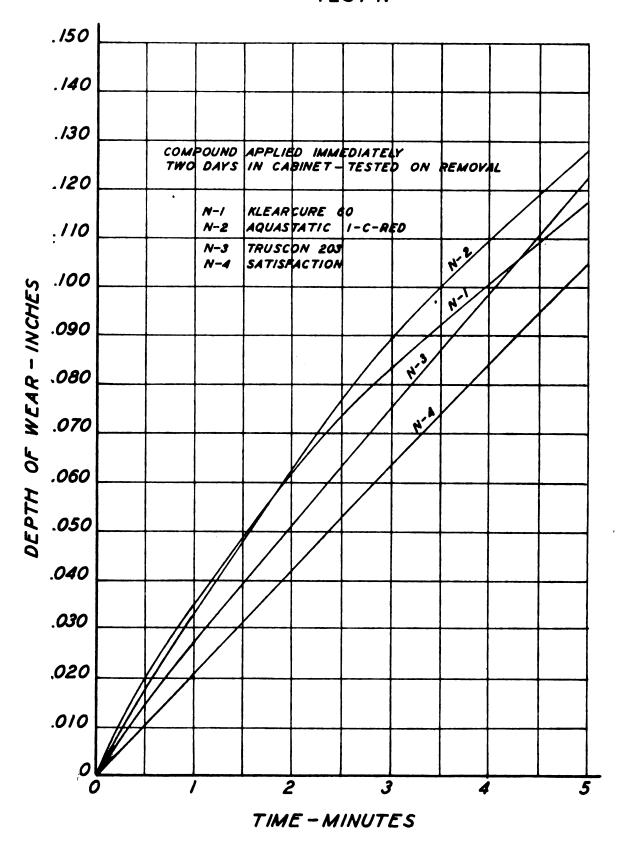


MEMBRANE CURING STUDY

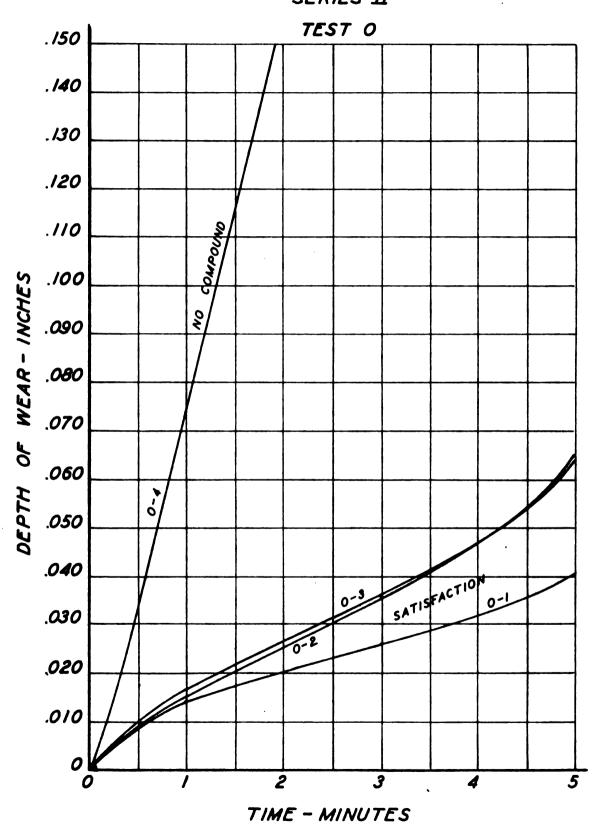
ABRASION TEST SERIES II



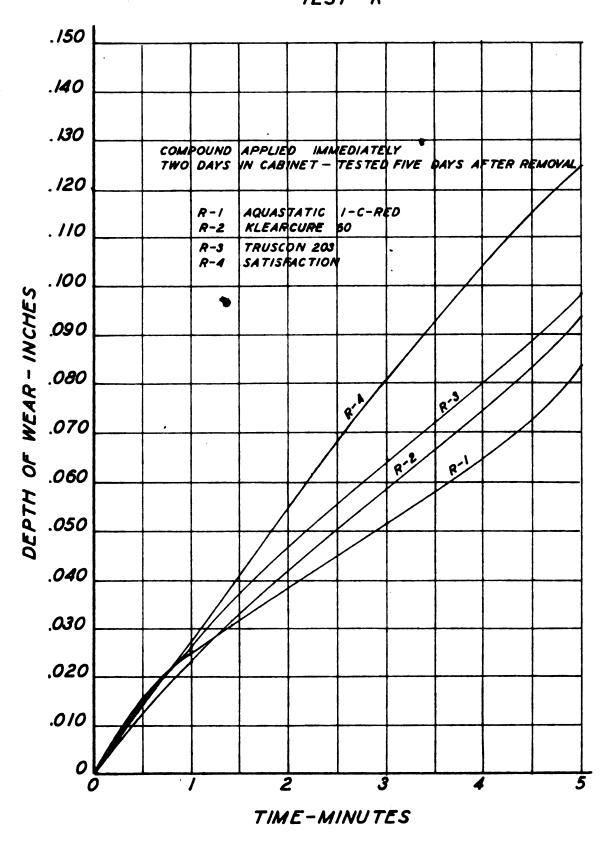
MEMBRANE CURING STUDY ABRASION TEST TEST N



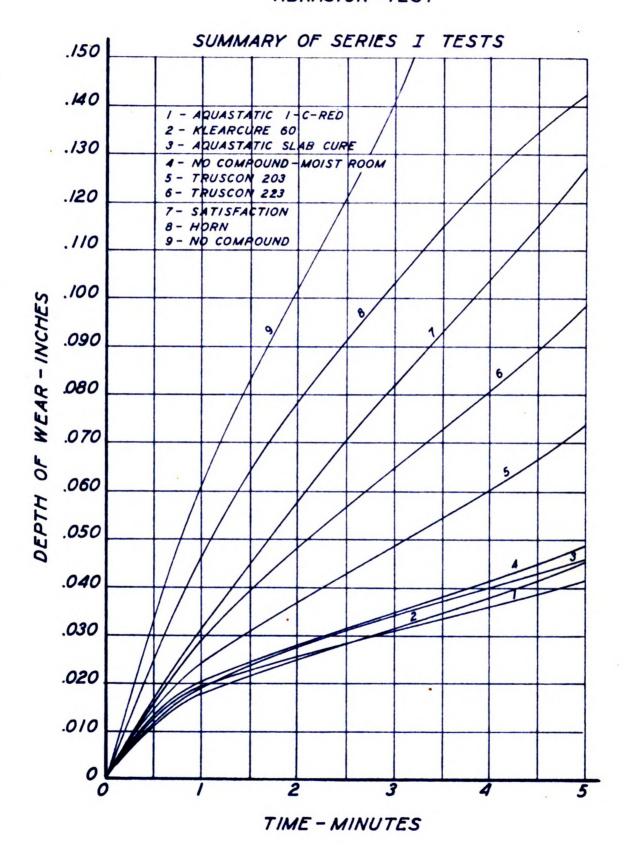
MEMBRANE CURING STUDY ABRASION TEST SERIES II



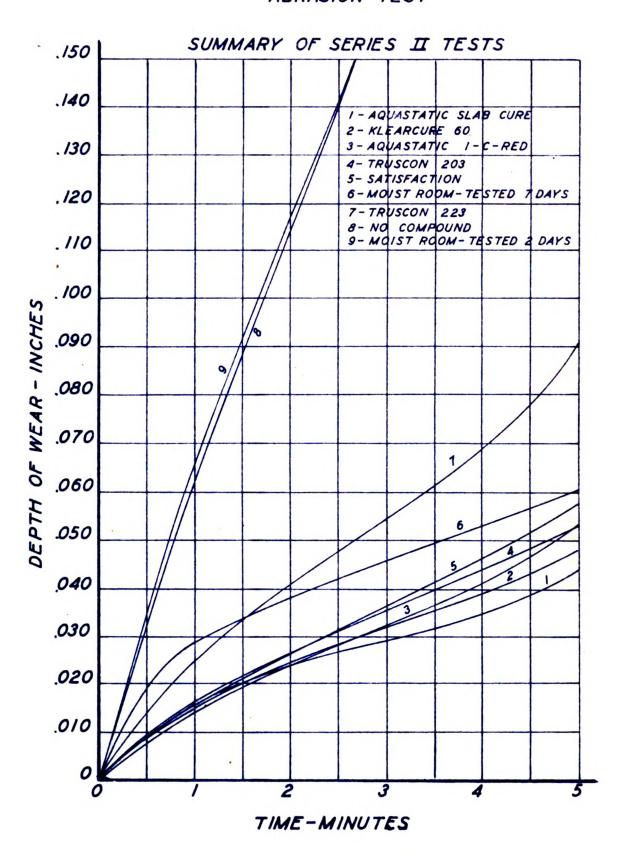
MEMBRANE CURING STUDY ABRASION TEST TEST R



MEMBRANE CURING STUDY ABRASION TEST



MEMBRANE CURING STUDY ABRASION TEST



UNCERTAINTIES

In this test, as in any other, there are certain uncertainties introduced during the test which must be considered. These are not due necessarily to any fault of the tester (although there may be error introduced by the carelessness of operation,) but are caused rather by the nature of the elements being tested and the testing apparatus. In the abrasion test, some of the uncertainties arising are as follows:

- 1. Variations in the specimens themselves due to nonuniform water loss on curing. If the membrane is not evenly applied, one part of the specimen may lose more water than another part, and therefore, wear faster.
- 2. Differences in the surface characteristics of the various specimens. Irregularities, such as roughness, will cause a variation of the results.
- 5. Variations in the speed of the drill press operation. This error is small.
- 4. Aggregate in a specimen will introduce error since most aggregates will not wear as fast as the mortar itself will. Although fine aggregate was used in the preparation of the specimens for this study, in a few cases the arrangement was such as to cause uneven wear.
- 5. Impact effect of the tool. On a rough specimen, the tool showed a tendency to bounce; this might cause accelerated wear.

The results as shown in the accompanying graphs seem to be quite consistent; for example, the curves representing the wear of the specimens cured with Klearcure 60 vary only a little over one per cent. The widest variation is shown on the specimens which had no compound, and on these, the results are in close enough agreement to show a very definite trend.

Since the results do seem quite consistent, we feel that it is safe to proceed to draw definite conclusions from the test results.

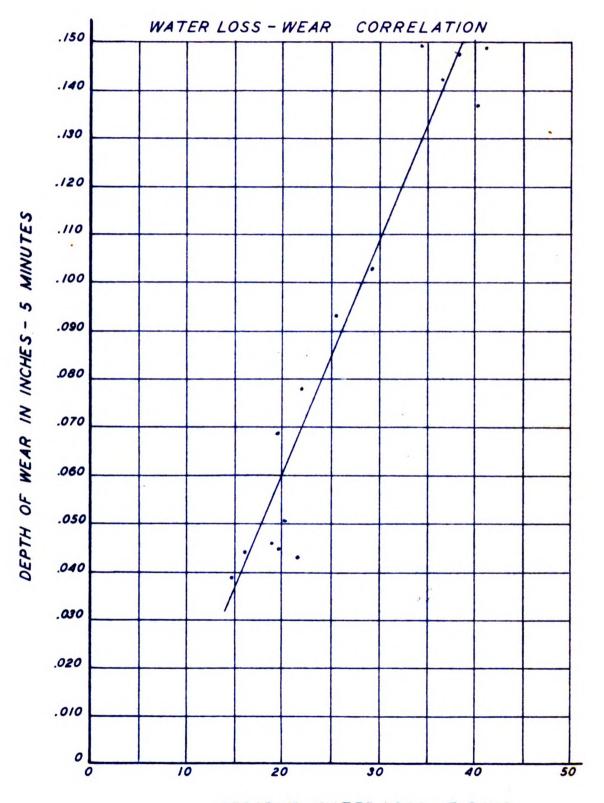
CONCLUSIONS

From the results of the abrasion test, the following can be safely concluded, we believe:

- Membrane cured concrete can be depended on to give good wearing qualities to approximately the same degree as water cured concrete. This does not apply, of course, to all of the membranes, but to only the more efficient preparations.
- 2. Not all membranes are effective. In Series I, Horn curing compound and Satisfaction gave results which are but little better than those obtained with no special curing. Truscon 223 is somewhat better and Truscon 203 gave fairly good results. The best results were given by Aquastatic 1-C-Red, Klearcure 60, and Aquastatic Slab Cure, all of which gave nearly the same results as the moist room cured specimens. In Series II, the order of merit was changed slightly, as shown on the summary graph. For a graphic picture of the relative effectiveness of the various compounds, see the summary graphs included with this test.
- 3. The wear of a mortar which receives no special curing will be about four times that of watercured or good membrane cured mortar.
- 4. There is a definite correlation between the water loss and the resistance to wear in a membrane cured specimen. Using the statistical method of least squares, a correlation coefficient of .74

- was obtained for this relationship. The graph on the page following also illustrates this correlation.
- 5. Membranes should not be applied immediately upon molding. Tests N and R in Series II were those in which the membrane was applied immediately after the specimen was molded; in the other tests, a period of about three hours elapsed between mixing and application of the compound. The increased wear on those specimens which were sprayed immediately may be due to chemical reaction between the compound and the cement in the mortar. Whatever the cause, however, a definite weakening of the surface is indicated.
- 6. Membrane cured specimens develop their wearresisting qualities in a shorter period of time
 than the water cured specimens. Test M in Series
 II shows the wear curves of specimens cured in the
 moist room with no compound. Those specimens
 tested at two days gave results practically the
 same as for specimens cured in the cabinet with
 no compound. When tested at seven days, however,
 the water cured specimens gave the same results
 as the two day membrane cured specimens. It may
 be claimed that the specimens cured in the cabinet
 with no compound would show good wear resisting
 qualities at seven days just as the moist room
 cured specimens did. The results of Series I

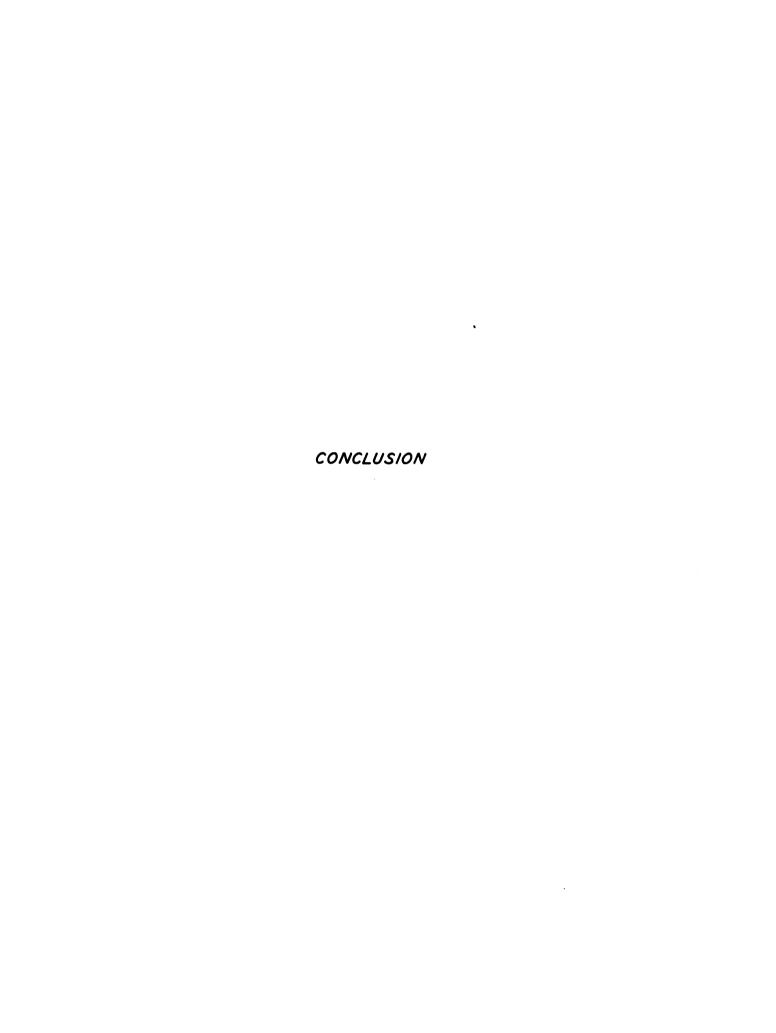
MEMBRANE CURING STUDY



PERCENT-WATER LOSS - 7 DAYS

show that this is not true.

Of the six points stated, the first two contain the most important findings of the abrasion test, and from these, it seems that membrane curing compounds are not merely manufacturer's dreams, but on the contrary, have a definite place in concrete work, and if the results of this study can be taken as an indication (and we naturally believe it can) the future of membrane curing materials is anything but gloomy.



In this report, even though we have made several definite conclusions, we do not wish to convey the idea that the investigation was as extensive as we might have The time element hindered our investigation of many important items in connection with the relative merits of membrane curing compared with the older types of curing. The Abrasion Test, in particular, has opened up new possibilities in the testing of various curing methods. The cycle of testing, Water-Retention Test, Flexural Test, Surface Dehydration Analysis, and the Abrasion Test, has many advantages and we heartily recommend its use in future testing. By running several different tests on the same specimen, the correlation between tests is obtained, and the several tests may substantiate the validity of results. We realize that many important items have been touched only lightly, but we feel that this study might form a basis for future work and a suggestion for more thorough investigation in the future.

APPENDIX A - WATER RETENTION TEST DATA

APPENDIX A - WATER RETENTION TEST DATA

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III.	Wate	r Retention Test							
	Α.	1. Data applicable to every specimen under series. 2. Test A. 3. Test B. 4. Test C. 5. Test D. 6. Test E. 7. Test F. 8. Explanation of computations under tabulated data. 9. Tabulated data (Test A - Test F).	8 9 11 16 20 26 32						
	В.	Series II 1. Data applicable to every specimen under this series	. 46						
		2. Test H = Test R	47						

MEMBRANE CURING STUDY WATER RETENTION TEST

<u>Humidity Control of Cabinet</u>

March 23, 1943

Trial	Dew	Dew	De w	Back of	Fan	Front of	Fan
		(Going	Point Average			Air Temp. (Dry bulb)	
1				100.5°F. 99.8			73 [°] F.
5	9.0	9.0		100	74.0 74	101	73
2	8.5	9.5	9.0	97	73	98	72
3	8.8	9.5	9.15	100	74.5	101	73
3	8.8	9.4	9.1	9 7	73.5	98	72

Trial	. Dew	Vapor	Air	Vapor for Sat.	Humidity	Wet & Dry	Bulb Humid.
	Point	in Air gr. per	Temp.	gr. per	from Dew	Back of	Front of
	Average	~ -	Average		Point	Fan	Fan
ı	48.2°F.	3.871	100.75°F	r. 20.38	19.0%	29%	25%
1	47.7	3.804	100.4	20.19	18.8	31	25'
2	48.5	3.911	100.5	20.25	19.3	29	25
2	48.2	3.871	97.5	18.65	20.8	31	28
3	48.5	3.911	100.5	20.25	19.3	30	25
3	48.4	3.898	97.5	18.65	20.9	32	28

Average correction to be applied to wet and dry bulb apparatus in back of fan is: 10.8 %

Average correction to be applied to wet and dry bulb apparatus in front of fan is: 6.3%

MEMBRANE CURING STUDY WATER RETENTION TEST

Humidity Control of Cabinet

April 2, 1943

	Dew	Point	Pack c	f Fan	Vapor	Humidity	Humidit	у
Trial			Air	Wet	in Air	from	Wet &	Difference
	°C.	°F•	Temp.	Bulb	gr./cu.ft.	Dew Pt.	Dry Bul	р
1	17.8	64	100	80	6.65	34.2	42	7.8
2	17.6	63.7	100	7 9	6.58	33.8	40	6.2
3	17.0	62.6	100	80	6.35	32.7	42	9.3
4	18.0	64.4	100	80	6.73	34.6	42	7.4
							Average	7.7

Since the dew point apparatus which gives a correct humidity reading cannot be used, as it was borrowed, the humidity will be maintained by correcting the wet and dry bulb reading and then maintaining the humidity at this desired level. Since the humidity should be maintained at 32.5 %, the wet and dry bulb reading to maintain this desired humidity is 40.2 %, or the wet bulb reading should be between 79 and 80° F., if the air temperature is 100° F.

WATER RETENTION TEST

Measurement of Air Flow in Control Cabinet

Velometer Serial No. Type No.	3314	•	Date Tested 2-19-43
13 20 170	2002		

Readings taken at 3 1/2" height

Across right edge

Depth from Front of Cabinet	Velocity of Air Feet per Min.
3 " 6 9	101 101 95
12 15 18	101 101 117

Across center

Depth from Front of Cabinet	Velocity of Air Feet per Min.
3 " 6 9	101 117 101
12 15	90 95
18	100

Across left edge

Depth from Front of Cabinet	Velocity of A Feet per Mir			
3 "	143			
6	154			
9	154			
12	148			
15	143			
18	148			

These readings are corrected for temperature.

Minor Test

in Connection with

WATER RETENTION TEST

SPECIFIC GRAVITY OF MEMBRANE CURING COMPOUNDS

Curing Material		of Flask	Wt. of 250 ml. Curing Compound	
Truscon 223	97.8 g.	297 .7 g.	199.9 g.	.800
Truscon 203	97.8	307 .7	209.9	.840
Truscon 214	97.9	312.9	215.0	.860
Truscon 199	97.9	317.8	219.9	.880
Klearcure 60	97.7	330.1	232.4	.929
Satisfaction 45	98.1	315.8	217.7	.871
Horn	97.7	420.5	322.8	1.291
Aquastatic Slab Cure Red	97.8	307.0	209.2	.837
Aquastatic 1-C-Red	97.8	328.5	230.6	.923

4

MINOR TESTS

in connection with

WATER RETENTION TEST

PERCENT SOLIDS OF CURING MATERIALS

Curing Material	Weight Liquid	Weight Dry Solids	Percent Solids
Klearcure 60	3.3243 g.	1.8916 g.	56.90 g.
Aquastatic 1-C-Red	2.7740	1.3063	47.09
Aquastatic Slab Cure Red	3.3645	1.4693	43.67
Horn	6.0959	2.3452	38.47
Satisfaction 45			45.00
Truscon 203	3.4417	1.5758	45 .7 9
Truscon 223	2.5832	0.6904	26.73
Truscon 199	2.6108	1.1472	43.94
Truscon 214	1.8322	0.8148	44.47

MINOR TESTS

in connection with

WATER RETENTION TEST

WATER CONTENT OF OXFORD SAND AT SATURATED SURFACE DRY CONDITION

Wt. of can - 78.59 g.

Wt. of can and sand (moist) - 614.70 11:00 a.m. March 12, 1943

Wt. of can and sand (dry) - 607.73 11:50 a.m. March 16, 1943

Wt. of sand (moist) = 614.70 - 78.59 = 536.11 g.

Wt. of sand (dry) = 607.73 - 78.59 = 529.14 g.

Percent of moisture = $\frac{536.11 - 529.14}{529.14}$ = 1.1282 %

PERCENT SOLIDS OF LATEX SEALER

Wt. of can - 19.88 g.

Wt. of can and latex (liquid) - 26.73 4:45 p.m. 3-2-43

Wt. of can and latex (solids) - 21.93 12:30 p.m. 3-3-43

Wt. of can and latex (solids) - 21.93 12:30 p.m. 3-4-43

Wt. of latex (liquid)= 26.73 - 19.88 = 6.85 g.

Wt. of latex (solids)= 21.93 - 19.88 = 2.05 g.

Percent of solids = $\frac{100 \times 2.05}{6.35}$ = 30.0 %

MINOR TESTS

in connection with

WATER RETENTION TEST

Series I

EVAPORATION OF MOISTURE WHILE MIXING

This test is to determine the amount of water lost, due to evaporation while mixing. Mixing takes approximately thirty minutes.

4750 g. sand

475 g. water

5225 g. at 11:30 a.m. March 16, 1943

- 5204 g. at 12:00 m. March 16, 1943

21 g. water evaporated

Since in each specimen there is approximately 4500 grams of material, excluding water, the allowance for evaporation is 4500 x 21 + 4700 is 20 grams.

Therefore in the computations 20 grams will be subtracted from the mixing water to determine the original water in the specimen.

WATER RETENTION TEST

Series I

Data applicable to every specimen under this series.

Mortar Data

Brand Sand	of	cement (a)	- Huron Source -	Standard Oxford, M	√ichigan		
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		(b)		- Absolute			
			Fass	ing No. 4	100 %		
				16	60 %		
				50	15 %		
				100	2 %		
		(c)	Moisture	(saturated	surface-drie	∍đ	
				condition	-	1.128	%

Proportioning of Mix

Cement 2700 g.

Water 1080 g. (.40 of cement by weight)

Sand 7460 g. (sufficient for 25% flow)

Total 11240 g.

Percent water - 9.60854%

This batch is sufficient for two specimens.

Application of Membrane Curing Compound

After sufficient time had elapsed after finishing the specimens for the surface moisture to disappear (approximately 3 hours), the membrane was applied by spraying with an atomizer at the rate of 200 sq. ft. to the gallon.

Sealing of Edges

The edges where the mortar met the pan were sealed with a Latex material as soon as the membrane had dried. (approximately 1/2 hour after the application of the membrane).

Weighing of Specimens

The specimens were weighed daily to determine the water loss. This weighing was done as close to the time of day of the application of the membrane as feasible.

WATER RETENTION TEST

Series I Test A

Specimen_A-l
Curing Method Moist Room

Date February 6, 1943
Tested by L. T. O.

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Moist Temp.	Room Humidity
Tituat don	2-6-43	4:00 p.m.	6063 g.	66° F.	100%
First day Second day	2-8-43	2:30	6068	H	11
Third day	2-9-43	2:00	6074	11	11
Fourth day	2-10-43	2:00	6081	tt	11
Fifth day	2-11-43	4:30	6086	11	10
Sixth day	2-12-43	2:45	6093	11	tt
Seventh day	2-13-43	2:00	6099	11	11

Wt. of mortar and pan 6063 g.

Wt. of pan <u>1066</u> g.

Wt. of mortar 4997 g.

Original water in specimen $4997 \times 9.60854\% - 20 = 460.1 \text{ g}$.

WATER RETENTION TEST

Series I Test A

Specimen A-2
Curing Method Moist Room

Date February 6, 1943
Tested by I. T. O.

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Moist Temp.	Room Humidity
	2-6-43	4:00 p.m.	5899 g.	66° F.	100%
First day					
Second day	2-8-43	2:30	5908	tt .	11
Third day	2-9-43	2:00	5912	н	16
Fourth day	2-10-43	2:00	5916	11	11
Fifth day	2-11-43	4:30	5924	T1	H
Sixth day	2-12-43	2:45	592 7	11	tt
Seventh day	2-13-43	2:00	5938	11	n

Weight of mortar and pan 5899 g. Weight of pan 1038 g. Weight of mortar 4861 g.

Original water in specimen $4861 \times 9.60854\% - 20 = 447.1 \text{ g}.$

WATER RETENTION TEST

Series I Test E

Specimen E-3

Date March 25, 1943

Curing Material Truscon 203

Tested by L. T. C.

Position in Cabinet 3

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Temp. of Cabinet	Wet & Dry Bulb Humidity Reading	Correct Humidity
Before membrane After membrane Before sealer After sealer First day Second day Third day Fourth day Fifth day Sixth day Seventh day	3-25-43 3-25-43 3-25-43 3-25-43 3-26-43 3-27-43 3-28-43 3-29-43 3-31-43 4-1-43	10:05 a.m. 1:15 p.m. 1:20 1:50 1:55 4:00 12:00 m. 3:30 p.m. 12:00 m. 1:45 p.m. 1:15	6009 6014 6011 6018 5965 5949 5936 5929	100° F. 100 100 100 100 100 100 100 100 100	33% 36 36 36 36 31 334 335 35 35	22% 255 255 222222222222222222222222222

Weight of mortar and pan $\frac{6054}{1.065}$ g. Weight of mortar $\frac{4989}{9}$ g.

Original water in specimen $4989 \times 9.60854\% - 20 = 459.4$ g.

Membrane Application
Exposed area, 72 sq. in.
Amt. of mat'l. applied
Sp. Gr. of mat'l.
Checking by weight

9.5 ml.
840
8.3 g.

WATER RETENTION TEST

Series I Test B

Specimen B-2

Date February 20, 1943

Curing Mat'l. Klearcure 60

Tested by L. T. O.

Position in Cabinet 6

TEST RECORD

Remarks	Da te	Time	Weight of Specimen	Temp. of Cabinet	Wet & Dry Bulb Humidity Reading	Correct Humidity
Before membrane After membrane	2-20-43	2:58 p.m.	6039 g.	98° F.	36%	25%
	2-20-43	6:00 p.m.	6009	100	36	25
	2-20-43	6:10 p.m.	6016	100	36	25
Before sealer	2-20-43	6:45 p.m.	6008	100	40	29
After sealer	2-20-43	6:50 p.m.	6012	100	40	
First day	2-21-43	4:15 p.m.	598 7	100	33	29 22
Second day	2-22-43	2:30 p.m.	596 7	99	33	22
Third day	2-23-43	2:00 p.m.	5956	99	33	22
Fourth day	2-24-43	2:45 p.m.	59 51	99	33	22
Fifth day	2-25-43	12:15 p.m.	59 3 9	1 00	31	2 0
Sixth day	2-26-43	2:45 p.m.	59 3 2	100	34	23
Seventh day	2-27-43	2:30 p.m.	5927	99	32	21

Wt. of mortar and pan 6039 g. Wt. of pan 1041 g. Wt. of mortar 4998 g.

Original water in specimen $4998 \times 9.60854\% - 20 = 459.1 g$.

Membrane Application
Exposed area, 72 sq. in.
Amt. of mat'l. applied 9.5 ml.
Sp. Gr. of mat'l. .929
Checking by weight 9.0 g.

WATER RETENTION TEST

Series I Test D

Specimen D-2

Date <u>March 13, 1943</u>

Curing Material Aquastatic 1-C-Red

Tested by L. T. O.

Position in Cabinet_6_

TEST RECORD

Remark s	Date	Time	Weight of Specimen	Temp. of Cabinet	Wet & Dry Bulb Humidity Reading	Correct Humidity
Before membrane After membrane Before sealer After sealer First day Second day Third day Fourth day Fifth day	3-13-43 3-13-43 3-13-43 3-13-43 3-14-43 3-15-43 3-16-43 3-17-43 3-18-43	1:15 p.m. 3:50 3:55 4:50 5:00 4:15 4:00 4:00 3:45 10:00 a.m.	6079 g. 6045 6052 6048 6054 6028 6016 6006 5998	100° F. 100 100 100 100 100 100 100	29% 39 39 39 39 34 33 29	18% 28 28 28 28 28 22 22 18
Sixth day Seventh day	3-19-43 3-20-43	10:00 1:30 p.m.	5986 5982	100 100	2 7 35	16 24

Weight of mortar and pan $\frac{6079}{1041}$ g. Weight of mortar $\frac{5038}{5038}$ g.

Original water in specimen $5038 \times 9.60854\% - 20 = 464.1 \text{ g}$.

WATER RETENTION TEST

Series I Test D

Specimen D-5
Curing Material none

Date March 13, 1943

Tested by L. T. O.

Position in Cabinet_5_

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Temp. of Cabinet	Wet & Dry Bulb Humidity Reading	Correct Humidity
	3-13-43	2:45 p.m.	6132 g.	100° F.	36%	25%
Before sealer	3-13-43	5 :5 0	61 00	100	35	24
After sealer	3-13-43	6:00	6108	100	35	24
First day	3-14-43	4 : 15	5956	99	34	23
Second day	3-15-43	4:00	5937	100	33	22
Third day	3-16-43	4:00	5927	100	33	22
Fourth day	3-17-43	3:45	5919	100	29	18
Fifth day	3-18-43	10:00 a.m.	5913	100	29	18
Sixth day	3-19-43	10:00	590 7	100	27	16
Seventh day	3-20-43	1:30 p.m.	5902	100	35	24

Weight of mortar and pan $\frac{6132}{1061}$ g. Weight of mortar $\frac{5071}{5}$ g.

Original water in specimen $5071 \times 9.60854\% - 20 = 467.2 \text{ g}.$

Exposed area, 72 sq. in.

WATER RETENTION TEST

Series I Test E

Specimen <u>E-6</u>
Curing Material none
Position in Cabinet 6

Date March 25, 1943

Tested by L. T. C.

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Temp. of Cabinet	Wet & Dry Bulb Humidity Reading	Correct Humidity
Before sealer After sealer First day Second day Third day Fourth day Fifth day Sixth day Seventh day	3-25-43 3-25-43 3-26-43 3-27-43 3-28-43 3-29-43 3-30-43 4-1-43	11:10 a.m. 2:05 p.m. 2:10 4:00 12:00 m. 3:30 p.m. 12:00 m. 1:45 p.m. 1:15 1:00	5933 g. 5901 5908 5760 5746 5734 5727 5720 5716 5712	100° F. 100 100 100 99 100 100 100	36% 36 31 34 33 34 33 35	25% 25 25 20 23 22 23 24 24

Weight of mortar and pan 5933 g. Weight of pan 1049 g. Weight of mortar 4884 g.

Original water in specimen $4884 \times 9.60854\% - 20 = 449.3 \text{ g}$.

Exposed area, 72 sq. in.

WATER RETENTION TEST

Series I Test F

Specimen F-1
Curing Method Moist Room

Date <u>April 1, 1943</u>

Tested by L. T. O.

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Moist Temp.	Room Humidity
First day Second day	4-1-43 4-2-43 4-3-43	2:05 p.m. 4:30 12:00 m.	6007 g. 6032 6038	66° F.	100%
Third day Fourth day	4-4-43 4-5-43	4:30 p.m. 4:00	6041 6046	11 11	11 11
Fifth day Sixth day	4-6-43 4-7-43	3:30 3:15	6047 6048	11 11	18 11
Seventh day	4-8-43	7:00	6047	11	18

Weight of mortar and pan $\underline{6007}$ g.

Weight of pan 1068 g.

Weight of mortar 4939 g.

Original water in specimen $4939 \times 9.60854\% - 20 = 454.5 \text{ g}$.

WATER RETENTION TEST

Series I Test F

Specimen F-2
Curing Method Moist Room

Date April 1,1943
Tested by L. T.O.

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Moist Temp.	Room Humidity
	4-1-43	2:20 p.m.	5932 g.	66° F.	100%
First day	4-2-43	4:30	5965	IT	11 '
Second day	4-3-43	12:00 m.	5978	H	11
Third day	4-4-43	4:30	5984	H	11
Fourth day	4-5-43	4:00	598 7	11	H
Fifth day	4-6-43	3:30	5990	11	11
Sixth day	4-7-43	3:15	5990	It	11
Seventh day	4-8-43	7:00	5990	11	11

Weight of mortar and pan 5932 g.

Weight of pan 1040 g.

Weight of mortar 4892 g.

Original water in specimen $450.6 \times 9.60854\% - 20 = 450.6$ g.

WATER RETENTION TEST

Series I Test F

Specimen F-3
Curing Method Moist Room

Date April 1, 1943
Tested by L. T. O.

		TEST REC	ORD		
Remarks	Date	Time	Weight of Specimen	Moi:	st Room Humidity
First day Second day Third day Fourth day Fifth day Sixth day	4-1-43 4-2-43 4-3-43 4-4-43 4-5-43 4-6-43 4-7-43	3:50 p.m. 4:30 12:00 m. 4:30 p.m. 4:00 3:30 3:15	6060 g. 6094 6105 6107 6113 6114 6115	66° F.	100%
Seventh day	4-8-43	7:00	6117	***	11

Weight	of	mortar	and	pan	<u>6060</u>	g.
Weight	of	pan			1068	g.
Weight	of	mortar			4992	g.

Original water in specimen $4992 \times 9.60854\% - 20 = 459.6$ g.

WATER RETENTION TEST

Series I Test F

Specimen F-4
Curing Method Moist Room

Date April 1, 1943
Tested by L. T. O.

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Mois Temp.	st Room Humidity
First day Second day Third day Fourth day Fifth day Sixth day	4-1-43 4-2-43 4-3-43 4-4-43 4-5-43 4-6-43 4-7-43 4-8-43	3:57 p.m. 4:30 12:00 m. 4:30 p.m. 4:00 3:30 3:15 7:00	5970 g. 6003 6017 6022 6027 6029 6030 6033	66° F.	100%

Weight of mortar and pan 5970 g.
Weight of pan 1040 g.
Weight of mortar 4930 g.

Original water in specimen $4930 \times 9.60854\% - 20 = 453.7 \text{ g}.$

WATER RETENTION TEST

Series I Test F

Specimen F-5
Curing Method Wet Burlap

Date April 1, 1943

Tested by L. T. O.

		TEST RECO	RD		
Remarks	Date	Time	Weight of Specimen	Laborato	ory Air Humidity
Start of Curing First day Second day Third day Fourth day Fifth day Sixth day Seventh day	4-2-43	4:35 p.m. 7:20 4:30 2:00 m. 4:30 p.m. 4:00 3:30 3:15 7:00	6146 g. 6135 6158 6160 6166 6174 6170 6170	72° F. 72 75 75 75 75	22% 41 24 32 34 38

Weight of mortar and pan 6146 g. Weight of pan 1063 g. Weight of mortar 5083 g.

Original water in specimen $5083 \times 9.60854\% - 20 = 468.4 \text{ g}$.

WATER RETENTION TEST

Series I Test F

Specimen F-6
Curing Method Ponding

Date April 1, 1943
Tested by L. T. O.

TEST RECORD

Remarks	Date	Time	Weight of Specimen	Labora Temp.	atory Air Humidity
Start of Curing First day Second day Third day Fourth day Fifth day Sixth day	4-1-43 4-1-43 4-2-43 4-3-43 4-4-43 4-5-43 4-6-43 4-7-43	4:45 p.m. 7:20 4:30 12:00 m. 4:30 p.m. 4:00 3:30 3:15	6005 g. 5995 6033 6041 6045 6047 6051 6052	72° F. 72 75 75 75	22% 41 24 32 34
Seventh day	4-8-43	7:00	6053	7 5	38

Weight of mortar and pan 6005 g.
Weight of pan 1050 g.
Weight of mortar 4955 g.

Original water in specimen $4955 \times 9.60854\% - 20 = 456.1 \text{ g}.$

Series I

Explanation of Computations under Tabulated Data

- Original Water (A) This is the water in the specimen at the time of finishing of the mortar. It was computed as follows: weight of mortar times percent water minus 20 grams. This correction is applied, because during the mixing operation, approximately 1/2 hour, the mortar loses moisture. (Please refer to datum under Evaporation Loss While Mixing under Minor Test).
- Correction for Curing Material (B) Because the membrane curing compounds are highly volatile, much of the weight disappears in a few hours. This correction is necessary or this loss of weight would be considered water loss, which is not correct. (Please refer to Percent Solids of Membrane Curing Materials under Minor Tests).
- Correction for Sealer (C) The Latex material used to prevent moisture from escaping around the edges of the pan is also a material which will evaporate considerably. Therefore, a correction should be used to discount this loss of weight, so that it will not be considered water loss. (Flease refer to Percent Solids of Sealing Material under Minor Tests).
- Water Loss While Blank (D) This is the water loss from the time of finishing until the time when the mortar was in a condition so that the membrane could be applied. (Approximately 3 hours).

- Water at Application of Membrane (E) This is the water in the specimen at the time the membrane was applied; or in other words, the Original Water minus the Water Loss While Elank.
- <u>Water Loss</u> (F) This is the corrected water loss as determined by the loss in weight of the specimen from the time that the membrane was applied.
- Percent Water Loss = $\frac{100 \text{ F}}{A}$ This is the percent water loss as determined by the water loss from the application of the curing material times 100, divided by the original water in the specimen. This was computed for the two-day and seven-day periods.
- Percent Water Loss = $\frac{100 \text{ F}}{E}$ This is the percent water loss as determined by the water loss from the application of the curing material times 100, divided by the water in the specimen at the time of application of the membrane. This percent water loss is probably the better one to use in comparing the results of the various curing materials.
- Percent Efficiency = $100 \frac{100 \text{ F/E}}{\text{F/E} \text{ (blank)}}$ This computation is also useful in comparing the various membrane curing compounds. A slight explanation is necessary. If the membrane were absolutely water-tight, the percent efficiency would be 100, while if the membrane were of no use whatever in conserving the water for the hydration of the cement, the efficiency would be 0. The higher the percent efficiency, the more the water is retained in the mortar and, consequently, the more water is available in the hydration of the cement.

TABULATED DATA - Test A

Specimen		A-l		A-2	
Curing			Moist Roc 66° F. 100 % Rel		
Original water	(A)	460.1	g.	447.1	g.
Water gain	(F)				
l day					
2 days		5.	g•	9	g.
3 days		11		13	
4 days		18		17	
5 days		23		25 [°]	
6 days		30		28	
7 days		36		39	
Percent water gain =	100 F				
2 days		1.0	8 %	2.01	. %
7 days		7.8	%	8.7	%
Percent efficiency =	100 F/A F/A (blank)				
2 days		103.3	%	106.1	%
7 days		118.9	%	121.1	%

TABULATED DATA - Test B

Specimen		B-1	B -2	B-3	B -4	B - 5
Curing Material	L	Horn	Klearcure	Klearcure	e Horn	Blank
Original water	(A)	466.2 g	. 459.1 g.	456.2 g.	475.2 g.	469.7 g.
Correction for curing material	L(B)	6	4	4	6	0
Correction for sealer	(C)	1	1	1	1	1
Water loss while blank	(D)	37	30	37	39	36
Water at appl. of membrane	(E)	429.2	429.1	419.2	436.2	433 .7
Water loss	(F)					
1 day 2 days 3 days 4 days 5 days 6 days 7 days		132 150 160 165 177 184 188	27 47 58 63 75 82 87	34 53 63 68 79 86 91	137 155 164 170 182 189	136 154 165 170 181 188 194
Percent water loss = 100 F						
2 days 7 days		32.2 40.3	10.25 18.98	11.61 19.92	32.6 41.1	32.8 41.3
Percent water loss = 100 F						
2 days 7 days		35.0 43.8	10.96 20.25	12.65 21.70	35.6 44.7	35.6 44.8
Percent efficient 100 - 100 F/E (b)	F/E					
2 days 7 days		1.50 2.20	69 . 2 54 . 8	64.4 51.6	0.0 0.20	0.0

TABULATED DATA - Test C

Specimen		C-1	C-2	C-5	c-6
Curing material		Satisfac	tion 45	Blank	Blank
Original water	(A)	459.0 g.	465.3 g.	478.3 g.	469.2 g.
Correction for curing material	(B)	4	4	0	0
Correction for sealer	(C)	4	2	2	3
Water loss while blank	(D)	52	49	51	51
Water at appl. of membrane	(E)	407.0	416.3	427.3	418.2
Water loss	(F)				
1 day 2 days 3 days 4 days 5 days 6 days 7 days		107 127 138 147 155 161 166	100 120 131 139 147 153 159	143 162 173 183 190 196 204	138 156 167 175 183 189
Percent water loss = 100 F					
2 days 7 days		27 . 7 36 . 2	25.8 34.2	33.9 42.7	33.3 41.6
Percent water loss = 100 F					
2 days 7 days		31.2 40.8	28.8 38.2	37.9 47.7	37.3 46.6
Percent efficient 100 - 100 F/E (black)	<u>/e</u>				
2 days 7 days		17.0 13.5	23.4 19.0	0.0	0.0

TABULATED DATA - Test D

Specimen	D-1	D-2	D-3	D-4	D - 5	D-6
Curing material		static C-Red		static ure Red	Blank	B la nk
Original water (A)	466.6g.	464.lg.	463.7g.	463.1g.	467.2g.	462.2g.
Correction for curing material (B) 4	4	4	4	0	0
Corr. for sealer(C)	2	2	3	3	3	2
Water loss while blank (D)	37	34	35	30	34	34
Water at appl. of membrane (E)	429.6	430.1	428.7	433.1	433.2	428.2
Water loss						
1 day 2 days 3 days 4 days 5 days 6 days 7 days	35 38 50 57 63 69 74	23 35 45 53 58 69	47 67 77 86 91 97 103	37 59 70 77 83 89 93	144 163 173 181 187 193	142 160 171 179 184 190 195
Percent water loss = $\frac{100 \text{ F}}{A}$						
2 days 7 days	8.1 15.8	7.5 14.9	14.4 22.2		34.9 42.4	34.6 42.2
Percent water loss = 100 F						
2 days 7 days	8.55 17.2	8.1 16.0	15.6 24.0	13.6 21.5	37.6 45.7	37.4 45.6
Percent efficiency 100 - 100 F/E F/E (blank)						
2 days 7 days	77.2 62.4	78.4 65.0	58.4 47.4	63.8 53.0	0.0	0.0

TABULATED DATA - Test E

Specimen		E-1	E-2	E-2	王-4	E-5	E- 6
Curing material		Trusc	on 223	Trusc	on 203	Blank	Blank
Original water	(A)	458.1g.	463.2g.	459.4g.	457.3g.	463.5g.	449.38.
Correction for curing material	(B)	2	2	4	4	0	0
Correction for sealer	(C)	2	3	2	3	2	2
Water loss while blank	(D)	40	35	45	44	41	41
Water at appl. of membrane	(E)	418.1	428.2	414.4	413.3	422.5	408.3
Water loss	(F)						
1 day 2 days 3 days 4 days 5 days 6 days 7 days		83 98 111 118 123 129 134	65 81 94 101 107 112	50 66 79 86 92 97 102	37 53 65 73 79 84 89	133 148 161 169 175 180 184	134 148 160 167 174 178 182
Percent water loss = $\frac{100 \text{ F}}{\text{A}}$							
2 days 7 days		21.4 29.2	17.5 25.2	14.4 22.2	11.6 19.5	32.0 39.7	33.0 40.5
Percent water loss = $\frac{100 \text{ F}}{\text{E}}$							
2 days 7 days		23.4 32.0	18.9 27.4	15.9 24.6	12.8 21.6	35.0 43.5	36 .3 44 . 6
Percent efficient 100 - 100 F/E (black)	/E						
2 days 7 days		34.5 27.4	47.0 37.8	55.5 44.2	64.2 51.0	0.0	0.0

TABULATED DATA - Test F

Specimen	F-1	F-2	F-3	F-4	F-5	F-6	
Curing	Moist 66° F.	Room 100% R.H	Moist 66° F.	Room 100% R.H.	Wet Burlap	Ponding	
Original water (A)	454.5 g.	450.6 g.	459.6 g.	453 .7 g.	468.4 g.	456.1 g	
Water gain (F)							
1 day 2 days 3 days 4 days 5 days 6 days 7 days	25 31 34 39 40 41 40	33 46 52 55 58 58 58	34 45 47 53 54 59	33 47 52 57 59 60 63	12 14 20 38 28 24 24	28 36 40 42 46 47 48	
Percent water gain	=						
100 F							
2 days	6.8 %	10.2 %	9.8 %	10.4 %	3.0 %	7.9 %	
7 days	8.8	13.3	12.8	13.9	5.1	10.5	
Percent efficiency = 100 - 100 F/A (blank)							
2 days	116.6	124.9	123.9	125.4	107.3	119.3	
7 days	121.5	132.4	131.2	133.9	112.4	125.6	

WATER RETENTION TEST

Series II

Data applicable to every specimen under this series

Mortar Data

Brand of cement - Huron Standard
Sand (a) Source - Oxford, Michigan
(b) Grading - Absolute
Passing No. 4 100 %
16 60 %
50 15 %
100 2 %

(c) Moisture (saturated surface-dried condition - 1.128 %)

Proportioning of Mix

Cement 680 g.

Water 272 g. (.40 of cement by weight)
Sand 2030 g. (sufficient for 25% flow)
Total 2982 g.

Percent water - 9.1214 %
This batch is sufficient for four specimens.

Sealing of Edges

Approximately 1 1/4 hours after finishing the specimens, they were taken from the cabinet, weighed, brushed, and re-weighed. Latex material was then placed in a small groove, formed for the purpose when finishing, sealing the specimen and the mould. This prevented water loss through shrinkage cracks.

Application of Membrane Curing Compound

Approximately 35 minutes after the edges had been sealed, the membrane was applied by spraying with an atomizer at the rate of 200 sq. ft. to the gallon.

Storage of Specimens

Temperature range - 100 ± 1° F.

Humidity range -31 - 35%

Air flow - 2 feet per second

WATER RETENTION TEST

Series II Test H

Specimen Curing material Weight pan & mortar Weight pan Weight mortar Weight before brushing Weight after brushing Weight after sealer Wt. before membrane Membrane should be applied Membrane was applied	583.3 585.3 583.9 3.12 3.09	591.8 g. 47.2 544.6 587.5 587.2 588.8 587.4	602.2 g. 42.9 559.3 597.6 599.3 597.8 3.12 3.12	H-4 Blank 585.7 g. 45.3 540.4 581.0 580.5 582.7 581.2			
4-14-43 1:00 p.m. 4-15-43 1:45 p.m.	584.2 583.7	587 . 9 58 7. 5	598 .1 59 7. 6	558 .1 555 . 5			
TABULATED DATA - TEST H							
Original water (A) Water loss while blank Water at time of	49.7 (D) 5.3	49 .7 5 . 0	51.0 5.1	49.3 5.3			
	44.4	44.7	45.9	44.0			
l day	•5 1•0	•5 •9	.6 1.1	22.5 25.1			
2 days Percent water loss = 1		• 9	1 • 1	27.1			
l day 2 days	1.125% 2.25 %	1.119% 2.01 %	1.309% 2.40 %	51.1% 57.0%			
Percent efficiency = (·	2.40 /0	J1 • 0/0			
l day	97.8 %	97.82 %	97.44 %	0.0%			
2 days Time of finishing Brushed and sealer app Membrane applied			95.79 % 11:45 a.m. 1:00 p.m. 1:35 p.m.	0.0%			

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WATER RETENTION TEST

Series II Test I

Specimen Curing material Weight pan & mortar Weight pan Weight mortar Weight before brushing Weight after brushing Weight after sealer Weight before membrane Memb. should be applie Membrane was applied 4-18-43 12:45 p.m. 4-19-43 10:40 a.m.	592.9 594.1 592.6	I-2 Aquastatic 1-C-Red 585.5 g. 45.4 540.1 581.5 581.3 582.9 581.3 3.44 3.36 580.1 579.4	I-3 Blank 596.5 g. 52.4 544.1 592.5 592.3 593.8 591.5 0.0 0.0 567.4	I-4 Aquastatic 1-C-Red 569.5 g. 44.0 525.5 565.3 565.1 567.0 565.3 3.44 3.38 564.7 563.9
	TABULATED	DATA - TEST	I	
Original water (A) Water loss while blank Water at time of	50.4 (D) 4.7	49.3 4.9	49.5 5.7	47.9 5.1
application (E) Water loss (F)	45.7	44.4	43.8	42.8
1 day 2 days Percent water loss = 1	2.1 2.9	2.4 3.1	23.6 25.6	1.7 2.5
l day 2 days Percent efficiency = (4.60% 6.35%	5.41% 7.0 % F/E)	54.0% 58.5%	3.95% 5.84%
l day 2 days	F/E (b 91.47% 89.14%		0.0%	92.68% 90.03%
Time of finishing Brushed and sealer app Membrane applied	lied 4-1	7-43 7-43 7-43	8:50 a.m 10:05 a.m 10:40 a.m	١•

WATER RETENTION TEST

Series II Test J

Specimen Curing material Wt. pan and mortar Wt. pan Wt. mortar Wt. before brushing Wt. after brushing Wt. after sealer Wt. before membrane Memb. should be applied Membrane was applied 4-18-43 1:00 p.m. 4-19-43 1:45 p.m.	J-1 Klearcure 60 574.1 g. 45.5 528.6 568.0 567.7 569.5 568.2 3.46 3.45 568.7 568.1 TABULATED DAT	575.0 g. 44.9 530.1 569.3 569.0 571.0 569.8 3.46 3.43 570.3 569.8	J-3 Klearcure 60 592.0 g. 44.9 547.1 585.5 585.3 586.7 585.4 3.46 3.44 585.0 584.9	J-4 Blank 590.4 g 44.0 546.4 583.6 583.7 583.5
Original water (A) Water loss while blank	48.2 (D) 6.7	48.4 6.1	49 . 9 7. 2	49.8 7.5
Water at time of application (E)	41.5	42.3	42.7	42.3
Water loss (F) 1 day 2 days	.9 1.4	.8 1.3	1.0 1.9	22.2 24.4
Percent water loss = 10 1 day 2 days Percent efficiency = (1	2.16% 3.38% 00 - 100 F/E		2.36% 4.45%	52•5% 57•7%
l day 2 days	F/E (blan 95.89% 94.14%	96.40% 94.66%	95.51% 92.28%	0.0% 0.0%
Time of finishing Brushed and sealer appl Membrane applied	4-17-43 ied 4-17-43 4-17-43	10:50 a	.m.	

WATER RETENTION TEST

Series II Test K

Specimen Curing material Weight pan & mortar Weight pan Weight mortar Wt. before brushing Wt. after brushing Wt. after sealer Wt. before membrane Memb. should be applied Membrane was applied 4-18-43 12:45 p.m. 4-19-43 12:55 p.m.	K-1 Aquastatic Slab Cure Red 562.1 g. 44.2 517.9 558.2 557.9 560.2 558.8 3.12 3.24 559.2 558.4			
•	TABULATED DATA	- TEST K		
Original water (A) Water loss while blank	47.3 (D) 4.2	48.4 5.2	46.6 5.1	47.7 6.0
Water at time of application (E)	43.1	43.2	41.5	41.7
Water loss (F) 1 day 2 days	.4 1.2	1.2 2.2	1.0 2.4	22.0 24.5
Percent water loss = 10 1 day 2 days Percent efficiency = (1	.929% 2.78 % 00 - <u>100 F/E</u>	2.78% 5.10%	2.41% 5.80%	52.8% 58.7%
l day 2 days	F/E (blank 98.24 % 95.60 %	94.74% 91.31%	95.44% 90.12%	0.0%
Time of finishing Brushed and sealer appl Membrane applied	4-17-43 ied 4-17-43 4-17-43	2:20 p.m	•	

WATER RETENTION TEST

Series II Test L

Specimen Curing material Wt. pan & mortar Wt. pan Wt. mortar Wt. before brushing Wt. after brushing Wt. after sealer Wt. before membrane Memb. should be applied Membrane was applied 4-18-43 12:45 p.m. 4-19-43 3:40 p.m.	L-1 Truscon 223 561.7 g. 43.4 518.3 556.4 556.2 558.1 556.6 2.98 3.07 556.8 555.5	L-2 Truscon 223 579.0 g. 47.0 532.0 574.3 574.1 576.3 574.8 2.98 3.00 574.9 573.4		L-4 Blank 580.3 g. 50.9 529.4 575.0 574.8 577.7 576.0
	TABULATED I	DATA - TEST 1		
Original water (A) Water loss while blank (Water at time of	47.3 D) 6.0	48.5 5.3	48.6 6.6	48.3 5.8
application (E) Water loss (F)	41.3	43.2	42.0	42.5
l day 2 days Percent water loss = 100	.1 1.4	1.7	2.4	21.2 23.8
l day 2 days	.242% 3.39 % 00 - <u>100 F</u> /		.238 <i>%</i> 5. 7 2 %	50 • 0 % 56 • 0%
l day 2 days	F/E (bla 99•52 % 93•94 %	99.07 % 92.95 %	99 .52 % 89 .98 %	0.0%
Time of finishing Brushed and sealer appli Membrane applied	4-17- ed 4-17- 4-17-	-43 3:05		

WATER RETENTION TEST

Series II Test M

Specimen	M-1	M-2	M-3	M-4			
Curing method	Moist R.	Moist R.	Moist R.	Moist R.			
Wt. pan and mort	ar 617.2 g.	615.8 g.	599•9 g•	603.7 g.			
Wt. pan	52.3	46.6	46.0	45.0			
Wt. mortar	564.9	569.2	553.9	558 .7			
4-21-43 12:35	p.m. 618.3	615.8	600.3	603.8			
4-22-43 10:00	a.m. 619.4	617.4	601.1	604.8			
Tabulated Data - Test M							
Original water (A) 51.5	51.9	50.5	50.9			
Water gain (F)							
l day	1.1	0.0	0.4	0.1			
2 days	2.2	1.6	1.2	1.1			
Percent water gain = $\frac{100 \text{ F}}{A}$							
1 day	2.16%	0.0 %	0.79%	0.20%			
2 days	4.27%	3.08%	2.38%	2.16%			

WATER RETENTION TEST

Series II Test N

Specimen		N-1	N-2	N-3	N-4
Curing mat	erial	Klearcure 60	Aquastatic 1-6-Red	Truscon 203	Satis. 45
Wt. pan		47.0 g.	42.8 g.	43.3 g.	50.2 g.
Wt. pan	mortar	591.2	592.9	584.3	591.8
Wt. mortar		544.2	550.1	541.0	541.6
4-28-43	2;50 P.M.	591.1	592.5	583.9	58 7. 2
4-29-43	9:30 P.M.	590.2	591.8	583.3	584.1

Tabulated Data - Test N

Original water (A) Water loss while blank	49.7 g. (D) 0	50.1 g.	49.4 g. O	49.4 g. 0
Water at time of	1.0	50.3	1.0 1.	1.0 1.
application (E)	49.6	50.1	49 .4	49.4
Water loss (F)			- 0	<i>-</i> -
l day	2.1	2.0	1.8 2.4	6.1
2 days	3. 0	2.7	2.4	9.2
Percent water loss . 1	00 x F/E			
1 day	4.23 %	4.00 %	3.65 %	12.35 %
2 days	6.05	5.40	3.65 % 4.86	18.61
Percent efficiency =	(100 - 100	F/E) blank)	·	•
1 day	91.80 %	92.25 %	92.92 %	76.1 %
2 days	89.48	91.61	91.55	67.6
e aays	0,010) 	J= 4 JJ	5,40

The membrane curing compound was applied immediately after finishing.

WATER RETENTION TEST

Series II Test O

Specimen	0-1	0-2	0-3	0-4
Curing material	Satis. 45	Satis. 45	Satis. 45	Blank
Weight pan	44.1 g.	44.8 g.	46.8 g.	44.4 g.
Wt. pan and mortar	583.5	573.7	574.1	582.7
Weight mortar	539.4	528.9	527.3	538.3
Wt. before brushing	578.0	568.2	568.8	577.4
Wt. after brushing	577.8	567.9	568.5	577.2
Wt. after sealer	579•9	569 .7	570 .7	579.4
Wt. before membrane	578.2	568.1	569.1	57 7. 8
Wt. membrane to apply	3.37	3.37	3.37	0
Wt. memb. was applied	3.37	3 .37	3.37	0
4-28-43 3:00 p.m.	574•9	564.3	566.1	555.0
4-29-43 3:00 p.m.	571.9	561.0	562.8	552.5

Tabulated Data - Test O

Original water Water loss	(A)	49.1 g.	48.2 g.	48.0 g.	49.0 g.
while blank	(D)	6.3	6.3	6.0	6.0
Water at time of application Water loss	(E) (F)	42.8	41.9	42.0	43.0
l day 2 days	(٢)	4.2 7.2	4.8 8.1	3.9 7.2	22.2 24.7
Percent water loss	Ξ		0.1	[• C	∠ ⊣•
1 day 2 days		9.81 % 16.80	11.45 % 19.32	9.29 % 1 7.1 2	51.6 % 57.5
Percent efficiency (100 - 100 F/E)				
(F/E (blank) l day 2 days)	81.0 70.8	77.8 66.4	82.0 70.2	0.0

Time of finishing	4-27-43	1:50 p.m.
Brushed and sealer applied	4-27-43	3:05 p.m.
Membrane applied	4-27-43	3:40 p.m.

MEMBRAYE CURING STUDY WATER RETENTION TEST

Series II Test P

Specimen Curing material	P-1 Truscon 203	P-2 Truscon 203	P-3 Truscon 203	P-4 Truscon 203
Coverage (sq. ft. to the gallon) Wt. pan Wt. pan & mortar Wt. mortar Wt. before brushing Wt. after brushing Wt. before membrane Wt. membrane should	100 49.9 g. 590.0 540.1 586.0 585.8 584.2	200 45.2 g. 572.7 527.5 568.8 568.6 566.7	600 44.6 g. 597.0 552.4 594.6 594.0 591.7	400 43.6 g. 586.6 543.0 582.8 582.4 579.8
be applied Wt. membrane was	6.24	3.12	1.04	1.56
applied 3:45 p.m. 4-30-43 3:30 p.m. 5- 1-43	6.24 586.0 585.7	3.12 567.1 566.5	1.04 585.2 582.1	1.56 576.1 573.4
	TABULATED	DATA - Test P	,	
Original water (A) Water loss while	49.2 g.	48.1 g.	50.4 g.	49.5 g.
blank (D) Water at time of	5.6	5.8	5.7	6.4
appl. of membr. (E) Water loss (F)	43.6	42.3	44.7	43.1
1 day 2 days Percent water loss = 1		1.0 1.6	7.0 10.1	4.4 7.1
l day 2 days Percent efficiency = (15.7 % 22.6 %	10.2 % 16.5 %
l day 2 days	F/E (bl 95.55 % 94.77 %	.ank)) 95.38 % 93.36 %	69.3 % 60.4 %	80.1 % 71.1 %
Time of finishing Brushed and sealer applied Membrane applied	4-29-43 4-29-43 4-29-43	12:40 p.m. 1:35 p.m. 2:10 p.m.		

MEMBRANE CURING STUDY WATER RETENTION TEST

Series II Test Q

Specimen Curing material Wt. pan Wt. pan and mortar Wt. mortar Wt. before brushing Wt. after brushing Wt. after sealer Wt. before membrane		Q-1 Aquastatic 1-C-Red 45.2 g. 575.5 530.3 570.4 570.1 572.7 570.6	Q-2 Aquastatic 1-C-Red 50.8 g. 600.2 549.4 595.8 595.6 596.5	Q-3 Aquastatic 1-C-Red 43.4 g. 598.9 555.5 593.9 593.1	Q-4 Aquastatic 1-C-Red 45.3 g. 578.9 533.6 573.6 573.4
Membrane should be applied Membrane was applied 4:15 p.m. 4-30-43 3:30 p.m. 5- 1-43		3.44 3.44 570.4 569.7	3.44 3.44 594.7 593.9	3.44 3.44 592.1 591.1	3.44 3.44 570.5 569.0
		TABULATED	DATA - Test	Q	
Original water	(A)	48.4 g.	50.2 g.	50.6 g.	48.6 g.
Water loss while blank	(D)	6.1	5 . 7	5.4	5•9
Water at time of application	(王)	42.3	44.5	45.2	42.7
Water loss (F) l day 2 days Fercent water loss = 1		1.0 1.7 00_x F	1.7 2.5	2.6 3.6	3.9 5.4
l day 2 days Percent efficiency	= (2.36 % 4.02 % 100 - 100		5•75 % 7•98%	9.14 % 12.64 %
l day 2 days	(F/E (6 95•38 % 92•95 %	92.56 % 90.15 %	88.78% 86.0%	82.13 % 77.80 %

Note: sealer was applied to edges of specimens Q-1 and Q-2, but not to Q-3 and Q-4. The results are quite apparent.

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WATER RETENTION TEST

Series II Test R

Specimen Curing material Weight pan Wt. pan and mortar Weight mortar Membrane should be applied Membrane applied 4:20 p.m. 4-30-43 3:30 p.m. 5-1-43	; }	R-1 Aquastatic 1-C-Red 44.6 8. 594.8 550.2 3.44 3.44 592.8 591.2 Tabulated	R-2 Klearcure 60 44.2 g. 584.3 540.1 3.46 3.46 584.1 582.6 Data - Test R	R-3 Truscon 203 45.3 g. 591.6 546.3 3.12 3.12 590.1 588.9	R-4 Satis. 45 45.0 g. 573.0 528.0 3.37 3.37 566.4 562.4
Original water Water loss while blank Water at time of application Water loss l day 2 days Percent water loss 100 x F/E 1 day 2 days Percent efficiency (100 - 100 F/E (F/E (blank)	· =)	50.3 g. 0 50.3 3.6 5.2 7.16 % 10.32	49.3 g. 0 49.3 2.2 3.7 4.46 % 7.51	49.9 5. 0 49.9 2.9 4.1 5.82 % 8.23	48.2 g. 0 48.2 8.1 12.1 16.80 % 25.10

The membrane was applied immediately after finishing.

APPENDIX B - ABRASION AND FLEXURE DATA

Abrasion Test

Series I

Specimen: B-5 Date tested: March 6, 1943

Compound: None Tested by: W. A. B.

Curing: One week in cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-14	-14	-12	-16	-13.75	0
	1	3 9	3 9	38	40	39.0	52.75
	3	113	110	111	116	112.5	126.25
	5	153	15 9	154	157	155.75	169.50
]	10	No	readi	ngs			

Weight before: 2491 Weight after: 2434 Loss: 57 grams

Time	in minutes		Dial	read	ings	l'ean	Total wear
	0	-1	-10	4	-8	-3.7 5	0
	1	50	47	48	48	48.25	52.0
	3	132	135	138	131	134.0	137.75
	4	160	162	157	161	160.0	163.75
	10	No	readi	ngs			

Weight before: 2340 Weight after: 2284 Loss: 56 grams

Flexural Test

Dial readings 24

Load at rupture 925 pounds

Modulus of rupture 529 pounds per square inch

Abrasion Test

Series I

Specimen: C-1

Compound: Satisfaction 45

Curing: One week in the cabinet and one week in lab air.

This speimen was cracked on removal from the mold, and therefore no tests could be run.

Abrasion Test

Series I

Specimen: C-2 Date tested: March 16, 1943

Compound: Satisfaction 45 Tested by: W. A. B.

Curing: One week in the cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-1 5	-14	-14	- 9	-13	0
	1	19	16	21	18	18.5	31.5
	3	76	72	75	72	73.75	86 .7 5
	5	133	130	130	129	130.5	143.50
3	10	No	readi	ngs			

Weight before: 2530 Weight after: 2484 Loss: 46 grams

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-10	-10	-14	-10	-11	O
	1	30	27	3 0	21	27	3 8
	3	105	101	103	108	104.25	115.25
	5	152	148	146	149	148.75	159.75
]	10	No	readin	ng s			

Weight before: 2285 Weight after: 2231 Loss: 54 grams

Flexural Test

Dial reading

This specimen was also cracked on removal from mold; therefore, no flexure test possible.

Abrasion Test

Series I

Specimen: E-1 Date tested: April 8, 1943

Compound: Trucure 223 Tested by: W. A. B.

Curing: One week in cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-15	-10	-12	- 6	-10.75	0
	1	16	14	13	14	14.25	25
	3	55	55	57	53	55.0	65.7 5
	5	9 5	9 5	9 7	99	96.5	107.25
	10	No	read	ings			

Weight before: 2413 Weight after: 2365 Loss: 48 grams at six minutes

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	- 9	-11	-12	-10	-10.5	0
	1	17	16	18	16	16.75	27.25
	3	56	5 5	5 0	50	52.75	63.25
	5	91	88	90	88	89.25	99.75
•	10	No	read	ings			

Weight before: 2347 Weight after: 2308 Loss: 37 grams

Flexural Test

Dial reading 26.5

Load at rupture 1025 pounds

Modulus of rupture 585 pounds per square inch

Abrasion Test

Series I

Specimen: B-3 Date tested: March 6, 1943

Compound: Klearcure 60 Tested by: W. A. B.

Curing: One week in cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-8	8-	-18	-10	-11	0
	1	6	6	4	4	5.0	16.0
	3	16	16	15	14	15.25	26.25
	5	25	25	28	25	25.75	36.75
1	LO	50	47	50	48	48.75	59.7 5

Weight before: 2281 Weight after: 2250 Loss: 31 grams

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-12	2	-8	0	-4.5	0
	1	11	16	16	17	15.0	19.5
	3	34	34	34	34	34.0	38.5
	5	48	50	52	4 9	49.75	54.2 5
-	10	92	92	92	9 5	92.75	97.25

Weight before: 2506 Weight after: 2463 Loss: 43 grams

Flexural Test

Dial reading 32

Load at rupture 1225 pounds

Modulus of rupture 700 pounds per square inch

Abrasion Test

Series I

Specimen: B-4 Date tested: March 6, 1943

Compound: Horn Tested by: W. A. B.

Curing: One week in cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	- 6	-3	-10	- 6	-6.25	0
	1	47	42	47	47	45.75	52.0
	3	107	104	111	114	109.0	115.25
	5	150	150	156	153	152.25	158.50
נ	LO	No	readi	ngs			

Weight before: 2394 Weight after: 2342 Loss: 52 grams

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-10	-8	- 15	-12	-11.25	0
	1	34	34	33	34	33.7 5	45.0
	3	85	87	85	83	85.0	96.25
	5	125	135	125	130	128.75	140.00
1	LO	No	readi	ngs			

Weight before: 2495 Weight after: 2448 Loss: 47 grams

Flexural Test

Dial reading 25

Load at rupture 970 pounds

Modulus of rupture 554 pounds per square inch

Abrasion Test

Series I

Specimen: E-2 Date tested: April 8, 1943

Compound: Trucure 223 Tested by: W. A. B.

Curing: One week in cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-28	-32	-24	-30	-28.5	0
	1	3	3	1	3	2.5	31.0
	3	2 9	28	28	28	28.25	56 .7 5
	5	60	55	57	5 5	56.75	85.25
:	10	108	105	107	105	106.25	134.75

Weight before: 2555 Weight after: 2510 Loss: 45 grams

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-15	-13	- 9	- 6	-10.75	0
	1	22	20	24	19	21.25	32.0
	3	63	57	63	60	60.75	71.5
	5	92	90	9 3	91	91.5	102.25
1	10	144	144	143	144	143.75	154.40

Weight before: 2295 Weight after: 2244 Loss: 51 grams

Flexural Test

Dial reading 29

Load at rupture 1125 pounds

Modulus of rupture 642 pounds per square inch

Abrasion Test

Series I

Speciment E-3 Date tested: April 8, 1943

Compound: Trucure 203 Tested by: W. A. B.

Curing: One week in the cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	- 7	- 6	-12	- 5	-7. 5	0
	1	15	17	15	18	16.25	23.75
	3	42	4 0	4 0	42	41.0	48.5
	5	69	66	6 9	6 6	67.5	75.0
:	10	132	130	132	136	132.5	140.0

Weight before: 2481 Weight after: 2435 Loss: 46 grams

Time	in minutes		Dial readings			Mean	Dial wear
	0	-3	-11	-7	-4	-6.25	0
	1	20	18	18	18	18.5	24.75
	3	44	43	4 6	47	4 5.0	51.25
	5	74	78	7 0	80	75.5	81.75
	LO	143	146	140	145	143.5	149.75

Weight before: 2321 Weight after: 2270 Loss: 51 grams

Flexural Test

Dial reading 28

Load at rupture 1075 pounds

Modulus of rupture 614 pounds per square inch

Abrasion Test

Series I

Specimen: E-4 Date tested: April 8, 1943

Compound: Trucure 203 Tested by: W. A. B.

Curing: One week in the cabinet and one week in lab air.

Time	in minutes		Dial readings			Mean	Total wear
	0	-16	-17	_18	-16	-16.75	0
	· ·	-10	-11	-10	-10	-10.70	O
	1	5	4	10	7	6.5	23.25
	3	27	29	26	2 5	26.75	43.50
	5	47	51	45	50	48.25	65.0
3	10	92	90	93	90	91.25	108.0

Weight before: 2502 Weight after: 2470 Loss: 32 grams

Time	in minutes		Dial	read	ing s	Vean	Total wear
	0	-24	-30	-25	-30	-27.2 5	0
	1	-1	-3	-1	- 5	-2.5	24.75
	3	23	19	24	24	2 2.5	49 .7 5
	5	46	48	4 6	46	46.5	73.75
	10	99	100	103	102	101.0	128.25

Weight before: 2308 Weight after: 2267 Loss: 41 grams

Flexural Test

Dial reading 27.5

Load at rupture 1063 pounds

Modulus of rupture 607 pounds per square inch

Abrasion Test

Series I

Specimen: E-5 Date tested: April 8, 1943

Compound: None Tested by: W. A. B.

Curing: One week in the cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	- 5	- 5	-4	- 6	- 5	0
	1	5 9	50	55	5 0	53.5	58.5
	3	15 9	161	160	161	160.25	165.25
-	5 10	No	readi	ngs			

Weight before: 2398 Weight after: 2340 Loss: 58 grams

Time	in minutes	Dial	read	ings	Mean	Total wear	
	0	-13	-16	-13	-18	-1 5	0
	1	52	5 8	53	58	5 5.2 5	70.25
	3	152	150	155	1 50	151.75	166.75
	5	N-		.			
]	10	NO	read:	ıngs			

Weight before: 2232 Weight after: 2175 Loss: 57 grams

Flexural Test

Dial reading 20

Load at rupture 775 pounds

Modulus of rupture 442 pounds per square inch

Abrasion Test

Series I

Specimen: E-6 Date tested: April 8, 1943

Compound: None Tested by: W. A. B.

Curing: One week in the cabinet and one week in lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-17	-22	- 16	-18	-18.25	0
	1	2 8	2 8	29	28	28.25	46.5
	3	90	90	92	93	91.25	109.5
	5	144	140	148	151	145.75	164.0
3	LO	No	read	ings			

Weight before: 2311 Weight after: 2255 Loss: 56 grans

Time in minut	Dial	read	ings	Mean	Total wear	
				•		
0	-21	-14	-22	-13	-17. 5	0
1	52	57	54	56	54.75	72.25
3	143	147	143	146	144.75	162.25
5	N.		•			
10	NO	read	ings			

Weight before: 2454 Weight after: 2403 Loss: 51 grams

Flexural Test

Dial reading 21

Load at rupture 813 pounds

Modulus of rupture 464 pounds per square inch

Abrasion Test

Series I

Specimen: F-1 Date tested: April 15, 1943

Compound: None Tested by: W. A. B.

Curing: One week in the moist room and one week in lab air.

Time	ime in minutes		Dial	read	ings	Mean	Total wear
	0	-19	-23	-29	-20	-22.75	0
	1	-4	-4	-8	-4	- 5	17.75
	3	1	3	8	3	3.75	26.5
	5	21	17	21	22	20.25	43.0
:	10	58	60	62	6 4	61.0	83.75

Weight before: 2533 Weight after: 2498 Loss: 35 grams

Time	in minutes		Dial	readi	ings	Mean	Total wear
	0	- 6	- 6	- 6	-3	-5.25	0
	1	11	7	7	5	7.5	12.75
	3	20	20	21	19	20.0	25.25
	5	3 0	27	3 0	31	29.5	34.7 5
1	10	73	72	7 0	73	72.0	77.2 5

Weight before: 2340 Weight after: 2307 Loss: 33 grams

Flexural Test

Dial reading 25

Load at rupture 975 pounds

Modulus of rupture 556 pounds per square inch

Abrasion Test

Series I

Specimen: F-2 Date tested: April 15, 1943

Compound: None Tested by: W. A. B.

Curing: One week in the moist room and one week in lab air.

Time	in minutes		Dial	re ad	ings	Mean	Total wear
	0	10	- 6	7	-10	.25	0
	1	16	16	20	16	17.0	16.75
	3	34	29	29	27	29.25	29.0
	5	3 6	37	3 5	3 6	36.0	35.7 5
3	10	5 2	57	56	5 6	55.25	55.00

Weight before: 2533 Weight after: 2506 Loss: 27 grams

Time	in minutes	Dial	read	ings	Mean	Total wear	
	0	-10	-8	-12	-10	-10	0
	1	14	12	11	12	12.25	22.25
	3	2 8	25	2 6	2 6	26.25	36.25
	5	42	36	4 0	3 9	39.25	49.25
]	10	73	7 5	73	72	73.25	83.25

Weight before: 2289 Weight after: 2252 Loss: 37 grams

Flexural Test

Dial reading 24

Load at rupture 925 pounds

Modulus of rupture 528 pounds per square inch

Abrasion Test

Series I

Specimen: F-3 Date tested: April 15, 1943

Compound: None Tested by: W. A. B.

Curing: One week in moist room and one week in lab air.

Time	in minutes		Dial readings			Mean	Total wear
	0	-3	-7	-3	1	-1.5	0
	12	20	18	22	21	20.25	21.75
	3	35	37	35	35	35.5	37.0
	5	4 5	50	52	50	49.25	50 .7 5
]	10	90	90	87	89	89.0	90.5

Weight before: 2412 Weight after: 2374 Loss: 38 grams

Time	in minutes		Dial	readi	ings	Mean	Total wear
	0	-9	-4	- 9	- 6	- 7	0
	1	12	12	12	13	12.25	19.25
	3	28	3 0	3 1	28	29.25	36.25
	5	44	50	44	46	46.0	53.0
:	10	87	84	80	87	84.5	91.5

Weight before: 2525 Weight after: 2488 Loss: 37 grams

Flexural Test

Dial reading 25

Load at rupture 975 pounds

Modulus of rupture 556 pounds per square inch

Abrasion Test

Series I

Specimen: F-4 Date tested: April 15, 1943

Compound: None Tested by: W. A. B.

Curing: One week in the moist room and one week in lab air.

Time	in minutes		Dial	readi	ings	Mean	Total wear
	0	- 6	- 6	- 9	-7	- 7	0
	1	12	10	12	13	11.75	18.75
	3	27	26	2 8	27	27.0	34.0
	5	47	43	4 5	45	45.0	52.0
	10	89	88	90	91	89.5	96.5

Weight before: 2441 Weight after: 2400 Loss: 41 grams

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-20	-18	-23	-14	-18.75	0
	1	1	6	1	3	2.75	21.5
	3	14	15	16	14	14.75	33.5
	5	27	2 5	25	2 5	25.5	44.25
•	10	50	53	50	50	50.75	69.50

Weight before: 2418 Weight after: 2387 Loss: 31 grams

Flexural Test

Dial reading 21

Load at rupture 813 pounds

Modulus of rupture 464 pounds per square inch

Abrasion Test

Series I

Specimen: F-5 Date tested: April 15, 1943

Compound: None Tested by: W. A. B.

Curing: One week under wet burlap and one week in lab air.

Time	ime in minutes		Dial	read	ings	Mean	Total wear
	0	-8	-13	-8	-13	-10.5	0
	1	8	8	11	7	8.5	19.0
	3	18	18	20	17	18.25	28.75
	5	26	2 9	28	27	27.5	38.0
1	10	66	66	62	68	65.5	76.0

Weight before: 2675 Weight after: 2649 Loss: 26 grams

Time	in minutes	•	Dial	readir	ngs	l'ean	Total wear
	0	- 14 ·	- 14 ·	-16 -	-18 -	-15.5	0
	1	3	3	3	2	2.75	18.25
	3	16	17	16	16	16.25	31.75
	5	27	3 0	27	2 9	28.25	43.75
1	0	69	68	7 0	7 0	69.25	84.75

Weight before: 2341 Weight after: 2311 Loss: 30 grams

Flexural Test

Dial reading 28.5

Load at rupture 1100 pounds

Modulus of rupture 627 pounds per square inch

Abrasion Test

Series I

Specimen: F-6 Date tested: April 15, 1943

Compound: None Tested by: W. A. B.

Curing: Ponded for one week and one week in lab air.

Time	in minutes		Dial	read	ing s	l'ean	Total wear
	0	-22	-3	-22	-2	-12.5	0
	1	4	4	0	10	4.5	17.0
	3	19	20	18	2 2	19.75	32.25
	5	23	26	3 0	28	26.75	39.25
נ	LO	4 9	4 8	4 6	48	47.75	60.25

Weight before: 2104 Weight after: 2085 Loss: 19 grams

Time	in minutes		Dial readings			Mean	Total wear
	0	-3	-12	-12	- 7	-8.5	0
	1	20	18	18	18	18.5	27.0
	3	27	29	32	30	2 9.5	38.0
	5	4 0	40	4 5	4 0	41.25	49.75
	10	59	60	60	5 5	5 8. 5	65.0

Weight before: 2751 Weight after: 2732 Loss: 19 grams

Flexural Test

Dial reading 21

Load at rupture 813 pounds

Modulus of rupture 464 pounds per square inch

Abrasion Test

Series II

Specimen: H-l Date tested: April 15, 1943

Compound: Trucure 203 Tested by: W. A. B.

Curing: Two days in the cabinet.

Tire	in minutes		Dial	read	ings	Mean	Total wear
	0	-13	-12	-17	- 16	-14.5	0
	1	9	6	4	7	6.5	21.0
	3	27	26	26	26	26.25	40.75
	5	49	4 9	47	4 9	48.5	63.0
	8	76	7 5	75	70	74.0	88.5

Weight before: 583.7 Weight after: 550.3 Loss: 33.4 grams

Specimen: H-2 Date tested: April 15, 1943

Compound: Trucure 203 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	7	0	1	1	2.25	0
	1	12	≘5	12	13	13.0	10.75
	3	29	28	27	27	27.75	25.50
	5	38	37	3 8	38	37.75	35.50
	8	60	62	61	60	60.75	58.50

Weight before: 587.5 Weight after: 565.1 Loss: 22.4 grams

Abrasion Test

Series II

Specimen: H-3 Date tested: April 15, 1943

Compound: Trucure 203 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-33	-34	-38	-31	-34	0
	1	-13	-18	-13	-18	-15.5	18.5
	3	6	6	6	7	6.25	40.25
	5	25	26	27	27	26.25	60.25
	8	60	61	61	60	60.5	94.5

Weight before: 597.6 Weight after: 562.3 Loss: 35.3 grams

Specimen: H-4 Date tested: April 15, 1943

Compound: None Tested by: W. A. B.

Curing: Two days in the cabinet.

Tire	in minutes		Dia	l rea	dings	Mean	Total wear
	0	- 9	-18	- 9	-14	-12.5	0
	1	25	23	23	23	23.5	3 6
	3	153	159	161	160	158.25	170.75
	5	N.					
	8	1.0	readi	rugs			

Weight before: 555.5 Weight after: 495.7 Loss: 59.8 grams

Abrasion Test

Series II

Specimen: I-l Date tested: April 19, 1943

Compound: Aquastatic 1-C-Red Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial readings			Mean	Total wear
	0	- 6	- 7	-8	- 5	-6.5	0
	1	4	8	3	3	4.5	11.0
	3	21	23	20	22	21.5	28.0
	5	40	41	3 8	45	41.0	47.5
	8	69	71	69	65	68.5	75.0

Weight before: 591.1 Weight after: 561.2 Loss: 29.9

Specimen: I-l Date tested: April 19, 1943

Compound: Aquastatic 1-C-Red Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	Dial readings		Mean	Total wear
	0	- 6	-12	-12	-12	-10.5	0
	1	-2	-4	- 5	-3	-3.5	7
	3	13	10	10	13	11.5	22.0
	5	36	3 5	34	38	35 .7 5	46.25
]	10	65	7 0	6 7	7 0	68.0	7 8.5

Weight before: 579.4 Weight after: 547.7 Loss: 31.7

Abrasion Test

Series II

Specimen: I-3 Date tested: April 19, 1943

Compound: None Tested by: W. A. B.

Curing: Two days in the cabinet.

Time in minutes	3	Dial	read	ings	Mean	Total wear	
0	-4	-4	-12	-4	- 6	0	
1	110	114	115	110	112.25	118.25	
1 <u>1</u>	160	157	156	157	157.5	163.5	
5	3 7 -	1:					
8	ΝO	readi	ngs				

Weight before: 565.4 Weight after: 506.9 Loss: 58.5

Specimen: I-4 Date tested: April 19, 1943

Compound: Aquastatic 1-C-Red Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-7	-11	-7	-11	- 9	0
	1	1 5	13	13	15	14	23
	3	37	38	40	38	38.25	47.25
	5	54	56	56	6 0	56.5	65.5
	8	85	88	85	89	86.75	95.75

Weight before: 563.9 Weight after: 531.4 Loss: 32.5

Abrasion Test

Series II

Specimen: J-l Date tested: April 19, 1943

Compound: Klearcure 60 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-1	0	-2	-3	-1.5	0
	1	1 5	16	15	13	14.75	16.25
	3	35	35	35	32	34.25	3 5. 7 5
	5	47	4 9	48	44	47.0	48.5
	8	72	71	71	71	71.25	72.75

Weight before: 568.1 Weight after: 543.6 Loss: 24.5 grams

Specimen: J-2 Date tested: April 19, 1943

Compound: Klearcure 60 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial readings			Mean	Total wear
	0	0	0	-3	1	5	0
	1	14	18	16	16	16.0	16.5
	3	32	3 3	3 3	33	32.75	33.25
	5	4 8	53	46	47	48.5	49.0
	8	76	7 5	7 8	7 5	76	76. 5

Weight before: 569.7 Weight after: 542.0 Loss: 27.7 grams

Abrasion Test

Series II

Specimen: J-3 Date tested: Aprli 19, 1943

Compound: Klearcure 60 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	7	3	5	7	5.5	. 0
	1	15	14	15	15	14.75	9.25
	3	35	33	33	33	33. 5	28.0
	5	52	52	50	52	51. 5	46.0
	8	7 5	73	75	78	75.25	69.75

Weight before: 584.9 Weight after: 560.2 Loss: 24.7 grams

Specimen: J-4 Date tested: April 19, 1943

Compound: None Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-4	8-	- 5	- 9	-6.5	0
	1	67	60	63	64	63.5	70.0
	2	135	140	135	130	135.0	141.5
	5	11-		.			
	8	NO	read	ings			

Weight before: 558.6 Weight after: 510.0 Loss: 48.6 grams

Abrasion Test

Series II

Specimen: K*l Date tested: April 19, 1943

Compound: Aquastatic Slab Cure Red Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial readings		Mean	Total wear	
	0	-7	- 8	- 9	- 6	-7. 5	0
	1	9	10	6	9	8.5	16.0
	3	22	23	20	2 0	21.25	28.75
	5	35	33	33	3 5	33.5	41.0
	8	55	54	56	53	54.5	62.0

Weight before: 558.4 Weight after: 534.2 Loss: 24.2 grams

Specimen: K-2 Date tested: April 19, 1943

Compound: Aquastatic Slab Cure Red Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	Dial readings		Mean	Total wear
	0	- 6	-18	- 9	-16	-12.25	0
	1	0	-2	2	4	1.0	13.25
	3	20	17	18	18	18.25	30.5
	5	32	3 9	35	37	35.75	48.0
	8	7 7	7 6	81	80	7 8.5	90.75

Weight before: 569.8 Weight after: 535 Loss: 34.8 grams

Abrasion Test

Series II

Specimen: K-3 Date tested: April 19, 1943

Compound: Aquastatic Slab Cure Red Tested by: W. A. B.

Curing: Two days in the cabinet.

Time in min	utes	Dial	read	ings	Mean	Total wear	
0	-4	14	-3	13	5.0	0	
1	25	2 5	2 6	25	25. 25	20.25	
3	36	36	32	30	33 .5 0	28.50	
5	54	51	4 8	48	50.25	45.25	
8	72	76	7 0	73	72.75	67.75	

Weight before: 548 Weight after: 520 Loss: 28 grams

Specimen: K-4 Date tested: April 19, 1943

Compound: None Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	0	-6	-1	- 6	-3.25	0
	1	70	7 5	70	74	74.75	7 8.0
	2	150	159	156	159	156.0	159.25
	5	N.					
	8	NO	readi:	ngs			

Weight before: 543.8 Weight after: 487.0 Loss: 56.8 grams

Abrasion Test

Series II

Specimen: L-1 Date tested: April 19, 1943

Compound: Truscon 223 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial readings		ings	l'ean	Total wear
	0	-10	- 16	-13	-18	-14.25	0
	1	15	16	11	11	13.25	27. 5
	3	5 5	48	52	54	52.2 5	66.5
	5	110	106	104	104	106.0	120.25
	8	157	154	156	159	156.5	170.75

Weight before: 556.8 Weight after: 502 Loss: 54.8 grams

Specimen: L-2 Date tested: April 19, 1943

Compound: Truscon 223 Tested by: W. A. B.

Curing: Two days in the cabinet

Time	in minutes		Dial	Dial readings		Mean	Total wear
	0	- 6	-1 6	- 9	- 9	-10.0	0
	1	10	12	12	10	11.0	21.0
	3	4 0	41	3 8	37	39.0	49.0
	5	67	76	71	67	70.25	80 .25
	8	118	118	120	122	119.5	129.5

Weight before: 573.4 Weight after: 527 Loss: 46.4 grams

Abrasion Test

Series II

Specimen: L-3 Date tested: April 19, 1943

Compound: Truscon 223 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial readings		Mean	Total wear	
	0	-30	-28	-27	-27	-28	0
	1	1	-3	-2	1	-175	27.2 5
	3	18	20	2 0	22	20.0	48.0
	5	4 8	47	48	45	47.0	75.0
	8	100	97	97	9 7	97.75	125.75

Weight before: 569.8 Weight after: 529.5 Loss: 40.3 grams

Specimen: L-4 Date tested: April 19, 1943

Compound: None Tested by: W. A. B.

Curing: Two days in the cabinet.

Time in minu	Dial readings			Mean	Total wear	
0	-14	-12	-16	-11	-13.25	0
1	40	41	44	44	42.25	55.5
3	160	158	161	155	158.5	171.75
5	N -					
8	MO	readi	ngs			

Weight before: 551.4 Weight after: 488.8 Loss: 62.6 grams

Abrasion Test

Series II

Specimen: M-l Date tested: April 22, 1943

Compound: None Tested by: W. A. B.

Curing: Two days in the moist room. Tested on removal.

Time	in minutes		Dial	read	ings	Mean	Total wear	
	0	-26	-34	-32	-38	-31.75	0	
	1	42	30	34	36	35.5	67.25	
	3	143	137	140	141	140.25	172.0	
	5	MO	moodii	na				
	8	NO	readi	ngs				

Weight before: 620 Weight after: 554 Loss: 66 grams

Specimen: M-4 Date tested: April 22, 1943

Compound: None Tested by: W. A. B.

Curing: Two days in the moist room. Tested on removal.

Time	in minutes		Dial	read	ings	Mean	Total wear	
	0	-25	-18	-20	-19	-20.5	0	
	1	4 3	43	42	4 3	42.75	63.25	
	3	144	142	15 0	147	145.75	166.25	
	5	3 7						
	.8	NO	readi	ngs				

Weight before: 605 Weight after: 540 Loss: 65 grams

Abrasiom Test

Series II

Specimen: M-2 Date tested: April 27, 1943

Compound: None Tested by: W. A. B.

Curing: Two daws in moist room and five days in lab air.

Time	Time in minutes		Dial	read	ings	Mean	Total wear	
	0	-2	- 9	-4	-18	-8.25	0	
	1	23	22	22	24	22.75	31.0	
	3	38	35	3 8	40	37.75	46.0	
	5	56	50	52	50	52.0	60.25	
	8	80	83	7 9	85	81.75	90.0	

Weight before: 599.7 Weight after: 568.0 Loss: 31.7 grams

Specimen: N-3

Compound: None

Curing: Two days in the moist room and five daysin lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	- 5	-17	-15	-12	-12.25	0
	1	14	1 5	14	17	15.0	27.25
	3	37	32	36	31	34.0	46.25
	5	50	4 8	48	52	48.5	6 0 .7 5
	8	8 7	85	8 4	87	85.75	98.0

Weight before: 583.5 Weifht after: 549.8 Loss: 33.7 grams

Abrasion Test

Series II

Specimen: N-1 Date tested: April 29, 1943

Compound: Klearcure 60 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes	Dial	read	ings	Mean	Total wear	
	0	-12	-15	-10	-17	-13.5	o
	1	19	22	21	22	21	34.5
	3	72	67	7 0	72	70.25	83.75
	5	100	107	106	101	103.5	117.0
	8	144	142	142	142	142.5	156.0

Weight before: 590.2 Weight after: 532.8 Loss: 57.4 grams

Specimen: N-2 Date tested: April 29, 1943

Compound: Aquastatic 1-C-Red Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-11	-16	-11	-16	-13.5	o
	1	19	20	18	18	18.75	32.25
	3	75	77	75	78	76.25	89.75
	5	110	115	112	118	114.75	128.25
	8	151	153	154	152	152.5	166.0

Weight before: 591.8 Weight after: 530.7 Loss: 61.1 grams

Abrasion Test

Series II

Specimen: N-3 Date tested: April 29, 1943

Compound: Truscon 203 Tested by: W. A. B.

Curing: Two days in the cabinet.

Time in minutes			Dial	read	ings	Mean	Total wear	
	0	-15	-15	-14	-12	-14	0	
	1	11	11	15	15	15	27	
	3	62	62	64	62	62.5	76.5	
	5	110	108	107	108	108.25	122.25	
	8	147	148	148	148	147.75	161.75	

Weight before: 583.3 Weightafter: 525.9 Loss: 57.4 grams

Specimen: N-4 Date tested: April 29, 1943

Compound: Satisfaction Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear	
	0	-3	-9	-5	-12	-7.25	0	
	1	12	15	12	16	13.75	21.0	
	3	58	57	60	55	57.5	64.75	
	5	97	95	100	95	96.75	104.0	
	8	144	144	145	144	144.25	151.50	

Weight before: 584.1 Weight after: 530.5 Loss: 53.6 grems

Abrasion Test

Series II

Specimen: 0-1 Date tested: April 29, 1943

Compound: Satisfaction Tested by: W. A. B.

Curing: Two daysin the cabinet.

Time in minutes			Dial	readi	ing s	Mean	Total wear	
	0	-7	-3	-4	0	-3.5	0	
	1	11	10	10	11	10.5	14.0	
	3	2 6	22	21	23	23.0	26.5	
	5	40	37	39	35	37.75	41.25	
	8	64	62	66	66	64.5	68. 0	

Weight before: 571.9 Weight after: 549.3 Loss: 22;6 grams

Specimen: 0-2 Date tested: April 29, 1943

Compound: Satisfaction Tested by: W. A. B.

Curing: Twodays in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear	
	0	5	-3	2	-4	0	0	
	1	17	13	16	14	15	15	
	3	35	37	36	35	35.75	35.75	
	5	68	65	67	67	66.75	66.75	
	8	96	10 0	96	101	98.25	98.25	

Weight before: 562.8 Weight after: 525.8 Loss: 37.0 grams

Abrasion Test

Series II

Specimen: 0-3 Date tested: April 29, 1943

Compound: Satisfaction Tested by: W. A. B.

Curing: Two days in the cabinet:

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-8	-13	- 6	-11	-7. 0	0
	1	9	13	6	12	10.0	17.0
	3	28	27	32	3 0	29.25	36.25
	5	61	55	57	5 9	58.0	65.0
	8	87	86	86	8 9	87.0	94.0

Weight before: 561.0 Weight after: 528.0 Loss: 33.0

Specimen: 0-4 Date tested: April 29, 1943

Compound: None Tested by: W. A. B.

Curing: Two days in the cabinet.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	- 7	-7	- 9	-11	-8.5	0
	1	66	63	63	6 9	65.25	73.75
	2	144	144	143	148	144.75	153.25
	5	37					
	8	NO	readi	ngs			

Weight before: 552.5 Weight after: 498.1 Loss: 54.4 grams

Abrasion Test

Series II

Specimen: R-1 Date tested: May 6, 1943

Compound: Aquastatic 1-C-Red Tested by: W. A. B.

Curing: Two days in the cabinet and five days in the lab air.

Time	in minutes		Dial readings		ings	Mean	Total wear	
	0	-3	-8	-5	-8	-6	0	
	1	19	17	16	23	19.25	25.25	
	3	46	46	45	4 5	45.5	51.5	
	5	7 6	78	80	76	77.5	83.5	
	8	118	117	117	118	117.5	123.5	

Weight before: 589.4 Weight after: 547.2 Loss: 42.2 grams

Specimen: R-2 Date tested: May 6, 1943

Compound: Klearcure 60 Tested by: W. A. B.

Curing: Two days in the cabinet and five days in the lab air.

Time	in minutes		Dial	Dial readings		Mean	Total wear
	0	0	-8	-3	-2	-3.25	o
	1	18	22	20	19	19.75	23.0
	3	54	58	55	55	55 .5	58.75
	5	85	92	90	90	89.25	93.50
	8	137	129	135	131	134.0	137.25

Weight before: 581.0 Weight after: 533.5 Loss: 47.5 grams

Abrasion Test

Series II

Specimen: R-3 Date tested: May 6, 1943

Compound: Truscon 203 Tested by: W. A. B.

Curing: Twp days in the cabinet and five days in lab air.

Time in minutes		Dial readings			Mean	Total wear	
	0	-19	-14	-18	-14	-16.25	0
	1	10	10	10	11	10.25	26.5
	3	50	51	45	4 8	48.5	64.75
	5	82	7 8	84	84	82.0	98.25
	8	135	133	131	134	133.25	149.5

Weight before: 587.4 Weight after: 534.3 Loss: 53.1 grams

Specimen: R-4 Date tested: May 6, 1943

Compound: Satisfaction Tested by: W. A. B.

Curing: Two days in the cabinet and five days in the lab air.

Time	in minutes		Dial	read	ings	Mean	Total wear
	0	-12	-10	-15	- 6	-10.75	0
	1	15	17	15	15	15.5	26.25
	3	70	7 0	72	7 0	70.5	81.25
	5	112	111	118	114	113.75	124.50
	8	160	153	152	154	154.75	165.50

Weight before: 558.8 Weight after: 503.2 Loss: 55.6 grams

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